Received by NCD: 51/15/2022 11:59:06 AM U.S. Department of the Interior BUREAU OF LAND MANAGEMENT		Sundry Print Report
Well Name: BURTON FLAT DEEP UNIT	Well Location: T20S / R28E / SEC 35 / SENW /	County or Parish/State:
Well Number: 333H	Type of Well: OIL WELL	Allottee or Tribe Name:
Lease Number: NMNM082992	Unit or CA Name:	Unit or CA Number:
US Well Number: 3001550148	Well Status: Approved Application for Permit to Drill	Operator: DEVON ENERGY PRODUCTION COMPANY LP

Notice of Intent

Sundry ID: 2701631

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Type of Submission: Notice of Intent

Date Sundry Submitted: 11/07/2022

Date proposed operation will begin: 11/07/2022

Type of Action: APD Change Time Sundry Submitted: 11:17

Procedure Description: Devon Energy Production Co., L.P. (Devon) respectfully requests a change to the casing design and a break test variance. Please see the attached updated plan.

NOI Attachments

Procedure Description

8.625_32lb_P110HSCY_TLW_20221107111602.PDF 13.375_54.5_J55_SEAH_20221107111602.pdf 5.50_20_P110EC_DWC_C_IS_PLUS_VST__2_20221107111602.pdf 10.75_45.50_J55_BTC_SC_BLP_Devon_20221107111602.pdf break_test_variance_BOP_20221107111038.pdf BURTON_FLAT_35_33_FED_COM_333H_Directional_Plan_11_01_22_20221107110259.pdf BURTON_FLAT_35_33_FED_COM_333H_20221107110258.pdf

I	eceived by OCD: 11/15/2022 11:59:06 AM Well Name: BURTON FLAT DEEP UNIT	Well Location: T20S / R28E / SEC 35 / SENW /	County or Parish/State: Page 2 of
	Well Number: 333H	Type of Well: OIL WELL	Allottee or Tribe Name:
	Lease Number: NMNM082992	Unit or CA Name:	Unit or CA Number:
	US Well Number: 3001550148	Well Status: Approved Application for Permit to Drill	Operator: DEVON ENERGY PRODUCTION COMPANY LP

Conditions of Approval

Additional

35_20_28_C_Sundry_ID_2701631_Burton_Flat_35_33_Fed_Com_333H_Eddy_NM82992_Devon_Energy_Production_ Company_LP_13_22d_10_28_2022_LV_20221108062242.pdf

Burton_Flat_35_33_Fed_Com_333H_Sundry_ID_2701631_P_A_20221108062242.pdf

Operator

I certify that the foregoing is true and correct. Title 18 U.S.C. Section 1001 and Title 43 U.S.C. Section 1212, make it a crime for any person knowingly and willfully to make to any department or agency of the United States any false, fictitious or fraudulent statements or representations as to any matter within its jurisdiction. Electronic submission of Sundry Notices through this system satisfies regulations requiring a

Operator Electronic Signature: CHELSEY GREEN

Name: DEVON ENERGY PRODUCTION COMPANY LP

Title: Regulatory Compliance Professional

Street Address: 333 West Sheridan Avenue

City: Oklahoma City State: OK

Phone: (405) 228-8595

Email address: Chelsey.Green@dvn.com

Field

Representative Name:			
Street Address:			
City:			
Phone:			
Email address:			

State:

Zip:

Signed on: NOV 07, 2022 10:41 AM

BLM Point of Contact

BLM POC Name: CHRISTOPHER WALLS BLM POC Phone: 5752342234 Disposition: Approved Signature: Chris Walls BLM POC Title: Petroleum Engineer BLM POC Email Address: cwalls@blm.gov Disposition Date: 11/14/2022

1. Geologic Formations

TVD of target	8641	Pilot hole depth	N/A
MD at TD:	19199	Deepest expected fresh water	

Basin

Dasin			
	Depth	Water/Mineral	
Formation	(TVD)	Bearing/Target	Hazards*
	from KB	Zone?	
Rustler	85		
Salt	441		
Base of Salt	640		
Lamar	854		
Capitan Reef Top	1130		
Delaware	2953		
Cherry Canyon	3192		
Brushy Canyon	3792		
1st Bone Spring Lime	5350		
Bone Spring 1st	6685		
Bone Spring 2nd	7327		
3rd Bone Spring Lime	7627		
Bone Spring 3rd	8522		

*H2S, water flows, loss of circulation, abnormal pressures, etc.

Hole Size	Csg. Size	Wt (PPF)	Grade	Conn	Top (MD)	Bottom (MD)	Top (TVD)	Bottom (TVD)
17 1/2	13 3/8	54.5	J-55	BTC	0	225 MD	0	225 TVD
12 1/4	10 3/4	45.5	J-55	BTC SC	0	780 MD	0	780 TVD
9 7/8	8 5/8	32.0	P110	TLW	0	3005 MD	0	3005 TVD
7 7/8	5 1/2	20.0	P110EC	DWC/C IS+	0	19199 MD	0	8641 TVD

2. Casing Program

• All casing strings will be tested in accordance with Onshore Oil and Gas Order #2 IILB.1.h Must have table for contingency casing.

• The Rustler top will be validated via drilling parameters (i.e. reduction in ROP), and the surface casing setting depth will be revised accordingly. In addition, surface casing will be set a minimum of 25' above the top of the salt.

3. Cementing Program (43-String Primary Design)						
Casing	# Sks	тос	Wt. (lb/gal)	Yld (ft3/sack)	Slurry Description	
Surface	201	Surf	13.2	1.4	Lead: Class C Cement + additives	
Int	21	Surf	9.0	3.3	Lead: Class C Cement + additives	
Int	101	500' above shoe	13.2	1.4	Tail: Class H / C + additives	
Int 1	98	Surf	9.0	3.3	Lead: Class C Cement + additives	
	67	500' above shoe	13.2	1.4	Tail: Class H / C + additives	
Int 1	As Needed	Surf	0.0	3.3	Squeeze Lead: Class C Cement + additives	
Intermediate	21	Surf	9.0	3.3	Lead: Class C Cement + additives	
Squeeze	101	500' above shoe	13.2	1.4	Tail: Class H / C + additives	
	421	1080	9.0	3.3	Lead: Class H /C + additives	
Production	1441	8311	13.2	1.4	Tail: Class H / C + additives	

3. Cementing Program (43-String Primary Design)

If a DV tool is ran the depth(s) will be adjusted based on hole conditions and cement volumes will be adjusted proportionally. Slurry weights will be adjusted based on estimated fracture gradient of the formation. DV tool will be set a minimum of 50 feet below previous casing and a minimum of 200 feet above current shoe. If cement is not returned to surface during the primary cement job on the surface casing string, a planned top job will be conducted immediately after completion of the primary job.

Casing String	% Excess
Surface	50%
Intermediate and Intermediate 1	30%
Production	10%

BOP installed and tested before drilling which hole?	Size?	Min. Required WP	Туре	*	Tested to:								
			Annular		N/A								
Int			Blind Ram										
IIIt			Pipe Ram		500psi								
			Double Ram		500psi								
			Other* Diverter	Х									
	13-5/8"	5M	Annular	Х	50% of rated working pressure								
Int 1			5M	Blind Ram	Х								
1111 1				5101	Pipe Ram		5M						
						Double Ram	Х	5111					
			Other*										
Production			Annular (5M)	Х	50% of rated working pressure								
	13-5/8"	5M	Blind Ram	Х									
	15-5/6	1 <i>3-3/</i> 0 <i>3</i> 1 V 1	13-3/8 3101	13-5/8 5IVI	1 <i>3-3/0</i> 31 VI	15-5/0 5IVI	15-5/6 5IVI	5101	5111	5 5111	Pipe Ram		- 5M
		l						Double Ram	Х	5171			
			Other*										

4. Pressure Control Equipment (Four String Design)

By definition, the diverter will only be used to divert flow from the well and not to shut in the well. Prior to drilling out, the diverter will be tested to 250 PSI to ensure functionality.

BURTON FLAT 35-33 FED COM 333H

5. Mud Program (Four String Design)

Section	Туре	Weight (ppg)
Surface	WBM	8.5-9
Intermediate	DBE / Cut Brine	10-10.5
Intermediate 1	WBM	8.5-9
Production	WBM	8.5-9

Sufficient mud materials to maintain mud properties and meet minimum lost circulation and weight increase requirements will be kept on location at all times.

What will be used to monitor the loss or gain of fluid? PVT/Pason/Visual Monitoring

6. Logging and Testing Procedures

Logging, C	Logging, Coring and Testing						
	Will run GR/CNL from TD to surface (horizontal well - vertical portion of hole). Stated logs run will be in the						
Х	Completion Report and sbumitted to the BLM.						
	No logs are planned based on well control or offset log information.						
	Drill stem test? If yes, explain.						
	Coring? If yes, explain.						

Addition	al logs planned	Interval
	Resistivity	
	Density	
Х	CBL	Production casing
Х	Mud log	KOP to TD
	PEX	

7. Drilling Conditions

Condition	Specfiy what type and where?
BH pressure at deepest TVD	4044
Abnormal temperature	No

Mitigation measure for abnormal conditions. Describe. Lost circulation material/sweeps/mud scavengers.

Hydrogren Sulfide (H2S) monitors will be installed prior to drilling out the surface shoe. If H2S is detected in concentrations greater than 100 ppm, the operator will comply with the provisions of Onshore Oil and Gas Order #6. If Hydrogen Sulfide is encountered measured values and formations will be provided to the BLM.

Ν	H2S is present
Y	H2S plan attached.

8. Other facets of operation

Is this a walking operation? Potentially

- 1 If operator elects, drilling rig will batch drill the surface holes and run/cement surface casing; walking the rig to next wells on the pad.
- 2 The drilling rig will then batch drill the intermediate sections and run/cement intermediate casing; the wellbore will be isolated with a blind flange and pressure gauge installed for monitoring the well before walking to the next well.
- 3 The drilling rig will then batch drill the production hole sections on the wells with OBM, run/cement production casing, and install TA caps or tubing heads for completions.

