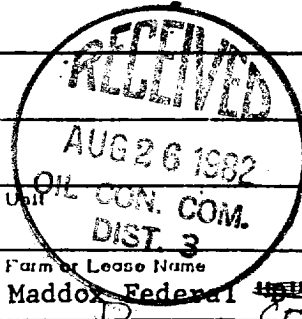


NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
 Revised 9-1-65

Type Test ☒ Initial ☐ Annual ☐ Special						Test Date 8/10/82					
Company Supron Energy Corporation				Connection El Paso Natural Gas Company							
Pool Basin				Formation Dakota							
Completion Date 7/17/82		Total Depth 6686		Plug Back TD 6630		Elevation 5832					
Csg. Size 4.500		Wt. 10.50		d 4.052		Set At 6679		Perforations: From 6433 To 6538		Well No. 1-E	
Tbg. Size 2.375		Wt. 4.70		d 1.995		Set At 6504		Perforations: From 6472 To 6478		Unit P Sec. 23 Twp. 30N Rge. 13W	
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single								Packer Set At - - -		County San Juan	
Producing Thru Tubing		Reservoir Temp. °F		Mean Annual Temp. °F		Baro. Press. - P _a 12		State New Mexico			
L 6462		H		Gg 0.700		% CO ₂		% N ₂		% H ₂ S	
Prover		Meter Run		Taps							

FLOW DATA							TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	
SI	2"		3/4"				1696		1696		7 Days
1.							147	72°	790		3 Hours
2.											
3.											
4.											
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1	12.3650		159	0.9887	0.9258	1.016	1828
2.							
3.							
4.							
5.							

NO.	P _i	Temp. °R	T _i	Z	Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.
1.					A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.
2.					Specific Gravity Separator Gas _____ X X X X X X X X
3.					Specific Gravity Flowing Fluid _____ X X X X X
4.					Critical Pressure _____ P.S.I.A. _____ P.S.I.A.
5.					Critical Temperature _____ R _____ R

P _c 1708		P _c ² 2,917,264	
NO.	P _i ²	P _w	P _w ²
1		802	643,204
2			
3			
4			
5			

$$(1) \frac{P_c^2}{P_c^2 - P_w^2} = \frac{1.2828}{1.2828 - 0.4176} = 1.2828$$

$$(2) \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = \frac{1.2054}{1.2054 - 0.4176} = 1.2054$$

$$AOF = Q \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 2203$$

Absolute Open Flow 2203	Mcf @ 15.025	Angle of Slope θ	Slope, n 0.75
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Remarks: _____

Approved by Commission:	Conducted by: Floyd Woodward	Calculated by: Kenneth E. Roddy	Checked by:
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