

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

Type Test <input checked="" type="checkbox"/> Initial <input type="checkbox"/> Annual <input type="checkbox"/> Special				Test Date 2-19-77							
Company AMOCO PRODUCTION COMPANY			Connection								
Pool Blanco		Formation Pictured Cliffs		Unit							
Completion Date 2-12-77		Total Depth 2786	Plug Back TD 2747	Elevation 5775	Farm or Lease Name Boyd Gas Com "B"						
Csg. Size 4.500	Wt. 10.5	d 4.052	Set At 2784	Perforations: From 2528 To 2602							
Tbg. Size 2.375	Wt. 4.7	d 1.995	Set At 2616	Perforations: From Open To Ended							
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single			Packer Set At None		Well No. 1						
Producing Thru Tbg.		Reservoir Temp. °F @	Mean Annual Temp. °F	Baro. Press. - P _a 12	State New Mexico						
L	H	Gg .65	% CO ₂	% N ₂	% H ₂ S						
Prover		Meter Run	Taps								
FLOW DATA			TUBING DATA		CASING DATA						
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	Duration of Flow
1.	2.375"		.750				755	60°	755		3 Hrs.
2.							100		340		
3.											
4.											
5.											
RATE OF FLOW CALCULATIONS											
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd				
1	12.365		112	1.000	.9608	1.010	1344				
2.											
3.											
4.											
5.											
NO.	P _t	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl. A.P.I. Gravity of Liquid Hydrocarbons _____ Deg. Specific Gravity Separator Gas _____ X X X X X X X X Specific Gravity Flowing Fluid _____ X X X X X Critical Pressure _____ P.S.I.A. _____ P.S.I.A. Critical Temperature _____ R _____ R						
1											
2.											
3.											
4.											
5.											
P _c 767 P _c ² 588,289											
NO.	P _t ²	P _w	P _w ²	P _c ² - P _w ²	(1) $\frac{P_c^2}{P_c^2 - P_w^2} =$		(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n =$				
1		352	123,904	464,385	1.2668		1.2227				
2											
3											
4											
5											
AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n =$					1643						
Absolute Open Flow 1643				Mcf/d @ 15.025		Angle of Slope θ		Slope, n .85			
Remarks:											
Original signed by:											
Approved By Commission:			Conducted By: T. M. Oliver			Calculated By: Oliver/W.R. Bloom			Checked By: H. D. MONTGOMERY		