STATE OF NEW MEXICO
ENERGY AND MINERALS DEPARTMENT

P. O. BOX 2088
SANTA FE, NEW MEXICO 87501

Form C-122
Revised 10-1-78

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

RECEIVED
MAR 19 1985
OIL CON. DIV.
DIST. 3

Type Test: [X] Initial [ ] Annual [ ] Special				Test Date: 3/14/85	
Company: Robert L. Bayless		Connection:			
Pool: Basin Dakota		Formation: Dakota			Unit:
Completion Date: 3/6/85	Total Depth: 6187 TD	Plug Back TD: 6139	Elevation: 5681 RKB	Farm or Lease Name: Coolidge Com	
Csg. Size: 4.500 / Wt.: 11.5#/ft. / d: 4.052 / Set At: 6183	Perforations: From 5912 To 6051	Well No.: 1			
Tbg. Size: 1.900 / Wt.: 2.9#/ft. / d: 1.610 / Set At: 5941	Perforations: From To	Unit: A / Sec.: 22 / Twp.: 30N / Rge.: 14W			
Type Well – Single – Bradenhead – G.G. or G.O. Multiple: Gas - single		Packer Set At: none		County: San Juan	
Producing Thru: tubing	Reservoir Temp. °F:	Mean Annual Temp. °F:	Baro. Press. – P_a: 12.0	State: NM	
L	H	Gg: est .60	% CO_2	% N_2	% H_2S

Prover | Meter Run | Taps

FLOW DATA / TUBING DATA / CASING DATA

NO.	Prover Line Size X Orifice Size	Press. p.s.i.g.	Diff. h_w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	Duration of Flow
SI	8 days				1880		1880		SIP
1.	2" x .750				233	66°F	541		3 hrs.
2.									
3.									
4.									
5.									

RATE OF FLOW CALCULATIONS

NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P_m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1	12.365		245	.9943	1.000	1.018	3066
2.							
3.							
4.							
5.							

NO.	P_t	Temp. °R	T_r	Z
1.				
2.				
3.				
4.				
5.				

Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.
A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.
Specific Gravity Separator Gas _____ XXXXXXXXX
Specific Gravity Flowing Fluid XXXXX _____
Critical Pressure _____ P.S.I.A. _____ P.S.I.A.
Critical Temperature _____ R _____ R

P_c 1892 P_c^2 3,579,664

NO	P_t^2	P_w	P_w^2	$P_c^2 - P_w^2$
1		553	305,809	3,273,855
2				
3				
4				
5				

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.0934$

(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 1.0693$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 3279$

Absolute Open Flow 3279 Mcfd @ 15.025 | Angle of Slope θ _____ | Slope, n .75

Remarks: was making considerable condensate

Approved By Division	Conducted By:	Calculated By:	Checked By:
	Tom Smith	Kevin McCord	Robert L. Bayless