

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

Type Test ☒ Initial ☐ Annual ☐ Special						Test Date 4-4-77			
Company Odessa Natural Corporation						Connection Waiting on Pipeline			
Pool Basin Dakota				Formation Dakota				Unit	
Completion Date 3-23-77		Total Depth 6579'		Plug Back TD 6525'		Elevation 5910' KB		Farm or Lease Name Little Federal	
Csg. Size 4.500	Wt. 10.50	d 4.052	Set At 6578'	Perforations: From 6274' To 6350'				Well No. 3	
Tbg. Size 2.375	Wt. 4.70	d 1.995	Set At 6308'	Perforations: From open To ended				Unit Sec. Twp. Rge. C 12-30N-14W	
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single						Packer Set At None		County San Juan	
Producing Thru Tubing		Reservoir Temp. °F 166 @ 6579		Mean Annual Temp. °F -----		Baro. Press. - P _a 12.0		State New Mexico	
L 6308	H 6308	G _g 0.65	% CO ₂ -----	% N ₂ -----	% H ₂ S -----	Prover -----	Meter Run -----	Taps -----	

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F
SI							1950		1500		7 da.
1.	3/4" THC						150	60	700		3 hrs.
2.											
3.											
4.											
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor F _t	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1	12.3650		162	1.0000	0.9608	1.0000	1.925
2.							
3.							
4.							
5.							

NO.	P _t	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.			
1.					A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.			
2.					Specific Gravity Separator Gas _____ XXXXXXXXXX			
3.					Specific Gravity Flowing Fluid _____ XXXXXX			
4.					Critical Pressure _____ P.S.I.A. _____ P.S.I.A.			
5.					Critical Temperature _____ R _____ R			

P _c 1962	P _c ² 3,849,444		
NO.	P _t ²	P _w	P _w ²
1		712	506,944
2			
3			
4			
5			

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.1516$ (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.1117$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 2,140$

Absolute Open Flow 2,140		Mcf @ 15.025	Angle of Slope °	Slope, n 0.75
Remarks:				

Approved By Commission:	Conducted By: Lon Cuningham	Calculated By: Ewell N. Walsh	Checked By:
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