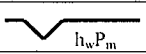
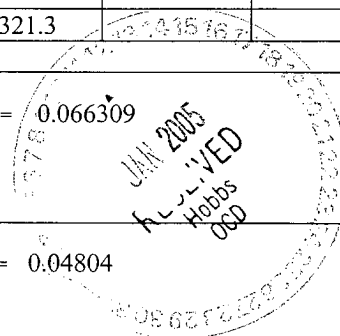


**DELIVERABILITY TEST REPORT**

30-025-24559

Operator Yates Petroleum Corporation					Lease or Unit Name RL Burns ATL					
Type Test <input type="checkbox"/> Initial <input type="checkbox"/> Annual <input checked="" type="checkbox"/> Special					Test Date 12/29/04		Well No. 1			
Completion Date 6/16/2000		Total Depth 12593'		Plug Back TD 12225'		Elevation 3985'		Unit Ltr. - Sec. - TWP - Rge. P 11 16S 35E		
Csg. Size 5.500	Wt. 17.00	d 4.892	Set At 12593'	Perforations: From: 12204' To: 12211'			County Lea			
Thg. Size 2.875	Wt. 6.500	d 2.441	Set At 11700'	Perforations: From: To:			Pool North Shoebar Atoka Gas and Townsend Morrow			
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single				Packer Set At 11700'			Formation Atoka and Morrow			
Producing Thru Tubing		Reservoir Temp. °F 187		Mean Annual Temp. °F 60		Baro. Press - P <sub>s</sub> 13.2		Connection Agave Energy Company		
L 11700'	H 12004'	Gg 0.689	%CO <sub>2</sub> 0.635	%N <sub>2</sub> 0.976	%H <sub>2</sub> S 0.000	Prover 0.000	Meter Run 4.029	Taps Flange		
FLOW DATA					TUBING DATA			CASING DATA		Duration Of Flow
No.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h <sub>w</sub>	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	
SI	0.000	X	0.000	0	0.0	0	600	60		
1.	4.026	X	0.625	54.3	452.3	85.5	216	60		2 hr.
RATE OF FLOW CALCULATIONS										
No.	COEFFICIENT (24 HOUR)			Pressure P <sub>m</sub>	Flow Temp. Factor Ft.	Gravity Factor F <sub>g</sub>	Super Compress. Factor, F <sub>pv</sub>	Rate of Flow Q, Mcfd		
1.	1.845		174.7	67.5	0.9759	1.205	1.006	381		
No.	P <sub>r</sub>	Temp. °R	T <sub>r</sub>	Z	Gas Liquid Hydrocarbon Ratio <u>N/A</u> Mcf/bbl.					
1.	0.1004	546	1.432	0.988	A. P. I. Gravity of Liquid Hydrocarbons <u>60.0</u> Deg.					
	P <sub>d</sub>					Specific Gravity Separator Gas <u>0.689</u>			XXXXXXXXXX	
	P <sub>d</sub> <sup>2</sup>					Specific Gravity Flowing Fluid <u>XXXXXX</u>			N/A	
	P <sub>c</sub>	P <sub>c</sub> <sup>2</sup>					Critical Pressure <u>672</u> P.S.I.A.			N/A P.S.I.A.
	P <sub>r</sub>	P <sub>r</sub> <sup>2</sup>					Critical Temperature <u>384</u> R.			N/A R
No.	P <sub>i</sub>	P <sub>i</sub> <sup>2</sup>	P <sub>c</sub> <sup>2</sup> - P <sub>i</sub> <sup>2</sup>	P <sub>w</sub>	P <sub>w</sub> <sup>2</sup>	P <sub>c</sub> <sup>2</sup> - P <sub>w</sub> <sup>2</sup>	P <sub>s</sub>	P <sub>s</sub> <sup>2</sup>	P <sub>r</sub> <sup>2</sup> - P <sub>s</sub> <sup>2</sup>	
1.				233.9	54.73	321.3				
$\left[ \frac{P_c^2 - P_d^2}{P_c^2 - P_w^2} \right] = \left[ \frac{374.3}{321.3} \right] = 1.165$					$\text{Log} \left[ \frac{P_c^2 - P_d^2}{P_c^2 - P_w^2} \right] = 0.066309$					
$\left[ \frac{P_c^2 - P_d^2}{P_c^2 - P_w^2} \right]^n = 1.117$					$n \text{ Log} \left[ \frac{P_c^2 - P_d^2}{P_c^2 - P_w^2} \right] = 0.04804$					
$\text{Deliv.} = Q \left[ \frac{P_c^2 - P_d^2}{P_c^2 - P_w^2} \right]^n = (381) (1.117)$					Commission <u><i>Paul Hobbs</i></u> Company <u>George Freeman</u> Others _____					
Deliv. <u>426</u> Mcfd n <u>0.7245</u> Previous back-pressure test										



WORKSHEET FOR CALCULATION OF STATIC COLUMN WELLHEAD PRESSURE (Pw) C-122D

DATE 12/29/2004

COMPANY Yates Petroleum Corporation LEASE R.L. Burns ATL WELL NO. 1

LOCATION: Unit P Section 11 Township 16S RANGE 35E

L 11700 H 12004 L/H 0.974 G 0.689 %CO2 0.635 %N2 0.976 %H2S 0.000

d 2.441 Fr 0.010763 GH 8271 Pcr 672 Tcr 381

LINE	1 <sup>st</sup> Trial	2 <sup>nd</sup> Trial	3 <sup>rd</sup> Trial	4 <sup>th</sup> Trial	5 <sup>th</sup> Trial
1 Qm	381	381			
2 Tw(W.H.°R)	520	520			
3 Ts(B.H.°R)	647	647			
4 T = (Tw + Ts) / 2	583.5	583.5			
5 Z (Est.)	0.962	0.961			
6 TZ	561.1	560.6			
7 GH / TZ	14.74	14.75			
8 e <sup>-s</sup> (Table XIV)	1.738	1.739			
9 1-e <sup>-s</sup> (Table XIV)	0.425	0.425			
10 Pt	229.2	229.2			
11 Pt <sup>2</sup> / 1000	52.53	52.53			
12 Fr (Table XV)	0.010763	0.010763			
13 Fc = FrTZ	6.039	6.034			
14 FcQm	2.304	2.302			
15 L / H(FcQm) <sup>2</sup>	5.173	5.164			
16 Fw = L/H(FcQm) <sup>2</sup> (1-e <sup>-s</sup> )	2.197	2.194			
17 Pw <sup>2</sup> = Pt <sup>2</sup> + Fw	54.73	54.73			
18 Ps <sup>2</sup> = e <sup>s</sup> Pw <sup>2</sup>	95.12	95.16			
19 Ps	308.4	308.5			
20 P = (Pt + Ps) / 2	268.8	268.8			
21 Pr = (P / Pcr)	0.400	0.400			
22 Tr = (T / Tcr)	1.520	1.520			
23 Z (Table XI)	0.961	0.961			