

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Revised 9-1-65

RECEIVED

Type Test ☒ Initial ☐ Annual ☐ Special				Test Date 9-3-85			
Company Blackwood & Nichols Co., Ltd.				Connection Northwest Pipeline			
Pool S Los Pinos Ft/PC				Formation Fruitland-Pictured Cliffs			
Completion Date 8-23-85		Total Depth 3439'		Plug Back TD 3390'		Elevation 6326'	
Csg. Size 4.500		Wt. 10.5		d 4.052		Set At 3439'	
Perforations: From 3274'		To 3356'		Well No. 215			
Tlg. Size 2.375		Wt. 4.7		d 1.995		Set At 3337'	
Perforations: From		To		Unit D 26 31N 7W			
Type Well - Single - Blindhead - G.G. or G.O. Multiple Single				Packer Set At		County San Juan	
Producing Thru Tubing L.		Reservoir Temp. °F #		Mean Annual Temp. °F		Baro. Press. - P _a 12.0	
H		Gg .65		% CO ₂		% N ₂	
				% H ₂ S		Prover 3/4"	
						Meter Run	
						Taps	

FLOW DATA							TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	
SI							1515		1515		
1.	3/4" choke						940	30°	1100		3 hours
2.											
3.											
4.											
5.											

RATE OF FLOW CALCULATIONS

NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor F _t	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1	12.365		952				11.771
2.							
3.							
4.							
5.							

NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.
1.					A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.
2.					Specific Gravity Separator Gas _____ X X X X X X X X
3.					Specific Gravity Flowing Fluid _____ X X X X X
4.					Critical Pressure _____ P.S.I.A. _____ P.S.I.A.
5.					Critical Temperature _____ R _____ R

P_c 1527 P_c^2 2,331,729					$(1) \frac{P_c^2}{P_c^2 - P_w^2} = 2.1291$		$(2) \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.9009$	
NO.	P_t^2	P_w	P_w^2	$P_c^2 - P_w^2$				
1	906,304	1112	1,236,544	1,095,85				
2								
3								
4								
5								

$AOF = Q \left[\frac{P_c^2 - P_w^2}{P_c^2 - P_w^2} \right]^n = 22,376$

Absolute Open Flow 22,376		Mcf @ 15.025		Angle of Slope θ		Slope, n 0.85	
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Remarks:			
Approved By Commission:		Conducted By: Thompson & Loos	
Calculated By: W. F. Clark		Checked By:	