NOTE: During batch operations the drilling rig will be moved from well to well however, it will not be removed from the pad until all wells have production casing run/cemented.

Will be pre-setting casing? Potentially

- 1 Spudder rig will move in and batch drill surface hole.
 - a. Rig will utilize fresh water based mud to drill surface hole to TD. Solids control will be handled entirely on a closed loop basis.
- 2 After drilling the surface hole section, the spudder rig will run casing and cement following all of the applicable rules and regulations (OnShore Order 2, all COAs and NMOCD regulations).

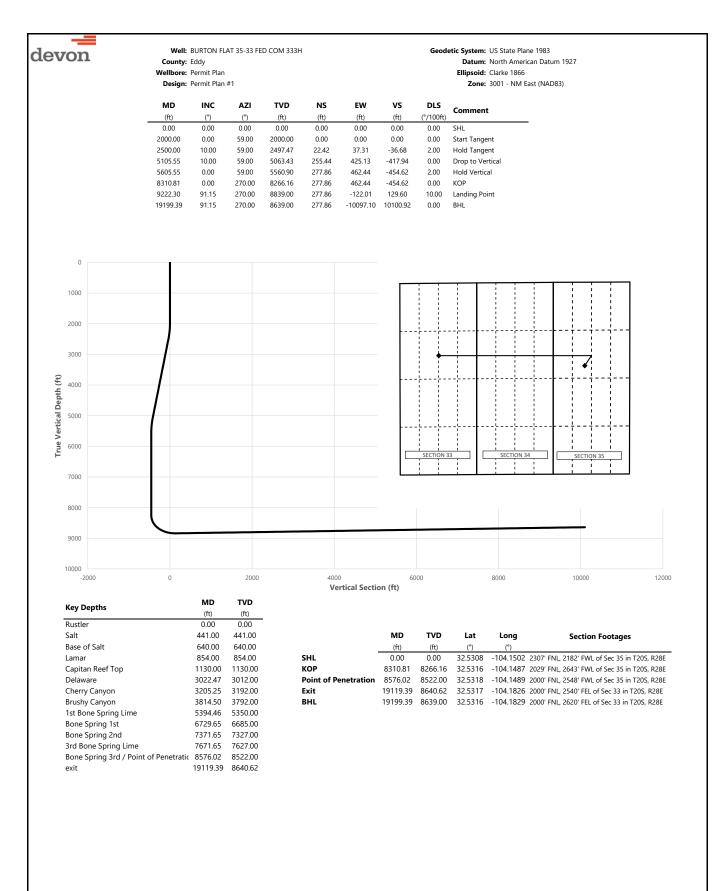
 3 The wellhead will be installed and tested once the surface casing is cut off and the WOC time has been reached.

- 4 A blind flange with the same pressure rating as the wellhead will be installed to seal the wellbore. Pressure will be monitored with a pressure gauge installed on the wellhead.
- 5 Spudder rig operations is expected to take 4-5 days per well on a multi-well pad.
- 6 The NMOCD will be contacted and notified 24 hours prior to commencing spudder rig operations.
- 7 Drilling operations will be performed with drilling rig. At that time an approved BOP stack will be nippled up and tested on the wellhead before drilling operations commences on each well.
 - a. The NMOCD will be contacted / notified 24 hours before the drilling rig moves back on to the pad with the pre-set surface casing.

Attachments

X Directional Plan

Other, describe



devon		County: Wellbore:	Eddy Permit Plan		D COM 333H				Geodetic System: US State Plane 1983 Datum: North American Datum 1927 Ellipsoid: Clarke 1866
	MD	Design:	Permit Plan	TVD	NS	EW	vs	DLS	Zone: 3001 - NM East (NAD83)
_	(ft)	(°)	(°)	(ft)	(ft)	(ft)	(ft)	(°/100ft)	Comment
	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	SHL
	85.00	0.00	59.00	85.00	0.00	0.00	0.00	0.00	Rustler
	100.00 200.00	0.00 0.00	59.00 59.00	100.00 200.00	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00	
	300.00	0.00	59.00	300.00	0.00	0.00	0.00	0.00	
	400.00	0.00	59.00	400.00	0.00	0.00	0.00	0.00	
	441.00	0.00	59.00	441.00	0.00	0.00	0.00	0.00	Salt
	500.00	0.00	59.00	500.00	0.00	0.00	0.00	0.00	
	600.00 640.00	0.00 0.00	59.00 59.00	600.00 640.00	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00	Base of Salt
	700.00	0.00	59.00	700.00	0.00	0.00	0.00	0.00	base of Sait
	800.00	0.00	59.00	800.00	0.00	0.00	0.00	0.00	
	854.00	0.00	59.00	854.00	0.00	0.00	0.00	0.00	Lamar
	900.00	0.00	59.00	900.00	0.00	0.00	0.00	0.00	
	1000.00	0.00	59.00	1000.00	0.00	0.00	0.00	0.00	
	1100.00 1130.00	0.00	59.00	1100.00	0.00 0.00	0.00	0.00 0.00	0.00	Capitan Boof Ton
	1200.00	0.00 0.00	59.00 59.00	1130.00 1200.00	0.00	0.00 0.00	0.00	0.00 0.00	Capitan Reef Top
	1300.00	0.00	59.00	1300.00	0.00	0.00	0.00	0.00	
	1400.00	0.00	59.00	1400.00	0.00	0.00	0.00	0.00	
	1500.00	0.00	59.00	1500.00	0.00	0.00	0.00	0.00	
	1600.00	0.00	59.00	1600.00	0.00	0.00	0.00	0.00	
	1700.00 1800.00	0.00 0.00	59.00 59.00	1700.00 1800.00	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00	
	1900.00	0.00	59.00	1900.00	0.00	0.00	0.00	0.00	
	2000.00	0.00	59.00	2000.00	0.00	0.00	0.00	0.00	Start Tangent
	2100.00	2.00	59.00	2099.98	0.90	1.50	-1.47	2.00	
	2200.00	4.00	59.00	2199.84	3.59	5.98	-5.88	2.00	
	2300.00 2400.00	6.00 8.00	59.00 59.00	2299.45 2398.70	8.08 14.36	13.45 23.90	-13.22 -23.49	2.00 2.00	
	2500.00	10.00	59.00	2398.70	22.42	37.31	-36.68	2.00	Hold Tangent
	2600.00	10.00	59.00	2595.95	31.36	52.19	-51.31	0.00	
	2700.00	10.00	59.00	2694.43	40.30	67.08	-65.94	0.00	
	2800.00	10.00	59.00	2792.91	49.25	81.96	-80.57	0.00	
	2900.00	10.00	59.00	2891.39	58.19	96.84	-95.21	0.00	
	3000.00 3022.47	10.00 10.00	59.00 59.00	2989.87 3012.00	67.13 69.14	111.73 115.07	-109.84 -113.13	0.00 0.00	Delaware
	3100.00	10.00	59.00	3088.35	76.08	126.61	-124.47	0.00	Delaware
	3200.00	10.00	59.00	3186.83	85.02	141.50	-139.11	0.00	
	3205.25	10.00	59.00	3192.00	85.49	142.28	-139.87	0.00	Cherry Canyon
	3300.00	10.00	59.00	3285.31	93.96	156.38	-153.74	0.00	
	3400.00	10.00 10.00	59.00 59.00	3383.79 3482.27	102.91	171.27	-168.37	0.00 0.00	
	3500.00 3600.00	10.00	59.00 59.00	3482.27 3580.75	111.85 120.79	186.15 201.04	-183.00 -197.64	0.00	
	3700.00	10.00	59.00	3679.23	129.74	215.92	-212.27	0.00	
	3800.00	10.00	59.00	3777.72	138.68	230.81	-226.90	0.00	
	3814.50	10.00	59.00	3792.00	139.98	232.96	-229.03	0.00	Brushy Canyon
	3900.00	10.00	59.00	3876.20	147.63	245.69	-241.54	0.00	
	4000.00 4100.00	10.00 10.00	59.00 59.00	3974.68 4073.16	156.57 165.51	260.57 275.46	-256.17 -270.80	0.00 0.00	
	4100.00	10.00	59.00 59.00	4073.16 4171.64	174.46	275.46 290.34	-270.80	0.00	
	4300.00	10.00	59.00	4270.12	183.40	305.23	-300.07	0.00	
	4400.00	10.00	59.00	4368.60	192.34	320.11	-314.70	0.00	
	4500.00	10.00	59.00	4467.08	201.29	335.00	-329.33	0.00	
	4600.00	10.00	59.00	4565.56	210.23	349.88	-343.97	0.00	
	4700.00 4800.00	10.00 10.00	59.00 59.00	4664.04 4762.52	219.17 228.12	364.77 379.65	-358.60 -373.23	0.00 0.00	
	4900.00 4900.00	10.00	59.00 59.00	4762.52 4861.00	228.12	379.65 394.53	-373.23	0.00	
	5000.00	10.00	59.00	4959.48	246.00	409.42	-402.50	0.00	
	5100.00	10.00	59.00	5057.97	254.95	424.30	-417.13	0.00	
	5105.55	10.00	59.00	5063.43	255.44	425.13	-417.94	0.00	Drop to Vertical
	5200.00	8.11	59.00	5156.70	263.10	437.87	-430.47	2.00	
	5300.00	6.11	59.00	5255.93	269.48	448.48	-440.90	2.00	1st Rope Spring Lime
	5394.46 5400.00	4.22 4.11	59.00 59.00	5350.00 5355.52	273.86 274.06	455.77 456.12	-448.07 -448.41	2.00 2.00	1st Bone Spring Lime
	5500.00	2.11	59.00 59.00	5355.52 5455.37	274.06	450.12	-440.41	2.00	
	5600.00	0.11	59.00	5555.35	277.86	462.43	-454.61	2.00	
	5605.55	0.00	59.00	5560.90	277.86	462.44	-454.62	2.00	Hold Vertical
	F700.00	0.00	270.00	5655.35	277.86	462.44	-454.62	0.00	
	5700.00 5800.00	0.00	270.00	5755.35	277.86	462.44	-454.62	0.00	

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devon		Well:	BURTON FL	.AT 35-33 FEI	COM 333H	1			Geodetic System: US State Plane 1983
devon		County:							Datum: North American Datum 1927
			Permit Plan						Ellipsoid: Clarke 1866
		Design:	Permit Plan	#1					Zone: 3001 - NM East (NAD83)
	MD	INC	AZI	TVD	NS	EW	vs	DLS	Comment
_	(ft)	(°)	(°)	(ft)	(ft)	(ft)	(ft)	(°/100ft)	Comment
	5900.00 6000.00	0.00 0.00	270.00 270.00	5855.35 5955.35	277.86 277.86	462.44 462.44	-454.62 -454.62	0.00 0.00	
	6100.00	0.00	270.00	6055.35	277.86	462.44	-454.62	0.00	
	6200.00	0.00	270.00	6155.35	277.86	462.44	-454.62	0.00	
	6300.00	0.00	270.00	6255.35	277.86	462.44	-454.62	0.00	
	6400.00 6500.00	0.00 0.00	270.00 270.00	6355.35 6455.35	277.86 277.86	462.44 462.44	-454.62 -454.62	0.00 0.00	
	6600.00	0.00	270.00	6555.35	277.86	462.44	-454.62	0.00	
	6700.00	0.00	270.00	6655.35	277.86	462.44	-454.62	0.00	
	6729.65	0.00	270.00	6685.00	277.86	462.44	-454.62	0.00	Bone Spring 1st
	6800.00 6900.00	0.00 0.00	270.00 270.00	6755.35 6855.35	277.86 277.86	462.44 462.44	-454.62 -454.62	0.00 0.00	
	7000.00	0.00	270.00	6955.35	277.86	462.44	-454.62	0.00	
	7100.00	0.00	270.00	7055.35	277.86	462.44	-454.62	0.00	
	7200.00 7300.00	0.00	270.00	7155.35	277.86	462.44	-454.62	0.00 0.00	
	7300.00	0.00 0.00	270.00 270.00	7255.35 7327.00	277.86 277.86	462.44 462.44	-454.62 -454.62	0.00	Bone Spring 2nd
	7400.00	0.00	270.00	7355.35	277.86	462.44	-454.62	0.00	r <u>a</u> .
	7500.00	0.00	270.00	7455.35	277.86	462.44	-454.62	0.00	
	7600.00 7671.65	0.00 0.00	270.00 270.00	7555.35 7627.00	277.86 277.86	462.44 462.44	-454.62 -454.62	0.00 0.00	3rd Bone Spring Lime
	7700.00	0.00	270.00	7655.35	277.86	462.44	-454.62 -454.62	0.00	Sid bolle spring Line
	7800.00	0.00	270.00	7755.35	277.86	462.44	-454.62	0.00	
	7900.00	0.00	270.00	7855.35	277.86	462.44	-454.62	0.00	
	8000.00 8100.00	0.00 0.00	270.00 270.00	7955.35 8055.35	277.86 277.86	462.44 462.44	-454.62 -454.62	0.00 0.00	
	8200.00	0.00	270.00	8155.35	277.86	462.44	-454.62	0.00	
	8300.00	0.00	270.00	8255.35	277.86	462.44	-454.62	0.00	
	8310.81	0.00	270.00	8266.16	277.86	462.44	-454.62	0.00	КОР
	8400.00 8500.00	8.92 18.92	270.00 270.00	8354.99 8451.93	277.86 277.86	455.51 431.48	-447.69 -423.68	10.00 10.00	
	8576.02	26.52	270.00	8522.00	277.86	402.14	-394.35	10.00	Bone Spring 3rd / Point of Penetration
	8600.00	28.92	270.00	8543.22	277.86	390.99	-383.20	10.00	
	8700.00	38.92	270.00	8626.10	277.86	335.26	-327.49	10.00	
	8800.00 8900.00	48.92 58.92	270.00 270.00	8698.04 8756.86	277.86 277.86	265.98 185.27	-258.24 -177.56	10.00 10.00	
	9000.00	68.92	270.00	8800.77	277.86	95.57	-87.89	10.00	
	9100.00	78.92	270.00	8828.43	277.86	-0.40	8.04	10.00	
	9200.00 9222.30	88.92	270.00 270.00	8839.01	277.86	-99.71	107.32	10.00	Landing Point
	9222.30 9300.00	91.15 91.15	270.00	8839.00 8837.44	277.86 277.86	-122.01 -199.69	129.60 207.26	10.00 0.00	Landing Point
	9400.00	91.15	270.00	8835.44	277.86	-299.67	307.20	0.00	
	9500.00	91.15	270.00	8833.43	277.86	-399.65	407.15	0.00	
	9600.00 9700.00	91.15 91.15	270.00 270.00	8831.43 8829.42	277.86 277.86	-499.63 -599.61	507.09 607.03	0.00 0.00	
	9800.00	91.15	270.00	8827.42	277.86	-699.59	706.97	0.00	
	9900.00	91.15	270.00	8825.42	277.86	-799.57	806.91	0.00	
	10000.00	91.15	270.00	8823.41	277.86	-899.55	906.86	0.00	
	10100.00 10200.00	91.15 91.15	270.00 270.00	8821.41 8819.40	277.86 277.86	-999.53 -1099.51	1006.80 1106.74	0.00 0.00	
	10200.00	91.15	270.00	8817.40	277.86	-1199.49	1206.68	0.00	
	10400.00	91.15	270.00	8815.39	277.86	-1299.47	1306.63	0.00	
	10500.00	91.15	270.00	8813.39	277.85	-1399.45	1406.57	0.00	
	10600.00 10700.00	91.15 91.15	270.00 270.00	8811.38 8809.38	277.85 277.85	-1499.43 -1599.41	1506.51 1606.45	0.00 0.00	
	10800.00	91.15	270.00	8807.38	277.85	-1699.39	1706.39	0.00	
	10900.00	91.15	270.00	8805.37	277.85	-1799.37	1806.34	0.00	
	11000.00	91.15	270.00	8803.37	277.85	-1899.35	1906.28	0.00	
	11100.00 11200.00	91.15 91.15	270.00 270.00	8801.36 8799.36	277.85 277.85	-1999.33 -2099.31	2006.22 2106.16	0.00 0.00	
	11200.00	91.15	270.00	8797.35	277.85	-2199.29	2206.10	0.00	
	11400.00	91.15	270.00	8795.35	277.85	-2299.27	2306.05	0.00	
	11500.00	91.15	270.00	8793.34	277.85	-2399.25	2405.99	0.00	
	11600.00 11700.00	91.15 91.15	270.00 270.00	8791.34 8789.34	277.85 277.85	-2499.23 -2599.21	2505.93 2605.87	0.00 0.00	
	11800.00	91.15	270.00	8787.33	277.85	-2699.19	2705.81	0.00	
	11900.00	91.15	270.00	8785.33	277.85	-2799.17	2805.76	0.00	
	12000.00	91.15	270.00	8783.32	277.85	-2899.15	2905.70	0.00	
	12100.00 12200.00	91.15 91.15	270.00 270.00	8781.32 8779.31	277.85 277.85	-2999.13 -3099.11	3005.64 3105.58	0.00 0.00	
								2.50	

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devon		Well: County:		AT 35-33 FED	D COM 333H	4			Geodetic System: US State Plane 1983 Datum: North American Datum 1927
			Permit Plan						Ellipsoid: Clarke 1866
		Design:	Permit Plan	#1					Zone: 3001 - NM East (NAD83)
	MD	INC	AZI	TVD	NS	EW	vs	DLS	Comment
	(ft) 12300.00	(°) 91.15	(°) 270.00	(ft) 8777.31	(ft) 277.85	(ft) -3199.09	(ft) 3205.52	(°/100ft) 0.00	
	12400.00	91.15	270.00	8775.30	277.85	-3299.07	3205.52	0.00	
	12500.00	91.15	270.00	8773.30	277.85	-3399.05	3405.41	0.00	
	12600.00 12700.00	91.15 91.15	270.00 270.00	8771.30 8769.29	277.85 277.85	-3499.03 -3599.01	3505.35 3605.29	0.00 0.00	
	12700.00	91.15	270.00	8767.29	277.85	-3698.99	3705.23	0.00	
	12900.00	91.15	270.00	8765.28	277.85	-3798.97	3805.18	0.00	
	13000.00	91.15	270.00	8763.28	277.84	-3898.95	3905.12	0.00	
	13100.00 13200.00	91.15 91.15	270.00 270.00	8761.27 8759.27	277.84 277.84	-3998.93 -4098.91	4005.06 4105.00	0.00 0.00	
	13200.00	91.15	270.00	8757.26	277.84	-4098.91	4103.00	0.00	
	13400.00	91.15	270.00	8755.26	277.84	-4298.87	4304.89	0.00	
	13500.00	91.15	270.00	8753.26	277.84	-4398.85	4404.83	0.00	
	13600.00 13700.00	91.15 91.15	270.00 270.00	8751.25 8749.25	277.84 277.84	-4498.83 -4598.81	4504.77 4604.71	0.00 0.00	
	13800.00	91.15	270.00	8747.24	277.84	-4698.79	4704.66	0.00	
	13900.00	91.15	270.00	8745.24	277.84	-4798.77	4804.60	0.00	
	14000.00	91.15	270.00	8743.23	277.84	-4898.75	4904.54	0.00	
	14100.00 14200.00	91.15 91.15	270.00 270.00	8741.23 8739.22	277.84 277.84	-4998.73 -5098.71	5004.48 5104.42	0.00 0.00	
	14300.00	91.15	270.00	8737.22	277.84	-5198.69	5204.37	0.00	
	14400.00	91.15	270.00	8735.22	277.84	-5298.67	5304.31	0.00	
	14500.00	91.15	270.00	8733.21	277.84	-5398.65	5404.25	0.00	
	14600.00 14700.00	91.15 91.15	270.00 270.00	8731.21 8729.20	277.84 277.84	-5498.63 -5598.61	5504.19 5604.13	0.00 0.00	
	14800.00	91.15	270.00	8727.20	277.84	-5698.59	5704.08	0.00	
	14900.00	91.15	270.00	8725.19	277.84	-5798.57	5804.02	0.00	
	15000.00	91.15	270.00	8723.19	277.84	-5898.55 -5998.53	5903.96	0.00	
	15100.00 15200.00	91.15 91.15	270.00 270.00	8721.18 8719.18	277.84 277.84	-6098.51	6003.90 6103.84	0.00 0.00	
	15300.00	91.15	270.00	8717.18	277.84	-6198.49	6203.79	0.00	
	15400.00	91.15	270.00	8715.17	277.84	-6298.47	6303.73	0.00	
	15500.00 15600.00	91.15 91.15	270.00 270.00	8713.17 8711.16	277.84 277.83	-6398.45 -6498.43	6403.67 6503.61	0.00 0.00	
	15700.00	91.15	270.00	8709.16	277.83	-6598.41	6603.55	0.00	
	15800.00	91.15	270.00	8707.15	277.83	-6698.39	6703.50	0.00	
	15900.00	91.15	270.00	8705.15	277.83	-6798.37	6803.44	0.00	
	16000.00 16100.00	91.15 91.15	270.00 270.00	8703.14 8701.14	277.83 277.83	-6898.35 -6998.33	6903.38 7003.32	0.00 0.00	
	16200.00	91.15	270.00	8699.13	277.83	-7098.31	7103.26	0.00	
	16300.00	91.15	270.00	8697.13	277.83	-7198.29	7203.21	0.00	
	16400.00	91.15	270.00	8695.13	277.83	-7298.27	7303.15	0.00	
	16500.00 16600.00	91.15 91.15	270.00 270.00	8693.12 8691.12	277.83 277.83	-7398.25 -7498.23	7403.09 7503.03	0.00 0.00	
	16700.00	91.15	270.00	8689.11	277.83	-7598.21	7602.97	0.00	
	16800.00	91.15	270.00	8687.11	277.83	-7698.19	7702.92	0.00	
	16900.00	91.15	270.00	8685.10	277.83	-7798.17	7802.86	0.00	
	17000.00 17100.00	91.15 91.15	270.00 270.00	8683.10 8681.09	277.83 277.83	-7898.15 -7998.13	7902.80 8002.74	0.00 0.00	
	17200.00	91.15	270.00	8679.09	277.83	-8098.11	8102.69	0.00	
	17300.00	91.15	270.00	8677.09	277.83	-8198.09	8202.63	0.00	
	17400.00 17500.00	91.15 91.15	270.00 270.00	8675.08 8673.08	277.83 277.83	-8298.07 -8398.05	8302.57 8402.51	0.00 0.00	
	17600.00	91.15 91.15	270.00	8673.08 8671.07	277.83	-8398.05 -8498.03	8402.51 8502.45	0.00	
	17700.00	91.15	270.00	8669.07	277.83	-8598.01	8602.40	0.00	
	17800.00	91.15	270.00	8667.06	277.83	-8697.99	8702.34	0.00	
	17900.00 18000.00	91.15 91.15	270.00 270.00	8665.06 8663.05	277.83 277.83	-8797.97 -8897.95	8802.28 8902.22	0.00 0.00	
	18000.00	91.15 91.15	270.00	8661.05	277.83	-8997.93	8902.22 9002.16	0.00	
	18200.00	91.15	270.00	8659.05	277.82	-9097.91	9102.11	0.00	
	18300.00	91.15	270.00	8657.04	277.82	-9197.89	9202.05	0.00	
	18400.00	91.15 01.15	270.00	8655.04	277.82	-9297.87	9301.99	0.00	
	18500.00 18600.00	91.15 91.15	270.00 270.00	8653.03 8651.03	277.82 277.82	-9397.85 -9497.83	9401.93 9501.87	0.00 0.00	
	18700.00	91.15	270.00	8649.02	277.82	-9597.81	9601.82	0.00	
	18800.00	91.15	270.00	8647.02	277.82	-9697.79	9701.76	0.00	
	18900.00 19000.00	91.15 91.15	270.00	8645.01 8643.01	277.82 277.82	-9797.77 -9897.75	9801.70 9901.64	0.00	
	19000.00	91.15 91.15	270.00 270.00	8643.01 8641.01	277.82	-9897.75	10001.58	0.00 0.00	
	19119.39	91.15	270.00	8640.62	277.82	-10017.12		0.00	exit

.

devon		County: Wellbore:) COM 333F	1			Geodetic System: US State Plane 1983 Datum: North American Datum 1927 Ellipsoid: Clarke 1866 Zone: 3001 - NM East (NAD83)
	MD (ft)	INC (°)	AZI (°)	TVD (ft)	NS (ft)	EW (ft)	VS (ft)	DLS (°/100ft)	Comment
-	19199.39	91.15	270.00	8639.00	277.86	-10097.10		0.00	BHL

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	Well: BURTON FLAT 35-33 FED COM 333H County: Eddy Wellbore: Permit Plan Design: Permit Plan #1						Geodetic System: US State Plane 1983 Datum: North American Datum 1927 Ellipsoid: Clarke 1866 Zone: 3001 - NM East (NAD83)			
MD (ft)	INC (°)	AZI (°)	TVD (ft)	NS (ft)	EW (ft)	VS (ft)	DLS (°/100ft)	Comment		

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Section 2 - Blowout Preventer Testing Procedure

Variance Request

Devon Energy requests to only test BOP connection breaks after drilling out of surface casing and while skidding between wells which conforms to API Standard 53 and industry standards. This test will include the Top Pipe Rams, HCR, Kill Line Check Valve, QDC (quick disconnect to wellhead) and Shell of the 10M BOPE to 5M for 10 minutes. If a break to the flex hose that runs to the choke manifold is required due to repositioning from a skid, the HCR will remain open during the shell test to include that additional break. The variance only pertains to intermediate hole-sections and no deeper than the Bone Springs Formation where 5M BOP tests are required. The initial BOP test will follow OOGO2.III.A.2.i, and subsequent tests following a skid will only test connections that are broken. The annular preventer will be tested to 100% working pressure. This variance will meet or exceed OOGO2.III.A.2.i per the following: Devon Energy will perform a full BOP test per OOGO2.III.A.2.i before drilling out of the intermediate casing string(s) and starting the production hole, before starting any hole section that requires a 10M test, before the expiration of the allotted 14-days for 5M intermediate batch drilling or when the drilling rig is fully mobilized to a new well pad, whichever is sooner. We will utilize a 200' TVD tolerance between intermediate shoes as the cutoff for a full BOP test. The BLM will be contacted 4hrs prior to a BOPE test. The BLM will be notified if and when a well control event is encountered. Break test will be a 14 day interval and not a 30 day full BOPE test interval. If in the event break testing is not utilized, then a full BOPE test would be conducted.

1. Well Control Response:

1. Primary barrier remains fluid

2. In the event of an influx due to being underbalanced and after a realized gain or flow, the order of closing BOPE is as follows:

- a) Annular first
- b) If annular were to not hold, Upper pipe rams second (which were tested on the skid BOP test)
- c) If the Upper Pipe Rams were to not hold, Lower Pipe Rams would be third





<u>13-3/8"</u> <u>54.50#</u> <u>.380</u> <u>J-55</u>

Dimensions (Nominal)

Outside Diameter	13.375	in.
Wall	0.380	in.
Inside Diameter	12.615	in.
Drift	12.459	in.
Weight, T&C	54.500	lbs/ft
Weight, PE	52.790	lbs/ft

Performance Ratings, Minimum

Collapse, PE	1130	psi
Internal Yields Pressure		
PE	2730	psi
STC	2730	PSI
BTC	2730	psi
Yield Strength, Pipe Body	853	1000 lbs
Joint Strength, STC	514	1000 lbs
Joint Strength, BTC	909	1000 lbs

Note: SeAH Steel has produced this specification sheet for general information only. SeAH does not assume liability or responsibility for any loss or injury resulting from the use of information or data contained herein. All applications for the material described are at the customer's own risk and responsibility.





<u>10-3/4"</u>	<u>45.50#</u>	<u>0.400"</u>	<u>J-55</u>	
Dimensions ((Nominal)			
Outside Diameter Wall Inside Diameter			10.750 0.400 9.950	in. in. in.
Drift			9.875	in.
Weight, T&C Weight, PE			45.500 44.260	lbs/ft lbs/ft
<u>Performance</u>	e Properties			
Collapse			2090	psi
Internal Yield Pres	sure at Minimum Yield			
	PE		3580	psi
	STC		3580	psi
	BTC		3580	psi
Yield Strength, Pip	e Body		715	1000 lbs
Joint Strength				
	STC		493	1000 lbs
	BTC		796	1000 lbs
	BTC Special Clearance (11.25" OD Cplg)	506	1000 lbs

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TEC-LOCK WEDGE

8.625" 32.00 LB/FT (.352" Wall) BORUSAN MANNESMANNP110 HSCY

Pipe Body Data

Nominal OD:	8.625	in
Nominal Wall:	.352	in
Nominal Weight:	32.00	lb/ft
Plain End Weight:	31.13	lb/ft
Material Grade:	P110 HSCY	
Mill/Specification:	BORUSAN M	IANNESMANN
Yield Strength:	125,000	psi
Tensile Strength:	125,000	psi
Nominal ID:	7.921	in
API Drift Diameter:	7.796	in
Special Drift Diameter:	7.875	in
RBW:	87.5 %	
Body Yield:	1,144,000	lbf
Burst:	8,930	psi
Collapse:	4,230	psi

Connection Data

Standard OD:	9.000	in	
Pin Bored ID:	7.921	in	
Critical Section Area:	8.61433	in²	
Tensile Efficiency:	94.2 %		
Compressive Efficiency:	100.0 %		
Longitudinal Yield Strength:	1,077,000	lbf	
Compressive Limit:	1,144,000	lbf	
Internal Pressure Rating:	8,930	psi	
External Pressure Rating:	4,230	psi	
Maximum Bend:	62.6	°/100	

Operational Data

l	Minimum Makeup Torque:		ft*lbf
l	Optimum Makeup Torque:	37,375	ft*lbf
l	Maximum Makeup Torque:	80,900	ft*lbf
l	Minimum Yield:	89,900	ft*lbf
	Makeup Loss:	5.97	in

Notes

Operational Torque is equivalent to the Maximum Make-Up Torque.



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Please visit http://www.huntingplc.com for the latest technical information.



Connection Data Sheet

16.600

17.850

19,100

1.660

13,280

0.200

24,300

26,730

ft.lb

ft.lb

ft.lb

ft.lb

ft.lb

Turns

Turns

ft.lb

ft.lb

OD (in.)	WEIGHT (lbs./ft.)	WALL (in.)	GRADE	API DRIFT (in.)	RBW%	CONNECTION
5.500	Nominal: 20.00	0.361	VST P110EC	4.653	87.5	DWC/C-IS PLUS
	Plain End: 19.83					<u>.</u>

	PIPE PROPERTIES	
	PIPE PROPERTIES	
Naminal OD		
Nominal OD	5.500	in.
Nominal ID	4.778	in.
Nominal Area	5.828	sq.in.
Grade Type	API 5CT; Vallourec Sourced Mat	erial Only
Min. Yield Strength	125	ksi
Max. Yield Strength	140	ksi
Min. Tensile Strength	135	ksi
Yield Strength	729	klb
Ultimate Strength	787	klb
Min. Internal Yield Pressure	14,360	psi
Collapse Pressure	12,090	psi

	PERTIES	
Connection Type	Semi-Pren	nium T&C
Connection OD (nom)	6.300	in.
Connection ID (nom)	4.778	in.
Make-Up Loss	4.125	in.
Coupling Length	9.250	in.
Critical Cross Section	5.828	sq.in.
Tension Efficiency	100.0%	of pipe
Compression Efficiency	100.0%	of pipe
Internal Pressure Efficiency	100.0%	of pipe
External Pressure Efficiency	100.0%	of pipe

RMANCES		
	729	klb
	129	KID
	787	klb
	729	klb
	14,360	psi
	12,090	psi
	104.2	°/100 ft
	26,040	ft.

Min. Internal Yield External Pressure Maximum Uniaxial Bend Rating Reference String Length w 1.4 Design Factor Need Help? Contact: <u>tech.support@vam-usa.com</u>

CONNECTION PERFO

Reference Drawing: 8074PP Rev.06 & 8074BP Rev.05 Date: 08/04/2020 Time: 04:27:16 PM

Yield Strength

Parting Load

Compression Rating

* Maximum Operational Torque and Maximum Torsional Value Only Valid with Vallourec P110EC Material

For detailed information on performance properties, refer to DWC Connection Data Notes on following page(s).

Connection specifications within the control of VAM USA were correct as of the date printed. Specifications are subject to change without notice. Certain connection specifications are dependent on the mechanical properties of the pipe. Mechanical properties of mill proprietary pipe grades were obtained from mill publications and are subject to change. Properties of mill proprietary grades should be confirmed with the mill. Users are advised to obtain current connection specifications and verify pipe mechanical properties for each application.

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DWC Connection Data Sheet Notes:

1. DWC connections are available with a seal ring (SR) option.

2. All standard DWC/C connections are interchangeable for a given pipe OD. DWC connections are interchangeable with DWC/C-SR connections of the same OD and wall.

3. Connection performance properties are based on nominal pipe body and connection dimensions.

4. DWC connection internal and external pressure resistance is calculated using the API rating for buttress connections. API Internal pressure resistance is calculated from formulas 31, 32, and 35 in the API Bulletin 5C3.

5. DWC joint strength is the minimum pipe body yield strength multiplied by the connection critical area.

6. API joint strength is for reference only. It is calculated from formulas 42 and 43 in the API Bulletin 5C3.

7. Bending efficiency is equal to the compression efficiency.

8. The torque values listed are recommended. The actual torque required may be affected by field conditions such as temperature, thread compound, speed of make-up, weather conditions, etc.

9. Connection yield torque is not to be exceeded.

10. Reference string length is calculated by dividing the joint strength by both the nominal weight in air and a design factor (DF) of 1.4. These values are offered for reference only and do not include load factors such as bending, buoyancy, temperature, load dynamics, etc.

11. DWC connections will accommodate API standard drift diameters.

12. DWC/C family of connections are compatible with API Buttress BTC connections. Please contact tech.support@vam-usa.com for details on connection ratings and make-up.

Connection specifications within the control of VAM USA were correct as of the date printed. Specifications are subject to change without notice. Certain connection specifications are dependent on the mechanical properties of the pipe. Mechanical properties of mill proprietary pipe grades were obtained from mill publications and are subject to change. Properties of mill proprietary grades should be confirmed with the mill. Users are advised to obtain current connection specifications and verify pipe mechanical properties for each application.

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PECOS DISTRICT DRILLING CONDITIONS OF APPROVAL

	Devon Energy Production Company LP
	NMNM082992
	Section 35, T.20 S., R.28 E., NMPM
COUNTY:	Eddy County, New Mexico

WELL NAME & NO.:	Burton Flat 35-33 Fed Com 333H
SURFACE HOLE FOOTAGE:	2307'/N & 2182'/W
BOTTOM HOLE FOOTAGE	2000'/N & 2620'/E
ATS/API ID:	N/A
APD ID:	N/A
Sundry ID:	2701631

COA

H2S	• Yes	🖸 No	
Potash	O None	Secretary	🖸 R-111-P
Cave/Karst Potential	🖸 Low	🖸 Medium	🖸 High
Cave/Karst Potential	Critical		
Variance	🖸 None	Flex Hose	C Other
Wellhead	Conventional	🖸 Multibowl	🖸 Both
Wellhead Variance	Diverter		
Other	✓4 String	Capitan Reef	WIPP
Other	□Fluid Filled	🗌 Pilot Hole	🗌 Open Annulus
Cementing	Cement Squeeze	□ EchoMeter	
Special Requirements	U Water Disposal	COM	Unit Unit
Special Requirements	Break Testing	Offline	
Variance		Cementing	

A. HYDROGEN SULFIDE

A Hydrogen Sulfide (H2S) Drilling Plan shall be activated 500 feet prior to drilling into the **Delaware, Bone Springs, Wolfcamp** formation. As a result, the Hydrogen Sulfide area must meet Onshore Order 6 requirements, which includes equipment and personnel/public protection items. If Hydrogen Sulfide is encountered, please provide measured values and formations to the BLM.

B. CASING

1. The **13-3/8** inch surface casing shall be set at approximately **350 feet** (a minimum of **70 feet (Eddy County)** into the Rustler Anhydrite, above the salt, and below usable fresh water) and cemented to the surface.

- a. If cement does not circulate to the surface, the appropriate BLM office shall be notified and a temperature survey utilizing an electronic type temperature survey with surface log readout will be used or a cement bond log shall be run to verify the top of the cement. Temperature survey will be run a minimum of six hours after pumping cement and ideally between 8-10 hours after completing the cement job.
- b. Wait on cement (WOC) time for a primary cement job will be a minimum of <u>8</u> <u>hours</u> or 500 pounds compressive strength, whichever is greater. (This is to include the lead cement)
- c. Wait on cement (WOC) time for a remedial job will be a minimum of 4 hours after bringing cement to surface or 500 pounds compressive strength, whichever is greater.
- d. If cement falls back, remedial cementing will be done prior to drilling out that string.
- 2. The minimum required fill of cement behind the **10-3/4** inch intermediate casing shall be set at approximately **1250 feet** is:
 - Cement to surface. If cement does not circulate see B.1.a, c-d above. Add 30 sxs to the lead cement. Wait on cement (WOC) time for a primary cement job is to include the lead cement slurry due to cave/karst, potash or capitan reef. Cement excess is less than 25%, more cement is required if washout occurs. Adjust cement volume and excess based on a fluid caliper or similar method that reflects the as-drilled size of the wellbore.
 - In <u>High Cave/Karst Areas</u> if cement does not circulate to surface on the first two casing strings, the cement on the 3rd casing string must come to surface.
 - In <u>Capitan Reef Areas</u> if cement does not circulate to surface on the first two casing strings, the cement on the 3rd casing string must come to surface.
- 3. The minimum required fill of cement behind the **8-5/8** inch intermediate casing shall be set at approximately **2500 feet** is:
 - Cement should tie-back at least 50 feet on top of Capitan Reef top or 200 feet into the previous casing, whichever is greater. If cement does not circulate see B.1.a, c-d above.
 Wait on cement (WOC) time for a primary cement job is to include

the lead cement (WOC) time for a primary cement job is to include the lead cement slurry due to cave/karst, potash or capitan reef.

Operator has proposed to pump down 10-3/4" X 8-5/8" annulus after primary cementing stage. <u>Operator must run a CBL from TD of the 8-5/8" casing to surface.</u> <u>Submit results to the BLM.</u>

If cement does not tie-back into the previous casing shoe, a third stage remediation BH may be performed. The appropriate BLM office shall be notified.

- 4. The minimum required fill of cement behind the 5-1/2 inch production casing is:
 - Cement should tie-back at least 200 feet into previous casing string. Operator shall provide method of verification.
 Wait on cement (WOC) time for a primary cement job is to include the lead cement slurry due to cave/karst, potash or capitan reef. Cement excess is less than 25%, more cement is required if washout occurs. Adjust cement volume and excess based on a fluid caliper or similar method that reflects the as-drilled size of the wellbore.

C. PRESSURE CONTROL

1. Variance approved to use flex line from BOP to choke manifold. Manufacturer's specification to be readily available. No external damage to flex line. Flex line to be installed as straight as possible (no hard bends).'

2.

Option 1:

- a. Minimum working pressure of the blowout preventer (BOP) and related equipment (BOPE) required for drilling below the surface casing shoe shall be tested to **500** psi. A Diverter system is approved as a variance to drill the **10-3/4** inch intermediate casing in a **12 1/4** inch hole.
- b. Minimum working pressure of the blowout preventer (BOP) and related equipment (BOPE) required for drilling below the **10-3/4** inch intermediate casing shoe shall be **5000 (5M)** psi.
- c. Minimum working pressure of the blowout preventer (BOP) and related equipment (BOPE) required for drilling below the **8-5/8** inch intermediate casing shoe shall be **5000 (5M)** psi.

Option 2:

- a. Minimum working pressure of the blowout preventer (BOP) and related equipment (BOPE) required for drilling below the surface casing shoe shall be tested to 500 psi. A Diverter system is approved as a variance to drill the 10-3/4 inch intermediate casing in a 12 1/4 inch hole.
- b. Operator has proposed a multi-bowl wellhead assembly. This assembly will only be tested when installed on the 10-3/4 inch intermediate casing.
 Minimum working pressure of the blowout preventer (BOP) and related

equipment (BOPE) required for drilling below the intermediate casing shoe shall be **5000 (5M)** psi.

- a. Wellhead shall be installed by manufacturer's representatives, submit documentation with subsequent sundry.
- b. If the welding is performed by a third party, the manufacturer's representative shall monitor the temperature to verify that it does not exceed the maximum temperature of the seal.
- c. Manufacturer representative shall install the test plug for the initial BOP test.
- d. If the cement does not circulate and one inch operations would have been possible with a standard wellhead, the well head shall be cut off, cementing operations performed and another wellhead installed.
- e. Whenever any seal subject to test pressure is broken, all the tests in OOGO2.III.A.2.i must be followed.

D. SPECIAL REQUIREMENT (S)

<u>Unit Wells</u>

The well sign for a unit well shall include the unit number in addition to the surface and bottom hole lease numbers. This also applies to participating area numbers. If a participating area has not been established, the operator can use the general unit designation, but will replace the unit number with the participating area number when the sign is replaced.

Commercial Well Determination

A commercial well determination shall be submitted after production has been established for at least six months.

BOPE Break Testing Variance

- BOPE Break Testing is ONLY permitted for 5M BOPE or less. (Annular preventer must be tested to a minimum of 70% of BOPE working pressure and shall be higher than the MASP)
- BOPE Break Testing is NOT permitted to drilling the production hole section.
- Variance only pertains to the intermediate hole-sections and no deeper than the Bone Springs formation.
- While in transfer between wells, the BOPE shall be secured by the hydraulic carrier or cradle.
- Any well control event while drilling require notification to the BLM Petroleum Engineer (575-706-2779) prior to the commencement of any BOPE Break Testing operations.
- A full BOPE test is required prior to drilling the first deep intermediate hole section. If any subsequent hole interval is deeper than the first, a full BOPE test will be required. (200' TVD tolerance between intermediate shoes is allowable).
- The BLM is to be contacted **(575-361-2822 Eddy County)** 4 hours prior to BOPE tests.

- As a minimum, a full BOPE test shall be performed at **14**-day intervals.
- In the event any repairs or replacement of the BOPE is required, the BOPE shall test as per Onshore Oil and Gas Order No. 2.
- If in the event break testing is not utilized, then a full BOPE test would be conducted.

GENERAL REQUIREMENTS

The BLM is to be notified in advance for a representative to witness:

- a. Spudding well (minimum of 24 hours)
- b. Setting and/or Cementing of all casing strings (minimum of 4 hours)
- c. BOPE tests (minimum of 4 hours)
 - Eddy County Call the Carlsbad Field Office, 620 East Greene St., Carlsbad, NM 88220, (575) 361-2822
 - Lea County
 Call the Hobbs Field Station, 414 West Taylor, Hobbs NM 88240, (575)
 689-5981
- 1. Unless the production casing has been run and cemented or the well has been properly plugged, the drilling rig shall not be removed from over the hole without prior approval.
 - a. In the event the operator has proposed to drill multiple wells utilizing a skid/walking rig. Operator shall secure the wellbore on the current well, after installing and testing the wellhead, by installing a blind flange of like pressure rating to the wellhead and a pressure gauge that can be monitored while drilling is performed on the other well(s).
 - b. When the operator proposes to set surface casing with Spudder Rig
 - Notify the BLM when moving in and removing the Spudder Rig.
 - Notify the BLM when moving in the 2nd Rig. Rig to be moved in within 90 days of notification that Spudder Rig has left the location.
 - BOP/BOPE test to be conducted per Onshore Oil and Gas Order No. 2 as soon as 2nd Rig is rigged up on well.
- 2. Floor controls are required for 3M or Greater systems. These controls will be on the rig floor, unobstructed, readily accessible to the driller and will be operational at all times during drilling and/or completion activities. Rig floor is defined as the area immediately around the rotary table; the area immediately above the substructure on which the draw works are located, this does not include the dog house or stairway area.
- 3. The record of the drilling rate along with the GR/N well log run from TD to surface (horizontal well vertical portion of hole) shall be submitted to the BLM office as well as all other logs run on the borehole 30 days from completion. If available, a digital copy of the logs is to be submitted in addition to the paper copies. The Rustler top and top and bottom of Salt are to be recorded on the Completion Report.

A. CASING

- 1. Changes to the approved APD casing program need prior approval if the items substituted are of lesser grade or different casing size or are Non-API. The Operator can exchange the components of the proposal with that of superior strength (i.e. changing from J-55 to N-80, or from 36# to 40#). Changes to the approved cement program need prior approval if the altered cement plan has less volume or strength or if the changes are substantial (i.e. Multistage tool, ECP, etc.). The initial wellhead installed on the well will remain on the well with spools used as needed.
- <u>Wait on cement (WOC) for Potash Areas:</u> After cementing but before commencing any tests, the casing string shall stand cemented under pressure until both of the following conditions have been met: 1) cement reaches a minimum compressive strength of 500 psi for all cement blends, 2) until cement has been in place at least <u>24</u> <u>hours</u>. WOC time will be recorded in the driller's log. The casing intergrity test can be done (prior to the cement setting up) immediately after bumping the plug.
- 3. <u>Wait on cement (WOC) for Water Basin:</u> After cementing but before commencing any tests, the casing string shall stand cemented under pressure until both of the following conditions have been met: 1) cement reaches a minimum compressive strength of 500 psi at the shoe, 2) until cement has been in place at least <u>8 hours</u>. WOC time will be recorded in the driller's log. See individual casing strings for details regarding lead cement slurry requirements. The casing intergrity test can be done (prior to the cement setting up) immediately after bumping the plug.
- 4. Provide compressive strengths including hours to reach required 500 pounds compressive strength prior to cementing each casing string. Have well specific cement details onsite prior to pumping the cement for each casing string.
- 5. No pea gravel permitted for remedial or fall back remedial without prior authorization from the BLM engineer.
- 6. On that portion of any well approved for a 5M BOPE system or greater, a pressure integrity test of each casing shoe shall be performed. Formation at the shoe shall be tested to a minimum of the mud weight equivalent anticipated to control the formation pressure to the next casing depth or at total depth of the well. This test shall be performed before drilling more than 20 feet of new hole.
- 7. If hardband drill pipe is rotated inside casing, returns will be monitored for metal. If metal is found in samples, drill pipe will be pulled and rubber protectors which have a larger diameter than the tool joints of the drill pipe will be installed prior to continuing drilling operations.
- 8. Whenever a casing string is cemented in the R-111-P potash area, the NMOCD requirements shall be followed.
- B. PRESSURE CONTROL

- 1. All blowout preventer (BOP) and related equipment (BOPE) shall comply with well control requirements as described in Onshore Oil and Gas Order No. 2 and API RP 53 Sec. 17.
- 2. If a variance is approved for a flexible hose to be installed from the BOP to the choke manifold, the following requirements apply: The flex line must meet the requirements of API 16C. Check condition of flexible line from BOP to choke manifold, replace if exterior is damaged or if line fails test. Line to be as straight as possible with no hard bends and is to be anchored according to Manufacturer's requirements. The flexible hose can be exchanged with a hose of equal size and equal or greater pressure rating. Anchor requirements, specification sheet and hydrostatic pressure test certification matching the hose in service, to be onsite for review. These documents shall be posted in the company man's trailer and on the rig floor.
- 3. 5M or higher system requires an HCR valve, remote kill line and annular to match. The remote kill line is to be installed prior to testing the system and tested to stack pressure.
- 4. If the operator has proposed a multi-bowl wellhead assembly in the APD. The following requirements must be met:
 - a. Wellhead shall be installed by manufacturer's representatives, submit documentation with subsequent sundry.
 - b. If the welding is performed by a third party, the manufacturer's representative shall monitor the temperature to verify that it does not exceed the maximum temperature of the seal.
 - c. Manufacturer representative shall install the test plug for the initial BOP test.
 - d. Whenever any seal subject to test pressure is broken, all the tests in OOGO2.III.A.2.i must be followed.
 - e. If the cement does not circulate and one inch operations would have been possible with a standard wellhead, the well head shall be cut off, cementing operations performed and another wellhead installed.
- 5. The appropriate BLM office shall be notified a minimum of 4 hours in advance for a representative to witness the tests.
 - a. In a water basin, for all casing strings utilizing slips, these are to be set as soon as the crew and rig are ready and any fallback cement remediation has been done. The casing cut-off and BOP installation can be initiated four hours after installing the slips, which will be approximately six hours after bumping the plug. For those casing strings not using slips, the minimum wait time before cut-off is eight hours after bumping the plug. BOP/BOPE testing can begin after cut-off or once cement reaches 500 psi compressive strength (including lead when specified), whichever is greater. However, if the float does not

hold, cut-off cannot be initiated until cement reaches 500 psi compressive strength (including lead when specified).

- b. In potash areas, for all casing strings utilizing slips, these are to be set as soon as the crew and rig are ready and any fallback cement remediation has been done. For all casing strings, casing cut-off and BOP installation can be initiated at twelve hours after bumping the plug. However, **no tests** shall commence until the cement has had a minimum of 24 hours setup time, except the casing pressure test can be initiated immediately after bumping the plug (only applies to single stage cement jobs).
- c. The tests shall be done by an independent service company utilizing a test plug not a cup or J-packer. The operator also has the option of utilizing an independent tester to test without a plug (i.e. against the casing) pursuant to Onshore Order 2 with the pressure not to exceed 70% of the burst rating for the casing. Any test against the casing must meet the WOC time for water basin (8 hours) or potash (24 hours) or 500 pounds compressive strength, whichever is greater, prior to initiating the test (see casing segment as lead cement may be critical item).
- d. The test shall be run on a 5000 psi chart for a 2-3M BOP/BOP, on a 10000 psi chart for a 5M BOP/BOPE and on a 15000 psi chart for a 10M BOP/BOPE. If a linear chart is used, it shall be a one hour chart. A circular chart shall have a maximum 2 hour clock. If a twelve hour or twenty-four hour chart is used, tester shall make a notation that it is run with a two hour clock.
- e. The results of the test shall be reported to the appropriate BLM office.
- f. All tests are required to be recorded on a calibrated test chart. A copy of the BOP/BOPE test chart and a copy of independent service company test will be submitted to the appropriate BLM office.
- g. The BOP/BOPE test shall include a low pressure test from 250 to 300 psi. The test will be held for a minimum of 10 minutes if test is done with a test plug and 30 minutes without a test plug. This test shall be performed prior to the test at full stack pressure.
- h. BOP/BOPE must be tested by an independent service company within 500 feet of the top of the Wolfcamp formation if the time between the setting of the intermediate casing and reaching this depth exceeds 20 days. This test does not exclude the test prior to drilling out the casing shoe as per Onshore Order No. 2.
- C. DRILLING MUD

Mud system monitoring equipment, with derrick floor indicators and visual and audio alarms, shall be operating before drilling into the Wolfcamp formation, and shall be used until production casing is run and cemented.

D. WASTE MATERIAL AND FLUIDS

All waste (i.e. drilling fluids, trash, salts, chemicals, sewage, gray water, etc.) created as a result of drilling operations and completion operations shall be safely contained and disposed of properly at a waste disposal facility. No waste material or fluid shall be disposed of on the well location or surrounding area.

Porto-johns and trash containers will be on-location during fracturing operations or any other crew-intensive operations.

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Burton Flat 35-33 Fed Com 333H

13 3/8	S	urface csg in a	17 1/2	inch hole.		Design I	Factors			Surface		
Segment	#/ft	Grade		Coupling	Body	Collapse	Burst	Length	B@s	a-B	a-C	Weight
"A"	54.50		i 55	btc	44.73	6.91	4	350	18	6.71	13.04	19,075
"B"			,	btc				0				0
	w/8.4	4#/g mud, 30min Sfc Csg Test	psig: 1,500	Tail Cmt	does not	circ to sfc.	Totals:	350				19,075
Comparison o	of Proposed to	Minimum Required Cem	ent Volumes									
Hole	Annular	1 Stage	1 Stage	Min	1 Stage	Drilling	Calc	Reg'd				Min Dist
Size	Volume	Cmt Sx	CuFt Cmt	Cu Ft	% Excess	Mud Wt	MASP	BOPE				Hole-Cpl
17 1/2	0.6946	201	281	243	16	9.00	407	2M				1.56
10.274		cing incide the	12 2 /0			Design I	Eastara			Int 1		·· <i>—·</i>
10 3/4	ca #/ft	sing inside the Grade	13 3/8	Coupling	Joint	Collapse	Burst	Longth	D@a		a-C	Waight
Segment "A"	#/n 45.50	Graue	i 55	Coupling btc scc	8.90	3.07	3.06	Length	B@s 5	a-B 5.79	a-c 5.14	Weight 56,875
"B"	40.00] 55	DIC 500	0.90	3.07	3.00	1,250 0	Э	5.19	5.14	0,075 0
	w/8.4	4#/g mud, 30min Sfc Csg Test	psig: 1,500				Totals:	1,250	-			56,875
		The cement	volume(s) are inten	ided to achieve a top of	0	ft from su	rface or a	350				overlap.
Hole	Annular	1 Stage	1 Stage	Min	1 Stage	Drilling	Calc	Req'd				Min Dist
Size	Volume	Cmt Sx	CuFt Cmt	Cu Ft	% Excess	Mud Wt	MASP	BOPE				Hole-Cpl
12 1/4	0.1882	152	310	253	23	10.50	619	2M				0.50
							sum of sx	<u>Σ CuFt</u>				Σ%exces
) V Tool(s):							3011 01 37	2 001 1				
by stage % :	nt yld > 1.35	#VALUE!	#VALUE!				152	310				23
by stage % : Class 'C' tail cm						Design Fac	152			Int 2		23
by stage % : Class 'C' tail cm 8 5/8	ca	sing inside the	#VALUE!	Coupling	Joint	Design Fac	152	310	BØs	Int 2 a-B	a-C	
by stage % : class 'C' tail cm 8 5/8	ca #/ft		10 3/4	Coupling	Joint 13.46	Collapse	152 ctors Burst	310	B@s	a-B	a-C 6.84	Weight
by stage % : Class 'C' tail cm 8 5/8 Segment	ca	sing inside the			Joint 13.46		152	310 Length 2,500	B@s 8		a-C 6.84	Weight
by stage % : Class 'C' tail cm 8 5/8 Segment "A"	ca #/ft 32.00	sing inside the Grade	10 3/4 p 110			Collapse	152 ctors Burst	310 Length 2,500 0	<u> </u>	a-B		Weight 80,000 0
by stage % : Class 'C' tail cm 8 5/8 Segment "A"	ca #/ft 32.00	sing inside the Grade 4#/g mud, 30min Sfc Csg Test	10 3/4 p 110 psig: 1,500	tiw		Collapse	152 ctors Burst 2.21 Totals:	310 Length 2,500	<u> </u>	a-B	6.84	Weight 80,000 0
by stage % : Class 'C' tail cm 8 5/8 Segment "A"	ca #/ft 32.00	sing inside the Grade 4#/g mud, 30min Sfc Csg Test	10 3/4 p 110 psig: 1,500		13.46	Collapse 3.62	152 ctors Burst 2.21 Totals:	310 Length 2,500 0 2,500	<u> </u>	a-B	6.84	Weight 80,000 0 80,000 overlap.
by stage % : Class 'C' tail cm 8 5/8 Segment "A" "B"	ca #/ft 32.00 w/8.4	sing inside the Grade 4#/g mud, 30min Sfc Csg Test The cement	10 3/4 p 110 psig: 1,500 volume(s) are inten	tlw Ided to achieve a top of	13.46 1050	Collapse 3.62 ft from su	152 ctors Burst 2.21 Totals: rface or a	310 Length 2,500 0 2,500 200	<u> </u>	a-B	6.84	Weight 80,000 0 80,000 overlap. Min Dist
Segment "A" "B" Hole	ca #/ft 32.00 w/8.4	sing inside the Grade 4#/g mud, 30min Sfc Csg Test The cement 1 Stage	10 3/4 p 110 psig: 1,500 volume(s) are inten 1 Stage	tiw Ided to achieve a top of Min	13.46 1050 1 Stage	Collapse 3.62 ft from su Drilling	152 ctors Burst 2.21 Totals: rface or a Calc	310 Length 2,500 0 2,500 200 Req'd	<u> </u>	a-B	6.84	Weight 80,000 0 80,000
by stage % : class 'C' tail or 8 5/8 Segment "A" "B" Hole Size 9 7/8	ca #/ft 32.00 w/8. Annular Volume 0.1261	sing inside the Grade 4#/g mud, 30min Sfc Csg Test The cement 1 Stage Cmt Sx	10 3/4 p 110 psig: 1,500 volume(s) are inten 1 Stage CuFt Cmt	tiw Ided to achieve a top of Min Cu Ft	13.46 1050 1 Stage % Excess	Collapse 3.62 ft from su Drilling Mud Wt	152 ctors Burst 2.21 Totals: rface or a Calc MASP	310 Length 2,500 0 2,500 200 Req'd BOPE	<u> </u>	a-B	6.84	Weight 80,000 0 80,000 overlap. Min Dist Hole-Cpl
by stage % : Class 'C' tail or 8 5/8 Segment "A" "B" Hole Size	ca #/ft 32.00 w/8.4 Annular Volume 0.1261 nt yld > 1.35	sing inside the Grade 4#/g mud, 30min Sfc Csg Test The cement 1 Stage Cmt Sx	10 3/4 p 110 psig: 1,500 volume(s) are inten 1 Stage CuFt Cmt	tiw Ided to achieve a top of Min Cu Ft	13.46 1050 1 Stage % Excess	Collapse 3.62 ft from su Drilling Mud Wt	152 ctors Burst 2.21 Totals: rface or a Calc MASP 2139	310 Length 2,500 0 2,500 200 Req'd BOPE	<u> </u>	a-B	6.84	Weight 80,000 0 80,000 overlap. Min Dist Hole-Cpl
by stage % : class 'C' tail cm 8 5/8 Segment "A" "B" Hole Size 9 7/8 class 'C' tail cm 5 1/2	ca #/ft 32.00 w/8.4 Annular Volume 0.1261 nt yld > 1.35	sing inside the Grade 4#/g mud, 30min Sfc Csg Test The cement 1 Stage Cmt Sx 165	10 3/4 p 110 psig: 1,500 volume(s) are inten 1 Stage CuFt Cmt 417	tiw Ided to achieve a top of Min Cu Ft	13.46 1050 1 Stage % Excess	Collapse 3.62 ft from su Drilling Mud Wt 9.00	152 ctors Burst 2.21 Totals: rface or a Calc MASP 2139	310 Length 2,500 0 2,500 200 Req'd BOPE	<u> </u>	a-B 4.17	6.84	Weight 80,000 0 80,000 overlap. Min Dist Hole-Cpl. 0.44
by stage % : class 'C' tail cm 8 5/8 Segment "A" "B" Hole Size 9 7/8 class 'C' tail cm 5 1/2	ca #/ft 32.00 w/8. Annular Volume 0.1261 0.1261 nt yld > 1.35	sing inside the Grade 4#/g mud, 30min Sfc Csg Test The cement 1 Stage Cmt Sx 165 sing inside the	10 3/4 p 110 psig: 1,500 volume(s) are inten 1 Stage CuFt Cmt 417	thw Ided to achieve a top of Min Cu Ft 185	13.46 1050 1 Stage % Excess 126	Collapse 3.62 ft from su Drilling Mud Wt 9.00 Design I	152 ctors Burst 2.21 Totals: rface or a Calc MASP 2139 Factors	310 Length 2,500 0 2,500 200 Req'd BOPE 3M	8	a-B 4.17 Prod 1	6.84	Weight 80,000 0 80,000 overlap. Min Dist Hole-Cpl
by stage % : class 'C' tail cm 8 5/8 Segment "A" "B" Hole Size 9 7/8 class 'C' tail cm 5 1/2 Segment	ca #/ft 32.00 w/8. Annular Volume 0.1261 nt yld > 1.35 ca #/ft	sing inside the Grade 4#/g mud, 30min Sfc Csg Test The cement 1 Stage Cmt Sx 165 sing inside the	10 3/4 p 110 psig: 1,500 volume(s) are inten 1 Stage CuFt Cmt 417 8 5/8	thw Ided to achieve a top of Min Cu Ft 185 Coupling	13.46 1050 1 Stage % Excess 126 Joint	Collapse 3.62 ft from su Drilling Mud Wt 9.00 <u>Design I</u> Collapse	152 ctors Burst 2.21 Totals: rface or a Calc MASP 2139 Factors Burst	310 Length 2,500 2,500 200 Req'd BOPE 3M	8 B@s	a-B 4.17 Prod 1 a-B	6.84 a-C	Weight 80,000 0 80,000 overlap. Min Dist Hole-Cpl 0.44 Weight
by stage % : Class 'C' tail cm 8 5/8 Segment "A" "B" Hole Size 9 7/8 Class 'C' tail cm 5 1/2 Segment "A"	ca #/ft 32.00 w/8.4 Annular Volume 0.1261 nt yld > 1.35 ca #/ft 20.00	sing inside the Grade 4#/g mud, 30min Sfc Csg Test The cement 1 Stage Cmt Sx 165 sing inside the	10 3/4 p 110 psig: 1,500 volume(s) are inten 1 Stage CuFt Cmt 417 8 5/8 p 110	thw Ided to achieve a top of Min Cu Ft 185 Coupling	13.46 1050 1 Stage % Excess 126 Joint	Collapse 3.62 ft from su Drilling Mud Wt 9.00 <u>Design I</u> Collapse	152 ctors Burst 2.21 Totals: rface or a Calc MASP 2139 Factors Burst	310 Length 2,500 2,500 200 Req'd BOPE 3M	8 B@s	a-B 4.17 Prod 1 a-B	6.84 a-C	Weight 80,000 0 80,000 overlap. Min Dist Hole-Cpl 0.44 Weight 383,980 0
by stage % : Class 'C' tail cm 8 5/8 Segment "A" "B" Hole Size 9 7/8 Class 'C' tail cm 5 1/2 Segment "A"	ca #/ft 32.00 w/8.4 Annular Volume 0.1261 nt yld > 1.35 ca #/ft 20.00	sing inside the Grade 4#/g mud, 30min Sfc Csg Test The cement 1 Stage Cmt Sx 165 sing inside the Grade 4#/g mud, 30min Sfc Csg Test	10 3/4 p 110 psig: 1,500 volume(s) are inter 1 Stage CuFt Cmt 417 8 5/8 p 110 psig: 1,901	thw Ided to achieve a top of Min Cu Ft 185 Coupling	13.46 1050 1 Stage % Excess 126 Joint	Collapse 3.62 ft from su Drilling Mud Wt 9.00 <u>Design I</u> Collapse	152 ctors Burst 2.21 Totals: rface or a Calc MASP 2139 Factors Burst 3.48 Totals:	310 Length 2,500 0 2,500 200 200 80PE 3M	8 B@s	a-B 4.17 Prod 1 a-B	6.84 a-C 5.65	Weigh 80,000 overlap. Min Dist Hole-Cpl 0.44 Weigh 383,980 0
by stage % : Class 'C' tail cm 8 5/8 Segment "A" "B" Hole Size 9 7/8 Class 'C' tail cm 5 1/2 Segment "A"	ca #/ft 32.00 w/8.4 Annular Volume 0.1261 nt yld > 1.35 ca #/ft 20.00	sing inside the Grade 4#/g mud, 30min Sfc Csg Test The cement 1 Stage Cmt Sx 165 sing inside the Grade 4#/g mud, 30min Sfc Csg Test	10 3/4 p 110 psig: 1,500 volume(s) are inter 1 Stage CuFt Cmt 417 8 5/8 p 110 psig: 1,901	tiw ided to achieve a top of Min Cu Ft 185 Coupling dwc/c is+	13.46 1050 1 Stage % Excess 126 Joint 4.22	Collapse 3.62 If from su Drilling Mud Wt 9.00 Design I Collapse 2.99	152 ctors Burst 2.21 Totals: rface or a Calc MASP 2139 Factors Burst 3.48 Totals:	310 Length 2,500 2,500 200 Req'd BOPE 3M Length 19,199	8 B@s	a-B 4.17 Prod 1 a-B	6.84 a-C 5.65	Weight 80,000 0 everlap. Min Dist Hole-Cpl 0.44 Weight 383,980 0 383,980 overlap.
by stage % : Class 'C' tail cm 8 5/8 Segment "A" "B" Hole Size 9 7/8 Class 'C' tail cm 5 1/2 Segment "A" "B"	ca #/ft 32.00 w/8. Annular Volume 0.1261 nt yld > 1.35 ca #/ft 20.00 w/8.	sing inside the Grade 4#/g mud, 30min Sfc Csg Test The cement 1 Stage Cmt Sx 165 sing inside the Grade 4#/g mud, 30min Sfc Csg Test The cement	10 3/4 p 110 psig: 1,500 volume(s) are inten 1 Stage CuFt Cmt 417 8 5/8 p 110 psig: 1,901 volume(s) are inten	tiw ided to achieve a top of Min Cu Ft 185 Coupling dwc/c is+	13.46 1050 1 Stage % Excess 126 Joint 4.22 2300	Collapse 3.62 ft from su Drilling Mud Wt 9.00 <u>Design I</u> Collapse 2.99 ft from su	152 tors Burst 2.21 Totals: rface or a Calc MASP 2139 Eactors Burst 3.48 Totals: rface or a	310 Length 2,500 2,500 200 Req'd BOPE 3M Length 19,199 0 19,199 200	8 B@s	a-B 4.17 Prod 1 a-B	6.84 a-C 5.65	Weight 80,000 overlap. Min Dist Hole-Cpl, 0.44 Weight 383,980 overlap. Min Dist
by stage % : class 'C' tail cm 8 5/8 Segment "A" "B" Hole Size 9 7/8 class 'C' tail cm 5 1/2 Segment "A" "B" Hole	ca #/ft 32.00 w/8.4 Annular Volume 0.1261 nt yld ≥ 1.35 ca #/ft 20.00 w/8.4	sing inside the Grade 4#/g mud, 30min Sfc Csg Test The cement 1 Stage Cmt Sx 165 sing inside the Grade 4#/g mud, 30min Sfc Csg Test The cement 1 Stage	10 3/4 p 110 psig: 1,500 volume(s) are inten 1 Stage CuFt Cmt 417 8 5/8 p 110 psig: 1,901 volume(s) are inten 1 Stage	tiw ded to achieve a top of Min Cu Ft 185 Coupling dwc/c is+ ded to achieve a top of Min	13.46 1050 1 Stage % Excess 126 Joint 4.22 2300 1 Stage	Collapse 3.62 ft from su Drilling Mud Wt 9.00 <u>Design I</u> Collapse 2.99 ft from su Drilling	152 ctors Burst 2.21 Totals: rface or a Calc MASP 2139 Factors Burst 3.48 Totals: rface or a Calc	310 Length 2,500 200 200 200 200 200 200 200 200 200	8 B@s	a-B 4.17 Prod 1 a-B	6.84 a-C 5.65	Weight 80,000 0 80,000 overlap. Min Dist Hole-Cpl 0.44 Weight 383,980 0 383,980

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State of New Mexico Energy, Minerals and Natural Resources Oil Conservation Division 1220 S. St Francis Dr. Santa Fe, NM 87505

CONDITIONS

Operator:	OGRID:
DEVON ENERGY PRODUCTION COMPANY, LP	6137
333 West Sheridan Ave.	Action Number:
Oklahoma City, OK 73102	158944
	Action Type:
	[C-103] NOI Change of Plans (C-103A)

CONDITIONS

Created By	Condition	Condition Date
kpickford	Adhere to previous NMOCD Conditions of Approval	11/16/2022

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Action 158944