

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

Type Test ☒ Initial ☐ Annual ☐ Special					Test Date 10-23-72	
Company AMOCO PRODUCTION COMPANY				Connection		
Pool Ute Dome				Formation Dakota		Unit
Completion Date 10-23-72		Total Depth 3060		Plug Back TD 3022		Elevation 6343 GL
Farm or Lease Name Mt. Ute Gas Com "E"		Well No. 1				
Csg. Size 5.5"	Wt. 15#	d	Set At 3055	Perforations: From 2920 To 2988		Unit G
Tbg. Size 2-3/8"	Wt.	d	Set At 2965	Perforations: From 2960 To 2965		Sec. 10 Twp. 31N Rge. 14W
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single				Packer Set At 2960		County San Juan
Producing Thru Tubing		Reservoir Temp. *F 104° @ 3060		Mean Annual Temp. *F Est. 60°		State New Mexico
L 2960	H	Gg .70	% CO ₂	% N ₂	% H ₂ S	Prover Meter Run Taps

FLOW DATA					TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	X XXXXXX Size Choke	Press. p.s.i.g.	Diff. h _w	Temp. *F	Press. p.s.i.g.	Temp. *F	Press. p.s.i.g.	
SI	11 Day					750		750	
1.	2-Inch	3/4				303	60° Est.	715	3 Hrs.
2.									
3.									
4.									
5.									

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1	12.3650		315	1.00	.9258	1.037	3739
2.							
3.							
4.							
5.							

NO.	P _r	Temp. *R	T _r	Z	Gas Liquid Hydrocarbon Ratio	Mcf/bbl.
1.					A.P.I. Gravity of Liquid Hydrocarbon	_____ Deg.
2.					Specific Gravity Separator Gas	XXXXXXX
3.					Specific Gravity Flowing Fluid	XXXXXXX
4.					Critical Pressure	_____ P.S.I.A.
5.					Critical Temperature	_____ R

P _c 762	P _c ² 580,644		
NO.	P _t ²	P _w	P _w ²
1		727	528,529
2			
3			
4			
5			

$$(1) \frac{P_c^2}{P_c^2 - P_w^2} = 11.14$$

$$AOF = Q \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 28,940$$

$$(2) \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 7.74$$

Absolute Open Flow 28,940	Mcfd @ 15.025	Angle of Slope ϕ	Slope, n .85
Remarks:			
Approved By Commission:	Conducted By: B. D. Dukas	Calculated By: P. C. Ellison	Checked By: J. Arnold Snell