

COMPLETION HISTORY

GOVERNMENT UNION - GOVERNMENT 1-19

San Juan County, New Mexico

1000' from South Line
1000' from West Line
Sec. 19-T2N-R12W

1) Drilled 8 3/4" hole, mechanical oil circulation used to 3000'. Drilling to this depth was generally uneventful except for lost circulation (bore hole believed filled with cement) at 3000'. Returns (75%) regained in 10 hours.

2) Ran 7"-20 API casing and set at 3000'. Cemented with 150 sacks with OK gel. Hole stopped full with negligible to moderate loss while running in. Circulated lost joint to bottom with 75% returns. Recirculated casing 30 minutes with 20-75% returns. Returns dropped to 25% and recirculation stopped. Mixed and displaced cement with water to 30% returns throughout job. Dumped plugs with 1400 poig -- purposely bled to 700 poig and shut in.

Control valves (recirculating) and overbore from shoe to 4400'. Ran Baker differential fill-up float shoe and collar on lower joint. String consists of 66 lbs.-1971' of 2 3/4"-J-55 on bottom and 139 lbs.-3017' of 2 3/4"-J-55 on top.

3) WOC 12 hours - - released pressure - - ran temperature survey. Found cement top at 4500'.

4) Flow well dry with supply gas and drilled plug (reportedly hard cement) after 24 hours WOC.

5) Drilled 6 1/2" hole with gas to 6000'. Drilling time indicated Bohco top at 6747'. Natural gas flow test at 6005' indicated no flow - - test at 6015' indicated 700 MCFD.

6) Ran Nelson Radioactivity Log, but depth component failed. Plan to run log after setting liner.

EXPLANATION OF RESULTS

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7) Ran 1910' (60 joints) of 3 1/2"-14 and 15.50-3-15 liner with couplings turned to 1.875". (String consists of 1800' of 3 1/2" casing and 4' Burns liner hanger-packer. Jet through 6th joints from bottom are 140 (220'), remainder 15.50. Liner extends from 4009' to 4019'. Cemented by displacing 100 sacks with oil gel around liner in dry hole. Displaced with water and banded plug with 1500 poig. Released pressure and set packing element on hanger. Pulled up 20' and reversed out excess cement.

It was necessary to stimulate last three joints to bottom with gas, presumably because of continuous accumulation. Could not get below 4000'.

8) WOC 34 hours and then found only soft waxy cement around liner top - - - this believed due to gas cutting and not representative of that behind liner. Found lower plug as expected at 4700' and drilled hard cement to 4800'.

9) Ran Schlumberger temperature survey and confirmed cement to liner top.

10) Ran Waco Radioactivity Log.

11) Tested everything below surface to 4000' to 3000 poig.

12) Perforated with 4 Waco Dyna Jets per foot: 6747'-6779' and 6786'-6801'.

13) Broke down blocks with water at 500 poig - - - took 10 RPM at 900 poig.

14) Sand-water forced blocks through casing at 51 RPM with 40,000 (40-60 mesh) sand. Slow gradual pressure buildup throughout job from 2000 to 2400 poig --- no sharp buildups or hiccups. Had 1000 hbls. water --- 150 hbls. bottom sand, 500 hbls., with sand, 500 hbls. flush. Pressure held steady after job to 2000 poig in 5 minutes, 500 poig in 20 minutes, 140 poig in 1 hour 40 minutes. Opened well and flowed 2" stream water for 20 minutes.

Injected rubber balls as follows: 20 after 10,000 sand, 20 after 22,000 sand, 20 after 34,000 sand, and 20 after 40,000 sand.

Ran wireline and found no sand fill-up.

15) Started blowing well dry with supply gas. Well blew in naturally after 6 hours blowing at 1500'. Cleaned to bottom with bit (4 3/4") and made 2" hole to 6811' - Plus Both Total Depth.

16) Settled back after 15 hours blowing was 3.5 MMCFD.

17) Set Baker Magnesium Bridge Plug on wireline at 6725'. Filled with water and pressure tested to 700 psig.

18) Perforated Baker Lockout (Glass Verde) with 2 Baker Dyna Jets per foot: 4613'-4630', 4723'-4732', 4737'-4744', 4757'-4764', 4773'-4787', 4794'-4800', 4814'-4819'. (Shocked Bridge Plug with first gun and found properly in place.)

19) Sand-water forced fluid lockout (Glass Verde) at 67 MM with 100,000# (20-40 mesh) sand. Bore down at 300 psig, minimum pressure 700 psig, minimum pressure 2100 psig. Injected 120 rubber balls with distinct results as follows: 30 balls after 10,000 sand (caused buildup from 300 psig to 1300 psig), 30 balls after 25,000 sand (caused buildup from 1300 psig to 2000 psig -- bore back to 1300 psig), 25 balls after 62,000 sand (caused buildup from 1300 psig to 1800 psig -- bore back to 1300 psig), 25 balls after 65,000 sand (caused buildup from 1600 psig to 2000 psig). Flushed with 200 barrels water. Used total of 300 barrels water (200 bbls. before sand - 200 barrels with sand - 300 barrels after flush). Pressure held to 200 psig immediately and to zero 10 minutes after pumping stopped. Found 170' of sand fill-up in 3 1/2" casing above Bridge Plug.

20) Blew well dry with supply gas and cleaned out sand. Well did not blow in naturally but made 1 MMCFD when cleaned below parts.

21) Drilled Bridge Plug at 6725' and cleaned to 7020 of 6011'.

22) Both zones together made 3.9 MMCFD, blowing generally dry after 7 hours. Later when Sahara shut off the Glass Verde made 1.25 MMCFD. Therefore, Sahara making 4.5 MMCFD.

23) Effected dual completion as detailed by attached schematic diagram dated 9-11-57.

Pertinent data regarding physical aspects of dual completion equipment are:

- A) Baker Model B-45 set in 3 1/2" casing 6578'-6582'.
- B) Baker Model B-67-22 set in 7" casing 4567'-4591 1/2'.
- C) 1902' of 2 3/8" EWH tubing with a Baker Right Hand Release sub at 5724' is included in the string between packers.
- D) 8 1/2' of sealing element coverage is centered through the lower packer.
- E) A 5' orange painted, slotted 2" regular production tube hangs below the sand tube.

***** 3.1 new subrole added to table and deleted (1)

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- F) A 6 1/2' Baker Dual Line Flow Tube supports the 2 1/8" tubing. A leather sub situated 1/2' below the top of the Flow Tube seats about 2" below the top of the top packer. Also, gasket - tubing sealing elements are contained on the Flow Tube.
- G) A 2 1/2' Otis Type X Cross-Over Assembly ties on top of the Baker Dual Line Flow Tube. A Type X choke now allows the fluids to be diverted into the annulus above the top packer. This could be replaced with a Type 2 Choke which would divert the upper flow fluids through the annulus.
- H) 4573' of 2 7/8" NPH tubing extends from the top of the Otis Cross-Over Nipple to the surface tubing landing down in a Hunter Type HNL, lined with neoprene rubber.

24) Initial surface pressure buildup data were:

	BARRETT	WELLS
After 24 hours	2025 psig	1920 psig
After 48 hours	2030 psig	1940 psig
After 72 hours	2040 psig	1930 psig
After 96 hours	2075 psig	1930 psig
After 120 hours	2080 psig	1940 psig
After 144 hours		

Note: All mentioned depths are Kelly Logging reference.
The tubing is landed at ground level or 12' below Kelly Logging.

By J. B. Ladd
J. B. LADD
September 12, 1957

(1) A 1/2" O.D. x 1/4" wall tube was used for the flow tube. A location was situated 1' below the top of the flow tube. The flow tube was about 1" below the top of the top cover. Also, a check - tapping sealing element was contained on the flow tube.

(2) A 1/2" O.D. x 1/4" wall tube was used for the flow tube. A location was situated 1' below the top of the flow tube. The flow tube was about 1" below the top of the top cover. Also, a check - tapping sealing element was contained on the flow tube.

(3) A 1/2" O.D. x 1/4" wall tube was used for the flow tube. A location was situated 1' below the top of the flow tube. The flow tube was about 1" below the top of the top cover. Also, a check - tapping sealing element was contained on the flow tube.

(4) Initial surface pressure build-up data were:

TIME	DATA	TIME
1000	1000	1000
1000	1000	1000
1000	1000	1000
1000	1000	1000
1000	1000	1000
1000	1000	1000

Note: All mentioned depths are Kelly Building reference. The tubing is located at ground level or 1' below Kelly Building.

[Signature]
 J. R. LADD
 September 12, 1957