

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
 Revised 9-1-65

Type Test ☒ Initial ☐ Annual ☐ Special				Test Date 5-2-80	
Company Getty Oil Co			Connection Not Connected		
Pool Blanco			Formation Pictured Cliffs		Unit
Completion Date 4-23-80		Total Depth 3200		Plug Back TD 3135	Elevation 6294 GL
Farm or Lease Name Don Turrietta					
Csg. Size 4.50	Wt. 9.5	d 1.090	Set At 3193	Perforations: From 2990 To 3032	
Well No. 1					
Thg. Size 1.90	Wt. 2.90	d 1.610	Set At 2995	Perforations: From open To ended	
Unit Sec. Twp. Rye. 0 32 30N 8R					
Type Well - Single - Brodenhead - G.G. or G.O. Multiple Single Gas				Packer Set At County San Juan	
Producing Thru tubing		Reservoir Temp. °F @		Mean Annual Temp. °F 12.0	
State New Mexico					
L 2995	H 2995	Gg .645	% CO ₂	% N ₂	% H ₂ S
Prover 2000				Meter Run Taps	

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F
SI							1038		1039		186 hr SI
1.	2.000 x .750						287	60	760		1st Hr
2.	2.000 x .750						227	60	616		2nd Hr
3.	2.000 x .750						200	60	542		3rd Hr
4.											
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1	11.00		299	1.000	1.245	1.029	1214
2	11.00		239	1.000	1.245	1.023	3348
3	11.00		212	1.000	1.245	1.020	2961
4.							
5.							

NO.	P _t	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.
1					A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.
2.					Specific Gravity Separator Gas _____ X X X X X X X X
3.					Specific Gravity Flowing Fluid _____ X X X X X
4.					Critical Pressure _____ P.S.I.A. _____ P.S.I.A.
5.					Critical Temperature _____ R _____ R

P _c 1051	P _c ² 1104601	(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.385$	(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.3190$	
NO.	P _t ²	P _w	P _w ²	P _c ² - P _w ²
1				
2				
3				
4	44914	554	306916	797685
5				

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 3,906$

Absolute Open Flow	3,906	Mcfd @ 15.025	Angle of Slope θ	Slope, n .85
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Remarks:			
Approved By Commission:	Conducted By: Mark Kramer	Calculated By: Paul D. Berhost	Checked By: