Sundry Print Report

U.S. Department of the Interior BUREAU OF LAND MANAGEMENT

SAWTOOTH

Well Name: JAMES RANCH UNIT DI 7 Well Location: T23S / R31E / SEC 6 /

LOT 4 / 32.339942 / -103.821891

County or Parish/State: EDDY /

Well Number: 111H Type of Well: OIL WELL Allottee or Tribe Name:

Lease Number: NMNM02887D Unit or CA Name: JAMES RANCH, **Unit or CA Number:**

NMNM070965Z, NMNM70965X JAMES RANCH UNIT

US Well Number: 3001550085 Well Status: Approved Application for **Operator: XTO PERMIAN**

OPERATING LLC Permit to Drill

Notice of Intent

Sundry ID: 2753464

Type of Submission: Notice of Intent Type of Action: APD Change

Date Sundry Submitted: 09/26/2023 **Time Sundry Submitted: 02:56**

Date proposed operation will begin: 11/01/2023

Procedure Description: ** Surface hole Change, First and Last Take Point Changes, Bottomhole Location Change, Drilling Plan Change, Casing/Cement Change XTO Permian Operating, LCC. requests permission to make the following changes to the original APD: No Additional Surface Disturbance SHL: fr/300'FNL & 1149'FWL to 155'FNL & 1070'FWL, NMNM02887D FTP: fr/1000'FNL & 2310'FWL to 330'FNL & 2310'FWL, NMNM02887D PPP #1: 2636' FNL & 2310' FWL, NMNM04473 PPP#2: 0' FNL & 2310' FWL, NMNM02887D LTP: fr/2440'FNL & 2310'FWL to 2539'FNL & 2310'FWL, NMNM02887A BHL: fr/2490'FNL & 2310'FWL to 2589'FNL & 2310'FWL, Section 18-T23S-R31E NMNM02887A Additionally, XTO Permian Operating, LLC. respectfully requests permission to change from a threestring design to a four-string design. The surface, intermediate and production hole, casing, and cement based on the attached drilling program. Due to the design change in these strings, the wellhead configuration has also changed based on the attached drilling program. Casing/Cement design per the attached drilling program. Attachments: C102 Drilling Program MBS Directional Plan OLCV Spud BOP BTV Cement Variance

NOI Attachments

Procedure Description

JRU_7_Sawtooth_111H__Sundry_Attachments_20230926144124.pdf

Page 1 of 2

Well Name: JAMES RANCH UNIT DI 7

SAWTOOTH

Well Location: T23S / R31E / SEC 6 / LOT 4 / 32.339942 / -103.821891

County or Parish/State: Page 2 of

NM

Zip:

Well Number: 111H

Type of Well: OIL WELL

Allottee or Tribe Name:

Lease Number: NMNM02887D

Unit or CA Name: JAMES RANCH,

JAMES RANCH UNIT

Unit or CA Number: NMNM070965Z, NMNM70965X

US Well Number: 3001550085

Well Status: Approved Application for

Permit to Drill

Operator: XTO PERMIAN

OPERATING LLC

Conditions of Approval

Additional

Sec 06 23S 31E NMP Sundry 2753464 James Ranch Unit DI 7 Sawtooth 111H COAs 20231017155316.pdf

Operator

I certify that the foregoing is true and correct. Title 18 U.S.C. Section 1001 and Title 43 U.S.C. Section 1212, make it a crime for any person knowingly and willfully to make to any department or agency of the United States any false, fictitious or fraudulent statements or representations as to any matter within its jurisdiction. Electronic submission of Sundry Notices through this system satisfies regulations requiring a

Operator Electronic Signature: CASSIE EVANS Signed on: OCT 18, 2023 03:15 PM

Name: XTO PERMIAN OPERATING LLC

Title: Regulatory Analyst

Street Address: 6401 Holiday Hill Road, Bldg 5

City: Midland State: TX

Phone: (432) 218-3671

Email address: CASSIE.EVANS@EXXONMOBIL.COM

State:

Field

Representative Name:

Street Address:

City:

Phone:

Email address:

BLM Point of Contact

BLM POC Name: CHRISTOPHER WALLS

BLM POC Title: Petroleum Engineer

BLM POC Phone: 5752342234 BLM POC Email Address: cwalls@blm.gov

Disposition: Approved **Disposition Date:** 10/20/2023

Signature: Chris Walls

Page 2 of 2

Form 3160-5 (June 2019)

UNITED STATES DEPARTMENT OF THE INTERIOR BUREAU OF LAND MANAGEMENT

FORM APPROVED
OMB No. 1004-0137
Expires: October 31, 202

DORI	EAU OF LAND MANAGEMENT		N	NMNM02887D
Do not use this f	OTICES AND REPORTS ON Worm for proposals to drill or to Jse Form 3160-3 (APD) for suc	re-enter an	6. If Indian, Allottee	or Tribe Name
SUBMIT IN 1	FRIPLICATE - Other instructions on pag	e 2	7. If Unit of CA/Agre	eement, Name and/or No.
1. Type of Well		<u> </u>	1	AMES RANCH UNIT/NMNM070965Z,
Oil Well Gas W	Vell Other		8. Well Name and No	. JAMES RANCH UNIT DI 7 SAWTO
2. Name of Operator XTO PERMIAN	OPERATING LLC		9. API Well No. 300	 1550085
3a. Address 6401 HOLIDAY HILL RO		(include area code)	10. Field and Pool or Purple Sage/WOL	Exploratory Area
4. Location of Well (Footage, Sec., T.,R SEC 6/T23S/R31E/NMP	.,M., or Survey Description)		11. Country or Parish	, State
12. CHE	CK THE APPROPRIATE BOX(ES) TO INI	DICATE NATURE OF NOT	TICE, REPORT OR OT	HER DATA
TYPE OF SUBMISSION		TYPE OF AC	CTION	
✓ Notice of Intent	Acidize Deep Alter Casing Hydr	_	duction (Start/Resume)	Water Shut-Off Well Integrity
Subsequent Report			omplete nporarily Abandon	Other
Final Abandonment Notice	Convert to Injection Plug	Back Wat	er Disposal	
completion of the involved operation completed. Final Abandonment Not is ready for final inspection.) ** Surface hole Change, First at XTO Permian Operating, LCC. No Additional Surface Disturbation SHL: fr/300FNL & 1149FWL to	o 155FNL & 1070FWL, NMNM02887D to 330FNL & 2310FWL, NMNM02887D	npletion or recompletion in a s, including reclamation, har ole Location Change, Drill	new interval, a Form 3 ve been completed and ing Plan Change, Ca	3160-4 must be filed once testing has been the operator has detennined that the site
Continued on page 3 additional	information			
14. I hereby certify that the foregoing is CASSIE EVANS / Ph: (432) 218-36	true and correct. Name (Printed/Typed) 71	Regulatory Analysi	i	
Signature (Electronic Submissio	n)	Date	10/18/2	2023
	THE SPACE FOR FEDI	ERAL OR STATE O	FICE USE	
Approved by				
CHRISTOPHER WALLS / Ph: (575	s) 234-2234 / Approved	Petroleum En Title	gineer	10/20/2023 Date
	ned. Approval of this notice does not warran quitable title to those rights in the subject le duct operations thereon.	t or)	
		<u> </u>		

Title 18 U.S.C Section 1001 and Title 43 U.S.C Section 1212, make it a crime for any person knowingly and willfully to make to any department or agency of the United States any false, fictitious or fraudulent statements or representations as to any matter within its jurisdiction.

(Instructions on page 2)

GENERAL INSTRUCTIONS

This form is designed for submitting proposals to perform certain well operations and reports of such operations when completed as indicated on Federal and Indian lands pursuant to applicable Federal law and regulations. Any necessary special instructions concerning the use of this form and the number of copies to be submitted, particularly with regard to local area or regional procedures and practices, are either shown below, will be issued by or may be obtained from the local Federal office.

SPECIFIC INSTRUCTIONS

Item 4 - Locations on Federal or Indian land should be described in accordance with Federal requirements. Consult the local Federal office for specific instructions.

Item 13: Proposals to abandon a well and subsequent reports of abandonment should include such special information as is required by the local Federal office. In addition, such proposals and reports should include reasons for the abandonment; data on any former or present productive zones or other zones with present significant fluid contents not sealed off by cement or otherwise; depths (top and bottom) and method of placement of cement plugs; mud or other material placed below, between and above plugs; amount, size, method of parting of any casing, liner or tubing pulled and the depth to the top of any tubing left in the hole; method of closing top of well and date well site conditioned for final inspection looking for approval of the abandonment. If the proposal will involve **hydraulic fracturing operations**, you must comply with 43 CFR 3162.3-3, including providing information about the protection of usable water. Operators should provide the best available information about all formations containing water and their depths. This information could include data and interpretation of resistivity logs run on nearby wells. Information may also be obtained from state or tribal regulatory agencies and from local BLM offices.

NOTICES

The privacy Act of 1974 and the regulation in 43 CFR 2.48(d) provide that you be furnished the following information in connection with information required by this application.

AUTHORITY: 30 U.S.C. 181 et seq., 351 et seq., 25 U.S.C. 396; 43 CFR 3160.

PRINCIPAL PURPOSE: The information is used to: (1) Evaluate, when appropriate, approve applications, and report completion of subsequent well operations, on a Federal or Indian lease; and (2) document for administrative use, information for the management, disposal and use of National Resource lands and resources, such as: (a) evaluating the equipment and procedures to be used during a proposed subsequent well operation and reviewing the completed well operations for compliance with the approved plan; (b) requesting and granting approval to perform those actions covered by 43 CFR 3162.3-2, 3162.3-3, and 3162.3-4; (c) reporting the beginning or resumption of production, as required by 43 CFR 3162.4-1(c)and (d) analyzing future applications to drill or modify operations in light of data obtained and methods used.

ROUTINE USES: Information from the record and/or the record will be transferred to appropriate Federal, State, local or foreign agencies, when relevant to civil, criminal or regulatory investigations or prosecutions in connection with congressional inquiries or to consumer reporting agencies to facilitate collection of debts owed the Government.

EFFECT OF NOT PROVIDING THE INFORMATION: Filing of this notice and report and disclosure of the information is mandatory for those subsequent well operations specified in 43 CFR 3162.3-2, 3162.3-4.

The Paperwork Reduction Act of 1995 requires us to inform you that:

The BLM collects this information to evaluate proposed and/or completed subsequent well operations on Federal or Indian oil and gas leases.

Response to this request is mandatory.

The BLM would like you to know that you do not have to respond to this or any other Federal agency-sponsored information collection unless it displays a currently valid OMB control number.

BURDEN HOURS STATEMENT: Public reporting burden for this form is estimated to average 8 hours per response, including the time for reviewing instructions, gathering and maintaining data, and completing and reviewing the form. Direct comments regarding the burden estimate or any other aspect of this form to U.S. Department of the Interior, Bureau of Land Management (1004-0137), Bureau Information Collection Clearance Officer (WO-630), 1849 C St., N.W., Mail Stop 401 LS, Washington, D.C. 20240

(Form 3160-5, page 2)

Additional Information

Additional Remarks

PPP#2: 0 FNL & 2310 FWL, NMNM02887D

LTP: fr/2440FNL & 2310FWL to 2539FNL & 2310FWL, NMNM02887A

BHL: fr/2490FNL & 2310FWL to 2589FNL & 2310FWL, Section 18-T23S-R31E NMNM02887A

Additionally, XTO Permian Operating, LLC. respectfully requests permission to change from a three-string design to a four-string design. The surface, intermediate and production hole, casing, and cement based on the attached drilling program. Due to the design change in these strings, the wellhead configuration has also changed based on the attached drilling program.

Casing/Cement design per the attached drilling program.

Attachments:

C102

Drilling Program

MBS

Directional Plan

OLCV

Spud

BOP BTV

Cement Variance

Location of Well

0. SHL: LOT 4 / 300 FNL / 1149 FWL / TWSP: 23S / RANGE: 31E / SECTION: 6 / LAT: 32.339942 / LONG: -103.821891 (TVD: 0 feet, MD: 0 feet)

PPP: LOT 3 / 1000 FNL / 2310 FWL / TWSP: 23S / RANGE: 31E / SECTION: 6 / LAT: 32.338008 / LONG: -103.818134 (TVD: 11168 feet, MD: 11570 feet)

PPP: NENW / 330 FNL / 2310 FWL / TWSP: 23S / RANGE: 31E / SECTION: 7 / LAT: 32.32523 / LONG: -103.81905 (TVD: 11168 feet, MD: 16520 feet)

PPP: NESW / 2310 FSL / 2310 FWL / TWSP: 23S / RANGE: 31E / SECTION: 6 / LAT: 32.33263 / LONG: -103.81965 (TVD: 11168 feet, MD: 13880 feet)

BHL: SENW / 2490 FNL / 2310 FWL / TWSP: 23S / RANGE: 31E / SECTION: 18 / LAT: 32.304883 / LONG: -103.818153 (TVD: 11168 feet, MD: 23621 feet)

PECOS DISTRICT DRILLING CONDITIONS OF APPROVAL

OPERATOR'S NAME: | XTO Permian Operating

WELL NAME & NO.: James Ranch Unit DI 7 Sawtooth 111H

LOCATION: Sec 06-23S-31E-NMP Eddy County, New Mexico

Changes approved through engineering via **Sundry 2753464** on 10/17/2023. Any previous COAs not addressed within the updated COAs still apply.

COA

H ₂ S	O No	Yes		
Potash / WIPP	O None	Secretary	⊙ R-111-P	□ WIPP
Cave / Karst	C Low	• Medium	High	Critical
Wellhead	Conventional	Multibowl	Both	O Diverter
Cementing	☐ Primary Squeeze	Cont. Squeeze	EchoMeter	□ DV Tool
Special Req	Break Testing	☐ Water Disposal	□ COM	Unit
Variance	▼ Flex Hose	☐ Casing Clearance	☐ Pilot Hole	☐ Capitan Reef
Variance	▼ Four-String	Offline Cementing	☐ Fluid-Filled	☐ Open Annulus
		Batch APD / Sundry		

A. HYDROGEN SULFIDE

A Hydrogen Sulfide (H2S) Drilling Plan shall be activated 500 feet prior to drilling into the **H2S Stream** (per BLM geologist). As a result, the Hydrogen Sulfide area must meet all requirements from 43 CFR 3176, which includes equipment and personnel/public protection items. If Hydrogen Sulfide is encountered, please provide measured values and formations to the BLM.

B. CASING

1. The 13-3/8 inch surface casing shall be set at approximately 571 feet (a minimum of 70 feet (Eddy County) into the Rustler Anhydrite, above the salt, and below usable fresh water) and cemented to the surface. Notes from the BLM geologist regarding this set point dictate: Operator has extensive drilling experience in this area and has encountered lost circulation in BLM's preferred setpoint for the surface casing just below the Magenta Dolomite. BLM accepts the base of the Rustler Formation and Top of the Salt as surface casing setpoint. Operator must set surface casing at this depth and not deeper in the salt. If operator's proposed setpoint is deeper than top of salt, Operator will set surface casing at top of salt.

- a. If cement does not circulate to the surface, the appropriate BLM office shall be notified and a temperature survey utilizing an electronic type temperature survey with surface log readout will be used or a cement bond log shall be run to verify the top of the cement. Temperature survey will be run a minimum of six hours after pumping cement and ideally between 8-10 hours after completing the cement job.
- b. Wait on cement (WOC) time for a primary cement job will be a minimum of **24 hours in the Potash Area** or 500 pounds compressive strength, whichever is greater. (This is to include the lead cement)
- c. Wait on cement (WOC) time for a remedial job will be a minimum of 4 hours after bringing cement to surface or 500 pounds compressive strength, whichever is greater.
- d. If cement falls back, remedial cementing will be done prior to drilling out that string.
- 2. The minimum required fill of cement behind the 9-5/8 inch intermediate casing is:
 - Cement to surface. If cement does not circulate see B.1.a, c-d above.
 Wait on cement (WOC) time for a primary cement job is to include the lead cement slurry due to cave/karst, Capitan Reef, or potash.
 - ❖ In <u>R111 Potash Areas</u> if cement does not circulate to surface on the first two salt protection casing strings, the cement on the 3rd casing salt string must come to surface.
- 3. The minimum required fill of cement behind the **7-5/8** inch intermediate casing is:

Operator has proposed to cement in two stages by conventionally cementing the first stage and performing a bradenhead squeeze on the second stage, contingent upon no returns to surface.

- a. First stage: Operator will cement with intent to reach the top of the **Brushy** Canyon at 6550'
- b. Second stage:
 - Operator will perform bradenhead squeeze and top-out. Cement to surface. If cement does not reach surface, the appropriate BLM office shall be notified. Wait on cement (WOC) time for a primary cement job is to include the lead cement slurry due to cave/karst, Capitan Reef, or potash.

Operator has proposed to pump down 9-5/8" X 7-5/8" annulus after primary cementing stage. Operator must run Echo-meter to verify Cement Slurry/Fluid top in the annulus OR operator shall run a CBL from TD of the 7-5/8" casing to surface after the second stage BH to verify TOC.

Submit results to the BLM. No displacement fluid/wash out shall be utilized at the top of the cement slurry between second stage BH and top out.

If cement does not reach surface, the next casing string must come to surface.

Operator must use a limited flush fluid volume of 1 bbl following backside cementing procedures.

- 4. The minimum required fill of cement behind the 5-1/2 inch production casing is:
 - Cement should tie-back at least 500 feet into previous casing string.
 Operator shall provide method of verification. Wait on cement (WOC) time for a primary cement job is to include the lead cement slurry due to cave/karst, Capitan Reef, or potash.

C. PRESSURE CONTROL

- 1. Variance approved to use flex line from BOP to choke manifold. Manufacturer's specification to be readily available. No external damage to flex line. Flex line to be installed as straight as possible (no hard bends).
- 2. Operator has proposed a multi-bowl wellhead assembly. Minimum working pressure of the blowout preventer (BOP) and related equipment (BOPE) required for drilling below the surface casing shoe shall be **5000 (5M)** psi.
 - a. Wellhead shall be installed by manufacturer's representatives, submit documentation with subsequent sundry.
 - b. If the welding is performed by a third party, the manufacturer's representative shall monitor the temperature to verify that it does not exceed the maximum temperature of the seal.
 - c. Manufacturer representative shall install the test plug for the initial BOP test.
 - d. If the cement does not circulate and one inch operations would have been possible with a standard wellhead, the well head shall be cut off, cementing operations performed and another wellhead installed.
 - e. Whenever any seal subject to test pressure is broken, all the tests in 43 CFR 3172 must be followed.

D. SPECIAL REQUIREMENT (S)

Unit Wells

The well sign for a unit well shall include the unit number in addition to the surface and bottom hole lease numbers. This also applies to participating area numbers. If a participating area has not been established, the operator can use the general unit designation, but will replace the unit number with the participating area number when the sign is replaced.

Commercial Well Determination

A commercial well determination shall be submitted after production has been established for at least six months.

(Note: For a minimum 5M BOPE or less (Utilizing a 10M BOPE system) BOPE Break Testing Variance

- BOPE Break Testing is ONLY permitted for 5M BOPE or less. (Annular preventer must be tested to a minimum of 70% of BOPE working pressure and shall be higher than the MASP)
- BOPE Break Testing is NOT permitted to drilling the production hole section.
- Variance only pertains to the intermediate hole-sections and no deeper than the Bone Springs formation.
- While in transfer between wells, the BOPE shall be secured by the hydraulic carrier or cradle.
- Any well control event while drilling require notification to the BLM Petroleum Engineer (575-706-2779) prior to the commencement of any BOPE Break Testing operations.
- A full BOPE test is required prior to drilling the first deep intermediate hole section. If any subsequent hole interval is deeper than the first, a full BOPE test will be required. (200' TVD tolerance between intermediate shoes is allowable).
- The BLM is to be contacted (575-361-2822 Eddy County) 4 hours prior to BOPE tests.
- As a minimum, a full BOPE test shall be performed at 21-day intervals.
- In the event any repairs or replacement of the BOPE is required, the BOPE shall test as per Onshore Oil and Gas Order No. 2.
- If in the event break testing is not utilized, then a full BOPE test would be conducted.

Offline Cementing

Contact the BLM prior to the commencement of any offline cementing procedure.

GENERAL REQUIREMENTS

The BLM is to be notified in advance for a representative to witness:

- a. Spudding well (minimum of 24 hours)
- b. Setting and/or Cementing of all casing strings (minimum of 4 hours)
- c. BOPE tests (minimum of 4 hours)
 - Eddy County
 Email or call the Carlsbad Field Office, 620 East Greene St., Carlsbad, NM 88220, BLM_NM_CFO_DrillingNotifications@BLM.GOV (575) 361-2822
 - Lea County
 Call the Hobbs Field Station, 414 West Taylor, Hobbs NM 88240, (575) 689-5981

- 1. Unless the production casing has been run and cemented or the well has been properly plugged, the drilling rig shall not be removed from over the hole without prior approval.
 - a. In the event the operator has proposed to drill multiple wells utilizing a skid/walking rig. Operator shall secure the wellbore on the current well, after installing and testing the wellhead, by installing a blind flange of like pressure rating to the wellhead and a pressure gauge that can be monitored while drilling is performed on the other well(s).
 - b. When the operator proposes to set surface casing with Spudder Rig
 - Notify the BLM when moving in and removing the Spudder Rig.
 - Notify the BLM when moving in the 2nd Rig. Rig to be moved in within 90 days of notification that Spudder Rig has left the location.
 - BOP/BOPE test to be conducted per **43 CFR part 3170 Subpart 3172** as soon as 2nd Rig is rigged up on well.
- 2. Floor controls are required for 3M or Greater systems. These controls will be on the rig floor, unobstructed, readily accessible to the driller and will be operational at all times during drilling and/or completion activities. Rig floor is defined as the area immediately around the rotary table; the area immediately above the substructure on which the draw works are located, this does not include the dog house or stairway area.
- 3. The record of the drilling rate along with the GR/N well log run from TD to surface (horizontal well vertical portion of hole) shall be submitted to the BLM office as well as all other logs run on the borehole 30 days from completion. If available, a digital copy of the logs is to be submitted in addition to the paper copies. The Rustler top and top and bottom of Salt are to be recorded on the Completion Report.

