Form 3160-5 (June 2019)

# UNITED STATES DEPARTMENT OF THE INTERIOR

FORM APPROVED
OMB No. 1004-0137
Expires: October 31, 202

BUR	EAU OF LAND MANAGEMENT		5. Lease Serial No.	NMNM90			
Do not use this t	IOTICES AND REPORTS ON W form for proposals to drill or to Use Form 3160-3 (APD) for suc	re-enter an	6. If Indian, Allottee or Tribe Name				
SUBMIT IN	TRIPLICATE - Other instructions on pag	e 2	7. If Unit of CA/Agree	eement, Name and/or No.			
1. Type of Well Gas W	Vell Other		8. Well Name and No	O. AMAZING 19 FED/801H			
2. Name of Operator EOG RESOURG	<del></del>		9. API Well No. 3002				
		(include area code)	10. Field and Pool or				
3a. Address 1111 BAGBY SKY LOB	(713) 651-70	'		n, Bone Spring South			
4. Location of Well (Footage, Sec., T., R SEC 19/T22S/R32E/NMP	2.,M., or Survey Description)		11. Country or Parish LEA/NM	ı, State			
12. CHE	CK THE APPROPRIATE BOX(ES) TO INI	DICATE NATURE OF NOT	TCE, REPORT OR OT	HER DATA			
TYPE OF SUBMISSION		TYPE OF AC	CTION				
✓ Notice of Intent	Acidize Deep Alter Casing Hydr	_	duction (Start/Resume)	Water Shut-Off Well Integrity			
Cubecquent Depart		_	complete	Other			
Subsequent Report	Change Plans Plug	and Abandon Ten	nporarily Abandon	<del></del>			
Final Abandonment Notice	Convert to Injection Plug	Back Wat	ter Disposal				
completion of the involved operation completed. Final Abandonment Notice is ready for final inspection.)  EOG respectfully requests and the following changes:  Amazing 19 Fed 402H (FKA 8)  Change name from Amazing 1  Change SHL from T-22-S, R-3 to T-22-S, R-32-E, Sec 19, 43  Change BHL from T-22-S, R-3 to T-22-S, R-32-E, Sec 30, 100 Continued on page 3 additional	19 Fed 801H to Amazing 19 Fed 402H. 32-E, Sec 19, 371' FNL, 1359' FEL, Lea 1' FNL, 1270' FEL, Lea Co., N.M. 32-E, Sec 30, 100' FSL, 660' FEL, Lea C 0' FSL, 440' FEL, Lea Co., N.M.	npletion or recompletion in a s, including reclamation, has s well to reflect  Co., NM,	a new interval, a Form 3	3160-4 must be filed once testing has been			
14. I nereby certify that the foregoing is	true and correct. Name (Printed/Typea)	Regulatory Special	list				
(Electronic Submissic	on)	Date	11/01/2	2023			
	THE SPACE FOR FED	ERAL OR STATE O	FICE USE				
Approved by							
CHRISTOPHER WALLS / Ph: (575	5) 234-2234 / Approved	Petroleum En Title	gineer	11/22/2023 Date			
	hed. Approval of this notice does not warran equitable title to those rights in the subject le duct operations thereon.		)				

Title 18 U.S.C Section 1001 and Title 43 U.S.C Section 1212, make it a crime for any person knowingly and willfully to make to any department or agency of the United States any false, fictitious or fraudulent statements or representations as to any matter within its jurisdiction.

(Instructions on page 2)

DISTRICT IV

DISTRICT I
1623 N French Dr., Hobbs, NM 88240
Phone: (575) 393-6161 Fax: (575) 393-0720
DISTRICT II
811 S First St., Artesia, NM 88210
Phone: (575) 748-1283 Fax: (575) 748-9720
DISTRICT III
100 Riso Bayon Rd., Artes NM 87410

1220 S. St. Francis Dr., Santa Fe, NM 87505 Phone: (505) 476-3460 Fax: (505) 476-3462

# State of New Mexico Energy, Minerals & Natural Resources Department OIL CONSERVATION DIVISION 1220 South St. Francis Dr. Santa Fe, New Mexico 87505

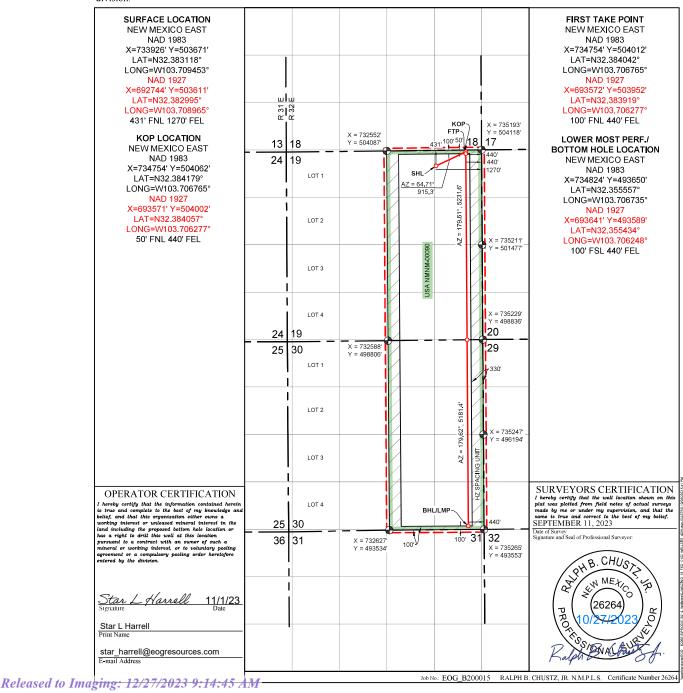
Form C-102 Revised August 1, 2011 Submit one copy to appropriate District Office

☐ AMENDED REPORT

#### WELL LOCATION AND ACREAGE DEDICATION PLAT

30 <b>-</b> 025 <b>-</b> 52	PI Number 2074			Pool Code <b>97366</b>		Pool Name Bilbrey Basin; Bone Spring, South				
	Property Code         Property Name           333115         AMAZING 19 FED						Well Number 402H			
							Elevation 3652'			
	Surface Location									
UL or lot no.	Section	Township	Range	Lot Idn	Feet from the	North/South line	Feet from the	East/West line	County	
Α	19	22 S	32 E 43		431	NORTH	1270	EAST	LEA	
	Bottom Hole Location If Different From Surface									
UL or lot no.	Section	Township	Range	Lot Idn	Feet from the	North/South line	Feet from the	East/West line	County	
Р	30	22 S	32 E		100	SOUTH	440	EAST	LEA	
Dedicated Acres	Joint or	Infill	Consolidated Cod	le Orde	Order No.  LEASE WELL					

No allowable will be assigned to this completion until all interests have been consolidated or a non-standard unit has been approved by the division





#### **Revised Permit Information 10/24/2023:**

Well Name: Amazing 19 Fed 402H

Location: SHL: 431' FNL & 1270' FEL, Section 19, T-22-S, R-32-E, Lea Co., N.M.

BHL: 100' FSL & 440' FEL, Section 30, T-22-S, R-32-E, Lea Co., N.M.

**Casing Program A:** 

Hole	Interv	al MD	Interval TVD		Csg			
Size	From (ft)	To (ft)	From (ft)	To (ft)	OD	Weight	Grade	Conn
16"	0	940	0	940	13-3/8"	54.5#	J-55	STC
11"	0	5,225	0	5,140	9-5/8"	40#	J-55	LTC
6-3/4"	0	20,377	0	10,093	5-1/2"	17#	HCP-110	LTC

Variance is requested to waive the centralizer requirements for the 9-5/8" casing in the 11" hole size. An expansion additive will be utilized, in the cement slurry, for the entire length of the 11" hole interval to maximize cement bond and zonal isolation.

Variance is also requested to waive any centralizer requirements for the 5-1/2" casing in the 6-3/4" hole size. An expansion additive will be utilized, in the cement slurry, for the entire length of the 6-3/4" hole interval to maximize cement bond and zonal isolation.

EOG requests permission to allow deviation from the 0.422" annulus clearance requirement for the intermediate (salt) section from Onshore Order #2 under the following conditions:

- The variance is not applicable within the Potash Boundaries or Capitan Reef areas.
- Operator takes responsibility to get casing to set point in the event that the clearance causes stuck pipe issues.

**Cementing Program:** 

Ctint	mung rros	51 4111.		
Depth	No. Sacks	Wt.	Yld Ft3/sk	Slurry Description
940'	240	13.5	1.73	Lead: Class C + 4.0% Bentonite Gel + 0.5% CaCl2 + 0.25 lb/sk Cello-Flake (TOC @ Surface)
	160	14.8	1.34	Tail: Class C + 0.6% FL-62 + 0.25 lb/sk Cello-Flake + 0.2% Sodium Metasilicate (TOC @ 740')
5,140' 9-5/8"	470	12.7	2.22	Lead: Class C + 10% NaCl + 6% Bentonite Gel + 3% MagOx (TOC @ Surface)
	100	14.8	1.32	Tail: Class C + 10% NaCL + 3% MagOx (TOC @ 4,110')
20,377' 5-1/2"	300	10.5	3.21	Lead: Class H + 0.4% Halad-344 + 0.35% HR-601 + 3% Microbond (TOC @ 4,410')
	750	13.2	1.52	Tail: Class H + 5% NEX-020 + 0.2% NAC-102 + 0.15% NAS-725 + 0.5% NFL-549 + 0.2% NFP-703 + 1% NBE-737 + 0.3% NRT-241 (TOC @ 9700')



Additive	Purpose
Bentonite Gel	Lightweight/Lost circulation prevention
Calcium Chloride	Accelerator
Cello-flake	Lost circulation prevention
Sodium Metasilicate	Accelerator
MagOx	Expansive agent
Pre-Mag-M	Expansive agent
Sodium Chloride	Accelerator
FL-62	Fluid loss control
Halad-344	Fluid loss control
Halad-9	Fluid loss control
HR-601	Retarder
Microbond	Expansive Agent

Note: Cement volumes based on bit size plus at least 25% excess in the open hole plus 10% excess in the cased-hole overlap section.

#### **Mud Program:**

Depth (TVD)	Type	Type Weight (ppg)		Water Loss
0 – 940'	Fresh - Gel	8.6-8.8	28-34	N/c
940' - 5,140'	Brine	8.6-8.8	28-34	N/c
5,140' - 20,377'	Oil Base	8.8-9.5	58-68	N/c - 6



#### **TUBING REQUIREMENTS**

EOG respectively requests an exception to the following NMOCD rule:

• 19.15.16.10 Casing AND TUBING RQUIREMENTS:

J (3): "The operator shall set tubing as near the bottom as practical and tubing perforations shall not be more than 250 feet above top of pay zone."

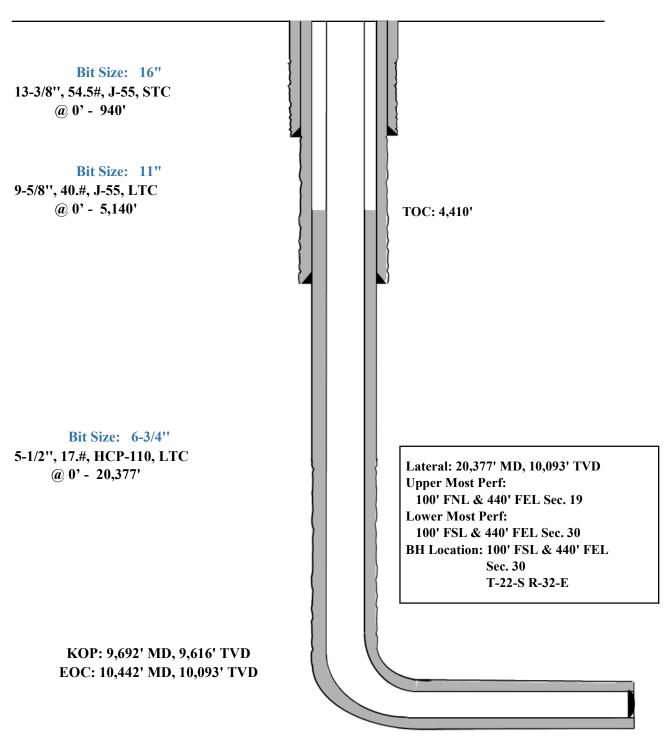
With horizontal flowing and gas lifted wells an end of tubing depth placed at or slightly above KOP is a conservative way to ensure the tubing stays clean from debris, plugging, and allows for fewer well interventions post offset completion. The deeper the tubulars are run into the curve, the higher the probability is that the tubing will become stuck in sand and or well debris as the well produces over time. An additional consideration for EOT placement during artificial lift installations is avoiding the high dog leg severity and inclinations found in the curve section of the wellbore to help improve reliability and performance. Dog leg severity and inclinations tend not to hamper gas lifted or flowing wells, but they do effect other forms of artificial lift like rod pump or ESP (electric submersible pump). Keeping the EOT above KOP is an industry best practice for those respective forms of artificial lift.



431' FNL Revised Wellbore A: KB: 3677' 1270' FEL GL: 3652'

**Section 19** 

T-22-S, R-32-E API: 30-025-52074





#### Revised Permit Information 10/24/2023:

Well Name: Amazing 19 Fed 402H

Location: SHL: 431' FNL & 1270' FEL, Section 19, T-22-S, R-32-E, Lea Co., N.M.

BHL: 100' FSL & 440' FEL, Section 30, T-22-S, R-32-E, Lea Co., N.M.

**Casing Program B:** 

Hole	Interv	al MD	Interval TVD		Csg			
Size	From (ft)	To (ft)	From (ft)	To (ft)	OD	Weight	Grade	Conn
13-1/2"	0	940	0	940	10-3/4"	40.5#	J-55	STC
9-7/8"	0	5,225	0	5,140	8-5/8"	32#	J-55	BTC-SC
6-3/4"	0	20,377	0	10,093	5-1/2"	17#	HCP-110	LTC

**Cementing Program:** 

Depth	No. Sacks	Wt.	Yld Ft3/sk	Slurry Description
940'	320	13.5	1.73	Lead: Class C + 4.0% Bentonite Gel + 0.5% CaCl2 + 0.25 lb/sk Cello- Flake (TOC @ Surface)
	110	14.8	1.34	Tail: Class C + 0.6% FL-62 + 0.25 lb/sk Cello-Flake + 0.2% Sodium Metasilicate (TOC @ 740')
5,140' 8-5/8''	410	12.7	2.22	Lead: Class C + 10% NaCl + 6% Bentonite Gel + 3% MagOx (TOC @ Surface)
	650	14.8	1.32	Tail: Class C + 10% NaCL + 3% MagOx (TOC @ 4,110')
20,377 <sup>'</sup> 5-1/2''	480	10.5	3.21	Lead: Class H + 0.4% Halad-344 + 0.35% HR-601 + 3% Microbond (TOC @ 4,410')
	1040	13.2	1.52	Tail: Class H + 5% NEX-020 + 0.2% NAC-102 + 0.15% NAS-725 + 0.5% NFL-549 + 0.2% NFP-703 + 1% NBE-737 + 0.3% NRT-241 (TOC @ 9700')



Variance is requested to waive the centralizer requirements for the 8-5/8" casing in the 9-7/8" hole size. An expansion additive will be utilized, in the cement slurry, for the entire length of the 9-7/8" hole interval to maximize cement bond and zonal isolation.

Variance is also requested to waive any centralizer requirements for the 5-1/2" casing in the 6-3/4" hole size. An expansion additive will be utilized, in the cement slurry, for the entire length of the 6-3/4" hole interval to maximize cement bond and zonal isolation.

EOG requests permission to allow deviation from the 0.422" annulus clearance requirement for the intermediate (salt) section from Onshore Order #2 under the following conditions:

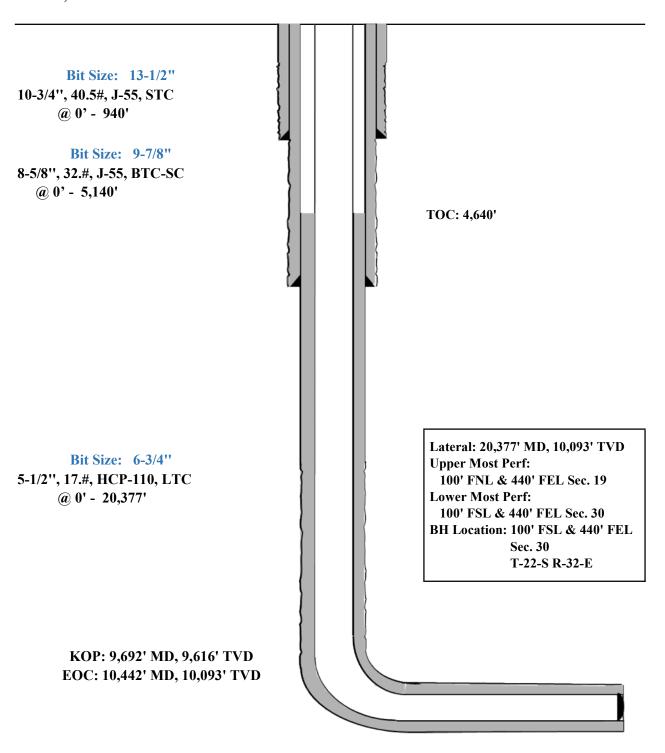
- The variance is not applicable within the Potash Boundaries or Capitan Reef areas.
- Operator takes responsibility to get casing to set point in the event that the clearance causes stuck pipe issues.



431' Revised Wellbore B: KB: 3677' 1270' GL: 3652'

**Section 19** 

T-22-S, R-32-E API: 30-025-52074





#### GEOLOGIC NAME OF SURFACE FORMATION:

Permian

#### ESTIMATED TOPS OF IMPORTANT GEOLOGICAL MARKERS:

Rustler	831'
Tamarisk Anhydrite	912'
Top of Salt	1,168'
Base of Salt	4,808'
Lamar	5,044'
Bell Canyon	5,071'
Cherry Canyon	6,102'
Brushy Canyon	8,095'
Bone Spring Lime	9,240'
Leonard (Avalon) Shale	9,313'
1st Bone Spring Sand	10,191'
2nd Bone Spring Shale	10,355'
2nd Bone Spring Sand	10,727'
3rd Bone Spring Carb	11,164'
3rd Bone Spring Sand	11,814'
Wolfcamp	12,238'
Penn	14,391'
<del></del>	

#### ESTIMATED DEPTHS OF ANTICIPATED FRESH WATER, OIL OR GAS:

Upper Permian Sands	0-400'	Fresh Water
Bell Canyon	5,071'	Oil
Cherry Canyon	6,102'	Oil
Brushy Canyon	8,095'	Oil
Leonard (Avalon) Shale	9,313'	Oil
1st Bone Spring Sand	10,191'	Oil
2nd Bone Spring Shale	10,355'	Oil
2nd Bone Spring Sand	10,727'	Oil



### **Midland**

Lea County, NM (NAD 83 NME) Amazing 19 Fed #402H

OH

Plan: Plan #0.1 RT

### **Standard Planning Report**

31 October, 2023



Database: Company: PEDM Midland

Lea County, NM (NAD 83 NME)

Project: Site:

Amazing 19 Fed

Well: #402H Wellbore: ОН

Plan #0.1 RT Design:

**Local Co-ordinate Reference:** 

**TVD Reference:** MD Reference: North Reference:

**Survey Calculation Method:** 

Well #402H

kn=25' @ 3677.0usft kn=25' @ 3677.0usft

Grid

Minimum Curvature

Project Lea County, NM (NAD 83 NME)

Map System: Geo Datum:

Map Zone:

**Well Position** 

US State Plane 1983 North American Datum 1983 New Mexico Eastern Zone

System Datum:

Mean Sea Level

Amazing 19 Fed Site

Northing: 503,794.00 usft Site Position: From: Мар Easting: 734,151.00 usft

**Position Uncertainty:** 0.0 usft Slot Radius: 13-3/16 " 32° 23' 0.425 N

Well #402H

> +N/-S +E/-W

0.0 usft 0.0 usft 0.0 usft

Northing: Easting:

Wellhead Elevation:

503,671.00 usft 733,926.00 usft

Latitude:

Longitude:

Latitude: Longitude:

32° 22' 59.221 N 103° 42' 34.032 W

103° 42' 31.400 W

**Position Uncertainty** usft **Ground Level:** 3,652.0 usft

0.33° **Grid Convergence:** 

ОН Wellbore

Declination Field Strength Magnetics **Model Name** Sample Date Dip Angle (°) (°) (nT) 47,324.61218971 IGRF2020 10/31/2023 6.34 59.94

Design Plan #0.1 RT

Audit Notes:

Version:

Phase: Vertical Section: Depth From (TVD) PLAN

+N/-S

Tie On Depth: +E/-W

0.0 Direction

(usft) (usft) (usft) (°) 174.88 0.0 0.0 0.0

**Plan Survey Tool Program** 

Date 10/31/2023

**Depth From** Depth To (usft)

(usft) Plan #0.1 RT (OH) 0.0 20,377.1

Survey (Wellbore)

**Tool Name** EOG MWD+IFR1

Remarks

MWD + IFR1



Database: Company:

Wellbore:

PEDM

Midland Lea County, NM (NAD 83 NME)

Project: Site: Well:

#402H OH

Design:

OH Plan #0.1 RT

Amazing 19 Fed

Local Co-ordinate Reference:

TVD Reference: MD Reference: North Reference:

Survey Calculation Method:

