

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Type Test ☒ Initial ☐ Annual ☐ Special					Test Date 1/24/85					RECEIVED									
Company Union Texas Petroleum Corp.					Connection El Paso Natural Gas Company										JAN 28 1985				
Pool Basin					Formation Dakota										OIL CON. DIV. DIST. 3				
Completion Date 1/4/85			Total Depth 6370		Plug Back TD 6256		Elevation 5576		Farm or Lease Name McCord										
Csg. Size 4.5	Wt. 10.8	d 4.051	Set At 6370	Perforations: From 6240 To 6160		Well No. 3-5													
Inq. Size 2.375	Wt. 4.70	d 1.995	Set At 6168	Perforations: Open-Ended From To		Unit P	Sec. 28	Twp. 30N	Rge. 13W										
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single							Packer Set At ---		County San Juan										
Producing Thru Tubing		Reservoir Temp. °F 8		Mean Annual Temp. °F		Baro. Press. - P _a 12		State New Mexico											
L 6158	H	Gg 0.650	% CO ₂	% N ₂	% H ₂ S	Prover	Meter Run	Taps											

FLOW DATA							TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	
SI	2"		3/4"				1850		2012		7 days
1.							334	93°	821		3 hours
2.											
3.											
4.											
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor F _t	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1	12.3650		346	0.9697	0.9608	1.028	4098
2.							
3.							
4.							
5.							

NO.	P _t	Temp. °R	T _f	Z	Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.	
1					A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.	
2.					Specific Gravity Separator Gas _____ X X X X X X X X	
3.					Specific Gravity Flowing Fluid _____ X X X X X	
4.					Critical Pressure _____ P.S.I.A. _____ P.S.I.A.	
5.					Critical Temperature _____ R _____ R	

P _c 2024	P _c ² 4,096,576		
NO.	P _t ²	P _w	P _w ²
1		833	693,889
2			
3			
4			
5			

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = \frac{1.2039}{1.2039 - 0.6939} = 1.2039$

(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = \frac{1.1493}{1.1493 - 0.6939} = 1.1493$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 4710$

Absolute Open Flow	4710	Mcfd @ 15.025	Angle of Slope θ	Slope, n 0.75
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Remarks: _____

Approved By Division	Conducted By: Floyd Woodward	Calculated By: Ken Roddy	Checked By:
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