A. CASING

- 1. Changes to the approved APD casing program need prior approval if the items substituted are of lesser grade or different casing size or are Non-API. The Operator can exchange the components of the proposal with that of superior strength (i.e. changing from J-55 to N-80, or from 36# to 40#). Changes to the approved cement program need prior approval if the altered cement plan has less volume or strength or if the changes are substantial (i.e. Multistage tool, ECP, etc.). The initial wellhead installed on the well will remain on the well with spools used as needed.
- 2. Wait on cement (WOC) for Potash Areas: After cementing but before commencing any tests, the casing string shall stand cemented under pressure until both of the following conditions have been met: 1) cement reaches a minimum compressive strength of 500 psi for all cement blends, 2) until cement has been in place at least 24 hours. WOC time will be recorded in the driller's log. The casing intergrity test can be done (prior to the cement setting up) immediately after bumping the plug.

- 3. Wait on cement (WOC) for Water Basin: After cementing but before commencing any tests, the casing string shall stand cemented under pressure until both of the following conditions have been met: 1) cement reaches a minimum compressive strength of 500 psi at the shoe, 2) until cement has been in place at least 8 hours. WOC time will be recorded in the driller's log. See individual casing strings for details regarding lead cement slurry requirements. The casing integrity test can be done (prior to the cement setting up) immediately after bumping the plug.
- 4. Provide compressive strengths including hours to reach required 500 pounds compressive strength prior to cementing each casing string. Have well specific cement details onsite prior to pumping the cement for each casing string.
- 5. No pea gravel permitted for remedial or fall back remedial without prior authorization from the BLM engineer.
- 6. On that portion of any well approved for a 5M BOPE system or greater, a pressure integrity test of each casing shoe shall be performed. Formation at the shoe shall be tested to a minimum of the mud weight equivalent anticipated to control the formation pressure to the next casing depth or at total depth of the well. This test shall be performed before drilling more than 20 feet of new hole.
- 7. If hardband drill pipe is rotated inside casing, returns will be monitored for metal. If metal is found in samples, drill pipe will be pulled and rubber protectors which have a larger diameter than the tool joints of the drill pipe will be installed prior to continuing drilling operations.
- 8. Whenever a casing string is cemented in the R-111-P potash area, the NMOCD requirements shall be followed.

B. PRESSURE CONTROL

- 1. All blowout preventer (BOP) and related equipment (BOPE) shall comply with well control requirements as described in 43 CFR part 3170 Subpart 3172 and API STD 53 Sec. 5.3.
- 2. If a variance is approved for a flexible hose to be installed from the BOP to the choke manifold, the following requirements apply: The flex line must meet the requirements of API 16C. Check condition of flexible line from BOP to choke manifold, replace if exterior is damaged or if line fails test. Line to be as straight as possible with no hard bends and is to be anchored according to Manufacturer's requirements. The flexible hose can be exchanged with a hose of equal size and equal or greater pressure rating. Anchor requirements, specification sheet and hydrostatic pressure test certification matching the hose in service, to be onsite for review. These documents shall be posted in the company man's trailer and on the rig floor.

- 3. 5M or higher system requires an HCR valve, remote kill line and annular to match. The remote kill line is to be installed prior to testing the system and tested to stack pressure.
- 4. If the operator has proposed a multi-bowl wellhead assembly in the APD. The following requirements must be met:
 - a. Wellhead shall be installed by manufacturer's representatives, submit documentation with subsequent sundry.
 - b. If the welding is performed by a third party, the manufacturer's representative shall monitor the temperature to verify that it does not exceed the maximum temperature of the seal.
 - c. Manufacturer representative shall install the test plug for the initial BOP test.
 - d. Whenever any seal subject to test pressure is broken, all the tests in 43 CFR part 3170 Subpart 3172 must be followed.
 - e. If the cement does not circulate and one inch operations would have been possible with a standard wellhead, the well head shall be cut off, cementing operations performed and another wellhead installed.
- 5. The appropriate BLM office shall be notified a minimum of 4 hours in advance for a representative to witness the tests.
 - a. In a water basin, for all casing strings utilizing slips, these are to be set as soon as the crew and rig are ready and any fallback cement remediation has been done. The casing cut-off and BOP installation can be initiated four hours after installing the slips, which will be approximately six hours after bumping the plug. For those casing strings not using slips, the minimum wait time before cut-off is eight hours after bumping the plug. BOP/BOPE testing can begin after cut-off or once cement reaches 500 psi compressive strength (including lead cement), whichever is greater. However, if the float does not hold, cut-off cannot be initiated until cement reaches 500 psi compressive strength (including lead when specified).
 - b. In potash areas, for all casing strings utilizing slips, these are to be set as soon as the crew and rig are ready and any fallback cement remediation has been done. For all casing strings, casing cut-off and BOP installation can be initiated at twelve hours after bumping the cement plug. The BOPE test can be initiated after bumping the cement plug with the casing valve open. (only applies to single stage cement jobs, prior to the cement setting up.)
 - c. The tests shall be done by an independent service company utilizing a test plug not a cup or J-packer and can be initiated immediately with the casing valve open. The operator also has the option of utilizing an independent tester to test without a plug (i.e. against the casing) pursuant to **43 CFR part 3170**

Subpart 3172 with the pressure not to exceed 70% of the burst rating for the casing. Any test against the casing must meet the WOC time for water basin (8 hours) or potash (24 hours) or 500 pounds compressive strength, whichever is greater, prior to initiating the test (see casing segment as lead cement may be critical item).

- d. The test shall be run on a 5000 psi chart for a 2-3M BOP/BOP, on a 10000 psi chart for a 5M BOP/BOPE and on a 15000 psi chart for a 10M BOP/BOPE. If a linear chart is used, it shall be a one hour chart. A circular chart shall have a maximum 2 hour clock. If a twelve hour or twenty-four hour chart is used, tester shall make a notation that it is run with a two hour clock.
- e. The results of the test shall be reported to the appropriate BLM office.
- f. All tests are required to be recorded on a calibrated test chart. A copy of the BOP/BOPE test chart and a copy of independent service company test will be submitted to the appropriate BLM office.
- g. The BOP/BOPE test shall include a low pressure test from 250 to 300 psi. The test will be held for a minimum of 10 minutes if test is done with a test plug and 30 minutes without a test plug. This test shall be performed prior to the test at full stack pressure.
- h. BOP/BOPE must be tested by an independent service company within 500 feet of the top of the Wolfcamp formation if the time between the setting of the intermediate casing and reaching this depth exceeds 20 days. This test does not exclude the test prior to drilling out the casing shoe as per 43 CFR part 3170 Subpart 3172.

C. DRILLING MUD

Mud system monitoring equipment, with derrick floor indicators and visual and audio alarms, shall be operating before drilling into the Wolfcamp formation, and shall be used until production casing is run and cemented.

D. WASTE MATERIAL AND FLUIDS

All waste (i.e. drilling fluids, trash, salts, chemicals, sewage, gray water, etc.) created as a result of drilling operations and completion operations shall be safely contained and disposed of properly at a waste disposal facility. No waste material or fluid shall be disposed of on the well location or surrounding area.

Porto-johns and trash containers will be on-location during fracturing operations or any other crew-intensive operations.

<u>District I</u> 1625 N. French Dr., Hobbs, NM 88240 Phone: (575) 393-6161 Fax: (575) 393-0720 District II 811 S. First St., Artesia, NM 88210 Phone: (575) 748-1283 Fax: (575) 748-9720

District III 1000 Rio B razos Road, Aztec, NM 87410 Phone: (505) 334-6178 Fax: (505) 334-6170

District IV 1220 S. St. Francis Dr., Santa Fe, NM 87505 Phone: (505) 476-3460 Fax: (505) 476-3462

C-102.dwg

111H\DWG\SAWTOOTH 111H

1

EDDY\Wells\-02

1

_

 $\overline{\Box}$

Unit\.06

Ranch

James

NM\002

ı

Energy

X TO

State of New Mexico Energy, Minerals & Natural Resources Department OIL CONSERVATION DIVISION 1220 South St. Francis Dr. Santa Fe, NM 87505

Form C-102 Revised August 1, 2011 Submit one copy to appropriate District Office

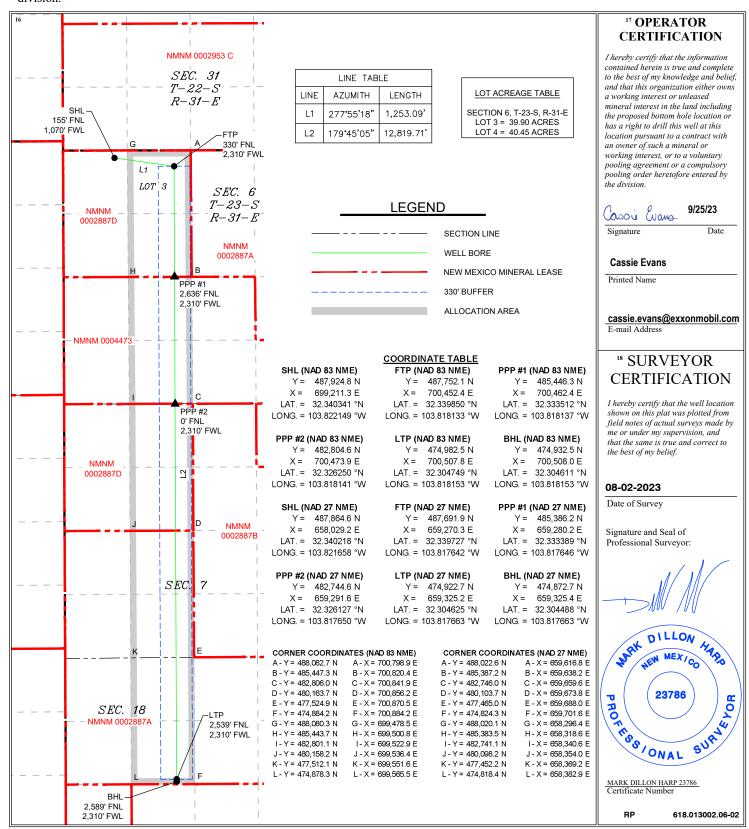
☐ AMENDED REPORT

WELL LOCATION AND ACREAGE DEDICATION PLAT

¹ API Number	r	² Pool Code	³ Pool Name	
30-015-		96336	LOS MEDANOS (WOLFCAMP) SOUTH	
⁴ Property Code	,	⁵ Property Name		⁶ Well Number
333473		JAMES RANCH UNIT DI 7 SAWTOOTH		111H
⁷ OGRID No.		⁸ Operator Name		⁹ Elevation
373075		XTO PERMIAN OPERATING, LLC		3,315'

¹⁰ Surface Location UL or lot no. Section Township Range North/South line Feet from the East/West line Feet from the 23 S 31 E **NORTH** 1,070 **WEST EDDY** 4 6 "Bottom Hole Location If Different From Surface UL or lot no. Section East/West line Feet from the County Township Range Lot Idn Feet from the North/South line 18 23 S 31 E 2,589 **NORTH** 2,310 WEST **EDDY** 12 Dedicated Acres ³ Joint or Infill ¹⁵Order No. 14 Consolidation Code 399.9

No allowable will be assigned to this completion until all interests have been consolidated or a non-standard unit has been approved by the division.



(618.013 Released to Imaging: 11/22/2023 10:42:22 AM

Instructions:

Released to Imaging: 11/22/2023 10:42:22 AM

- 1) Enter all data into table below using the plat, geoprog, and directional plan
- 2) Enter GeoProg data directly into permit -- surface and intermediate casing/cement calculations are based on salt top & bot
- 3) If there is not a 3rd bone or Wolfcamp X/Y then hide the row from columns A M
- 4) Enter Casing Specs on "Casing Design Page" for Burst, Collapse, and Tension

Field Needs an Input Calculated Field Pull Down Menu

Input Data				
Well Name	JRU DI 7 Sawtooth 111H			
Well Formation and Lateral	Wolfcamp Y 2.5 Mile			
Date Created	9/25/2023			
	SHL Data	BHL Da		
Section	6	18		
Т	23	S	23	
R	31	Е	31	
Northing	155	N	2589	
Easting	1070 W 2310			
County	Eddy			

Formations		
<u>Formation</u>	Well Depth (TVD)	Water/Oil/Gas
Rustler	230'	Water
Top of Salt	577'	Water
Base of Salt	3684'	Water
Delaware	3917'	Water
Brushy Canyon	6452'	Water/Oil/Gas
Bone Spring	7745'	Water
1st Bone Spring Ss	8787'	Water/Oil/Gas
2nd Bone Spring Ss	9625'	Water/Oil/Gas
3rd Bone Spring Sh	10187'	Water/Oil/Gas
3rd Bone Spring Ss	10620'	Water/Oil/Gas
Wolfcamp	11047'	Water/Oil/Gas
Wolfcamp X	11062'	Water/Oil/Gas
Wolfcamp Y	11128'	Water/Oil/Gas
Target/Land Curve	11182'	Water/Oil/Gas
BHL	11297'	Water/Oil/Gas

Match Directional Plan wh

le Sizes Hole Section	Hole Size		
Surface	17.5		
Intermediate 1	12.25		
Intermediate 2	8.75		
Production Curve	6.75		
Production Lateral	6.75		
i Toddollott Editoral	3.70		
d Weights		1	
rface	8.5		
ermediate 1	10		
ermediate 2	8.6		
oduction	10		
sing Points			
rface	552'	25' above Top Salt	
ermediate 1	3784'	100' below Base of	
ermediate 2	9860'	~200' above KOP,	but ensure casing is set in
Tool &/or Int 2 XO	3884'	100' below previous casing shoe (if need	
oduction	23857'	Equals BHL	
sing			
Hole Section	Name	Size	Weight
Surface	13.375 54.5 J-55 BTC	13.375 54.5	
Ouridoo	10.070 04.0 0-00 010		
Intermediate 1	9.625 40 J-55 BTC	9.625	40
		9.625	40 29.7
Intermediate 1	9.625 40 J-55 BTC	9.625	
Intermediate 1 Intermediate 2	9.625 40 J-55 BTC 7.625 29.7 RY P-110 Flush Joint 7.625 29.7 HC L-80 Flush Joint 5.5 23 RY P-110 Semi-Premium	9.625 7.625	29.7
Intermediate 1 Intermediate 2 Intermediate 2	9.625 40 J-55 BTC 7.625 29.7 RY P-110 Flush Joint 7.625 29.7 HC L-80 Flush Joint 5.5 23 RY P-110 Semi-Premium 5.5 23 RY P-110 Semi-Flush	9.625 7.625 7.625	29.7 29.7 23 23
Intermediate 1 Intermediate 2 Intermediate 2 Production	9.625 40 J-55 BTC 7.625 29.7 RY P-110 Flush Joint 7.625 29.7 HC L-80 Flush Joint 5.5 23 RY P-110 Semi-Premium	9.625 7.625 7.625 5.5	29.7 29.7 23
Intermediate 1 Intermediate 2 Intermediate 2 Production Production	9.625 40 J-55 BTC 7.625 29.7 RY P-110 Flush Joint 7.625 29.7 HC L-80 Flush Joint 5.5 23 RY P-110 Semi-Premium 5.5 23 RY P-110 Semi-Flush	9.625 7.625 7.625 5.5 5.5	29.7 29.7 23 23
Intermediate 1 Intermediate 2 Intermediate 2 Production Production	9.625 40 J-55 BTC 7.625 29.7 RY P-110 Flush Joint 7.625 29.7 HC L-80 Flush Joint 5.5 23 RY P-110 Semi-Premium 5.5 23 RY P-110 Semi-Flush	9.625 7.625 7.625 5.5 5.5	29.7 29.7 23 23
Intermediate 1 Intermediate 2 Intermediate 2 Production Production Production	9.625 40 J-55 BTC 7.625 29.7 RY P-110 Flush Joint 7.625 29.7 HC L-80 Flush Joint 5.5 23 RY P-110 Semi-Premium 5.5 23 RY P-110 Semi-Flush	9.625 7.625 7.625 5.5 5.5	29.7 29.7 23 23
Intermediate 1 Intermediate 2 Intermediate 2 Production Production Production	9.625 40 J-55 BTC 7.625 29.7 RY P-110 Flush Joint 7.625 29.7 HC L-80 Flush Joint 5.5 23 RY P-110 Semi-Premium 5.5 23 RY P-110 Semi-Flush 5.5 23 RY P-110 Semi-Flush	9.625 7.625 7.625 5.5 5.5 5.5	29.7 29.7 23 23
Intermediate 1 Intermediate 2 Intermediate 2 Production Production Production Production	9.625 40 J-55 BTC 7.625 29.7 RY P-110 Flush Joint 7.625 29.7 HC L-80 Flush Joint 5.5 23 RY P-110 Semi-Premium 5.5 23 RY P-110 Semi-Flush 5.5 23 RY P-110 Semi-Flush MD 10,629 11,754	9.625 7.625 7.625 5.5 5.5 5.5 TVD 10,466 11,182	29.7 29.7 23 23
Intermediate 1 Intermediate 2 Intermediate 2 Production Production Production	9.625 40 J-55 BTC 7.625 29.7 RY P-110 Flush Joint 7.625 29.7 HC L-80 Flush Joint 5.5 23 RY P-110 Semi-Premium 5.5 23 RY P-110 Semi-Flush 5.5 23 RY P-110 Semi-Flush MD 10,629	9.625 7.625 7.625 5.5 5.5 5.5 TVD	29.7 29.7 23 23
Intermediate 1 Intermediate 2 Intermediate 2 Production Production Production Production	9.625 40 J-55 BTC 7.625 29.7 RY P-110 Flush Joint 7.625 29.7 HC L-80 Flush Joint 5.5 23 RY P-110 Semi-Premium 5.5 23 RY P-110 Semi-Flush 5.5 23 RY P-110 Semi-Flush MD 10,629 11,754	9.625 7.625 7.625 5.5 5.5 5.5 TVD 10,466 11,182	29.7 29.7 23 23
Intermediate 1 Intermediate 2 Intermediate 2 Production Production Production Production	9.625 40 J-55 BTC 7.625 29.7 RY P-110 Flush Joint 7.625 29.7 HC L-80 Flush Joint 5.5 23 RY P-110 Semi-Premium 5.5 23 RY P-110 Semi-Flush 5.5 23 RY P-110 Semi-Flush MD 10,629 11,754	9.625 7.625 7.625 5.5 5.5 5.5 TVD 10,466 11,182	29.7 29.7 23 23
Intermediate 1 Intermediate 2 Intermediate 2 Production Production Production Production	9.625 40 J-55 BTC 7.625 29.7 RY P-110 Flush Joint 7.625 29.7 HC L-80 Flush Joint 5.5 23 RY P-110 Semi-Premium 5.5 23 RY P-110 Semi-Flush 5.5 23 RY P-110 Semi-Flush MD 10,629 11,754	9.625 7.625 7.625 5.5 5.5 5.5 TVD 10,466 11,182	

Released to Imaging: 11/22/2023 10:42:22 AM

Received by OCD: 10/31/2023 1:36:22 PM

Max Frac Pressure					
12000	psi				
Temps					
Surf Temp	ВНТ				
85	185				

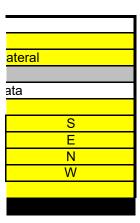
** Calculated off LP TVD

		Cas	ing Table
Name	OD	Weight	Grade
20 169 K-55 BTC	20	169	K-55
18.625 87.5 J-55 BTC	18 5/8	87.5	J-55
13.375 68 HC L-80 BTC	13 3/8	68	HC L-80
13.375 54.5 J-55 BTC	13 3/8	54.5	J-55
9.625 40 J-55 BTC	9 5/8	40	J-55
9.625 40 HC L-80 BTC	9 5/8	40	HC L-80
9.625 53.5 HC P-110 BTC	9 5/8	53.5	HC P-110
9.625 40 HC P-110 BTC	9 5/8	40	HC P-110
7.625 29.7 RY P-110 Flush Joint	7 5/8	29.7	RY P-110
7.625 29.7 CY P-110 Flush Joint	7 5/8	29.7	CY P-110
7.625 29.7 HC L-80 Flush Joint	7 5/8	29.7	HC L-80
6 26 P-110 Semi-Flush	6	26	P-110
5.5 23 RY P-110 Semi-Flush	5 1/2	23	RY P-110
5.5 23 RY P-110 Semi-Premium	5 1/2	23	RY P-110
5.5 20 RY P-110 Semi-Flush	5 1/2	20	RY P-110
5.5 20 RY P-110 Semi-Premium	5 1/2	20	RY P-110

Open hole logging will not be done on this we

tom.

