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See Rule 401 & Rule 1122

State of New Mexico
Energy, Minerals and Natural Resources Department

Form C-122
Revised 4-1-91

OIL CONSERVATION DIVISION

P.O. Box 2088
Santa Fe, New Mexico 87504-2088

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Operator Dugan Production Corp.						Lease or Unit Name Lisbon Com					
Type Test ☒ Initial ☐ Annual ☐ Special						Test Date 12-1-92		Well No. #1			
Completion Date 11-20-92		Total Depth 5953'		Plug Back TD 5859'		Elevation 5575' GL		Unit Lr. - Sec. - TWP - Rge. I - 5- 30N- 14W			
Csg. Size 4 1/2"		Wt. 11.6#		Set At 5948'		Perforations: From: 5669 To: 5778'		Country San Juan			
Tbg. Size 1 1/2"		Wt. 2.9#		Set At 5705'		Perforations: From: open end To:		Pool Basin Dakota			
Type Well - Single - Bradenhead - G.G. or G.O. Multiple single						Packer Set At		Formation Dakota			
Producing Thru tubing		Reservoir Temp. °F		Mean Annual Temp. °F		Baro. Press - P _a		Connection			
L		H		G _g 0.71		% CO ₂		% N ₂		% H ₂ S	
Prover		Meter Run		Taps							

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	
SI						1670		1670		7 days
1.	2" x 3/4"					530		950		1 hr.
2.	2" x 3/4"					340		735		2 hrs.
3.	2" x 3/4"					231	35°	725		3 hrs.
4.										
5.										

RATE OF FLOW CALCULATIONS							
NO.	COEFFICIENT (24 HOUR)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft	Gravity Factor F _g	Super Compress. Factor, F _{sp}	Rate of Flow Q, Mcfd
1.							
2.							
3.							
4.	11.0		243	1.025	1.1868	1.0017	3257
5.							

NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	Mcft/bbl
1.				0.9966	A.P. L Gravity of Liquid Hydrocarbons	Deg
2.					Specific Gravity Separator Gas	XXXXXXXXXX
3.					Specific Gravity Flowing Fluid	XXXXXX
4.					Critical Pressure	P.S.I.A. P.S.I.A.
5.					Critical Temperature	R R

P_c 1682 P_c² 2829124

NO.	P _i ²	P _w	P _w ²	P _c ² - P _w ²
1.				
2.				
3.		737	543169	2285955
4.				
5.				

1) $\frac{P_i^2}{P_c^2 - P_w^2} = 1.2376$ (2) $\left[\frac{P_i^2}{P_c^2 - P_w^2} \right]^n = 1.17$

AOF = Q $\left[\frac{P_i^2}{P_c^2 - P_w^2} \right]^n = 3822$

Absolute Open Flow	3822	Mcfd @ 15.025	Angle of Slope θ	Slope, n .75
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Remarks: Test conducted through separator. Small amount of water and oil produced during test.

Approved By Division	Conducted By: C. Hall	Calculated By: C. Hall	Checked By:
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