N. M. O. C. C. COPY

NEW MEXICO OIL CONSERVATION COMMISSION

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

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JUL 1 - 1974
O. C. C.
ARTESIA, OFFICE

Type Test: ☒ Initial ☐ Annual ☐ Special			Test Date: 6-29-74	
Company: DALPORT OIL CORPORATION	Connection: TO AIR			
Pool: UNDESIGN	Formation: QUEEN			Unit:
Completion Date: 6-15-74	Total Depth: 2300	Plug Back TD: 2250	Elevation:	Farm or Lease Name: HOLBROOK FEDERAL
Csg. Size: 2 7/8" / Wt.: 6.50 / d: 2.441 / Set At:		Perforations: From 2224 To 2236.5		Well No.: 1
Tbg. Size: / Wt.: / d: / Set At:		Perforations: From To		Unit: E / Sec.: 9 / Twp.: 15S / Rge.: 30E
Type Well – Single – Bradenhead – G.G. or G.O. Multiple: SINGLE		Packer Set At: NONE		County: CHAVES
Producing Thru: CASING	Reservoir Temp. °F: 86 @ 2230	Mean Annual Temp. °F: 60	Baro. Press. – P_a: 13.2	State: NEW MEXICO
L: 2230 / H: 2230	Gg: 0.915	% CO_2: -0-	% N_2: 65%	% H_2S: -0-
Prover: POSITIVE CHOKES	Meter Run:	Taps:		

FLOW DATA

NO.	Prover Line Size	X Orifice Size	Press. p.s.i.g.	Diff. h_w	Temp. °F	TUBING DATA Press. p.s.i.g.	TUBING DATA Temp. °F	CASING DATA Press. p.s.i.g.	CASING DATA Temp. °F	Duration of Flow
SI	POSITIVE CHOKES					CASING PROD.		723.0		
1.	14/64"		713.0		81			713.0	81	60 MIN.
2.	16/64"		690.0		80			690/0	80	60 "
3.	20/64"		665.0		75			665.0	75	60 "
4.	23/64"		645.0		75			645.0	75	60 "
5.										

RATE OF FLOW CALCULATIONS

NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P_m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1	0.8419	-	726.2	0.9804	1.045	1.025	642
2.	1.112	-	703.2	0.9813	1.045	1.24	821
3.	1.771	-	678.2	0.9859	1.045	1.025	1268
4.	2.371	-	658.2	0.9859	1.045	1.024	1646
5.							

NO.	P_t	Temp. °R	T_r	Z
1	1.32	541	1.90	0.952
2.	1.27	540	1.90	0.953
3.	1.23	535	1.88	0.952
4.	1.19	535	1.88	0.953
5.				

Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.
A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.
Specific Gravity Separator Gas 0.915 XXXXXXXXX
Specific Gravity Flowing Fluid XXXXX
Critical Pressure 552 * P.S.I.A. _____ P.S.I.A.
Critical Temperature 284 * R _____ R

P_c 736.2 P_c^2 542.0

NO	P_t^2	P_w	P_w^2	$P_c^2 - P_w^2$
1	527.4		529.1	12.9
2	494.5		497.3	44.7
3	460.0		466.8	65.2
4	433.2		444.7	97.3
5				

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 5.5704$

(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right] = 4.6512$

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AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 7656$

Absolute Open Flow 7656 Mcfd @ 15.025 | Angle of Slope θ 48.2° | Slope, n 0.895

Remarks: * N_2 CONTENT EXCEEDS TABLES – THEREFORE PCR & TCR. ARE ESTIMATED.

Approved By Commission:	Conducted By:	Calculated By:	Checked By:
	C.P.	R.[illegible]	J.[illegible]