Released to Imaging: 11/22/2023 10:42:22 AM



en appropriate

.

competent rock per geo

Well Plan LP 11,182
Geoprog LP 11,182
Well Plan KOP 10,629
New KOP 10,629

Collar
BTC
BTC
Flush Joint
Flush Joint
Semi-Premium
Semi-Flush
Semi-Flush

Check Hole sizes on Cement Calcs

Connection	Tube ID	Collapse	Burst	Tension	
BTC	18.376	2,500	3,380	2,689,000	K-55
BTC	17.755	630	2,250	1,329,000	J-55
BTC	12.415	2,690	5,020	1,545,000	HCL-80
BTC	12.615	1,130	2,740	909,000	J-55
BTC	8.835	2,750	3,950	630,000	J-55
BTC	8.835	4,230	5,750	916,000	HCL-80
BTC	8.835	9,190	10,900	1,718,000	P110 HC
BTC	8.535	4,230	7,910	1,266,000	P110 HC
Flush Joint	6.875	5,350	9,460	558,000	P110 RY -IFJ
Flush Joint	6.875	5,350	9,460	960,000	P110 CY - IFJ
Flush Joint	6.875	5,780	6,880	406,000	HCL-80 - IFJ
Semi-Flush	5.128	13,570	14,010	838,000	P-110 - Talon HTQ
Semi-Flush	4.67	14,540	14,530	707,000	P110 RY - Talon HTQ
Semi-Premium	4.67	14,540	14,520	729,000	P110 RY - Freedom HT0
Semi-Flush	4.778	11,100	12,640	641,000	P110 RY - Talon HTQ
Semi-Premium	4.778	11,100	12,640	641,000	P110 RY - Freedom HT0

Released to Imaging: 11/22/2023 10:42:22 AM

DRILLING PLAN: BLM COMPLIANCE (Supplement to BLM 3160-3)

XTO Energy Inc. JRU DI 7 Sawtooth 111H Projected TD: 23856.6' MD / 11182' TVD SHL: 155' FNL & 1070' FWL, Section 6, T23S, R31E BHL: 2589' FNL & 2310' FWL, Section 18, T23S, R31E Eddy County, NM

1. Geologic Name of Surface Formation

Quaternary

2. Estimated Tops of Geological Markers & Depths of Anticipated Fresh Water, Oil or Gas

Formation	Well Depth (TVD)	Water/Oil/Gas
Rustler	230'	Water
Top of Salt	577'	Water
Base of Salt	3684'	Water
Delaware	3917'	Water
Brushy Canyon	6452'	Water/Oil/Gas
Bone Spring	7745'	Water
1st Bone Spring Ss	8787'	Water/Oil/Gas
2nd Bone Spring Ss	9625'	Water/Oil/Gas
3rd Bone Spring Sh	10187'	Water/Oil/Gas
Wolfcamp	11047'	Water/Oil/Gas
Wolfcamp X	11062'	Water/Oil/Gas
Wolfcamp Y	11128'	Water/Oil/Gas
Target/Land Curve	11182'	Water/Oil/Gas

Rows hidde

No other formations are expected to yield oil, gas or fresh water in measurable volumes. The surface fresh water sands will be protected by setting 13.375 inch casing @ 552' (25' above the salt) and circulating cement back to surface. The salt will be isolated by setting 9.625 inch casing at 3784' and circulating cement to surface. The second intermediate will isolate from the salt down to the next casing seat by setting 7.625 inch casing at 9860' and cementing to surface. A 6.75 inch curve and 6.75 inch lateral hole will be drilled to 23856.6 MD/TD and 5.5 inch production casing will be set at TD and cemented back up to 2nd intermediate (estimated TOC 9360 feet) per Potash regulations.

3. Casing Design

Hole Size	MD	TVD	OD Csg	Weight	Grade	Collar	New/Used	SF Burst	SF Collapse	SF Tension
17.5	0' – 552'	571'	13.375	54.5	J-55	ВТС	New	2.41	4.63	30.22
12.25	0' – 3784'	3688'	9.625	40	J-55	BTC	New	1.76	2.39	4.16
8.75	0' – 3884'	3788'	7.625	29.7	RY P-110	Flush Joint	New	2.82	3.08	1.91
8.75	3884' – 9860'	9502'	7.625	29.7	HC L-80	Flush Joint	New	2.05	3.68	2.29
6.75	0' – 9760'	9409'	5.5	23	RY P-110	Semi-Premium	New	1.21	2.86	1.98
6.75	9760' - 23856.6'	10451'	5.5	23	RY P-110	Semi-Flush	New	1.21	2.50	4.93

- · Production casing meets the clearance requiremenets as tapered string crosses over before encountering the intermediate shoe, per Onshore Order 2.3.B.1
- XTO requests the option to utilize a spudder rig (Atlas Copco RD20 or Equivalent) to set and cement surface and intermediate 1 casing per this Sundry
- · XTO requests to not utilize centralizers in the curve and lateral
- · 9.625 Collapse analyzed using 50% evacuation based on regional experience.
- · 7.625 Collapse analyzed using 50% evacuation based on regional experience.
- $\cdot\,5.5\,\text{Tension calculated using vertical hanging weight plus the lateral weight multiplied by a friction factor of 0.35$
- · Test on 2M annular & Casing will be limited to 70% burst of the casing or 1500 psi, whichever is less
- \cdot XTO requests the option to use 5" BTC Float equipment for the the production casing

Wellhead:

<u>Permanent Wellhead – Multibowl System</u>
A. Starting Head: 13-5/8" 10M top flange x 13-3/8" bottom

- B. Tubing Head: 13-5/8" 10M bottom flange x 7-1/16" 15M top flange
 - Wellhead will be installed by manufacturer's representatives.
 - · Manufacturer will monitor welding process to ensure appropriate temperature of seal.
 - · Operator will test the 7-5/8" casing per BLM Onshore Order 2
 - · Wellhead Manufacturer representative will not be present for BOP test plug installation

Check casing size her

^{***} Hydrocarbons @ Brushy Canyon

^{***} Groundwater depth 40' (per NM State Engineers Office).

4. Cement Program

Surface Casing: 13.375, 54.5 New BTC, J-55 casing to be set at +/- 552

Lead: 180 sxs EconoCem-HLTRRC (mixed at 12.9 ppg, 1.87 ft3/sx, 10.13 gal/sx water) Tail: 300 sxs Class C + 2% CaCl (mixed at 14.8 ppg, 1.35 ft3/sx, 6.39 gal/sx water) Top of Cement: Surface

12-hr = 250 psi 24 hr = 500 psiCompressives:

Due to the high probability of not getting cement to surface during conventional top-out jobs in the area, ~10-20 ppb gravel will be added on the backside of the 1" to get cement to surface, if required.

1st Intermediate Casing: 9.625, 40 New BTC, J-55 casing to be set at +/- 3784

Lead: 1570 sxs Class C (mixed at 12.9 ppg, 1.39 ft3/sx, 10.13 gal/sx water) Tail: 130 sxs Class C + 2% CaCl (mixed at 14.8 ppg, 1.35 ft3/sx, 6.39 gal/sx water)

Top of Cement: Surface

12-hr = 900 psi 24 hr = 1500 psi Compressives:

2nd Intermediate Casing: 7.625, 29.7 New casing to be set at +/- 9860

Optional Lead: 150 sxs Class C (mixed at 10.5 ppg, 2.77 ft3/sx, 15.59 gal/sx water

Tail: 310 sxs Class C (mixed at 14.8 ppg, 1.35 ft3/sx, 6.39 gal/sx water)

TOC: Brushy Canyon @ 6452

24 hr = 1150 psi Compressives: 12-hr = 900 psi

2nd Stage

Lead: 0 sxs Class C (mixed at 12.9 ppg, 2.16 ft3/sx, 9.61 gal/sx water) Tail: 400 sxs Class C (mixed at 14.8 ppg, 1.33 ft3/sx, 6.39 gal/sx water)

Top of Cement: 0

12-hr = 24 hr = 1150 psi Compressives: 900 psi

XTO requests to pump a two stage cement job on the 7-5/8" intermediate casing string with the first stage being pumped conventionally with the calculated top of cement at the Brush Canyon (6452') and the second stage performed as a bradenhead squeeze with planned cement from the Brushy Canyon to surface. If cement is not visually confirmed to circulate to surface, the final cement top after the second stage job will be verified by Echo-meter. If necessary, a top out consisting of 1,500 sack of Class C cement + 3% Salt + 1% PreMag-M + 6% Bentonite Gel (2.30 yld, 12.91 ppg) will be executed as a contingency. If cement is still unable to circulate to surface, another Echo-meter run will be performed for cement top

XTO will include the Echo-meter verified fluid top and the volume of displacement fluid above the cement slurry in the annulus in all post-drill sundries on wells utilizing this cement program.

XTO will report to the BLM the volume of fluid (limited to 5 bbls) used to flush intermediate casing valves following backside

XTO requests to pump an Optional Lead if well conditions dictate in an attempt to bring cement to surface. If cement reaches the desired height, the BLM will be notified and the second stage bradenhead squeeze and subsequent TOC verification will be negated.

XTO requests the option to conduct the bradenhead squeeze and TOC verification offline as per standard approval from BLM when unplanned remediation is needed and batch drilling is approved. In the event the bradenhead is conducted, we will ensure the first stage cement job is cemented properly and the well is static with floats holding and no pressure on the csg annulus as with all other casing strings where batch drilling operations occur before moving off the rig. The TA cap will also be installed per Cactus procedure and pressure inside the casing will be monitored via the valve on the TA cap as per standard batch drilling ops.

Production Casing: 5.5, 23 New Semi-Flush, RY P-110 casing to be set at +/- 23856.6

Lead: 50 sxs NeoCem (mixed at 11.5 ppg, 2.69 ft3/sx, 15.00 gal/sx water) Top of Cement: Tail: 950 sxs VersaCem (mixed at 13.2 ppg, 1.51 ft3/sx, 8.38 gal/sx water) Top of Cement: 10628.5 feet 12-hr = 1375 psi 24 hr = 2285 psi Compressives:

XTO requests the option to offline cement and remediate (if needed) surface and intermediate casing strings where batch drilling is approved and if unplanned remediation is needed. XTO will ensure well is static with no pressure on the csg annulus, as with all other casing strings where batch drilling operations occur before moving off the rig. The TA cap will also be installed when applicable per Cactus procedure and pressure inside the casing will be monitored via the valve on the TA cap as per standard batch drilling ops. Offline cement operations will then be conducted after the rig is moved off the current well to the next well in the batch sequence.

DV Tool can be hidder

Bradenhead squeeze

5. Pressure Control Equipment

Once the permanent WH is installed on the 13.375 casing, the blow out preventer equipment (BOP) will consist of a 13-5/8" minimum 5M Hydril and a 13-5/8" minimum 5M Double Ram BOP. MASP should not exceed 3355 psi. In any instance where 10M BOP is required by BLM, XTO requests a variance to utilize 5M annular with 10M ram preventers (a common BOP configuration, which allows use of 10M rams in unlikely event that pressures exceed 5M).

Check casing sizes he

Temporary wellhead/d

All BOP testing will be done by an independent service company. Annular pressure tests will be limited to 50% of the working pressure. When nippling up on the 13.375, 5M bradenhead and flange, the BOP test will be limited to 5000 psi. When nippling up on the 7.625, the BOP will be tested to a minimum of 5000 psi. All BOP tests will include a low pressure test as per BLM regulations. The 5M BOP diagrams are attached. Blind rams will be functioned tested each trip, pipe rams will be functioned tested each day.

A variance is requested to allow use of a flex hose as the choke line from the BOP to the Choke Manifold. If this hose is used, a copy of the manufacturer's certification and pressure test chart will be kept on the rig. Attached is an example of a certification and pressure test chart. The manufacturer does not require anchors.

XTO requests a variance to be able to batch drill this well if necessary. In doing so, XTO will set casing and ensure that the well is cemented properly (unless approval is given for offline cementing) and the well is static. With floats holding, no pressure on the csg annulus, and the installation of a 10K TA cap as per Cactus recommendations, XTO will contact the BLM to skid the rig to drill the remaining wells on the pad. Once surface and both intermediate strings are all completed, XTO will begin drilling the production hole on each of the wells.

A variance is requested to **ONLY** test broken pressure seals on the BOP equipment when moving from wellhead to wellhead which is in compliance with API Standard 53. API standard 53 states, that for pad drilling operation, moving from one wellhead to another within 21 days, pressure testing is required for pressure-containing and pressure-controlling connections when the integrity of a pressure seal is broken. Based on discussions with the BLM on February 27th 2020, we will request permission to **ONLY** retest broken pressure seals if the following conditions are met: 1. After a full BOP test is conducted on the first well on the pad 2. When skidding to drill an intermediate section that does not penetrate into the Wolfcamp.

6. Proposed Mud Circulation System

			MW	Viscosity	Fluid Loss
INTERVAL	Hole Size	Mud Type	(ppg)	(sec/qt)	(cc)
0' - 552'	17.5	FW/Native	8.5-9	35-40	NC
552' - 3784'	12.25	Brine	10-10.5	30-32	NC
3784' to 9860'	8.75	BDE/OBM or FW/Brine	8.6-9.1	30-32	NC
9860' to 23856.6'	6.75	ОВМ	10-10.5	50-60	NC - 20

The necessary mud products for weight addition and fluid loss control will be on location at all times

Spud with fresh water/native mud. Drill out from under 13-3/8" surface casing with brine solution. A 10.0 ppg -10.5 ppg brine mud will be used while drilling through the salt formation. Use fibrous materials as needed to control seepage and lost circulation. Pump viscous sweeps as needed for hole cleaning. Pump speed will be recorded on a daily drilling report after mudding up. A Pason or Totco will be used to detect changes in loss or gain of mud volume. A mud test will be performed every 24 hours to determine: density, viscosity, strength, filtration and pH as necessary. Use available solids controls equipment to help keep mud weight down after mud up. Rig up solids control equipment to operate as a closed loop system.

7. Auxiliary Well Control and Monitoring Equipment

- A. A Kelly cock will be in the drill string at all times.
- B. A full opening drill pipe stabbing valve having appropriate connections will be on the rig floor at all times.
- C. H2S monitors will be on location when drilling below the 13.375 casing.

8. Logging, Coring and Testing Program

Mud Logger: Mud Logging Unit (2 man) below intermediate casing.

Open hole logging will not be done on this well.

9. Abnormal Pressures and Temperatures / Potential Hazards

None Anticipated. BHT of 175 to 195 F is anticipated. No H2S is expected but monitors will be in place to detect any H2S occurrences. Should these circumstances be encountered the operator and drilling contractor are prepared to take all necessary steps to ensure safety of all personnel and environment. Lost circulation could occur but is not expected to be a serious problem in this area and hole seepage will be compensated for by additions of small amounts of LCM in the drilling fluid. The maximum anticipated bottom hole pressure for this well is 5815 psi.

10. Anticipated Starting Date and Duration of Operations

Anticipated spud date will be after BLM approval. Move in operations and drilling is expected to take 40 days.

Check properties

Double che

Collapse Assumes 1/2 evacuation & FW internal Fluid Top: 1892 MD/TVD

Burst Assumes MASP Equation (8.6)(0.052)(9860) - (.22)(9860)

Collapse Assumes full evacuation

Burst Assumes MASP Equation (10)(0.052)(11182) - (.22)(11182)

Collapse Assumes 1/3 evacuation & FW internal Fluid Top: 6573 MD/TVD

Burst Assumes MASP Equation (10)(0.052)(11182) - (.22)(11182)

13.375 54.5 J-55 BTC	552 MD/TVD 8.5	ppg mud		
	collapse = 1130	Burst =	2740	Tension = 909000
<u>Collapse</u>				
8.5)(0.052)(552) =	244 psi	1130/244 =	4.63	SF for collapse
Burst				
Max exp. surf pressure	1135 psi	2740/1135.2 =	2.41	SF for burst
ension	·	•		_
552)(54.5)=	30084 lb	909/30.1 =	30.22	SF for tension

23,857 ft TD 9/25/2023

Released to Imaging: 11/22/2023 10:42:22 AM

JRU DI 7 Sawtooth 111H

9.625 40 J-55 BTC	3784 MD/TVD	10 # mud		
	Collapse = 2750	Burst =	3950	Tension = 630000
Collapse				
(10)(0.052)(3784) * =	1151 psi	2750/1151 =	2.39	SF for collapse
*Less internal fluid height				
<u>Burst</u>				
Max expected surf pressure =	2240 psi	3950/2240.192 =	1.76	SF for burst
<u>Tension</u>				
(3784)(40)=	151360 lb	630/151.36 =	4.16	SF for tension

7.625 29.7 RY P-110 Flush Joint	0 Top MD/TVD	8.6 # mud	
	3884 Bottom MD/TVD		
	Collapse = 5350	Burst = 9460	Tension = 558000
<u>Collapse</u>			
(8.6)(0.052)(3884)=	1737 psi	5350/1737= 3.08	SF for collapse
Burst			
Max expected surf pressure =	3355 psi	9460/3354.6= 2.82	SF for burst
<u>Tension</u>			
(3884*29.7)+(5976*29.7)=	292842 lb	558/292.842= 1.91	SF for tension

7.625 29.7 HC L-80 Flush Joint	3884 Top MD/TVD			8.6 # mud
	9860 TD MD/TVD			
	Collapse = 5780	Burst =	6880	Tension = 406000
Collapse				
(8.6)(0.052)(9860) * =	1572 psi	5780/1572=	3.68	SF for collapse
*Less internal fluid height				
<u>Burst</u>	_			
Max expected surf pressure =	3355 psi	6880/3354.6=	2.05	SF for burst
Tension				
(5976)(29.7)=	177487.2 lb	406/177.4872=	2.29	SF for tension
				_

5.5 23 RY P-110 Semi-Premium	0 Top	9,760	TD (MD)		10 #	# mud
	0.35 FF					
	Collapse =	14540	Burst=	14520	Tension=	729000
<u>Collapse</u>			-			
(10)(0.052)(9760) =	5075	psi	14540/5075=	2.86	SF for collapse	
Burst						
Max expected surf pressure =	12000	psi *for frac	14520/12000=	1.21	SF for burst	
Tension						
#REF!	367760	lb	729/367.760455=	1.98	SF for tension	
5.5 23 RY P-110 Semi-Flush	9,760 Top	23,857	TD (MD)	11,182	TVD (max)	10 # mud
5.5 23 RY P-110 Semi-Flush	9,760 Top 0.35 FF		TD (MD) LP (MD)		TVD (max) Lat Length	10 # mud
5.5 23 RY P-110 Semi-Flush	0.35 FF	11,754	LP (MD)	12103.1	Lat Length	
		11,754				10 # mud
<u>Collapse</u>	0.35 FF Collapse=	11,754 14540	LP (MD) Burst=	12103.1 14530	Lat Length Tension=	707000
Collapse 10)(0.052)(11182) =	0.35 FF	11,754 14540	LP (MD)	12103.1	Lat Length	707000
Collapse 10)(0.052)(11182) = Burst	0.35 FF Collapse=	11,754 14540 psi	LP (MD) Burst= 14540/5815=	12103.1 14530 2.50	Lat Length Tension= SF for collapse	707000
5.5 23 RY P-110 Semi-Flush Collapse 10)(0.052)(11182) = Burst Max expected surf pressure = Tension	0.35 FF Collapse=	11,754 14540	LP (MD) Burst=	12103.1 14530	Lat Length Tension=	707000

Surface Cement		1st Intermediate	
Top of Cement: Casing Shoe:	0 ft, MD 552 ft, MD	Top of Cement: Casing Shoe:	0 3784
Hole Size: Casing Size:	17.5 in 13.375 in	Hole Size: Casing Size:	12.25 9.625
<u>Lead</u> % Excess, OH yield TOC for Lead	100 % 1.87 ft ³ / sack 0 ft, MD	<u>Lead</u> % Excess, OH yield TOC for Lead	100 1.39 0
<u>Tail</u> % Excess, OH yield TOC for Tail	100 % 1.35 ft ³ / sack 252 ft, MD	<u>Tail</u> % Excess, OH yield TOC for Tail	100 1.35 3,484
<u>Lead Calcs</u>		<u>Lead Calcs</u>	
Annular Volume: Cement Volume:	350.12 ft ³ (w/ excess) 187.2 sacks	Annular Volume: Cement Volume:	2182.42 1570.1
<u>Tail Calcs</u>		<u>Tail Calcs</u>	
Annular Volume: Cement Volume:	416.81 ft ³ (w/ excess) 308.7 sacks	Annular Volume: Cement Volume:	187.92 139.2

Field Needs an Input Calculated Field

	2nd Intermediate, 2nd Stage	1	2nd Intermediate,
ft, MD ft, MD	Top of Cement: Bottom of Cement:	0 ft, MD 3,584 ft, MD	Top of Cerr Casing Sho
in in	Hole Size: Casing Size:	8.75 in 7.625 in	Hole Size: Casing Siz∉
% ft³ / sack ft, MD	<u>Lead</u> % Excess, OH yield TOC for Lead	100 % 2.16 ft ³ / sack 0 ft, MD	<u>Lead</u> % Excess, yield TOC for Le
% ft ³ / sack ft, MD	<u>Tail</u> % Excess, OH yield TOC for Tail	50 % 1.33 ft ³ / sack 0 ft, MD	<u>Tail</u> % Excess, yield TOC for Ta
	<u>Lead Calcs</u>		<u>Lead Calcs</u>
ft ³ (w/ excess) sacks	Annular Volume: Cement Volume:	0.00 ft ³ (w/ excess) 0.0 sacks	Annular Vo Cement Vo
	<u>Tail Calcs</u>		<u>Tail Calcs</u>
ft ³ (w/ excess) sacks	Annular Volume: Cement Volume:	540.19 ft ³ (w/ excess) 406.2 sacks	Annular Vo Cement Vo

1st Stage		Production Cement	
nent: pe:	3584 ft, MD 9860 ft, MD 8.75 in 7.625 in	Top of Cement: Casing Shoe: Kick Off Point: Landing Point: Hole Size 1: Hole Size 2: Casing Size 1: Casing Size 2: XO Depth:	9360 ft, MD 23,857 ft, MD 10,629 ft, MD 11,754 ft, MD 6.75 in 6.75 in 5.5 in 5.5 in 0 ft, MD
OH ad	50 % 2.77 ft ³ / sack 3,584 ft, MD	<u>Lead</u> % Excess, OH yield TOC for Lead	30 % 2.69 ft ³ / sack 9,360 ft, MD
OH il	25 % 1.35 ft ³ / sack 6,452 ft, MD	<u>Tail</u> % Excess, OH yield TOC for Tail	30 % 1.51 ft ³ / sack 10,629 ft, MD
lume:	432.27 ft ³ (w/ excess) 156.1 sacks	<u>Lead Calcs</u> Annular Volume: Cement Volume: <u>Tail Calcs</u>	137.73 ft ³ (w/ excess) 51.2 sacks
lume:	428.05 ft ³ (w/ excess) 317.1 sacks	Annular Volume: Cement Volume:	1436.28 ft ³ (w/ excess) 951.2 sacks

= Calculate

Field Needs an Input Calculated Field

Permanent System

Prod MW = 10 ppg Max TVD = 11,182 ft

BHP = 5815 psi

MASP = 3355 psi

Permit for = 5M 5000 psi 3M system if MASP < 3000 5M system if 3000 < MASP < 5000 10M system if MASP > 5000

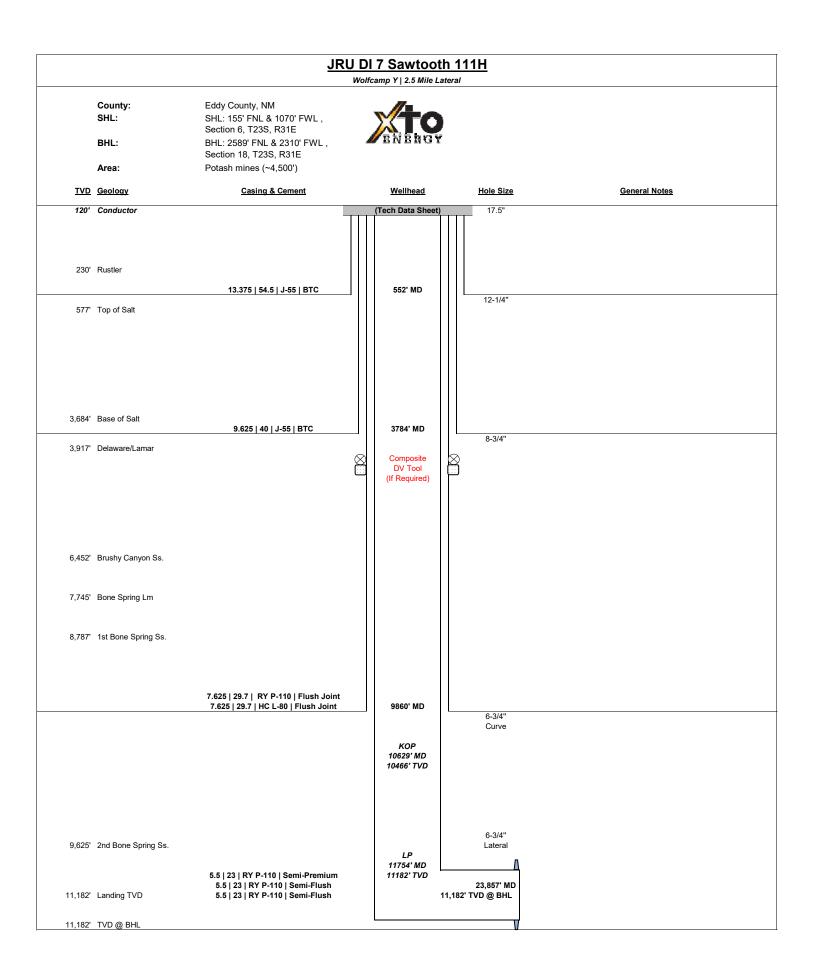
Temporary System (if required)

1st Int MW = 10 ppg Max TVD = 3784 ft

BHP = 1968 psi

MASP = 1135 psi

Permit for = 2M 2000 2M system if MASP < 3000 5M system if 2000 < MASP < 5000



Formations

1st Bone Spring
1st Bone Spring Sand
2nd Bone Spring Shale
2nd Bone Spring Shale
2nd Bone Spring Sand
3rd Bone Spring Shale
3rd Bone

Wolfcamp D/E

Wolfcamp D

Wolfcamp E

Lateral Length

- 1 Mile Lateral
- 1.5 Mile Lateral
- 2 Mile Lateral
- 2.25 Mile Lateral
- 2.5 Mile Lateral
- 3 Mile Lateral
- 3.5 Mile Lateral
- 4 Mile Lateral

- 1st Bone Spring
- 2nd Done Opinio
- 2nd Bone Spring
- 2nd Bone Spring 3rd Bone Spring
- 3rd Bone Spring
- ora pone opring
- 3rd Bone Spring 3rd Bone Spring
- 3rd Bone Spring
- 3rd Bone Spring
- Ord Done Opring
- 3rd Bone Spring
- 3rd Bone Spring Shale
- Wolfcamp X
- Wolfcamp Y
- Wolfcamp A

Wolfcamp A

Wolfcamp B

Wolfcamp D/E

1st Bone Spring Sand

2nd Bone Spring Shale

2nd Bone Spring Sand

2nd Bone Spring Sand 3rd Bone Spring Sand

3rd Bone Spring Sand

3rd Bone Spring Sand

3rd Bone Spring Sand

3rd Bone Spring Sand

3rd Bone Spring Sand

3rd Bone Spring Sand

Wolfcamp C

Wolfcamp B/C

Wolfcamp D

Wolfcamp E

Wolfcamp X/Y

1st Bone Spring

2nd Bone Spring

3rd Bone Spring

3rd Bone Spring Shale

Wolfcamp X

Wolfcamp Y

Wolfcamp A

Wolfcamp B

Wolfcamp D/E

1st Bone Spring Sand

2nd Bone Spring Shale

2nd Bone Spring Sand

3rd Bone Spring Sand

Wolfcamp C

Wolfcamp B/C

Wolfcamp D

Wolfcamp E

Wolfcamp X/Y

Target formation and Lateral Length:

Wolfcamp Y 2.5 Mile Lateral

Production 1

		1 Toddottori 1
1 Mile Lateral	1st Bone Spring 1 Mile Lateral	5.5 20 RY P-110 Semi-Premium
1.5 Mile Lateral	1st Bone Spring 1.5 Mile Lateral	5.5 20 RY P-110 Semi-Premium
2 Mile Lateral	1st Bone Spring 2 Mile Lateral	5.5 20 RY P-110 Semi-Premium
2.5 Mile Lateral	1st Bone Spring 2.5 Mile Lateral	5.5 23 RY P-110 Semi-Premium
3 Mile Lateral	1st Bone Spring 3 Mile Lateral	5.5 23 RY P-110 Semi-Premium
3.5 Mile Lateral	1st Bone Spring 3.5 Mile Lateral	6 26 P-110 Semi-Flush
4 Mile Lateral	1st Bone Spring 4 Mile Lateral	6 26 P-110 Semi-Flush
1 Mile Lateral	2nd Bone Spring 1 Mile Lateral	5.5 20 RY P-110 Semi-Premium
1.5 Mile Lateral	2nd Bone Spring 1.5 Mile Lateral	5.5 20 RY P-110 Semi-Premium
2 Mile Lateral	2nd Bone Spring 2 Mile Lateral	5.5 20 RY P-110 Semi-Premium
2.5 Mile Lateral	2nd Bone Spring 2.5 Mile Lateral	5.5 23 RY P-110 Semi-Premium
3 Mile Lateral	2nd Bone Spring 3 Mile Lateral	5.5 23 RY P-110 Semi-Premium
3.5 Mile Lateral	2nd Bone Spring 3.5 Mile Lateral	6 26 P-110 Semi-Flush
4 Mile Lateral	2nd Bone Spring 4 Mile Lateral	6 26 P-110 Semi-Flush
1 Mile Lateral	3rd Bone Spring 1 Mile Lateral	5.5 20 RY P-110 Semi-Premium
1.5 Mile Lateral	3rd Bone Spring 1.5 Mile Lateral	5.5 20 RY P-110 Semi-Premium
2 Mile Lateral	3rd Bone Spring 2 Mile Lateral	5.5 20 RY P-110 Semi-Premium
2.5 Mile Lateral	3rd Bone Spring 2.5 Mile Lateral	5.5 23 RY P-110 Semi-Premium
3 Mile Lateral	3rd Bone Spring 3 Mile Lateral	5.5 23 RY P-110 Semi-Premium
3.5 Mile Lateral	3rd Bone Spring 3.5 Mile Lateral	6 26 P-110 Semi-Flush
4 Mile Lateral	3rd Bone Spring 4 Mile Lateral	6 26 P-110 Semi-Flush
1 Mile Lateral	3rd Bone Spring Shale 1 Mile Lateral	5.5 20 RY P-110 Semi-Premium
1.5 Mile Lateral	3rd Bone Spring Shale 1.5 Mile Lateral	5.5 20 RY P-110 Semi-Premium
2 Mile Lateral	3rd Bone Spring Shale 2 Mile Lateral	5.5 20 RY P-110 Semi-Premium
2.5 Mile Lateral	3rd Bone Spring Shale 2.5 Mile Lateral	5.5 23 RY P-110 Semi-Premium
3 Mile Lateral	3rd Bone Spring Shale 3 Mile Lateral	5.5 23 RY P-110 Semi-Premium
3.5 Mile Lateral	3rd Bone Spring Shale 3.5 Mile Lateral	6 26 P-110 Semi-Flush
4 Mile Lateral	3rd Bone Spring Shale 4 Mile Lateral	6 26 P-110 Semi-Flush
1 Mile Lateral	Wolfcamp X 1 Mile Lateral	5.5 20 RY P-110 Semi-Premium
1.5 Mile Lateral	Wolfcamp X 1.5 Mile Lateral	5.5 20 RY P-110 Semi-Premium
2 Mile Lateral	Wolfcamp X 2 Mile Lateral	5.5 23 RY P-110 Semi-Premium
2.5 Mile Lateral	Wolfcamp X 2.5 Mile Lateral	5.5 23 RY P-110 Semi-Premium
3 Mile Lateral	Wolfcamp X 3 Mile Lateral	5.5 23 RY P-110 Semi-Premium
3.5 Mile Lateral	Wolfcamp X 3.5 Mile Lateral	6 26 P-110 Semi-Flush
4 Mile Lateral	Wolfcamp X 4 Mile Lateral	6 26 P-110 Semi-Flush
1 Mile Lateral	Wolfcamp Y 1 Mile Lateral	5.5 20 RY P-110 Semi-Premium
1.5 Mile Lateral	Wolfcamp Y 1.5 Mile Lateral	5.5 20 RY P-110 Semi-Premium
2 Mile Lateral	Wolfcamp Y 2 Mile Lateral	5.5 23 RY P-110 Semi-Premium
2.5 Mile Lateral	Wolfcamp Y 2.5 Mile Lateral	5.5 23 RY P-110 Semi-Premium
3 Mile Lateral	Wolfcamp Y 3 Mile Lateral	5.5 23 RY P-110 Semi-Premium
3.5 Mile Lateral	Wolfcamp Y 3.5 Mile Lateral	6 26 P-110 Semi-Flush
4 Mile Lateral	Wolfcamp Y 4 Mile Lateral	6 26 P-110 Semi-Flush
1 Mile Lateral	Wolfcamp A 1 Mile Lateral	5.5 20 RY P-110 Semi-Premium
1.5 Mile Lateral	Wolfcamp A 1.5 Mile Lateral	5.5 20 RY P-110 Semi-Premium
2 Mile Lateral	Wolfcamp A 2 Mile Lateral	5.5 23 RY P-110 Semi-Premium
2.5 Mile Lateral	Wolfcamp A 2.5 Mile Lateral	5.5 23 RY P-110 Semi-Premium
3 Mile Lateral	Wolfcamp A 3 Mile Lateral	5.5 23 RY P-110 Semi-Premium
3.5 Mile Lateral	Wolfcamp A 3.5 Mile Lateral	6 26 P-110 Semi-Flush
	-	•

4 Mile Lateral	Wolfcamp A 4 Mile Lateral	6 26 P-110 Semi-Flush
1 Mile Lateral	Wolfcamp B 1 Mile Lateral	5.5 20 RY P-110 Semi-Premium
1.5 Mile Lateral	Wolfcamp B 1.5 Mile Lateral	5.5 20 RY P-110 Semi-Premium
2 Mile Lateral	Wolfcamp B 2 Mile Lateral	5.5 23 RY P-110 Semi-Premium
2.5 Mile Lateral	Wolfcamp B 2.5 Mile Lateral	5.5 23 RY P-110 Semi-Premium
3 Mile Lateral	Wolfcamp B 3 Mile Lateral	5.5 23 RY P-110 Semi-Premium
3.5 Mile Lateral	Wolfcamp B 3.5 Mile Lateral	6 26 P-110 Semi-Flush
4 Mile Lateral	Wolfcamp B 4 Mile Lateral	6 26 P-110 Semi-Flush
1 Mile Lateral	Wolfcamp D/E 1 Mile Lateral	5.5 20 RY P-110 Semi-Premium
1.5 Mile Lateral	Wolfcamp D/E 1.5 Mile Lateral	5.5 20 RY P-110 Semi-Premium
2 Mile Lateral	Wolfcamp D/E 2 Mile Lateral	5.5 23 RY P-110 Semi-Premium
2.5 Mile Lateral	Wolfcamp D/E 2.5 Mile Lateral	5.5 23 RY P-110 Semi-Premium
3 Mile Lateral	Wolfcamp D/E 3 Mile Lateral	5.5 23 RY P-110 Semi-Premium
3.5 Mile Lateral	Wolfcamp D/E 3.5 Mile Lateral	6 26 P-110 Semi-Flush
4 Mile Lateral	Wolfcamp D/E 4 Mile Lateral	6 26 P-110 Semi-Flush
1 Mile Lateral	1st Bone Spring Sand 1 Mile Lateral	5.5 20 RY P-110 Semi-Premium
1.5 Mile Lateral	1st Bone Spring Sand 1.5 Mile Lateral	5.5 20 RY P-110 Semi-Premium
2 Mile Lateral	1st Bone Spring Sand 2 Mile Lateral	5.5 20 RY P-110 Semi-Premium
2.5 Mile Lateral	1st Bone Spring Sand 2.5 Mile Lateral	5.5 23 RY P-110 Semi-Premium
3 Mile Lateral	1st Bone Spring Sand 3 Mile Lateral	5.5 23 RY P-110 Semi-Premium
3.5 Mile Lateral	1st Bone Spring Sand 3.5 Mile Lateral	6 26 P-110 Semi-Flush
4 Mile Lateral	1st Bone Spring Sand 4 Mile Lateral	6 26 P-110 Semi-Flush
1 Mile Lateral	2nd Bone Spring Shale 1 Mile Lateral	5.5 20 RY P-110 Semi-Premium
1.5 Mile Lateral	2nd Bone Spring Shale 1.5 Mile Lateral	5.5 20 RY P-110 Semi-Premium
2 Mile Lateral	2nd Bone Spring Shale 2 Mile Lateral	5.5 20 RY P-110 Semi-Premium
2.5 Mile Lateral	2nd Bone Spring Shale 2.5 Mile Lateral	5.5 23 RY P-110 Semi-Premium
3 Mile Lateral	2nd Bone Spring Shale 3 Mile Lateral	5.5 23 RY P-110 Semi-Premium
3.5 Mile Lateral	2nd Bone Spring Shale 3.5 Mile Lateral	6 26 P-110 Semi-Flush
4 Mile Lateral	2nd Bone Spring Shale 4 Mile Lateral	6 26 P-110 Semi-Flush
1 Mile Lateral	2nd Bone Spring Sand 1 Mile Lateral	5.5 20 RY P-110 Semi-Premium
1.5 Mile Lateral	2nd Bone Spring Sand 1.5 Mile Lateral	5.5 20 RY P-110 Semi-Premium
2 Mile Lateral	2nd Bone Spring Sand 2 Mile Lateral	5.5 20 RY P-110 Semi-Premium
2.5 Mile Lateral	2nd Bone Spring Sand 2.5 Mile Lateral	5.5 23 RY P-110 Semi-Premium
3 Mile Lateral	2nd Bone Spring Sand 3 Mile Lateral	5.5 23 RY P-110 Semi-Premium
3.5 Mile Lateral	2nd Bone Spring Sand 3.5 Mile Lateral	6 26 P-110 Semi-Flush
4 Mile Lateral	2nd Bone Spring Sand 4 Mile Lateral	6 26 P-110 Semi-Flush
1 Mile Lateral	3rd Bone Spring Sand 1 Mile Lateral	5.5 20 RY P-110 Semi-Premium
1.5 Mile Lateral	3rd Bone Spring Sand 1.5 Mile Lateral	5.5 20 RY P-110 Semi-Premium
2 Mile Lateral	3rd Bone Spring Sand 2 Mile Lateral	5.5 20 RY P-110 Semi-Premium
2.5 Mile Lateral	3rd Bone Spring Sand 2.5 Mile Lateral	5.5 23 RY P-110 Semi-Premium
3 Mile Lateral	3rd Bone Spring Sand 3 Mile Lateral	5.5 23 RY P-110 Semi-Premium
3.5 Mile Lateral	3rd Bone Spring Sand 3.5 Mile Lateral	6 26 P-110 Semi-Flush
4 Mile Lateral	3rd Bone Spring Sand 4 Mile Lateral	6 26 P-110 Semi-Flush
1 Mile Lateral	Wolfcamp C 1 Mile Lateral	5.5 20 RY P-110 Semi-Premium
1.5 Mile Lateral	Wolfcamp C 1.5 Mile Lateral	5.5 20 RY P-110 Semi-Premium
2 Mile Lateral	Wolfcamp C 2 Mile Lateral	5.5 23 RY P-110 Semi-Premium
2.5 Mile Lateral	Wolfcamp C 2.5 Mile Lateral	5.5 23 RY P-110 Semi-Premium
3 Mile Lateral	Wolfcamp C 3 Mile Lateral	5.5 23 RY P-110 Semi-Premium
3.5 Mile Lateral	Wolfcamp C 3.5 Mile Lateral	6 26 P-110 Semi-Flush
4 Mile Lateral	Wolfcamp C 4 Mile Lateral	6 26 P-110 Semi-Flush
1 Mile Lateral	Wolfcamp B/C 1 Mile Lateral	5.5 20 RY P-110 Semi-Premium
1.5 Mile Lateral	Wolfcamp B/C 1.5 Mile Lateral	5.5 20 RY P-110 Semi-Premium
2 Mile Lateral	Wolfcamp B/C 2 Mile Lateral	5.5 23 RY P-110 Semi-Premium
2.5 Mile Lateral	Wolfcamp B/C 2.5 Mile Lateral	5.5 23 RY P-110 Semi-Premium
3 Mile Lateral	Wolfcamp B/C 3 Mile Lateral	5.5 23 RY P-110 Semi-Premium

3.5 Mile Lateral 4 Mile Lateral	Wolfcamp B/C 3.5 Mile Lateral Wolfcamp B/C 4 Mile Lateral	6 26 P-110 Semi-Flush 6 26 P-110 Semi-Flush
1 Mile Lateral 1.5 Mile Lateral	Wolfcamp D 1 Mile Lateral Wolfcamp D 1.5 Mile Lateral	5.5 20 RY P-110 Semi-Premium 5.5 20 RY P-110 Semi-Premium
2 Mile Lateral	Wolfcamp D 2 Mile Lateral	5.5 23 RY P-110 Semi-Premium
2.5 Mile Lateral	Wolfcamp D 2.5 Mile Lateral	5.5 23 RY P-110 Semi-Premium
3 Mile Lateral	Wolfcamp D 3 Mile Lateral	5.5 23 RY P-110 Semi-Premium
3.5 Mile Lateral	Wolfcamp D 3.5 Mile Lateral	6 26 P-110 Semi-Flush
4 Mile Lateral	Wolfcamp D 4 Mile Lateral	6 26 P-110 Semi-Flush
1 Mile Lateral	Wolfcamp E 1 Mile Lateral	5.5 20 RY P-110 Semi-Premium
1.5 Mile Lateral	Wolfcamp E 1.5 Mile Lateral	5.5 20 RY P-110 Semi-Premium
2 Mile Lateral	Wolfcamp E 2 Mile Lateral	5.5 23 RY P-110 Semi-Premium
2.5 Mile Lateral	Wolfcamp E 2.5 Mile Lateral	5.5 23 RY P-110 Semi-Premium
3 Mile Lateral	Wolfcamp E 3 Mile Lateral	5.5 23 RY P-110 Semi-Premium
3.5 Mile Lateral	Wolfcamp E 3.5 Mile Lateral	6 26 P-110 Semi-Flush
4 Mile Lateral	Wolfcamp E 4 Mile Lateral	6 26 P-110 Semi-Flush
1 Mile Lateral	Wolfcamp X/Y 1 Mile Lateral	5.5 20 RY P-110 Semi-Premium
1.5 Mile Lateral	Wolfcamp X/Y 1.5 Mile Lateral	5.5 20 RY P-110 Semi-Premium
2 Mile Lateral	Wolfcamp X/Y 2 Mile Lateral	5.5 23 RY P-110 Semi-Premium
2.5 Mile Lateral	Wolfcamp X/Y 2.5 Mile Lateral	5.5 23 RY P-110 Semi-Premium
3 Mile Lateral	Wolfcamp X/Y 3 Mile Lateral	5.5 23 RY P-110 Semi-Premium
3.5 Mile Lateral	Wolfcamp X/Y 3.5 Mile Lateral	6 26 P-110 Semi-Flush
4 Mile Lateral	Wolfcamp X/Y 4 Mile Lateral	6 26 P-110 Semi-Flush
2.25 Mile Lateral	1st Bone Spring 2.25 Mile Lateral	5.5 20 RY P-110 Semi-Premium
2.25 Mile Lateral	2nd Bone Spring 2.25 Mile Lateral	5.5 20 RY P-110 Semi-Premium
	3rd Bone Spring 2.25 Mile Lateral	5.5 20 RY P-110 Semi-Premium
	3rd Bone Spring Shale 2.25 Mile Lateral	5.5 20 RY P-110 Semi-Premium
	Wolfcamp X 2.25 Mile Lateral	5.5 23 RY P-110 Semi-Premium
	Wolfcamp Y 2.25 Mile Lateral	5.5 23 RY P-110 Semi-Premium
	Wolfcamp A 2.25 Mile Lateral	5.5 23 RY P-110 Semi-Premium
	Wolfcamp B 2.25 Mile Lateral	5.5 23 RY P-110 Semi-Premium
	Wolfcamp D/E 2.25 Mile Lateral	5.5 23 RY P-110 Semi-Premium
	1st Bone Spring Sand 2.25 Mile Lateral	5.5 20 RY P-110 Semi-Premium
	2nd Bone Spring Shale 2.25 Mile Lateral	5.5 20 RY P-110 Semi-Premium
	2nd Bone Spring Sand 2.25 Mile Lateral	5.5 20 RY P-110 Semi-Premium
2.25 Mile Lateral	3rd Bone Spring Sand 2.25 Mile Lateral	5.5 20 RY P-110 Semi-Premium
	Wolfcamp C 2.25 Mile Lateral	5.5 23 RY P-110 Semi-Premium
2.25 Mile Lateral	Wolfcamp B/C 2.25 Mile Lateral	5.5 23 RY P-110 Semi-Premium
	Wolfcamp D 2.25 Mile Lateral	5.5 23 RY P-110 Semi-Premium
	Wolfcamp E 2.25 Mile Lateral	5.5 23 RY P-110 Semi-Premium
2.25 Mile Lateral	Wolfcamp X/Y 2.25 Mile Lateral	5.5 23 RY P-110 Semi-Premium

F F 00 DV D 440 0 D	5 5 1 00 1 DV D
Production 1	Production 2

5.5 23 RY P-110 Semi-Premium 5.5	23 RY P-110	Semi-Flush
--	---------------	------------

Production 2	Production 3
5.5 20 RY P-110 Semi-Flush	5.5 20 RY P-110 Semi-Flush
5.5 20 RY P-110 Semi-Flush	5.5 20 RY P-110 Semi-Flush
5.5 20 RY P-110 Semi-Flush	5.5 20 RY P-110 Semi-Flush
5.5 23 RY P-110 Semi-Flush	5.5 23 RY P-110 Semi-Flush
5.5 23 RY P-110 Semi-Flush	5.5 23 RY P-110 Semi-Flush
6 26 P-110 Semi-Flush	6 26 P-110 Semi-Flush
6 26 P-110 Semi-Flush	6 26 P-110 Semi-Flush
5.5 20 RY P-110 Semi-Flush	5.5 20 RY P-110 Semi-Flush
5.5 20 RY P-110 Semi-Flush	5.5 20 RY P-110 Semi-Flush
5.5 20 RY P-110 Semi-Flush	5.5 20 RY P-110 Semi-Flush
5.5 23 RY P-110 Semi-Flush	5.5 23 RY P-110 Semi-Flush
5.5 23 RY P-110 Semi-Flush	5.5 23 RY P-110 Semi-Flush
6 26 P-110 Semi-Flush	6 26 P-110 Semi-Flush
6 26 P-110 Semi-Flush	6 26 P-110 Semi-Flush
5.5 20 RY P-110 Semi-Flush	5.5 20 RY P-110 Semi-Flush
5.5 20 RY P-110 Semi-Flush	5.5 20 RY P-110 Semi-Flush
5.5 20 RY P-110 Semi-Flush	5.5 20 RY P-110 Semi-Flush
5.5 23 RY P-110 Semi-Flush	5.5 23 RY P-110 Semi-Flush
5.5 23 RY P-110 Semi-Flush	5.5 23 RY P-110 Semi-Flush
6 26 P-110 Semi-Flush	6 26 P-110 Semi-Flush
6 26 P-110 Semi-Flush	6 26 P-110 Semi-Flush
5.5 20 RY P-110 Semi-Flush	5.5 20 RY P-110 Semi-Flush
5.5 20 RY P-110 Semi-Flush	5.5 20 RY P-110 Semi-Flush
5.5 20 RY P-110 Semi-Flush	5.5 20 RY P-110 Semi-Flush
5.5 23 RY P-110 Semi-Flush	5.5 23 RY P-110 Semi-Flush
5.5 23 RY P-110 Semi-Flush	5.5 23 RY P-110 Semi-Flush
6 26 P-110 Semi-Flush	6 26 P-110 Semi-Flush
· · · ·	6 26 P-110 Semi-Flush
6 26 P-110 Semi-Flush	
5.5 20 RY P-110 Semi-Flush	5.5 20 RY P-110 Semi-Flush
5.5 20 RY P-110 Semi-Flush	5.5 20 RY P-110 Semi-Flush
5.5 23 RY P-110 Semi-Flush	5.5 23 RY P-110 Semi-Flush
5.5 23 RY P-110 Semi-Flush	5.5 23 RY P-110 Semi-Flush
5.5 23 RY P-110 Semi-Flush	5.5 23 RY P-110 Semi-Flush
6 26 P-110 Semi-Flush	6 26 P-110 Semi-Flush
6 26 P-110 Semi-Flush	6 26 P-110 Semi-Flush
5.5 20 RY P-110 Semi-Flush	5.5 20 RY P-110 Semi-Flush
5.5 20 RY P-110 Semi-Flush	5.5 20 RY P-110 Semi-Flush
5.5 23 RY P-110 Semi-Flush	5.5 23 RY P-110 Semi-Flush
5.5 23 RY P-110 Semi-Flush	5.5 23 RY P-110 Semi-Flush
5.5 23 RY P-110 Semi-Flush	5.5 23 RY P-110 Semi-Flush
6 26 P-110 Semi-Flush	6 26 P-110 Semi-Flush
6 26 P-110 Semi-Flush	6 26 P-110 Semi-Flush
5.5 20 RY P-110 Semi-Flush	5.5 20 RY P-110 Semi-Flush
5.5 20 RY P-110 Semi-Flush	5.5 20 RY P-110 Semi-Flush
5.5 23 RY P-110 Semi-Flush	5.5 23 RY P-110 Semi-Flush
5.5 23 RY P-110 Semi-Flush	5.5 23 RY P-110 Semi-Flush
5.5 23 RY P-110 Semi-Flush	5.5 23 RY P-110 Semi-Flush
6 26 P-110 Semi-Flush	6 26 P-110 Semi-Flush

6 26 P-110 Semi-Flush	6 26 P-110 Semi-Flush
5.5 20 RY P-110 Semi-Flush	5.5 20 RY P-110 Semi-Flush
5.5 20 RY P-110 Semi-Flush	5.5 20 RY P-110 Semi-Flush
·	
5.5 23 RY P-110 Semi-Flush	5.5 23 RY P-110 Semi-Flush
5.5 23 RY P-110 Semi-Flush	5.5 23 RY P-110 Semi-Flush
5.5 23 RY P-110 Semi-Flush	5.5 23 RY P-110 Semi-Flush
6 26 P-110 Semi-Flush	6 26 P-110 Semi-Flush
6 26 P-110 Semi-Flush	6 26 P-110 Semi-Flush
5.5 20 RY P-110 Semi-Flush	5.5 20 RY P-110 Semi-Flush
5.5 20 RY P-110 Semi-Flush	5.5 20 RY P-110 Semi-Flush
5.5 23 RY P-110 Semi-Flush	5.5 23 RY P-110 Semi-Flush
5.5 23 RY P-110 Semi-Flush	5.5 23 RY P-110 Semi-Flush
5.5 23 RY P-110 Semi-Flush	5.5 23 RY P-110 Semi-Flush
6 26 P-110 Semi-Flush	6 26 P-110 Semi-Flush
6 26 P-110 Semi-Flush	6 26 P-110 Semi-Flush
5.5 20 RY P-110 Semi-Flush	5.5 20 RY P-110 Semi-Flush
5.5 20 RY P-110 Semi-Flush	5.5 20 RY P-110 Semi-Flush
5.5 20 RY P-110 Semi-Flush	5.5 20 RY P-110 Semi-Flush
5.5 23 RY P-110 Semi-Flush	5.5 23 RY P-110 Semi-Flush
5.5 23 RY P-110 Semi-Flush	5.5 23 RY P-110 Semi-Flush
6 26 P-110 Semi-Flush	6 26 P-110 Semi-Flush
6 26 P-110 Semi-Flush	6 26 P-110 Semi-Flush
5.5 20 RY P-110 Semi-Flush	5.5 20 RY P-110 Semi-Flush
5.5 20 RY P-110 Semi-Flush	5.5 20 RY P-110 Semi-Flush
5.5 20 RY P-110 Semi-Flush	5.5 20 RY P-110 Semi-Flush
5.5 23 RY P-110 Semi-Flush	5.5 23 RY P-110 Semi-Flush
5.5 23 RY P-110 Semi-Flush	5.5 23 RY P-110 Semi-Flush
6 26 P-110 Semi-Flush	6 26 P-110 Semi-Flush
6 26 P-110 Semi-Flush	6 26 P-110 Semi-Flush
5.5 20 RY P-110 Semi-Flush	5.5 20 RY P-110 Semi-Flush
5.5 20 RY P-110 Semi-Flush	5.5 20 RY P-110 Semi-Flush
5.5 20 RY P-110 Semi-Flush	
	5.5 20 RY P-110 Semi-Flush
5.5 23 RY P-110 Semi-Flush	5.5 23 RY P-110 Semi-Flush
5.5 23 RY P-110 Semi-Flush	5.5 23 RY P-110 Semi-Flush
6 26 P-110 Semi-Flush	6 26 P-110 Semi-Flush
6 26 P-110 Semi-Flush	6 26 P-110 Semi-Flush
5.5 20 RY P-110 Semi-Flush	5.5 20 RY P-110 Semi-Flush
5.5 20 RY P-110 Semi-Flush	5.5 20 RY P-110 Semi-Flush
5.5 20 RY P-110 Semi-Flush	5.5 20 RY P-110 Semi-Flush
5.5 23 RY P-110 Semi-Flush	5.5 23 RY P-110 Semi-Flush
5.5 23 RY P-110 Semi-Flush	5.5 23 RY P-110 Semi-Flush
6 26 P-110 Semi-Flush	6 26 P-110 Semi-Flush
6 26 P-110 Semi-Flush	6 26 P-110 Semi-Flush
5.5 20 RY P-110 Semi-Flush	5.5 20 RY P-110 Semi-Flush
5.5 20 RY P-110 Semi-Flush	5.5 20 RY P-110 Semi-Flush
5.5 23 RY P-110 Semi-Flush	5.5 23 RY P-110 Semi-Flush
5.5 23 RY P-110 Semi-Flush	5.5 23 RY P-110 Semi-Flush
5.5 23 RY P-110 Semi-Flush	5.5 23 RY P-110 Semi-Flush
6 26 P-110 Semi-Flush	6 26 P-110 Semi-Flush
6 26 P-110 Semi-Flush	6 26 P-110 Semi-Flush
5.5 20 RY P-110 Semi-Flush	5.5 20 RY P-110 Semi-Flush
5.5 20 RY P-110 Semi-Flush	5.5 20 RY P-110 Semi-Flush
5.5 23 RY P-110 Semi-Flush	5.5 23 RY P-110 Semi-Flush
5.5 23 RY P-110 Semi-Flush	5.5 23 RY P-110 Semi-Flush
5.5 23 RY P-110 Semi-Flush	5.5 23 RY P-110 Semi-Flush
0.0 20 101 1 - 110 0e1111-1 lust1	5.5 25 10 56 m-Flush

6 26 P-110 Semi-Flush	6 26 P-110 Semi-Flush
6 26 P-110 Semi-Flush	6 26 P-110 Semi-Flush
5.5 20 RY P-110 Semi-Flush	5.5 20 RY P-110 Semi-Flush
5.5 20 RY P-110 Semi-Flush	5.5 20 RY P-110 Semi-Flush
5.5 23 RY P-110 Semi-Flush	5.5 23 RY P-110 Semi-Flush
5.5 23 RY P-110 Semi-Flush	5.5 23 RY P-110 Semi-Flush
5.5 23 RY P-110 Semi-Flush	5.5 23 RY P-110 Semi-Flush
6 26 P-110 Semi-Flush	6 26 P-110 Semi-Flush
6 26 P-110 Semi-Flush	6 26 P-110 Semi-Flush
5.5 20 RY P-110 Semi-Flush	5.5 20 RY P-110 Semi-Flush
5.5 20 RY P-110 Semi-Flush	5.5 20 RY P-110 Semi-Flush
5.5 23 RY P-110 Semi-Flush	5.5 23 RY P-110 Semi-Flush
5.5 23 RY P-110 Semi-Flush	5.5 23 RY P-110 Semi-Flush
5.5 23 RY P-110 Semi-Flush	5.5 23 RY P-110 Semi-Flush
6 26 P-110 Semi-Flush	6 26 P-110 Semi-Flush
6 26 P-110 Semi-Flush	6 26 P-110 Semi-Flush
5.5 20 RY P-110 Semi-Flush	5.5 20 RY P-110 Semi-Flush
5.5 20 RY P-110 Semi-Flush	5.5 20 RY P-110 Semi-Flush
5.5 23 RY P-110 Semi-Flush	5.5 23 RY P-110 Semi-Flush
5.5 23 RY P-110 Semi-Flush	5.5 23 RY P-110 Semi-Flush
5.5 23 RY P-110 Semi-Flush	5.5 23 RY P-110 Semi-Flush
5.5 20 10 00 11 10 11 11 11	0.0 20 111 110 001111 14011
6 26 P-110 Semi-Flush	6 26 P-110 Semi-Flush
6 26 P-110 Semi-Flush	6 26 P-110 Semi-Flush
6 26 P-110 Semi-Flush 6 26 P-110 Semi-Flush	6 26 P-110 Semi-Flush 6 26 P-110 Semi-Flush
6 26 P-110 Semi-Flush 6 26 P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush	6 26 P-110 Semi-Flush 6 26 P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush
6 26 P-110 Semi-Flush 6 26 P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush	6 26 P-110 Semi-Flush 6 26 P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush
6 26 P-110 Semi-Flush 6 26 P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush	6 26 P-110 Semi-Flush 6 26 P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush
6 26 P-110 Semi-Flush 6 26 P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush	6 26 P-110 Semi-Flush 6 26 P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush
6 26 P-110 Semi-Flush 6 26 P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush 5.5 23 RY P-110 Semi-Flush	6 26 P-110 Semi-Flush 6 26 P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush 5.5 23 RY P-110 Semi-Flush
6 26 P-110 Semi-Flush 6 26 P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush 5.5 23 RY P-110 Semi-Flush 5.5 23 RY P-110 Semi-Flush	6 26 P-110 Semi-Flush 6 26 P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush 5.5 23 RY P-110 Semi-Flush 5.5 23 RY P-110 Semi-Flush
6 26 P-110 Semi-Flush 6 26 P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush 5.5 23 RY P-110 Semi-Flush 5.5 23 RY P-110 Semi-Flush 5.5 23 RY P-110 Semi-Flush 5.5 23 RY P-110 Semi-Flush	6 26 P-110 Semi-Flush 6 26 P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush 5.5 23 RY P-110 Semi-Flush
6 26 P-110 Semi-Flush 6 26 P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush 5.5 23 RY P-110 Semi-Flush	6 26 P-110 Semi-Flush 6 26 P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush 5.5 23 RY P-110 Semi-Flush
6 26 P-110 Semi-Flush 6 26 P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush 5.5 23 RY P-110 Semi-Flush	6 26 P-110 Semi-Flush 6 26 P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush 5.5 23 RY P-110 Semi-Flush
6 26 P-110 Semi-Flush 6 26 P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush 5.5 23 RY P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush	6 26 P-110 Semi-Flush 6 26 P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush 5.5 23 RY P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush
6 26 P-110 Semi-Flush 6 26 P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush 5.5 23 RY P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush	6 26 P-110 Semi-Flush 6 26 P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush 5.5 23 RY P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush
6 26 P-110 Semi-Flush 6 26 P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush 5.5 23 RY P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush 5.5 23 RY P-110 Semi-Flush	6 26 P-110 Semi-Flush 6 26 P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush 5.5 23 RY P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush 5.5 23 RY P-110 Semi-Flush
6 26 P-110 Semi-Flush 6 26 P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush 5.5 23 RY P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush 5.5 23 RY P-110 Semi-Flush	6 26 P-110 Semi-Flush 6 26 P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush 5.5 23 RY P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush 5.5 23 RY P-110 Semi-Flush 5.5 23 RY P-110 Semi-Flush 5.5 23 RY P-110 Semi-Flush 5.5 23 RY P-110 Semi-Flush
6 26 P-110 Semi-Flush 6 26 P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush 5.5 23 RY P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush 5.5 23 RY P-110 Semi-Flush	6 26 P-110 Semi-Flush 6 26 P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush 5.5 23 RY P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush 5.5 23 RY P-110 Semi-Flush
6 26 P-110 Semi-Flush 6 26 P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush 5.5 23 RY P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush 5.5 23 RY P-110 Semi-Flush	6 26 P-110 Semi-Flush 6 26 P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush 5.5 23 RY P-110 Semi-Flush 5.5 20 RY P-110 Semi-Flush 5.5 23 RY P-110 Semi-Flush 5.5 23 RY P-110 Semi-Flush 5.5 23 RY P-110 Semi-Flush 5.5 23 RY P-110 Semi-Flush

Production 3

Max Frac Pressure

5.5 | 23 | RY P-110 | Semi-Flush

12000

Max Frac Pressure

10000
10000
12000
12000
12000
12000
10000
10000
10000
12000
12000
12000
12000
10000
10000
10000
12000
12000
12000
12000
10000
10000
10000
12000
12000
12000 12000
12000
10000
10000
12000
12000 12000
12000
10000
10000
10000
12000
12000
12000
12000
10000
10000
. 0000

10000

Name
20 169 K-55 BTC
18.625 87.5 J-55 BTC
13.375 68 HC L-80 BT(
13.375 54.5 J-55 BTC
9.625 40 J-55 BTC
9.625 40 HC L-80 BTC
9.625 53.5 HC P110 B
9.625 40 HC P110 BTC
7.625 29.7 P110 RY -IFJ
7.625 29.7 P110 CY - IF
7.625 29.7 HCL-80 - IFJ
6 26 P-110 - Talon HTQ
5.5 23 P110 RY - Talon
5.5 23 P110 RY - VAM S
5.5 23 P110 RY - Freedo
5.5 20 P110 RY - Talon
5.5 20 P110 RY - Freedo

		C	asing Table
	OD	Weight	Grade
	20	169	K-55
	18 5/8	87.5	J-55
С	13 3/8	68	HC L-80
	13 3/8	54.5	J-55
	9 5/8	40	J-55
	9 5/8	40	HC L-80
TC	9 5/8	53.5	HC P110
	9 5/8	40	HC P110
J Flush Joint	7 5/8	29.7	P110 RY -IFJ
J Flush Joint	7 5/8	29.7	P110 CY - IFJ
Flush Joint	7 5/8	29.7	HCL-80 - IFJ
Semi-Flush	6	26	P-110 - Talon HT0
HTQ Semi-Flu	5 1/2	23	P110 RY - Talon HT
SPRINT Semi-F	5 1/2	23	P110 RY - VAM SPR
om HTQ Semi-	5 1/2	23	P110 RY - Freedom I
HTQ Semi-Flu	5 1/2	20	P110 RY - Talon HT
om HTQ Semi-	5 1/2	20	P110 RY - Freedom I

	Connection	Tube ID	Collapse	Burst	Tension
	BTC	18.376	2,500	3,380	2,689,000
	BTC	17.755	630	2,250	1,329,000
	BTC	12.415	2,690	5,020	1,545,000
	BTC	12.615	1,130	2,740	909,000
	BTC	8.835	2,750	3,950	630,000
	BTC	8.835	4,230	5,750	916,000
	BTC	8.835	9,190	10,900	1,718,000
	BTC	8.535	4,230	7,910	1,266,000
	Flush Joint	6.875	5,350	9,460	558,000
	Flush Joint	6.875	5,350	9,460	960,000
	Flush Joint	6.875	5,780	6,880	406,000
Q	Semi-Flush	5.128	13,570	14,010	838,000
Q	Semi-Flush	4.67	14,540	14,530	707,000
INT	Semi-Flush	4.67	14,550	14,530	671,000
HTQ	Semi-Premium	4.67	14,540	14,520	729,000
Q	Semi-Flush	4.778	11,100	12,640	641,000
HTQ.	Semi-Premium	4.778	11,100	12,640	641,000

Well Plan Report - 111H

Measured Depth: 23856.63 ft

TVD RKB: 11182.00 ft

Location

Cartographic New Mexico East -Reference System: NAD 27 487864.60 ft Northing: Easting: 658029.20 ft RKB: 3347.00 ft **Ground Level:** 3315.00 ft Grid North Reference: Convergence 0.27 Deg Angle:

Site: JRU DI7

Plan Sections 111H

Measured			TVD			Build	Turn	Dogleg
Depth	Inclination	Azimuth	RKB	Y Offset	X Offset	Rate	Rate	Rate
(ft)	(Deg)	(Deg)	(ft)	(ft)	(ft)	(Deg/100ft)	(Deg/100ft)	(Deg/100ft)
0	0	0	0	0	0	0	0	0
1200	0	0	1200	0	0	0	0	0
1984.16	15.68	97.92	1974.41	-14.7	105.64	2	0	2
5830.55	15.68	97.92	5677.59	-158	1135.46	0	0	0
6614.71	0	0	6452	-172.7	1241.1	-2	0	2
10628.51	0	0	10465.8	-172.7	1241.1	0	0	0
11753.51	90	179.75	11182	-888.89	1244.18	8	15.98	8
23806.63	90	179.75	11182	-12941.9	1295.97	0	0	0
23856.63	90	179.75	11182	-12991.9	1296.18	0	0	0

Position Uncertainty

111H

Measured			TVD	/D Highside Later			eral Vertical		
Depth	Inclination	Azimuth	RKB	Error	Bias	Error	Bias	Error	
(ft)	(°)	(°)	(ft)	(ft)	(ft)	(ft)	(ft)	(ft)	
0	0	0	0	0	0	0	0	0	
100	0	0	100	0.358	0	0.179	0	2.3	
200	0	0	200	0.717	0	0.538	0	2.309	
300	0	0	300	1.075	0	0.896	0	2.325	
400	0	0	400	1.434	0	1.255	0	2.347	
500	0	0	500	1.792	0	1.613	0	2.374	
600	0	0	600	2.151	0	1.972	0	2.406	
700	0	0	700	2.509	0	2.33	0	2.443	
800	0	0	800	2.868	0	2.689	0	2.485	
900	0	0	900	3.226	0	3.047	0	2.53	
1000	0	0	1000	3.585	0	3.405	0	2.58	
1100	0	0	1100	3.943	0	3.764	0	2.633	
1200	0	0	1200	4.302	0	4.122	0	2.69	
1300	2	97.922	1299.98	4.472	0	4.647	0	2.749	
1400	4	97.922	1399.838	4.806	0	4.99	0	2.809	
1500	6	97.922	1499.452	5.136	0	5.337	0	2.87	
1600	8	97.922	1598.702	5.464	0	5.687	0	2.931	
1700	10	97.922	1697.465	5.788	0	6.042	0	2.994	

1800	12	97.922	1795.623	6.109	0	6.402	0	3.06
1900	14	97.922	1893.055	6.428	0	6.768	0	3.128
1984.162	15.683	97.922	1974.407	6.694	0	7.082	0	3.187
2000	15.683	97.922	1989.655	6.751	0	7.141	0	3.195
2100	15.683	97.922	2085.932	7.115	0	7.521	0	3.285
2200	15.683	97.922	2182.209	7.483	0	7.906	0	3.38
2300	15.683	97.922	2278.486	7.855	0	8.295	0	3.479
2400	15.683	97.922	2374.763	8.23	0	8.688	0	3.582
2500	15.683	97.922	2471.04	8.608	0	9.084	0	3.688
2600	15.683	97.922	2567.317	8.989	0	9.482	0	3.797
2700	15.683	97.922	2663.594	9.372	0	9.883	0	3.91
2800	15.683	97.922	2759.871	9.756	0	10.286	0	4.024
2900	15.683	97.922	2856.149	10.143	0	10.691	0	4.142
3000	15.683	97.922	2952.426	10.531	0	11.097	0	4.262
3100	15.683	97.922	3048.703	10.92	0	11.505	0	4.384
3200	15.683	97.922	3144.98	11.31	0	11.915	0	4.509
3300	15.683	97.922	3241.257	11.702	0	12.325	0	4.635
3400	15.683	97.922	3337.534	12.095	0	12.737	0	4.764
3500	15.683	97.922	3433.811	12.488	0	13.149	0	4.894
3600	15.683	97.922	3530.088	12.882	0	13.563	0	5.027
3700	15.683	97.922	3626.365	13.277	0	13.977	0	5.161

3800	15.683	97.922	3722.642	13.673	0	14.392	0	5.297
3900	15.683	97.922	3818.919	14.069	0	14.808	0	5.434
4000	15.683	97.922	3915.196	14.466	0	15.225	0	5.574
4100	15.683	97.922	4011.473	14.864	0	15.642	0	5.714
4200	15.683	97.922	4107.751	15.262	0	16.059	0	5.857
4300	15.683	97.922	4204.028	15.66	0	16.477	0	6.001
4400	15.683	97.922	4300.305	16.059	0	16.896	0	6.147
4500	15.683	97.922	4396.582	16.458	0	17.315	0	6.294
4600	15.683	97.922	4492.859	16.857	0	17.734	0	6.443
4700	15.683	97.922	4589.136	17.257	0	18.153	0	6.594
4800	15.683	97.922	4685.413	17.657	0	18.574	0	6.746
4900	15.683	97.922	4781.69	18.058	0	18.994	0	6.899
5000	15.683	97.922	4877.967	18.458	0	19.414	0	7.055
5100	15.683	97.922	4974.244	18.859	0	19.835	0	7.211
5200	15.683	97.922	5070.521	19.261	0	20.257	0	7.37
5300	15.683	97.922	5166.798	19.662	0	20.678	0	7.53
5400	15.683	97.922	5263.076	20.064	0	21.1	0	7.691
5500	15.683	97.922	5359.353	20.465	0	21.521	0	7.854
5600	15.683	97.922	5455.63	20.867	0	21.944	0	8.019
5700	15.683	97.922	5551.907	21.269	0	22.366	0	8.186
5800	15.683	97.922	5648.184	21.672	0	22.788	0	8.354

5830.547	15.683	97.922	5677.593	21.795	0	22.917	0	8.406
5900	14.294	97.922	5744.682	22.096	0	23.207	0	8.524
6000	12.294	97.922	5841.997	22.502	0	23.613	0	8.69
6100	10.294	97.922	5940.056	22.875	0	24.005	0	8.851
6200	8.294	97.922	6038.738	23.213	0	24.384	0	9.005
6300	6.294	97.922	6137.924	23.516	0	24.748	0	9.154
6400	4.294	97.922	6237.492	23.783	0	25.1	0	9.297
6500	2.294	97.922	6337.322	24.015	0	25.439	0	9.435
6600	0.294	97.922	6437.291	24.21	0	25.765	0	9.569
6614.709	0	0	6452	25.722	0	24.331	0	9.588
6700	0	0	6537.291	25.991	0	24.599	0	9.701
6800	0	0	6637.291	26.308	0	24.915	0	9.836
6900	0	0	6737.291	26.626	0	25.231	0	9.974
7000	0	0	6837.291	26.945	0	25.549	0	10.114
7100	0	0	6937.291	27.265	0	25.868	0	10.258
7200	0	0	7037.291	27.586	0	26.188	0	10.404
7300	0	0	7137.291	27.907	0	26.509	0	10.553
7400	0	0	7237.291	28.23	0	26.831	0	10.705
7500	0	0	7337.291	28.554	0	27.154	0	10.861
7600	0	0	7437.291	28.878	0	27.478	0	11.019
7700	0	0	7537.291	29.203	0	27.802	0	11.18

78	300	0	0	7637.291	29.529	0	28.127	0	11.344
79	000	0	0	7737.291	29.856	0	28.454	0	11.511
80	000	0	0	7837.291	30.183	0	28.781	0	11.681
81	00	0	0	7937.291	30.511	0	29.108	0	11.854
82	000	0	0	8037.291	30.84	0	29.437	0	12.03
83	300	0	0	8137.291	31.169	0	29.766	0	12.21
84	000	0	0	8237.291	31.499	0	30.095	0	12.392
85	500	0	0	8337.291	31.83	0	30.426	0	12.578
86	500	0	0	8437.291	32.161	0	30.757	0	12.766
87	700	0	0	8537.291	32.493	0	31.089	0	12.958
88	800	0	0	8637.291	32.825	0	31.421	0	13.153
89	000	0	0	8737.291	33.158	0	31.754	0	13.351
90	000	0	0	8837.291	33.492	0	32.087	0	13.552
91	.00	0	0	8937.291	33.826	0	32.421	0	13.757
92	000	0	0	9037.291	34.16	0	32.755	0	13.964
93	300	0	0	9137.291	34.495	0	33.09	0	14.175
94	000	0	0	9237.291	34.83	0	33.426	0	14.389
95	500	0	0	9337.291	35.166	0	33.762	0	14.606
96	500	0	0	9437.291	35.502	0	34.098	0	14.826
97	700	0	0	9537.291	35.839	0	34.435	0	15.05
98	300	0	0	9637.291	36.176	0	34.772	0	15.276

9900	0	0	9737.291	36.514	0	35.11	0	15.506
10000	0	0	9837.291	36.852	0	35.448	0	15.739
10100	0	0	9937.291	37.19	0	35.786	0	15.975
10200	0	0	10037.291	37.529	0	36.125	0	16.215
10300	0	0	10137.291	37.868	0	36.464	0	16.458
10400	0	0	10237.291	38.207	0	36.804	0	16.703
10500	0	0	10337.291	38.547	0	37.144	0	16.953
10600	0	0	10437.291	38.887	0	37.484	0	17.205
10628.509	0	0	10465.8	38.984	0	37.581	0	17.277
10700	5.719	179.754	10537.172	39.097	0	37.821	0	17.46
10800	13.719	179.754	10635.657	38.723	0	38.142	0	17.715
10900	21.719	179.754	10730.836	37.759	0	38.455	0	17.966
11000	29.719	179.754	10820.856	36.243	0	38.757	0	18.211
11100	37.719	179.754	10903.965	34.236	0	39.046	0	18.45
11200	45.719	179.754	10978.546	31.83	0	39.318	0	18.684
11300	53.719	179.754	11043.147	29.154	0	39.574	0	18.917
11400	61.719	179.754	11096.51	26.383	0	39.811	0	19.152
11500	69.719	179.754	11137.598	23.762	0	40.028	0	19.393
11600	77.719	179.754	11165.61	21.609	0	40.224	0	19.644
11700	85.719	179.754	11180.001	20.295	0	40.398	0	19.906
11753.509	90	179.754	11181.997	20.05	0	40.479	0	20.05

11800	90	179.754	11181.997	20.179	0	40.548	0	20.179
11900	90	179.754	11181.997	20.475	0	40.713	0	20.475
12000	90	179.754	11181.997	20.797	0	40.896	0	20.797
12100	90	179.754	11181.997	21.143	0	41.097	0	21.143
12200	90	179.754	11181.997	21.513	0	41.317	0	21.513
12300	90	179.754	11181.997	21.904	0	41.553	0	21.904
12400	90	179.754	11181.997	22.316	0	41.807	0	22.316
12500	90	179.754	11181.997	22.748	0	42.078	0	22.748
12600	90	179.754	11181.997	23.198	0	42.366	0	23.198
12700	90	179.754	11181.997	23.665	0	42.669	0	23.665
12800	90	179.754	11181.997	24.149	0	42.989	0	24.149
12900	90	179.754	11181.998	24.649	0	43.324	0	24.649
13000	90	179.754	11181.998	25.163	0	43.674	0	25.163
13100	90	179.754	11181.998	25.691	0	44.04	0	25.691
13200	90	179.754	11181.998	26.231	0	44.419	0	26.231
13300	90	179.754	11181.998	26.784	0	44.813	0	26.784
13400	90	179.754	11181.998	27.348	0	45.22	0	27.348
13500	90	179.754	11181.998	27.923	0	45.641	0	27.923
13600	90	179.754	11181.998	28.508	0	46.075	0	28.508
13700	90	179.754	11181.998	29.102	0	46.521	0	29.102
13800	90	179.754	11181.998	29.705	0	46.98	0	29.705

13900	90	179.754	11181.998	30.316	0	47.451	0	30.316
14000	90	179.754	11181.998	30.935	0	47.933	0	30.935
14100	90	179.754	11181.998	31.562	0	48.426	0	31.562
14200	90	179.754	11181.998	32.195	0	48.93	0	32.195
14300	90	179.754	11181.998	32.835	0	49.445	0	32.835
14400	90	179.754	11181.998	33.482	0	49.97	0	33.482
14500	90	179.754	11181.998	34.134	0	50.505	0	34.134
14600	90	179.754	11181.998	34.791	0	51.05	0	34.791
14700	90	179.754	11181.998	35.454	0	51.604	0	35.454
14800	90	179.754	11181.998	36.121	0	52.166	0	36.121
14900	90	179.754	11181.998	36.794	0	52.738	0	36.794
15000	90	179.754	11181.998	37.47	0	53.318	0	37.47
15100	90	179.754	11181.998	38.151	0	53.906	0	38.151
15200	90	179.754	11181.998	38.835	0	54.502	0	38.835
15300	90	179.754	11181.998	39.524	0	55.105	0	39.524
15400	90	179.754	11181.998	40.216	0	55.716	0	40.216
15500	90	179.754	11181.998	40.911	0	56.335	0	40.911
15600	90	179.754	11181.998	41.609	0	56.96	0	41.609
15700	90	179.754	11181.998	42.311	0	57.591	0	42.311
15800	90	179.754	11181.998	43.015	0	58.23	0	43.015
15900	90	179.754	11181.998	43.722	0	58.874	0	43.722

16	5000	90	179.754	11181.998	44.432	0	59.524	0	44.432
16	5100	90	179.754	11181.998	45.144	0	60.181	0	45.144
16	5200	90	179.754	11181.998	45.859	0	60.843	0	45.859
16	5300	90	179.754	11181.998	46.575	0	61.51	0	46.575
16	5400	90	179.754	11181.998	47.294	0	62.183	0	47.294
16	5500	90	179.754	11181.998	48.015	0	62.861	0	48.015
16	6600	90	179.754	11181.998	48.738	0	63.544	0	48.738
16	5700	90	179.754	11181.998	49.463	0	64.232	0	49.463
16	5800	90	179.754	11181.998	50.19	0	64.924	0	50.19
16	5900	90	179.754	11181.998	50.918	0	65.621	0	50.918
17	7000	90	179.754	11181.998	51.648	0	66.323	0	51.648
17	7100	90	179.754	11181.998	52.38	0	67.028	0	52.38
17	7200	90	179.754	11181.998	53.113	0	67.738	0	53.113
17	7300	90	179.754	11181.999	53.848	0	68.451	0	53.848
17	7400	90	179.754	11181.999	54.584	0	69.169	0	54.584
17	7500	90	179.754	11181.999	55.321	0	69.89	0	55.321
17	7600	90	179.754	11181.999	56.06	0	70.615	0	56.06
17	7700	90	179.754	11181.999	56.8	0	71.343	0	56.8
17	7800	90	179.754	11181.999	57.541	0	72.075	0	57.541
17	7900	90	179.754	11181.999	58.283	0	72.81	0	58.283
18	3000	90	179.754	11181.999	59.026	0	73.548	0	59.026

18100	90	179.754	11181.999	59.771	0	74.289	0	59.771
18200	90	179.754	11181.999	60.516	0	75.034	0	60.516
18300	90	179.754	11181.999	61.262	0	75.781	0	61.262
18400	90	179.754	11181.999	62.01	0	76.531	0	62.01
18500	90	179.754	11181.999	62.758	0	77.284	0	62.758
18600	90	179.754	11181.999	63.507	0	78.04	0	63.507
18700	90	179.754	11181.999	64.257	0	78.798	0	64.257
18800	90	179.754	11181.999	65.008	0	79.558	0	65.008
18900	90	179.754	11181.999	65.759	0	80.321	0	65.759
19000	90	179.754	11181.999	66.512	0	81.087	0	66.512
19100	90	179.754	11181.999	67.265	0	81.855	0	67.265
19200	90	179.754	11181.999	68.019	0	82.625	0	68.019
19300	90	179.754	11181.999	68.773	0	83.397	0	68.773
19400	90	179.754	11181.999	69.528	0	84.172	0	69.528
19500	90	179.754	11181.999	70.284	0	84.948	0	70.284
19600	90	179.754	11181.999	71.041	0	85.727	0	71.041
19700	90	179.754	11181.999	71.798	0	86.507	0	71.798
19800	90	179.754	11181.999	72.555	0	87.289	0	72.555
19900	90	179.754	11181.999	73.314	0	88.074	0	73.314
20000	90	179.754	11181.999	74.072	0	88.86	0	74.072
20100	90	179.754	11181.999	74.832	0	89.647	0	74.832

2	0200	90	179.754	11181.999	75.591	0	90.437	0	75.591
2	0300	90	179.754	11181.999	76.352	0	91.228	0	76.352
2	0400	90	179.754	11181.999	77.113	0	92.021	0	77.113
2	0500	90	179.754	11181.999	77.874	0	92.815	0	77.874
2	0600	90	179.754	11181.999	78.636	0	93.611	0	78.636
2	0700	90	179.754	11181.999	79.398	0	94.409	0	79.398
2	0800	90	179.754	11181.999	80.161	0	95.207	0	80.161
2	0900	90	179.754	11181.999	80.924	0	96.008	0	80.924
2	1000	90	179.754	11181.999	81.687	0	96.809	0	81.687
2	1100	90	179.754	11181.999	82.451	0	97.613	0	82.451
2	1200	90	179.754	11181.999	83.215	0	98.417	0	83.215
2	1300	90	179.754	11181.999	83.98	0	99.223	0	83.98
2	1400	90	179.754	11181.999	84.745	0	100.03	0	84.745
2	1500	90	179.754	11181.999	85.51	0	100.838	0	85.51
2	1600	90	179.754	11181.999	86.276	0	101.647	0	86.276
2	1700	90	179.754	11182	87.042	0	102.458	0	87.042
2	1800	90	179.754	11182	87.808	0	103.27	0	87.808
2	1900	90	179.754	11182	88.575	0	104.082	0	88.575
2	2000	90	179.754	11182	89.342	0	104.896	0	89.342
2	2100	90	179.754	11182	90.11	0	105.711	0	90.11
2	2200	90	179.754	11182	90.877	0	106.528	0	90.877

22300	90	179.754	11182	91.645	0	107.345	0	91.645
22400	90	179.754	11182	92.413	0	108.163	0	92.413
22500	90	179.754	11182	93.182	0	108.982	0	93.182
22600	90	179.754	11182	93.951	0	109.802	0	93.951
22700	90	179.754	11182	94.72	0	110.623	0	94.72
22800	90	179.754	11182	95.489	0	111.445	0	95.489
22900	90	179.754	11182	96.258	0	112.267	0	96.258
23000	90	179.754	11182	97.028	0	113.091	0	97.028
23100	90	179.754	11182	97.798	0	113.916	0	97.798
23200	90	179.754	11182	98.568	0	114.741	0	98.568
23300	90	179.754	11182	99.339	0	115.567	0	99.339
23400	90	179.754	11182	100.11	0	116.394	0	100.11
23500	90	179.754	11182	100.88	0	117.222	0	100.88
23600	90	179.754	11182	101.652	0	118.05	0	101.652
23700	90	179.754	11182	102.423	0	118.879	0	102.423
23806.63	90	179.754	11182	103.246	0	119.765	0	103.246
23856.63	90	179.754	11182	103.631	0	120.179	0	103.631

Plan Targets 111H

	Measured Depth	Grid Northing	Grid Easting	TVD MSL Target Shape
Target Name	(ft)	(ft)	(ft)	(ft)
111H_LTP JRU	23806.63	474922.7	659325.2	7835 LOCATION

111H_BHLJRU	23856.63	474872.7	659325.4	7835 LOCATION
111H_PP2	15984.65	482744.6	659291.6	7835 LOCATION
111H_PP1	13343.03	485386.2	659280.2	7835 LOCATION
111H_FTP JRU	11496.85	487691.9	659270.3	7835 LOCATION
111H SHI IDII	0	187861 6	658020.2	-22/17 DECTANGLE

Target

111H_LTP JRU

111H_BHLJRU

	Magnitude	Semi-major	Semi-minor	Semi-minor Tool
Bias	of Bias	Error	Error	Azimuth Used
(ft)	(ft)	(ft)	(ft)	(°)
0	0	0	0	0 XOM_R2OWSG MWD+IFR1+MS
0	0	0.358	0.179	90 XOM_R2OWSG MWD+IFR1+MS
0	0	0.717	0.538	90 XOM_R2OWSG MWD+IFR1+MS
0	0	1.075	0.896	90 XOM_R2OWSG MWD+IFR1+MS
0	0	1.434	1.255	90 XOM_R2OWSG MWD+IFR1+MS
0	0	1.792	1.613	90 XOM_R2OWSG MWD+IFR1+MS
0	0	2.151	1.972	90 XOM_R2OWSG MWD+IFR1+MS
0	0	2.509	2.33	90 XOM_R2OWSG MWD+IFR1+MS
0	0	2.868	2.689	90 XOM_R2OWSG MWD+IFR1+MS
0	0	3.226	3.047	90 XOM_R2OWSG MWD+IFR1+MS
0	0	3.585	3.405	90 XOM_R2OWSG MWD+IFR1+MS
0	0	3.943	3.764	90 XOM_R2OWSG MWD+IFR1+MS
0	0	4.302	4.122	90 XOM_R2OWSG MWD+IFR1+MS
0	0	4.651	4.471	90.049 XOM_R2OWSG MWD+IFR1+MS
0	0	4.993	4.812	90.14 XOM_R2OWSG MWD+IFR1+MS
0	0	5.34	5.157	90.312 XOM_R2OWSG MWD+IFR1+MS
0	0	5.69	5.503	90.631 XOM_R2OWSG MWD+IFR1+MS
0	0	6.045	5.851	91.139 XOM_R2OWSG MWD+IFR1+MS

0	0	6.404	6.201	91.853	XOM_R2OWSG MWD+IFR1+MS
0	0	6.77	6.553	92.759	XOM_R2OWSG MWD+IFR1+MS
0	0	7.083	6.851	93.621	XOM_R2OWSG MWD+IFR1+MS
0	0	7.143	6.909	93.756	XOM_R2OWSG MWD+IFR1+MS
0	0	7.522	7.258	94.897	XOM_R2OWSG MWD+IFR1+MS
0	0	7.907	7.612	95.893	XOM_R2OWSG MWD+IFR1+MS
0	0	8.295	7.97	96.767	XOM_R2OWSG MWD+IFR1+MS
0	0	8.688	8.33	97.537	XOM_R2OWSG MWD+IFR1+MS
0	0	9.084	8.693	98.22	XOM_R2OWSG MWD+IFR1+MS
0	0	9.482	9.059	98.828	XOM_R2OWSG MWD+IFR1+MS
0	0	9.883	9.426	99.373	XOM_R2OWSG MWD+IFR1+MS
0	0	10.286	9.796	99.863	XOM_R2OWSG MWD+IFR1+MS
0	0	10.692	10.167	100.305	XOM_R2OWSG MWD+IFR1+MS
0	0	11.098	10.54	100.706	XOM_R2OWSG MWD+IFR1+MS
0	0	11.507	10.913	101.072	XOM_R2OWSG MWD+IFR1+MS
0	0	11.917	11.289	101.407	XOM_R2OWSG MWD+IFR1+MS
0	0	12.328	11.665	101.714	XOM_R2OWSG MWD+IFR1+MS
0	0	12.74	12.042	101.996	XOM_R2OWSG MWD+IFR1+MS
0	0	13.153	12.42	102.257	XOM_R2OWSG MWD+IFR1+MS
0	0	13.568	12.799	102.499	XOM_R2OWSG MWD+IFR1+MS
0	0	13.983	13.178	102.723	XOM_R2OWSG MWD+IFR1+MS

0	0	14.399	13.559	102.932 XOM_R2OWSG MWD+IFR1+MS
0	0	14.815	13.94	103.127 XOM_R2OWSG MWD+IFR1+MS
0	0	15.232	14.321	103.31 XOM_R2OWSG MWD+IFR1+MS
0	0	15.65	14.703	103.481 XOM_R2OWSG MWD+IFR1+MS
0	0	16.069	15.086	103.642 XOM_R2OWSG MWD+IFR1+MS
0	0	16.487	15.469	103.793 XOM_R2OWSG MWD+IFR1+MS
0	0	16.907	15.853	103.936 XOM_R2OWSG MWD+IFR1+MS
0	0	17.327	16.236	104.071 XOM_R2OWSG MWD+IFR1+MS
0	0	17.747	16.621	104.199 XOM_R2OWSG MWD+IFR1+MS
0	0	18.167	17.005	104.32 XOM_R2OWSG MWD+IFR1+MS
0	0	18.588	17.39	104.435 XOM_R2OWSG MWD+IFR1+MS
0	0	19.01	17.776	104.544 XOM_R2OWSG MWD+IFR1+MS
0	0	19.431	18.161	104.648 XOM_R2OWSG MWD+IFR1+MS
0	0	19.853	18.547	104.747 XOM_R2OWSG MWD+IFR1+MS
0	0	20.275	18.934	104.842 XOM_R2OWSG MWD+IFR1+MS
0	0	20.698	19.32	104.932 XOM_R2OWSG MWD+IFR1+MS
0	0	21.12	19.707	105.019 XOM_R2OWSG MWD+IFR1+MS
0	0	21.543	20.094	105.102 XOM_R2OWSG MWD+IFR1+MS
0	0	21.966	20.481	105.182 XOM_R2OWSG MWD+IFR1+MS
0	0	22.39	20.868	105.258 XOM_R2OWSG MWD+IFR1+MS
0	0	22.813	21.256	105.332 XOM_R2OWSG MWD+IFR1+MS

0	0	22.942	21.374	105.355 XOM_R2OWSG MWD+IFR1+MS
0	0	23.233	21.642	105.406 XOM_R2OWSG MWD+IFR1+MS
0	0	23.64	22.023	105.488 XOM_R2OWSG MWD+IFR1+MS
0	0	24.033	22.397	105.581 XOM_R2OWSG MWD+IFR1+MS
0	0	24.413	22.765	105.682 XOM_R2OWSG MWD+IFR1+MS
0	0	24.778	23.125	105.785 XOM_R2OWSG MWD+IFR1+MS
0	0	25.131	23.477	105.888 XOM_R2OWSG MWD+IFR1+MS
0	0	25.47	23.82	105.985 XOM_R2OWSG MWD+IFR1+MS
0	0	25.797	24.154	106.071 XOM_R2OWSG MWD+IFR1+MS
0	0	25.844	24.201	106.066 XOM_R2OWSG MWD+IFR1+MS
0	0	26.111	24.472	105.935 XOM_R2OWSG MWD+IFR1+MS
0	0	26.426	24.79	105.784 XOM_R2OWSG MWD+IFR1+MS
0	0	26.741	25.109	105.637 XOM_R2OWSG MWD+IFR1+MS
0	0	27.058	25.43	105.492 XOM_R2OWSG MWD+IFR1+MS
0	0	27.375	25.751	105.35 XOM_R2OWSG MWD+IFR1+MS
0	0	27.694	26.073	105.211 XOM_R2OWSG MWD+IFR1+MS
0	0	28.014	26.397	105.075 XOM_R2OWSG MWD+IFR1+MS
0	0	28.334	26.721	104.941 XOM_R2OWSG MWD+IFR1+MS
0	0	28.656	27.046	104.81 XOM_R2OWSG MWD+IFR1+MS
0	0	28.978	27.372	104.681 XOM_R2OWSG MWD+IFR1+MS
0	0	29.302	27.698	104.554 XOM_R2OWSG MWD+IFR1+MS

0	0	29.626	28.025	104.43 XOM_R2OWSG MWD+IFR1+MS
0	0	29.951	28.354	104.309 XOM_R2OWSG MWD+IFR1+MS
0	0	30.276	28.682	104.189 XOM_R2OWSG MWD+IFR1+MS
0	0	30.603	29.012	104.072 XOM_R2OWSG MWD+IFR1+MS
0	0	30.93	29.342	103.957 XOM_R2OWSG MWD+IFR1+MS
0	0	31.258	29.673	103.843 XOM_R2OWSG MWD+IFR1+MS
0	0	31.586	30.004	103.732 XOM_R2OWSG MWD+IFR1+MS
0	0	31.915	30.336	103.623 XOM_R2OWSG MWD+IFR1+MS
0	0	32.245	30.669	103.516 XOM_R2OWSG MWD+IFR1+MS
0	0	32.575	31.002	103.41 XOM_R2OWSG MWD+IFR1+MS
0	0	32.907	31.336	103.307 XOM_R2OWSG MWD+IFR1+MS
0	0	33.238	31.67	103.205 XOM_R2OWSG MWD+IFR1+MS
0	0	33.57	32.005	103.105 XOM_R2OWSG MWD+IFR1+MS
0	0	33.903	32.34	103.006 XOM_R2OWSG MWD+IFR1+MS
0	0	34.236	32.676	102.91 XOM_R2OWSG MWD+IFR1+MS
0	0	34.57	33.012	102.814 XOM_R2OWSG MWD+IFR1+MS
0	0	34.904	33.349	102.721 XOM_R2OWSG MWD+IFR1+MS
0	0	35.239	33.686	102.629 XOM_R2OWSG MWD+IFR1+MS
0	0	35.574	34.023	102.538 XOM_R2OWSG MWD+IFR1+MS
0	0	35.91	34.361	102.449 XOM_R2OWSG MWD+IFR1+MS
0	0	36.246	34.7	102.362 XOM_R2OWSG MWD+IFR1+MS

0	C	36.5	i82	35.038	102.275	XOM_R2OWSG MWD+IFR1+MS
0	C	36.9)19	35.377	102.191	XOM_R2OWSG MWD+IFR1+MS
0	C	37.2	157	35.717	102.107	XOM_R2OWSG MWD+IFR1+MS
0	C) 37.5	94	36.057	102.025	XOM_R2OWSG MWD+IFR1+MS
0	C	37.9)33	36.397	101.944	XOM_R2OWSG MWD+IFR1+MS
0	C	38.2	271	36.738	101.864	XOM_R2OWSG MWD+IFR1+MS
0	C) 38	.61	37.078	101.786	XOM_R2OWSG MWD+IFR1+MS
0	C	38.9	949	37.42	101.709	XOM_R2OWSG MWD+IFR1+MS
0	C	39.0)46	37.517	101.687	XOM_R2OWSG MWD+IFR1+MS
0	C	39.2	179	37.755	101.656	XOM_R2OWSG MWD+IFR1+MS
0	C) 39	.59	38.077	101.641	XOM_R2OWSG MWD+IFR1+MS
0	C	39.8	388	38.39	101.672	XOM_R2OWSG MWD+IFR1+MS
0	C) 40.1	.66	38.691	101.859	XOM_R2OWSG MWD+IFR1+MS
0	C) 40.4	¥16	38.976	102.333	XOM_R2OWSG MWD+IFR1+MS
0	C) 40.6	35	39.241	103.252	XOM_R2OWSG MWD+IFR1+MS
0	C) 40.8	322	39.482	104.795	XOM_R2OWSG MWD+IFR1+MS
0	C) 40.9	179	39.694	107.146	XOM_R2OWSG MWD+IFR1+MS
0	C) 41.1	.13	39.871	110.433	XOM_R2OWSG MWD+IFR1+MS
0	C) 41.2	232	40.005	114.587	XOM_R2OWSG MWD+IFR1+MS
0	C) 41.3	449	40.09	119.195	XOM_R2OWSG MWD+IFR1+MS
0	C) 41.4	113	40.113	121.581	XOM_R2OWSG MWD+IFR1+MS

0	0	41.472	40.126	123.574 XOM_R2OWSG MWD+IFR1+MS
0	0	41.613	40.155	127.711 XOM_R2OWSG MWD+IFR1+MS
0	0	41.774	40.182	131.51 XOM_R2OWSG MWD+IFR1+MS
0	0	41.956	40.208	134.956 XOM_R2OWSG MWD+IFR1+MS
0	0	42.158	40.231	-41.943 XOM_R2OWSG MWD+IFR1+MS
0	0	42.38	40.253	-39.165 XOM_R2OWSG MWD+IFR1+MS
0	0	42.62	40.274	-36.681 XOM_R2OWSG MWD+IFR1+MS
0	0	42.878	40.294	-34.46 XOM_R2OWSG MWD+IFR1+MS
0	0	43.154	40.313	-32.471 XOM_R2OWSG MWD+IFR1+MS
0	0	43.447	40.332	-30.684 XOM_R2OWSG MWD+IFR1+MS
0	0	43.757	40.351	-29.075 XOM_R2OWSG MWD+IFR1+MS
0	0	44.083	40.369	-27.619 XOM_R2OWSG MWD+IFR1+MS
0	0	44.424	40.388	-26.299 XOM_R2OWSG MWD+IFR1+MS
0	0	44.78	40.406	-25.098 XOM_R2OWSG MWD+IFR1+MS
0	0	45.152	40.425	-24 XOM_R2OWSG MWD+IFR1+MS
0	0	45.537	40.445	-22.993 XOM_R2OWSG MWD+IFR1+MS
0	0	45.937	40.464	-22.067 XOM_R2OWSG MWD+IFR1+MS
0	0	46.35	40.484	-21.213 XOM_R2OWSG MWD+IFR1+MS
0	0	46.776	40.505	-20.423 XOM_R2OWSG MWD+IFR1+MS
0	0	47.215	40.526	-19.69 XOM_R2OWSG MWD+IFR1+MS
0	0	47.666	40.547	-19.009 XOM_R2OWSG MWD+IFR1+MS

0	0	48.13	40.569	-18.373 XOM_R2OWSG MWD+IFR1+MS
0	0	48.605	40.592	-17.779 XOM_R2OWSG MWD+IFR1+MS
0	0	49.091	40.615	-17.223 XOM_R2OWSG MWD+IFR1+MS
0	0	49.588	40.638	-16.701 XOM_R2OWSG MWD+IFR1+MS
0	0	50.096	40.662	-16.21 XOM_R2OWSG MWD+IFR1+MS
0	0	50.614	40.687	-15.747 XOM_R2OWSG MWD+IFR1+MS
0	0	51.142	40.712	-15.311 XOM_R2OWSG MWD+IFR1+MS
0	0	51.68	40.738	-14.899 XOM_R2OWSG MWD+IFR1+MS
0	0	52.227	40.765	-14.508 XOM_R2OWSG MWD+IFR1+MS
0	0	52.783	40.792	-14.138 XOM_R2OWSG MWD+IFR1+MS
0	0	53.348	40.82	-13.787 XOM_R2OWSG MWD+IFR1+MS
0	0	53.921	40.848	-13.453 XOM_R2OWSG MWD+IFR1+MS
0	0	54.502	40.877	-13.135 XOM_R2OWSG MWD+IFR1+MS
0	0	55.092	40.907	-12.832 XOM_R2OWSG MWD+IFR1+MS
0	0	55.689	40.937	-12.544 XOM_R2OWSG MWD+IFR1+MS
0	0	56.294	40.968	-12.268 XOM_R2OWSG MWD+IFR1+MS
0	0	56.906	40.999	-12.004 XOM_R2OWSG MWD+IFR1+MS
0	0	57.524	41.031	-11.752 XOM_R2OWSG MWD+IFR1+MS
0	0	58.15	41.064	-11.51 XOM_R2OWSG MWD+IFR1+MS
0	0	58.782	41.097	-11.278 XOM_R2OWSG MWD+IFR1+MS
0	0	59.421	41.131	-11.056 XOM_R2OWSG MWD+IFR1+MS

0	0	60.065	41.166	-10.842	XOM_R2OWSG MWD+IFR1+MS
0	0	60.716	41.201	-10.637	XOM_R2OWSG MWD+IFR1+MS
0	0	61.372	41.236	-10.439	XOM_R2OWSG MWD+IFR1+MS
0	0	62.034	41.273	-10.249	XOM_R2OWSG MWD+IFR1+MS
0	0	62.701	41.31	-10.066	XOM_R2OWSG MWD+IFR1+MS
0	0	63.374	41.347	-9.889	XOM_R2OWSG MWD+IFR1+MS
0	0	64.051	41.386	-9.719	XOM_R2OWSG MWD+IFR1+MS
0	0	64.734	41.424	-9.555	XOM_R2OWSG MWD+IFR1+MS
0	0	65.421	41.464	-9.396	XOM_R2OWSG MWD+IFR1+MS
0	0	66.113	41.504	-9.243	XOM_R2OWSG MWD+IFR1+MS
0	0	66.809	41.544	-9.094	XOM_R2OWSG MWD+IFR1+MS
0	0	67.509	41.586	-8.951	XOM_R2OWSG MWD+IFR1+MS
0	0	68.214	41.628	-8.812	XOM_R2OWSG MWD+IFR1+MS
0	0	68.923	41.67	-8.677	XOM_R2OWSG MWD+IFR1+MS
0	0	69.636	41.713	-8.547	XOM_R2OWSG MWD+IFR1+MS
0	0	70.352	41.757	-8.42	XOM_R2OWSG MWD+IFR1+MS
0	0	71.072	41.801	-8.298	XOM_R2OWSG MWD+IFR1+MS
0	0	71.796	41.846	-8.179	XOM_R2OWSG MWD+IFR1+MS
0	0	72.523	41.891	-8.063	XOM_R2OWSG MWD+IFR1+MS
0	0	73.254	41.937	-7.951	XOM_R2OWSG MWD+IFR1+MS
0	0	73.988	41.984	-7.842	XOM_R2OWSG MWD+IFR1+MS

0	0	74.725	42.031	-7.736	XOM_R2OWSG MWD+IFR1+MS
0	0	75.465	42.079	-7.633	XOM_R2OWSG MWD+IFR1+MS
0	0	76.208	42.127	-7.533	XOM_R2OWSG MWD+IFR1+MS
0	0	76.954	42.176	-7.435	XOM_R2OWSG MWD+IFR1+MS
0	0	77.703	42.225	-7.34	XOM_R2OWSG MWD+IFR1+MS
0	0	78.454	42.276	-7.248	XOM_R2OWSG MWD+IFR1+MS
0	0	79.208	42.326	-7.158	XOM_R2OWSG MWD+IFR1+MS
0	0	79.965	42.377	-7.07	XOM_R2OWSG MWD+IFR1+MS
0	0	80.725	42.429	-6.984	XOM_R2OWSG MWD+IFR1+MS
0	0	81.486	42.482	-6.901	XOM_R2OWSG MWD+IFR1+MS
0	0	82.251	42.535	-6.819	XOM_R2OWSG MWD+IFR1+MS
0	0	83.017	42.588	-6.74	XOM_R2OWSG MWD+IFR1+MS
0	0	83.786	42.642	-6.662	XOM_R2OWSG MWD+IFR1+MS
0	0	84.557	42.697	-6.586	XOM_R2OWSG MWD+IFR1+MS
0	0	85.33	42.752	-6.512	XOM_R2OWSG MWD+IFR1+MS
0	0	86.105	42.808	-6.44	XOM_R2OWSG MWD+IFR1+MS
0	0	86.882	42.864	-6.369	XOM_R2OWSG MWD+IFR1+MS
0	0	87.661	42.921	-6.3	XOM_R2OWSG MWD+IFR1+MS
0	0	88.442	42.978	-6.233	XOM_R2OWSG MWD+IFR1+MS
0	0	89.225	43.036	-6.167	XOM_R2OWSG MWD+IFR1+MS
0	0	90.009	43.095	-6.102	XOM_R2OWSG MWD+IFR1+MS

0	0	90.796	43.154	-6.039 XOM_R2OWSG MWD+IFR1+MS
0	0	91.584	43.213	-5.977 XOM_R2OWSG MWD+IFR1+MS
0	0	92.373	43.273	-5.917 XOM_R2OWSG MWD+IFR1+MS
0	0	93.165	43.334	-5.858 XOM_R2OWSG MWD+IFR1+MS
0	0	93.958	43.395	-5.8 XOM_R2OWSG MWD+IFR1+MS
0	0	94.752	43.457	-5.743 XOM_R2OWSG MWD+IFR1+MS
0	0	95.548	43.519	-5.687 XOM_R2OWSG MWD+IFR1+MS
0	0	96.346	43.582	-5.633 XOM_R2OWSG MWD+IFR1+MS
0	0	97.145	43.645	-5.579 XOM_R2OWSG MWD+IFR1+MS
0	0	97.945	43.709	-5.527 XOM_R2OWSG MWD+IFR1+MS
0	0	98.747	43.773	-5.475 XOM_R2OWSG MWD+IFR1+MS
0	0	99.55	43.838	-5.425 XOM_R2OWSG MWD+IFR1+MS
0	0	100.354	43.904	-5.375 XOM_R2OWSG MWD+IFR1+MS
0	0	101.16	43.97	-5.327 XOM_R2OWSG MWD+IFR1+MS
0	0	101.967	44.036	-5.279 XOM_R2OWSG MWD+IFR1+MS
0	0	102.775	44.103	-5.233 XOM_R2OWSG MWD+IFR1+MS
0	0	103.584	44.17	-5.187 XOM_R2OWSG MWD+IFR1+MS
0	0	104.395	44.238	-5.142 XOM_R2OWSG MWD+IFR1+MS
0	0	105.206	44.307	-5.098 XOM_R2OWSG MWD+IFR1+MS
0	0	106.019	44.375	-5.054 XOM_R2OWSG MWD+IFR1+MS
0	0	106.833	44.445	-5.011 XOM_R2OWSG MWD+IFR1+MS

0	0	107.648	44.515	-4.97 XOM_R2OWSG MWD+IFR1+MS
0	0	108.463	44.585	-4.928 XOM_R2OWSG MWD+IFR1+MS
0	0	109.28	44.656	-4.888 XOM_R2OWSG MWD+IFR1+MS
0	0	110.098	44.727	-4.848 XOM_R2OWSG MWD+IFR1+MS
0	0	110.917	44.799	-4.809 XOM_R2OWSG MWD+IFR1+MS
0	0	111.737	44.872	-4.771 XOM_R2OWSG MWD+IFR1+MS
0	0	112.557	44.944	-4.733 XOM_R2OWSG MWD+IFR1+MS
0	0	113.379	45.018	-4.696 XOM_R2OWSG MWD+IFR1+MS
0	0	114.201	45.092	-4.659 XOM_R2OWSG MWD+IFR1+MS
0	0	115.025	45.166	-4.623 XOM_R2OWSG MWD+IFR1+MS
0	0	115.849	45.24	-4.588 XOM_R2OWSG MWD+IFR1+MS
0	0	116.674	45.316	-4.553 XOM_R2OWSG MWD+IFR1+MS
0	0	117.499	45.391	-4.519 XOM_R2OWSG MWD+IFR1+MS
0	0	118.326	45.467	-4.485 XOM_R2OWSG MWD+IFR1+MS
0	0	119.153	45.544	-4.452 XOM_R2OWSG MWD+IFR1+MS
0	0	120.037	45.626	-4.417 XOM_R2OWSG MWD+IFR1+MS
0	0	120.45	45.665	-4.401 XOM_R2OWSG MWD+IFR1+MS

ALL DIMENSIONS APPROXIMA

CACTUS WELLHEAD LLC

(20") x 13-3/8" x 9-5/8" x 7-5/8" x 5-1/2" MBU-4T-CFL-R-DBLO With 13-5/8" 10M x 7-1/16" 15M CTH-DBLHPS-SB Tubing Head And Drilling & Skid Configurations

XTO ENERGY INC DELAWARE BASIN					
RAWN	VJK	31MAF			

DRAWING NO.

