

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
 Revised 9-1-65

Type Test ☒ Initial ☐ Annual ☐ Special						Test Date 9-18-80			
Company SUPRON ENERGY CORPORATION				Connection Southern Union Gathering Company					
Pool Blanco				Formation Mesaverde				Unit	
Completion Date 8-23-80		Total Depth 8160		Plug Back TD 8145		Elevation 6553		Farm or Lease Name Nordhaus	
Dis. Size 7.625 5.500	Wt. 26.40 15.50	d 6.969 4.950	Set At 3655 3583-8160	Perforations: From 5351 To 5799		Well No. 2-A			
Thg. Size 2.0625	Wt. 3.25	d 1.750	Set At 5794	Perforations: From 5724 To 5730		Unit Sec. Twp. Rge. C 11 31N 9W			
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Dual - Gas - Gas						Packer Set At 7840		County San Juan	
Producing Thru Tubing		Reservoir Temp. °F 6		Mean Annual Temp. °F		Baro. Press. - P _a 12		State New Mexico	
L 5714	H	G _g 0.650	% CO ₂	% N ₂	% H ₂ S	Prover	Meter Run	Taps	

FLOW DATA							TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	
SI	2"		3/4"				722		720		14 days
1.							126	58 ⁰	578		3 hours
2.											
3.											
4.											
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1	12.3650		138	1.0019	0.9608	1.012	1662
2.							
3.							
4.							
5.							

NO.	P _t	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.
1					A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.
2.					Specific Gravity Separator Gas _____ X X X X X X X X
3.					Specific Gravity Flowing Fluid _____ X X X X X
4.					Critical Pressure _____ P.S.I.A. _____ P.S.I.A.
5.					Critical Temperature _____ R _____ R

$P_c = 734$ $P_c^2 = 538,756$				
NO.	P _t	P _w	P _w ²	P _c ² - P _w ²
1		590	348,100	190,656
2.				
3.				
4.				
5.				

$$(1) \frac{P_c^2}{P_c^2 - P_w^2} = 2.8258$$

$$(2) \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 2.1794$$

$$AOF = Q \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 3622$$

Absolute Open Flow	3622	Mcf @ 15.025	Angle of Slope θ	Slope, n	0.75
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Remarks:			
Approved By Commission:	Conducted By: Steve Moore	Calculated By: Kenneth E. Roddy	Checked By: