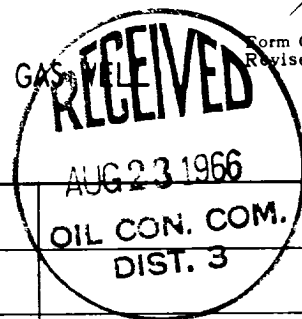


NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS

Form C-122
Revised 9-1-65



Type Test ☒ Initial ☐ Annual ☐ Special				Test Date 8/22/66		RECEIVED AUG 23 1966 OIL CON. COM. DIST. 3			
Company Artec Oil and Gas				Connection Southern Union Gathering					
Pool Basin Dakota				Formation Dakota					
Completion Date 8/15/66		Total Depth 6750		Plug Back TD 6732		Elevation 5857 GL		Farm or Lease Name Hudson	
Csg. Size 4 1/2	Wt. 10.5	d 4.000	Set At 6750	Perforations: From 6460 To 6680		Well No. 3			
Tbg. Size 1 1/2	Wt. 2.75	d 1.610	Set At 6597	Perforations: From 6567 To 6577		Unit E	Sec. 35	Twp. 30N	Rge. 12W
Type Well - Single - Bradenhead - G.G. or G.O. Multiple single - gas				Packer Set At		County San Juan			
Producing Thru tubing		Reservoir Temp. °F @		Mean Annual Temp. °F		Baro. Press. - P _a		State New Mexico	
L	H	Gg	% CO ₂	% N ₂	% H ₂ S	Prover	Meter Run	Taps	

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	
SI	2"		3/4"				1747		1719	
1.							170	60 (est)	747	60 (est)
2.										
3.										
4.										
5.										

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1	12.365		182	1.000	.9258	1.022	2129
2.							
3.							
4.							
5.							

NO.	P _t	Temp. °R	T _f	Z	Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.
1					A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.
2.					Specific Gravity Separator Gas _____ X X X X X X X X
3.					Specific Gravity Flowing Fluid _____ X X X X X
4.					Critical Pressure _____ P.S.I.A. _____ P.S.I.A.
5.					Critical Temperature _____ R _____ R

P _c 1750	P _c ² 3,091,081		
NO.	P _t ²	P _w ²	P _c ² - P _w ²
1			
2			
3			
4			
5			

$$(1) \frac{P_c^2}{P_c^2 - P_w^2} = \text{_____}$$

$$(2) \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = \text{_____}$$

$$ACF = Q \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = \text{2485}$$

Absolute Open Flow 2485 Mcfd @ 15.025	Angle of Slope θ _____	Slope, n .75
Remarks: _____		
Approved By Commission:	Conducted By:	Calculated By: Original Signed By Carl E. Jamison
		Checked By: