STATE OF NEW MEXICO
ENERGY AND MINERALS DEPARTMENT

OIL CONSERVATION DIVISION

P O. BOX 2088
SANTA FE, NEW MEXICO 87501

Form C-122
Revised 10-1-78

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Type Test: [X] Initial [ ] Annual [ ] Special				Test Date: 12/1/81	
Company: Supron Energy Corporation			Connection: Southern Union Gathering Company		
Pool: Basin			Formation: Dakota		Unit
Completion Date: 11/21/81	Total Depth: 6740		Plug Back TD: 6680	Elevation: 5847	Farm or Lease Name: Reid "A"
Csg. Size: 4.500 / Wt.: 10.50 / d: 4.052 / Set At: 6739			Perforations: From 6509 To 6616		Well No.: 1-E
Tbg. Size: 2.375 / Wt.: 4.70 / d: 1.995 / Set At: 6580			Perforations: No Perforations From To		Unit: O / Sec.: 1 / Twp.: 30N / Rge.: 13W
Type Well – Single – Bradenhead – G.G. or G.O. Multiple: Single			Packer Set At:		County: San Juan
Producing Thru: Tubing	Reservoir Temp. °F:	Mean Annual Temp. °F:	Baro. Press. – P_a: 12		State: New Mexico

L	H	Gg	% CO_2	% N_2	% H_2S	Prover	Meter Run	Taps
6570		0.700						

	FLOW DATA				TUBING DATA		CASING DATA		
NO.	Prover Line Size	X Orifice Size	Press. p.s.i.g.	Diff. h_w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	Duration of Flow
SI	2"	3/4"				1354		1345		7 days
1.						118	63°	591		3 hours
2.										
3.										
4.										
5.										

RATE OF FLOW CALCULATIONS

NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P_m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1	12.3650		130	0.9971	0.9258	1.014	1505
2.							
3.							
4.							
5.							

NO.	P_t	Temp. °R	T_r	Z
1.				
2.				
3.				
4.				
5.				

Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.
A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.
Specific Gravity Separator Gas _____ XXXXXXXXX
Specific Gravity Flowing Fluid XXXXX _____
Critical Pressure _____ P.S.I.A. _____ P.S.I.A.
Critical Temperature _____ R _____ R

P_c 1366 P_c^2 1,865,956

NO	P_t^2	P_w	P_w^2	$P_c^2 - P_w^2$
1		603	363,609	1,502,347
2				
3				
4				
5				

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.2420$ (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 1.1764$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 1770$

Absolute Open Flow 1770 Mcfd @ 15.025 Angle of Slope θ _____ Slope, n 0.75

Remarks: _____

Approved By Division	Conducted By:	Calculated By:	Checked By:
	Floyd Woodward	Ken Roddy	