NEW MEXICO OIL CONSERVATION COMMISSION

**Corrected Report**

Form C-122
Revised 12-1-55

MULTI-POINT BACK PRESSURE TEST FOR GAS WELLS

Pool **Basin-Dakota** Formation **Dakota** County **San Juan**

Initial **x** Annual _____ Special _____ Date of Test **2-4-61**

Company **Adobe Oil Company** Lease **Elliott** Well No. **1**

Unit **G** Sec. **20** Twp. **31N** Rge. **13W** Purchaser **El Paso Natural Gas Co.**

Casing **5.5** Wt. **15.5** I.D. **5.012** Set at **6650** Perf. **6518** To **6640**

Tubing **2 3/8** Wt. **4.7** I.D. **1.995** Set at **6615** Perf. **Open** To _____

Gas Pay: From **6518** To **6640** L _____ xG **.675** -GL _____ Bar.Press. **12**

Producing Thru: Casing _____ Tubing **x** Type Well **Single-Tubing**
Single-Bradenhead-G. G. or G.O. Dual

Date of Completion: **1-26-61** Packer **None** Reservoir Temp. _____

OBSERVED DATA

Tested Through (Prover) (Choke) (Meter) Type Taps _____

| | Flow Data | | | | | Tubing Data | | Casing Data | | |
|---|---|---|---|---|---|---|---|---|---|---|
| No. | (Prover) (Line) Size | (Choke) (Orifice) Size | Press. psig | Diff. $h_w$ | Temp. °F. | Press. psig | Temp. °F. | Press. psig | Temp. °F. | Duration of Flow Hr. |
| SI | | | | | | 2059 | 22 | 2063 | 22 | SI 7 days |
| 1. | | 3/4 | 223 | | 44 | 223 | 44 | 611 | 22 | 3 hrs. |
| 2. | | | | | | | | | | |
| 3. | | | | | | | | | | |
| 4. | | | | | | | | | | |
| 5. | | | | | | | | | | |

FLOW CALCULATIONS

| No. | Coefficient (24-Hour) | $\sqrt{h_w p_f}$ | Pressure psia | Flow Temp. Factor $F_t$ | Gravity Factor $F_g$ | Compress. Factor $F_{pv}$ | Rate of Flow Q-MCFPD @ 15.025 psia |
|---|---|---|---|---|---|---|---|
| 1. | | | | | | | |
| 2. | 12.365 | | 235 | 1.0158 | .9359 | 1.028 | 2795 |
| 3. | | | | | | | |
| 4. | | | | | | | |
| 5. | | | | | | | |

PRESSURE CALCULATIONS

Gas Liquid Hydrocarbon Ratio _____ cf/bbl. Specific Gravity Separator Gas _____
Gravity of Liquid Hydrocarbons _____ deg. Specific Gravity Flowing Fluid _____
$P_c$ _____ $(1-e^{-s})$ _____ $P_c$ **2075** $P_c^2$ **4306**

| No. | $P_w$ $P_t$ (psia) | $P_t^2$ | $F_cQ$ | $(F_cQ)^2$ | $\frac{(F_cQ)^2}{(1-e^{-s})}$ | $P_w^2$ | $P_c^2-P_w^2$ | Cal. $P_w$ | $\frac{P_w}{P_c}$ |
|---|---|---|---|---|---|---|---|---|---|
| 1. | | | | | | | | | |
| 2. | | | | | | 388 | 3918 | | |
| 3. | | | | | | | | | |
| 4. | | | | | | | | | |
| 5. | | | | | | | | | |

Absolute Potential: **2,999** MCFPD; n **.75**

COMPANY **Adobe Oil Company**

ADDRESS **1223 Petroleum Life Building, Midland, Texas**

AGENT and TITLE **A.T.Sindel, Vice-President** A T Sindel

WITNESSED **Lonnie Kramer**

COMPANY _____

REMARKS

## INSTRUCTIONS

This form is to be used for reporting multi-point back pressure tests on gas wells in the State, except those on which special orders are applicable. Three copies of this form and the back pressure curve shall be filed with the Commission at Box 871, Santa Fe.

The log log paper used for plotting the back pressure curve shall be of at least three inch cycles.

## NOMENCLATURE

Q = Actual rate of flow at end of flow period at W. H. working pressure ($P_w$). MCF/da. @ 15.025 psia and 60° F.

$P_c$ = 72 hour wellhead shut-in casing (or tubing) pressure whichever is greater. psia

$P_w$ = Static wellhead working pressure as determined at the end of flow period. (Casing if flowing thru tubing, tubing if flowing thru casing.) psia

$P_t$ = Flowing wellhead pressure (tubing if flowing through tubing, casing if flowing through casing.) psia

$P_f$ = Meter pressure, psia.

$h_w$ = Differential meter pressure, inches water.

$F_g$ = Gravity correction factor.

$F_t$ = Flowing temperature correction factor.

$F_{pv}$ = Supercompressability factor.

n = Slope of back pressure curve.

Note: If $P_w$ cannot be taken because of manner of completion or condition of well, then $P_w$ must be calculated by adding the pressure drop due to friction within the flow string to $P_t$.