

Type Test <input checked="" type="checkbox"/> Initial <input type="checkbox"/> Annual <input type="checkbox"/> Special			Test Date 12-6-77			
Company Aztec Oil & Gas Company			Connection Southern Union Gathering			
Pool Basin			Formation Dakota			
Completion Date 11-26-77		Total Depth 7150'		Plug Back TD 6965'	Elevation 5922' GR	
Crg. Size 4.500	Wt. 10.5# 11.6#	d 4.052 4.000	Set At 7148'	Perforations: From 6826' To 6933'		
Tbg. Size 2.375	Wt. 4.7#	d 1.995	Set At 6909	Perforations: From --- To -		
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single				Packer Set At ----		
Producing Thru Tbg		Reservoir Temp. °F p		Baro. Press. - P _a 12.2		
L	H	Gg .700	% CO ₂	% H ₂	% H ₂ S	
Prover	Meter Run	Taps				
FLOW DATA			TUBING DATA		CASING DATA	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F
SI						
1.	2"	X	3/4"			
2.						
3.						
4.						
5.						
RATE OF FLOW CALCULATIONS						
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress. Factor, F _{pv}
1	12.365		25.2	1.0000	.9258	1.0000
2.						
3.						
4.						
5.						
NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio _____ Mol/Std.	
1.					A.P.I. Gravity of Liquid Hydrocarbon _____ Deg.	
2.					Specific Gravity Separator Gas _____	
3.					Specific Gravity Flowing Fluid _____	
4.					Critical Pressure _____ P.S.I.A.	
5.					Critical Temperature _____ R	
$P_c = 1474.2 P_r^2 = 2,173,266$						
NO.	P _r ²	P _w	P _w ²	P _c ² - P _w ²	(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.0266$	
1		237.2	56,264	2,117,002	(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.0199$	
2						
3						
4						
5						
Absolute Open Flow <u>294</u> Mcfd @ 15.025 Angle of Slope θ _____ Slope, n <u>.75</u>						
Remarks: _____						
Approved By Commission		Conducted By Jim Choquette		Calculated By James Smith		Checked By