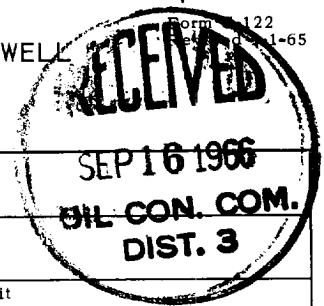


NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL



Type Test ☒ Initial ☐ Annual ☐ Special					Test Date 9/5/66		RECEIVED SEP 16 1966 OIL CON. COM. DIST. 3		
Company Aztec Oil and Gas				Connection Southern Union Gathering					
Pool Basin Dakota				Formation Dakota			Unit		
Completion Date 8/30/66		Total Depth 7320		Plug Back TD 7312		Elevation 6117		Farm or Lease Name Culpepper Martin	
Csg. Size 4 1/2	Wt. 10.5 & 11.6	d 4.000	Set At 7330	Perforations: From 4912 To 5009			Well No. 5		
Tbg. Size 1 1/2	Wt. 2.75	d 1.61	Set At 7125	Perforations: From 7130 To open ended			Unit M	Sec. 22	Twp. 32N
Type Well - Single - Bradenhead - G.G. or G.O. Multiple GG Dual					Packer Set At 7125		County San Juan		
Producing Thru casing		Reservoir Temp. °F @		Mean Annual Temp. °F		Baro. Press. - P _a		State New Mexico	
L 3438	H	Gg	% CO ₂	% N ₂	% H ₂ S	Prover	Meter Run	Taps	

FLOW DATA							TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	
SI	2"		3/4"		8 day SI		1944				
1.							141	60 (est)			3 hr
2.											
3.											
4.											
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1	12.365		153	1.000	.9258	1.019	1785
2.							
3.							
4.							
5.							

NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.
1.					A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.
2.					Specific Gravity Separator Gas _____ X X X X X X X X
3.					Specific Gravity Flowing Fluid _____ X X X X X
4.					Critical Pressure _____ P.S.I.A. _____ P.S.I.A.
5.					Critical Temperature _____ R _____ R

P _c 1956	P _c ² 3,825,936			
NO.	P _t ²	P _w	P _w ²	P _c ² - P _w ²
1		535	285,825	3,540,112
2				
3				
4				
5				

$$(1) \frac{P_c^2}{P_c^2 - P_w^2} = 1.08$$

$$(2) \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.06$$

$$AOF = Q \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1892$$

Absolute Open Flow 1892 Mcfd @ 15.025	Angle of Slope θ _____	Slope, n .75
Remarks: _____		
Approved By Commission:	Conducted By:	Calculated Original Signed By Carl E. Jameson
		Checked By: