

3 NMOCD

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1 File

1 NWPL

OIL CONSERVATION DIVISION

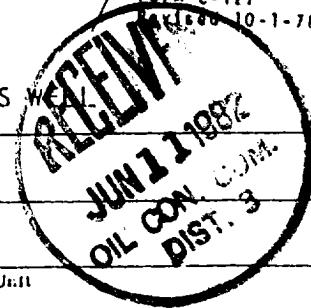
P. O. BOX 2088

STATE OF NEW MEXICO
ENERGY AND MINERALS DEPARTMENT

SANTA FE, NEW MEXICO 87501

Form C-127
Revised 10-1-78

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS



Type Test <input checked="" type="checkbox"/> Initial <input type="checkbox"/> Annual <input type="checkbox"/> Special		Test Date 6-4-82	
Company Dugan Production Corp.		Connection	
Pool Basin Dakota		Formation Dakota	
Completion Date 5-27-82		Total Depth 5650' RKB	
Plug Back TD 5586'		Elevation 5366' GL	
Farm or Lease Name Sly Slav		Well No. 1	
Csg. Size 4 1/2"	Wt. 10.5#	d 4.052	Set At 5663' RKB
Perforations: From 5442'		To 5558'	
Tbg. Size 1 1/2"	Wt. 2.9#	d 1.610	Set At 5496
Perforations: From open end			
Type Well - Single - Bradenhead - C.C. or G.O. Multiple Single - gas		Packer Set At None	
Producing Thru tbg.		Reservoir Temp. °F #	
Mean Annual Temp. °F		Baro. Press. - P _a	
State New Mexico		County San Juan	
L	H	G _g .65 est	% CO ₂
		% N ₂	% H ₂ S
Prover		Meter Run	
Taps			

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F
SI							1610		1610		7 days
1.											
2.											
3.	9/16"			223		58°			797		3 hrs
4.											
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow O, Mcfd
1							
2							
3	6.8294		235	1.002	.9608	1.025	1584
4							
5							

NO.	P ₁	Temp. °R	T ₁	Z	Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.
1					A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.
2					Specific Gravity Separator Gas _____ X X X X X X X X X
3					Specific Gravity Flowing Fluid _____ X X X X X
4					Critical Pressure _____ P.S.I.A. _____ P.S.I.A.
5					Critical Temperature _____ R _____ R

P _c	1622	P _c ²	2,630,884
NO.	P ₁	P _w	P _w ²
1			
2			
3	809	654,481	1,976,403
4			
5			

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.3311$ (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.2393$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1959$

Absolute Open Flow 1959 Mcfd @ 15,025 Angle of Slope θ _____ Slope, n .75

Remarks: Moderate spray of condensate and water at end of three hours.

Conducted By	Calculated By	Checked By
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