NEW MEXICO OIL CONSERVATION COMMSSION

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

Type Test: [X] Initial [ ] Annual [ ] Special				Test Date: 10-2-80	
Company: SUPRON ENERGY CORPORATION			Connection: Southern Union Gathering Company		
Pool: Blanco			Formation: Mesaverde		Unit
Completion Date: 9-17-80	Total Depth: 6860		Plug Back TD: 6844	Elevation: 5619	Farm or Lease Name: Haynie
Csg. Size: 5.500 / Wt.: 15.50 / d: 4.950 / Set At: 6859			Perforations: From 3899 To 4897		Well No.: 2
Tbg. Size: 2.0625 / Wt.: 3.25 / d: 1.750 / Set At: 4406			Perforations: From 4341 To 4346		Unit: B / Sec.: 4 / Twp.: 30-N / Rge.: 11-W
Type Well – Single – Bradenhead – G.G. or G.O. Multiple: Dual - Gas - Gas			Packer Set At: 6650		County: San Juan
Producing Thru: Tubing	Reservoir Temp. °F: @	Mean Annual Temp. °F:	Baro. Press. – P_a: 12		State: New Mexico
L: 4331	H:	Gg: 0.650	% CO_2:	% N_2:	% H_2S: / Prover: / Meter Run: / Taps:

FLOW DATA

NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h_w	Temp. °F	TUBING DATA Press. p.s.i.g.	TUBING DATA Temp. °F	CASING DATA Press. p.s.i.g.	CASING DATA Temp. °F	Duration of Flow
SI	2"		3/4"				1008		1012		15 days
1.							182	87°	846		3 hours
2.											
3.											
4.											
5.											

RATE OF FLOW CALCULATIONS

NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P_m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1	12.3650		194	0.9750	0.9608	1.016	2283
2.							
3.							
4.							
5.							

NO.	P_t	Temp. °R	T_t	Z
1.				
2.				
3.				
4.				
5.				

Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.
A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.
Specific Gravity Separator Gas _____ XXXXXXXXX
Specific Gravity Flowing Fluid _____ XXXXXX
Critical Pressure _____ P.S.I.A. _____ P.S.I.A.
Critical Temperature _____ R _____ R

P_c 1024 P_c^2 1,048,576

NO	P_t^2	P_w	P_w^2	$P_c^2 - P_w^2$
1		858	736,164	312,412
2				
3				
4				
5				

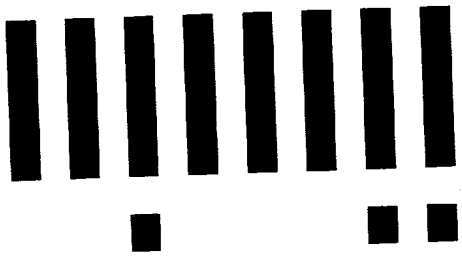
(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 3.3564$ (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 2.4796$

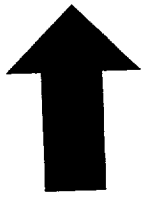
AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 5661$

Absolute Open Flow 5661 Mcfd @ 15.025 | Angle of Slope θ _____ | Slope, n 0.75

Remarks: _____

Approved By Commission:	Conducted By:	Calculated By:	Checked By:
	Steve Moore	Kenneth E. Roddy	





LTR

Job separation sheet

NEW MEXICO OIL CONSERVATION COMMSSION

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

Type Test			Test Date	
[X] Initial	[ ] Annual	[ ] Special	9-24-80	
Company: SUPRON ENERGY CORPORATION	Connection			
Pool: Basin	Formation: Dakota		Unit	
Completion Date: 9-17-80	Total Depth: 6860	Plug Back TD: 6844	Elevation: 5619	Farm or Lease Name: Haynie
Csg. Size: 5.500 / Wt.: 15.50 / d: 4.950 / Set At: 6859	Perforations: From 6702 To 6813			Well No.: 2
Tbg. Size: 2.0625 / Wt.: 3.25 / d: 1.750 / Set At: 6650	Perforations: From No Perforations To			Unit: B / Sec.: 4 / Twp.: 30-N / Rge.: 11-W
Type Well – Single – Bradenhead – G.G. or G.O. Multiple: Dual - Gas - Gas		Packer Set At: 6650		County: San Juan
Producing Thru: Tubing	Reservoir Temp. °F	Mean Annual Temp. °F	Baro. Press. – P_a: 12	State: New Mexico

L	H	Gg	% CO_2	% N_2	% H_2S	Prover	Meter Run	Taps
6640		0.700						

	FLOW DATA				TUBING DATA		CASING DATA		
NO.	Prover Line Size	X Orifice Size	Press. p.s.i.g.	Diff. h_w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	Duration of Flow
SI	2"	3/4"				1912				8 days
1.						78	64°			3 hours
2.										
3.										
4.										
5.										

RATE OF FLOW CALCULATIONS

NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P_m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1	12.3650		90	0.9962	0.9258	1.000	1026
2.							
3.							
4.							
5.							

NO.	P_t	Temp. °R	T_r	Z
1.				
2.				
3.				
4.				
5				

Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.
A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.
Specific Gravity Separator Gas _____ XXXXXXXXX
Specific Gravity Flowing Fluid XXXXX _____
Critical Pressure _____ P.S.I.A. _____ P.S.I.A.
Critical Temperature _____ R _____ R

P_c 1924 P_c^2 3,701,776

NO	P_t^2	P_w	P_w^2	$P_c^2 - P_w^2$
1			61,053	3,640,723
2				
3				
4				
5				

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.0168$ (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 1.0125$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 1039$

Absolute Open Flow 1039 Mcfd @ 15.025 Angle of Slope θ _____ Slope, n 0.75

Remarks: _____

Approved By Commission:	Conducted By:	Calculated By:	Checked By:
	Steve Moore	Kenneth E. Roddy	