

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELLS

Form C-122

RECEIVED

JUL 13 1983

Type Test ☐ Initial ☒ Annual ☒ Special				Test Date 6-24-83		OIL CON. DIV. DIST. 3	
Company AMOCO PRODUCTION COMPANY				Connection Southern Union Gas Co.			
Pool Ute Dome				Formation Dakota		Unit	
Completion Date 4-5-83		Total Depth 2436		Plug Back TD 2378		Elevation 6150	
Farm or Lease Name Ute Indians "A"		Well No. 5		Perforations: From 2220 To 2344		Unit Sec. Twp. Rge. K 35 32 14	
Csg. Size 4.500		Wt. 10.5		d 4.052		Set At 2436	
Tbg. Size 2.375		Wt. 4.7		d 1.995		Set At 2339	
Type Well - Single - Dradhead - G.C. or G.O. Multiple Single				Packer Set At None		County San Juan	
Producing Thru Tubing		Reservoir Temp. °F P		Mean Annual Temp. °F		Baro. Press. - P _a	
State New Mexico		L		H		Gg	
% CO ₂		% N ₂		% H ₂ S		Prover	
Meter Run		Taps					

FLOW DATA							TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	
SI	7 Days						468		468		
1.	2.375		.750				112		240		3 hrs
2.											
3.											
4.											
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor F _t	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1	12.365		124	1.000	.9258	1.013	1438
2.							
3.							
4.							
5.							

NO.	P _t	Temp. °R	T _f	Z	Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.
1.					A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.
2.					Specific Gravity Separator Gas _____ X X X X X X X X
3.					Specific Gravity Flowing Fluid _____ X X X X X
4.					Critical Pressure _____ P.S.I.A. _____ P.S.I.A.
5.					Critical Temperature _____ R _____ R

NO.	P _c	P _w	P _c ²	P _w ²	P _c ² - P _w ²
1	480	252	230400	63504	166896
2					
3					
4					
5					

$$(1) \frac{P_c^2}{P_c^2 - P_w^2} = \frac{1.3805}{1.3805 - 1.2736} = 1.3805$$

$$(2) \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = \frac{1.2736}{1.3805 - 1.2736} = 1.2736$$

$$AOIF = Q \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1831$$

$$Q = 1831$$

Absolute Open Flow	1831	Mcf/d @ 15.025	Angle of Slope θ	Slope, n	75
--------------------	------	----------------	------------------	----------	----

Remarks: Repair csg leak from 18 to 1500 ft by running a liner from TD to surface.
Well cased perf. & foam fractured.

Approved By Commission	Conducted By	Calculated By	Checked By
	J. J. Barnett	J. J. Barnett	