SDT-3301

FORMATION CONTAINED HEREIN IS THE PROPERTY OF CACTUS WELLHEAD, LLC. REPRODUCTION, SCLOSURE, OR USE THEREOF IS PERMISSIBLE ONLY AS PROVIDED BY CONTRACT OR AS EXPRESSLY SUTHORIZED BY CACTUS WELLHEAD, LLC.

Served by OCD: 10/31/2023 1:30:22

Cement Variance Request

XTO requests to pump a two stage cement job on the 7-5/8" intermediate casing string with the first stage being pumped conventionally with the calculated top of cement at the Brushy Canyon (6452') and the second stage performed as a bradenhead squeeze with planned cement from the Brushy Canyon to surface. If cement is not visually confirmed to circulate to surface, the final cement top after the second stage job will be verified by Echo-meter. If necessary, a top out consisting of 1,500 sack of Class C cement + 3% Salt + 1% PreMag-M + 6% Bentonite Gel (2.30 yld, 12.91 ppg) will be executed as a contingency. If cement is still unable to circulate to surface, another Echo-meter run will be performed for cement top verification.

XTO will include the Echo-meter verified fluid top and the volume of displacement fluid above the cement slurry in the annulus in all post-drill sundries on wells utilizing this cement program.

XTO will report to the BLM the volume of fluid (limited to 5 bbls) used to flush intermediate casing valves following backside cementing procedures.

XTO requests to pump an Optional Lead if well conditions dictate in an attempt to bring cement to surface on the first stage. If cement is brought to surface, the BLM will be notified and the second stage bradenhead squeeze and subsequent TOC verification will be negated.

In the event cement is not circulated to surface on the first stage, whether intentionally or unintentionally, XTO requests the option to conduct the bradenhead squeeze and TOC verification offline as per standard approval from BLM when unplanned remediation is needed and batch drilling is approved. In the event the bradenhead is conducted, we will ensure first stage cement job is cemented properly and the well is static with floats holding and no pressure on the csg annulus as with all other casing strings where batch drilling operations occur before moving off the rig. The TA cap will also be installed per GE procedure and pressure inside the casing will be monitored via the valve on the TA cap as per standard batch drilling ops.

Subject: Request for a Variance Allowing break Testing of the Blowout Preventer Equipment (BOPE)

XTO Energy requests a variance to ONLY test broken pressure seals on the BOPE and function test BOP when skidding a drilling rig between multiple wells on a pad.

Background

Onshore Oil and Gas Order (OOGO) No. 2, Drilling Operations, Sections III.A.2.i.iv.B states that the BOP test must be performed whenever any seal subject to test pressure is broken. The current interpretation of the Bureau of Land Management (BLM) requires a complete BOP test and not just a test of the affected component. OOGO No. 2, Section I.D.2 states, "Some situation may exist either on a well-by-well basis or field-wide basis whereby it is commonly accepted practice to vary a particular minimum standard(s) established in this order. This situation can be resolved by requesting a variance...". XTO Energy feels the break testing the BOPE is such a situation. Therefore, as per OOGO No. 2, Section IV., XTO Energy submits this request for the variance.

Supporting Documentation

OOGO No. 2 became effective on December 19, 1988 and has remained the standard for regulating BLM onshore drilling operations for over 30 years. During this time there have been significant changes in drilling technology. BLM continues to use the variance request process to allow for the use of modern technology and acceptable engineering practices that have arisen since OOGO No. 2 was originally released. The XTO Energy drilling rig fleet has many modern upgrades that allow the intact BOP stack to be moved between well slots on a multi-well pad, as well as, wellhead designs that incorporate quick connects facilitating release of the BOP from the wellhead without breaking any BOP stack components apart. These technologies have been used extensively offshore, and other regulators, API, and many operators around the world have endorsed break testing as safe and reliable.



Figure 1: Winch System attached to BOP Stack



Figure 2: BOP Winch System

American Petroleum Institute (API) standards, specification and recommended practices are considered the industry standard and are consistently utilized and referenced by the industry. OOGO No. 2 recognizes API recommended Practices (RP) 53 in its original development. API Standard 53, *Well Control Equipment Systems for Drilling Wells* (Fifth Edition, December 2018, Annex C, Table C.4) recognizes break testing as an acceptable practice. Specifically, API Standard 53, Section 5.3.7.1 states "A pressure test of the pressure containing component shall be performed following the disconnection or repair, limited to the affected component." See Table C.4 below for reference.

		Pressure Test—High Pressureac	
Component to be Pressure Tested	Pressure Test—Low Pressure ^{ac} psig (MPa)	Change Out of Component, Elastomer, or Ring Gasket	No Change Out of Component, Elastomer, or Ring Gasket
nnular preventer ^b	250 to 350 (1.72 to 2.41)	RWP of annular preventer	MASP or 70% annular RWP, whichever is lower.
ixed pipe, variable bore, lind, and BSR preventers ^{bd}	250 to 350 (1.72 to 2.41)	RWP of ram preventer or wellhead system, whichever is lower	ITP
choke and kill line and BOP ide outlet valves below ram reventers (both sides)	250 to 350 (1.72 to 2.41)	RWP of side outlet valve or wellhead system, whichever is lower	ITP
choke manifold—upstream of hokes ^e	250 to 350 (1.72 to 2.41)	RWP of ram preventers or wellhead system, whichever is lower	ITP
hoke manifold—downstream f chokese	250 to 350 (1.72 to 2.41)	RWP of valve(s), line(s), or MASP for the well program, whichever is lower	
elly, kelly valves, drill pipe afety valves, IBOPs	250 to 350 (1.72 to 2.41)	MASP for the well program	
No visible leaks. The pressure shall remain stab	37 No. 10	pressure shall not decrease below the	•

The Bureau of Safety and Environmental Enforcement (BSEE), Department of Interior, has also utilized the API standards, specification and best practices in the development of its offshore oil and gas regulations and incorporates them by reference within its regulations.

Break testing has been approved by the BLM in the past with other operators based on the detailed information provided in this document.

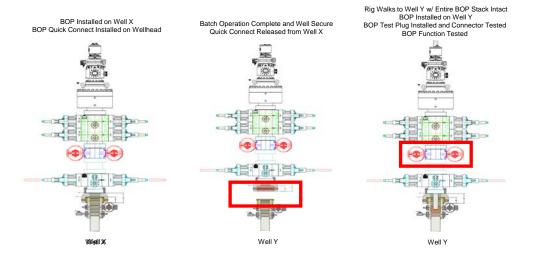
XTO Energy feels break testing and our current procedures meet the intent of OOGO No. 2 and often exceed it. There has been no evidence that break testing results in more components failing than seen on full BOP tests. XTO Energy's internal standards requires complete BOPE tests more often than that of OOGO No. 2 (Every 21 days). In addition to function testing the annular, pipe rams and blind rams after each BOP nipple up, XTO Energy performs a choke drill with the rig crew prior to drilling out every casing shoe. This is additional training for the rig crew that exceeds the requirements of the OOGO No. 2.

Procedures

- XTO Energy will use this document for our break testing plan for New Mexico Delaware basin.
 The summary below will be referenced in the APD or Sundry Notice and receive approval prior to implementing this variance.
- 2. XTO Energy will perform BOP break testing on multi-wells pads where multiple intermediate sections can be drilled and cased within the 21-day BOP test window.
 - a. A full BOP test will be conducted on the first well on the pad.
 - b. The first intermediate hole section drilled on the pad will be the deepest. All of the remaining hole sections will be the same depth or shallower.
 - i. Our Lower WC targets set the intermediate casing shoe no deeper than the Wolfcamp B.
 - ii. Our Upper WC targets set the intermediate casing shoe shallower than the Wolfcamp B.
 - c. A Full BOP test will be required if the intermediate hole section being drilled has a MASP over 5M.
 - d. A full BOP test will be required prior to drilling any production hole.
- 3. After performing a complete BOP test on the first well, the intermediate hole section will be drilled and cased, two breaks would be made on the BOP equipment.
 - a. Between the HCV valve and choke line connection
 - b. Between the BOP guick connect and the wellhead
- 4. The BOP is then lifted and removed from the wellhead by a hydraulic system.
- 5. After skidding to the next well, the BOP is moved to the wellhead by the same hydraulic system and installed.
- 6. The connections mentioned in 3a and 3b will then be reconnected.
- 7. Install test plug into the wellhead using test joint or drill pipe.
- 8. A shell test is performed against the upper pipe rams testing the two breaks.
- 9. The shell test will consist of a 250 psi low test and a high test to the value submitted in the APD or Sundry (e.g. 5,000 psi or 10,000psi).
- 10. Function test will be performed on the following components: lower pipe rams, blind rams, and annular.

- 11. For a multi-well pad the same two breaks on the BOP would be made and on the next wells and steps 4 through 10 would be repeated.
- 12. A second break test would only be done if the intermediate hole section being drilled could not be completed within the 21 day BOP test window.

Note: Picture below highlights BOP components that will be tested during batch operations



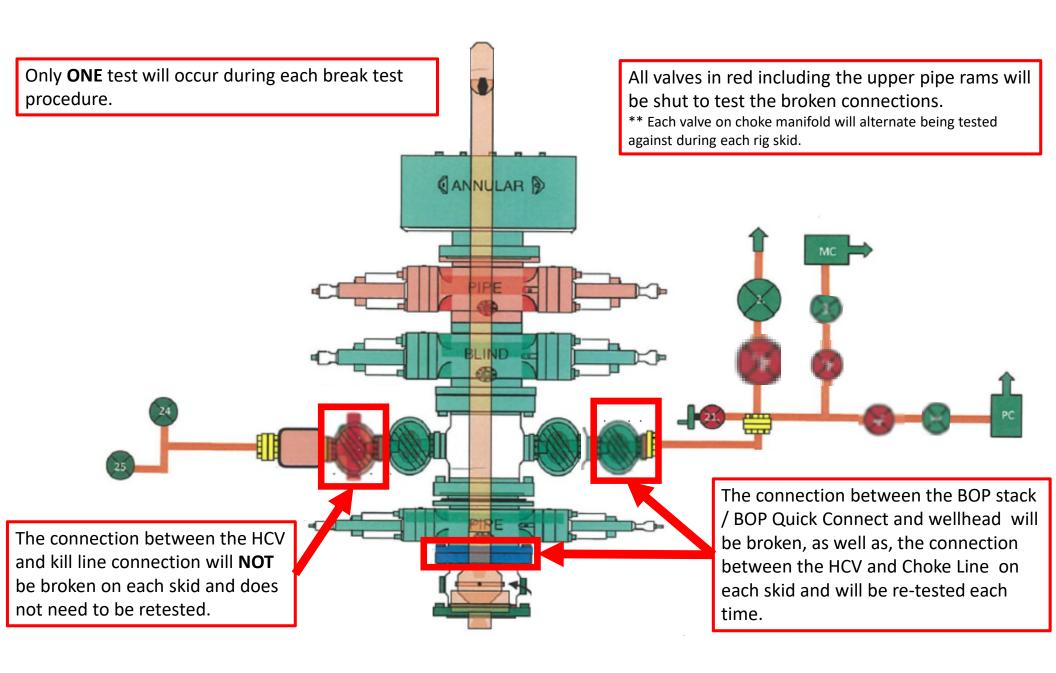
Summary

A variance is requested to **ONLY** test broken pressure seals on the BOP equipment when moving from wellhead to wellhead which is in compliance with API Standard 53. API Standard 53 states, that for pad drilling operation, moving from one wellhead to another within 21 days, pressure testing is required for pressure-containing and pressure-controlling connections when the integrity of a pressure seal is broken.

The BOP will be secured by a hydraulic carrier or cradle. The BLM will be contacted if a Well Control event occurs prior to the commencement of a BOPE Break Testing operation.

Based on discussions with the BLM on February 27th 2020 and the supporting documentation submitted to the BLM, we will request permission to ONLY retest broken pressure seals if the following conditions are met:

- 1. After a full BOP test is conducted on the first well on the pad.
- 2. The first intermediate hole section drilled on the pad will be the deepest. All of the remaining hole sections will be the same depth or shallower.
- 3. Full BOP test will be required if the intermediate hole section being drilled has a MASP over 5M.
- 4. Full BOP test will be required prior to drilling the production hole.



XTO Permian Operating, LLC Offline Cementing Variance Request

XTO requests the option to cement the surface and intermediate casing strings offline as a prudent batch drilling efficiency of acreage development.

1. Cement Program

No changes to the cement program will take place for offline cementing.

2. Offline Cementing Procedure

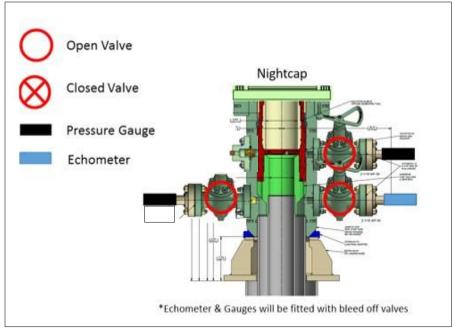
The operational sequence will be as follows. If a well control event occurs, the BLM will be contacted for approval prior to conducting offline cementing operations.

- 1. Run casing as per normal operations. While running casing, conduct negative pressure test and confirm integrity of the float equipment (float collar and shoe)
- 2. Land casing with mandrel
- 3. Fill pipe with kill weight fluid, do not circulate through floats and confirm well is static
- 4. Set annular packoff shown below and pressure test to confirm integrity of the seal. Pressure ratings of wellhead components and valves is 5,000 psi.
- 5. After confirmation of both annular barriers and internal barriers, nipple down BOP and install cap flange.
 - a. If any barrier fails to test, the BOP stack will not be nippled down until after the cement job is completed with cement 500ft above the highest formation capable of flow with kill weight mud above or after it has achieved 50-psi compressive strength if kill weight fluid cannot be verified.



Annular packoff with both external and internal seals

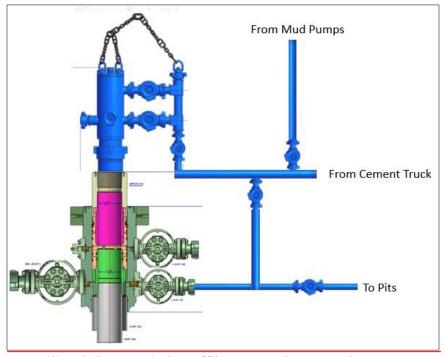
XTO Permian Operating, LLC Offline Cementing Variance Request



Wellhead diagram during skidding operations

- 6. Skid rig to next well on pad.
- 7. Confirm well is static before removing cap flange, flange will not be removed and offline cementing operations will not commence until well is under control. If well is not static, casing outlet valves will provide access to both the casing ID and annulus. Rig or third party pump truck will kill well prior to cementing or nippling up for further remediation.
 - a. Well Control Plan
 - i. The Drillers Method will be the primary well control method to regain control of the wellbore prior to cementing, if wellbore conditions do not permit the drillers method other methods of well control may be used
 - ii. Rig pumps or a 3rd party pump will be tied into the upper casing valve to pump down the casing ID
 - iii. A high pressure return line will be rigged up to lower casing valve and run to choke manifold to control annular pressure
 - iv. Once influx is circulated out of the hole, kill weight mud will be circulated
 - v. Well will be confirmed static
 - vi. Once confirmed static, cap flange will be removed to allow for offline cementing operations to commence
- 8. Install offline cement tool
- 9. Rig up cement equipment

XTO Permian Operating, LLC Offline Cementing Variance Request



Wellhead diagram during offline cementing operations

- 10. Circulate bottoms up with cement truck
 - a. If gas is present on bottoms up, well will be shut in and returns rerouted through gas buster to handle entrained gas
 - b. Max anticipated time before circulating with cement truck is 6 hrs
- 11. Perform cement job taking returns from the annulus wellhead valve
- 12. Confirm well is static and floats are holding after cement job
- 13. Remove cement equipment, offline cement tools and install night cap with pressure gauge for monitoring.

XTO respectfully requests approval to utilize a spudder rig to pre-set surface casing.

Description of Operations:

- 1. Spudder rig will move in to drill the surface hole and pre-set surface casing on the well.
 - a. After drilling the surface hole section, the spudder rig will run casing and cement following all of the applicable rules and regulations (OnShore Order 2, all COAs and NMOCD regulations).
 - b. The spudder rig will utilize fresh water-based mud to drill the surface hole to TD. Solids control will be handled entirely on a closed loop basis. No earth pits will be used.
- 2. The wellhead will be installed and tested as soon as the surface casing is cut off and WOC time has been reached.
- 3. A blind flange at the same pressure rating as the wellhead will be installed to seal the wellbore. Pressure will be monitored with needle valves installed on two wing valves.
 - a. A means for intervention will be maintained while the drilling rig is not over the well.
- 4. Spudder rig operations are expected to take 2-3 days per well on the pad.
- 5. The BLM will be contacted and notified 24 hours prior to commencing spudder rig operations.
- 6. Drilling Operations will begin with a larger rig and a BOP stack equal to or greater than the pressure rating that was permitted will be nippled up and tested on the wellhead before drilling operations resume on each well.
 - a. The larger rig will move back onto the location within 180 days from the point at which the wells are secured and the spudder rig is moved off location.
 - b. The BLM will be notified 24 hours before the larger rig moves back on the pre-set locations
- 7. XTO will have supervision on the rig to ensure compliance with all BLM and NMOCD regulations and to oversee operations.
- 8. Once the rig is removed, XTO will secure the wellhead area by placing a guard rail around the cellar area.

District I
1625 N. French Dr., Hobbs, NM 88240
Phone: (575) 393-6161 Fax: (575) 393-0720

District II 811 S. First St., Artesia, NM 88210 Phone:(575) 748-1283 Fax:(575) 748-9720

District III 1000 Rio Brazos Rd., Aztec, NM 87410 Phone:(505) 334-6178 Fax:(505) 334-6170

1220 S. St Francis Dr., Santa Fe, NM 87505 Phone:(505) 476-3470 Fax:(505) 476-3462

State of New Mexico Energy, Minerals and Natural Resources Oil Conservation Division 1220 S. St Francis Dr. **Santa Fe, NM 87505**

CONDITIONS

Action 281470

CONDITIONS

Note that the second se			
Operator:	OGRID:		
XTO PERMIAN OPERATING LLC.	373075		
6401 HOLIDAY HILL ROAD	Action Number:		
MIDLAND, TX 79707	281470		
	Action Type:		
	[C-103] NOI Change of Plans (C-103A)		

CONDITIONS

Created By	Condition	Condition Date
dmcclure	A CBL must be run for any string of casing for which cement did not circulate. This includes casing strings for which a "bradenhead squeeze" was performed.	11/22/2023
dmcclure	The entirety of the surface casing must have competent cement.	11/22/2023