Well #402H

kn=25' @ 3677.0usft kn=25' @ 3677.0usft

Grid

Plan Sections										
Measured Depth (usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)	TFO (°)	Target
0.0	0.00	0.00	0.0	0.0	0.0	0.00	0.00	0.00	0.00	
1,356.0	0.00	0.00	1,356.0	0.0	0.0	0.00	0.00	0.00	0.00	
1,851.3	9.91	64.72	1,848.8	18.2	38.6	2.00	2.00	0.00	64.72	
6,677.6	9.91	64.72	6,603.2	372.8	789.4	0.00	0.00	0.00	0.00	
7,172.9	0.00	0.01	7,096.0	391.0	828.0	2.00	-2.00	0.00	180.00	
9,692.4	0.00	0.01	9,615.5	391.0	828.0	0.00	0.00	0.00	0.00	KOP(Amazing 19 Fed
9,912.8	26.46	180.00	9,828.2	341.0	828.0	12.00	12.00	81.65	180.00	FTP(Amazing 19 Fed
10,442.4	90.00	179.61	10,092.9	-86.5	830.0	12.00	12.00	-0.07	-0.44	
20,377.1	90.00	179.61	10,093.0	-10,021.0	898.0	0.00	0.00	0.00	0.00	PBHL(Amazing 19 Fe

# eog resources

#### Planning Report

Database: PEDM Company: Midland

Project: Lea County, NM (NAD 83 NME)

 Site:
 Amazing 19 Fed

 Well:
 #402H

 Wellbore:
 OH

Design: Plan #0.1 RT

Local Co-ordinate Reference:

TVD Reference:
MD Reference:
North Reference:

**Survey Calculation Method:** 

Well #402H

kn=25' @ 3677.0usft kn=25' @ 3677.0usft

Grid

Jesigii.	FIAIT#U.TIXT								
Planned Survey									
Measured Depth (usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Vertical Section (usft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)
0.0	0.00	0.00	0.0	0.0	0.0	0.0	0.00	0.00	0.00
100.0	0.00	0.00	100.0	0.0	0.0	0.0	0.00	0.00	0.00
200.0	0.00	0.00	200.0	0.0	0.0	0.0	0.00	0.00	0.00
300.0	0.00	0.00	300.0	0.0	0.0	0.0	0.00	0.00	0.00
400.0	0.00	0.00	400.0	0.0	0.0	0.0	0.00	0.00	0.00
500.0	0.00	0.00	500.0	0.0	0.0	0.0	0.00	0.00	0.00
600.0	0.00	0.00	600.0	0.0	0.0	0.0	0.00	0.00	0.00
700.0	0.00	0.00	700.0	0.0	0.0	0.0	0.00	0.00	0.00
800.0	0.00	0.00	0.008	0.0	0.0	0.0	0.00	0.00	0.00
900.0	0.00	0.00	900.0	0.0	0.0	0.0	0.00	0.00	0.00
4 000 0	0.00		4 000 0				0.00	0.00	2.22
1,000.0	0.00	0.00	1,000.0	0.0	0.0	0.0	0.00	0.00	0.00
1,100.0	0.00	0.00	1,100.0	0.0	0.0	0.0	0.00	0.00	0.00
1,200.0	0.00	0.00	1,200.0	0.0	0.0	0.0	0.00	0.00	0.00
1,300.0	0.00	0.00	1,300.0	0.0	0.0	0.0	0.00	0.00	0.00
1,356.0	0.00	0.00	1,356.0	0.0	0.0	0.0	0.00	0.00	0.00
1,400.0	0.88	64.72	1,400.0	0.1	0.3	-0.1	2.00	2.00	0.00
1,500.0	2.88	64.72	1,499.9	1.5	3.3	-1.2	2.00	2.00	0.00
1,600.0	4.88	64.72	1,599.7	4.4	9.4	-3.6	2.00	2.00	0.00
1,700.0	6.88	64.72	1,699.2	8.8	18.7	-7.1	2.00	2.00	0.00
1,800.0	8.88	64.72	1,798.2	14.7	31.1	-11.8	2.00	2.00	0.00
,									
1,851.3	9.91	64.72	1,848.8	18.2	38.6	-14.7	2.00	2.00	0.00
1,900.0	9.91	64.72	1,896.8	21.8	46.2	-17.6	0.00	0.00	0.00
2,000.0	9.91	64.72	1,995.3	29.2	61.8	-23.5	0.00	0.00	0.00
2,100.0	9.91	64.72	2,093.8	36.5	77.3	-29.5	0.00	0.00	0.00
2,200.0	9.91	64.72	2,192.3	43.9	92.9	-35.4	0.00	0.00	0.00
2,300.0	9.91	64.72	2,290.8	51.2	108.4	-41.3	0.00	0.00	0.00
2,400.0	9.91	64.72	2,389.4	58.5	124.0	-47.2	0.00	0.00	0.00
2,500.0	9.91	64.72	2,487.9	65.9	139.5	-53.2	0.00	0.00	0.00
2,600.0	9.91	64.72	2,586.4	73.2	155.1	-59.1	0.00	0.00	0.00
2,700.0	9.91	64.72	2,684.9	80.6	170.6	-65.0	0.00	0.00	0.00
	0.04		0.700.4				0.00	0.00	0.00
2,800.0	9.91	64.72	2,783.4	87.9	186.2	-71.0	0.00	0.00	0.00
2,900.0	9.91	64.72	2,881.9	95.3	201.8	-76.9	0.00	0.00	0.00
3,000.0	9.91	64.72	2,980.4	102.6	217.3	-82.8	0.00	0.00	0.00
3,100.0	9.91	64.72	3,078.9	110.0	232.9	-88.7	0.00	0.00	0.00
3,200.0	9.91	64.72	3,177.4	117.3	248.4	-94.7	0.00	0.00	0.00
3,300.0	9.91	64.72	3,275.9	124.7	264.0	-100.6	0.00	0.00	0.00
3,400.0	9.91	64.72	3,374.4	132.0	279.5	-106.5	0.00	0.00	0.00
3,500.0	9.91	64.72	3,473.0	139.3	295.1	-112.5	0.00	0.00	0.00
3,600.0	9.91	64.72	3,571.5	146.7	310.6	-118.4	0.00	0.00	0.00
3,700.0	9.91	64.72	3,670.0	154.0	326.2	-124.3	0.00	0.00	0.00
3,800.0	9.91	64.72	3,768.5	161.4	341.8	-130.2	0.00	0.00	0.00
3,900.0	9.91	64.72	3,867.0	168.7	357.3	-136.2	0.00	0.00	0.00
4,000.0	9.91	64.72	3,965.5	176.1	372.9	-142.1	0.00	0.00	0.00
4,100.0	9.91	64.72	4,064.0	183.4	388.4	-148.0	0.00	0.00	0.00
4,200.0	9.91	64.72	4,162.5	190.8	404.0	-153.9	0.00	0.00	0.00
4,300.0	9.91	64.72	4,261.0	198.1	419.5	-159.9	0.00	0.00	0.00
4,400.0	9.91	64.72		205.5	435.1	-165.8	0.00	0.00	0.00
			4,359.5						
4,500.0	9.91	64.72	4,458.0	212.8	450.6	-171.7	0.00	0.00	0.00
4,600.0	9.91	64.72	4,556.6	220.1	466.2	-177.7	0.00	0.00	0.00
4,700.0	9.91	64.72	4,655.1	227.5	481.8	-183.6	0.00	0.00	0.00
4,800.0	0.01	64.72		224 0	497.3	-189.5	0.00	0.00	0.00
	9.91		4,753.6	234.8					
4,900.0	9.91	64.72	4,852.1	242.2	512.9	-195.4	0.00	0.00	0.00
5,000.0	9.91	64.72	4,950.6	249.5	528.4	-201.4	0.00	0.00	0.00
5,100.0	9.91	64.72	5,049.1	256.9	544.0	-207.3	0.00	0.00	0.00



Database: PEDM Company: Midland

Project: Lea County, NM (NAD 83 NME)

 Site:
 Amazing 19 Fed

 Well:
 #402H

 Wellbore:
 OH

Wellbore: OH

Design: Plan #0.1 RT

Local Co-ordinate Reference:

TVD Reference:
MD Reference:
North Reference:

**Survey Calculation Method:** 

Well #402H

kn=25' @ 3677.0usft kn=25' @ 3677.0usft

Grid

200.g									
Planned Survey									
Measured Depth (usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Vertical Section (usft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)
5,200.0	9.91	64.72	5,147.6	264.2	559.5	-213.2	0.00	0.00	0.00
5,300.0	9.91	64.72	5,246.1	271.6	575.1	-219.2	0.00	0.00	0.00
5,400.0	9.91	64.72	5,344.6	278.9	590.6	-225.1	0.00	0.00	0.00
5,500.0	9.91	64.72	5,443.1	286.3	606.2	-231.0	0.00	0.00	0.00
5,600.0	9.91	64.72	5,541.7	293.6	621.8	-236.9	0.00	0.00	0.00
5,700.0	9.91	64.72	5,640.2	301.0	637.3	-242.9	0.00	0.00	0.00
5,800.0	9.91	64.72	5,738.7	308.3	652.9	-248.8	0.00	0.00	0.00
5,900.0	9.91	64.72	5,837.2	315.6	668.4	-254.7	0.00	0.00	0.00
6,000.0	9.91	64.72	5,935.7	323.0	684.0	-260.7	0.00	0.00	0.00
6,100.0	9.91	64.72	6,034.2	330.3	699.5	-266.6	0.00	0.00	0.00
6,200.0	9.91	64.72	6,132.7	337.7	715.1	-272.5	0.00	0.00	0.00
6,300.0	9.91	64.72	6,231.2	345.0	730.6	-278.4	0.00	0.00	0.00
6,400.0	9.91	64.72	6,329.7	352.4	746.2	-284.4	0.00	0.00	0.00
6,500.0	9.91	64.72	6,428.2	359.7	761.8	-290.3	0.00	0.00	0.00
6,600.0	9.91	64.72	6,526.7	367.1	777.3	-296.2	0.00	0.00	0.00
6,677.6	9.91	64.72	6,603.2	372.8	789.4	-300.8	0.00	0.00	0.00
6.700.0	9.46	64.72	6,625.3	374.4	792.8	-302.1	2.00	-2.00	0.00
6,800.0	7.46	64.72	6,724.2	374.4	792.6 806.1	-307.2	2.00	-2.00 -2.00	0.00
6,900.0	5.46	64.72	6,823.5	385.5	816.3	-307.2 -311.1	2.00	-2.00 -2.00	0.00
7,000.0	3.46	64.72	6,923.2	388.8	823.3	-313.7	2.00	-2.00 -2.00	0.00
7,000.0	1.46	64.72	7,023.1	390.6	827.2	-315.2	2.00	-2.00	0.00
7,172.9	0.00	0.01	7,096.0	391.0	828.0	-315.5	2.00	-2.00	0.00
7,200.0	0.00	0.00	7,123.1	391.0	828.0	-315.5	0.00	0.00	0.00
7,300.0	0.00	0.00	7,223.1	391.0	828.0	-315.5	0.00	0.00	0.00
7,400.0	0.00	0.00	7,323.1	391.0	828.0	-315.5	0.00	0.00	0.00
7,500.0	0.00	0.00	7,423.1	391.0	828.0	-315.5	0.00	0.00	0.00
7,600.0	0.00	0.00	7,523.1	391.0	828.0	-315.5	0.00	0.00	0.00
7,700.0	0.00	0.00	7,623.1	391.0	828.0	-315.5	0.00	0.00	0.00
7,800.0	0.00	0.00	7,723.1	391.0	828.0	-315.5	0.00	0.00	0.00
7,900.0	0.00	0.00	7,823.1	391.0	828.0	-315.5	0.00	0.00	0.00
8,000.0	0.00	0.00	7,923.1	391.0	828.0	-315.5	0.00	0.00	0.00
8,100.0	0.00	0.00	8,023.1	391.0	828.0	-315.5	0.00	0.00	0.00
8,200.0	0.00	0.00	8,123.1	391.0	828.0	-315.5	0.00	0.00	0.00
8,300.0	0.00	0.00	8,223.1	391.0	828.0	-315.5	0.00	0.00	0.00
8,400.0	0.00	0.00	8,323.1	391.0	828.0	-315.5	0.00	0.00	0.00
8,500.0	0.00	0.00	8,423.1	391.0	828.0	-315.5	0.00	0.00	0.00
8,600.0	0.00	0.00	8,523.1	391.0	828.0	-315.5	0.00	0.00	0.00
8,700.0	0.00	0.00	8,623.1	391.0	828.0	-315.5	0.00	0.00	0.00
8,800.0	0.00	0.00	8,723.1	391.0	828.0	-315.5	0.00	0.00	0.00
8,900.0	0.00	0.00	8,823.1	391.0	828.0	-315.5	0.00	0.00	0.00
9,000.0	0.00	0.00	8,923.1	391.0	828.0	-315.5	0.00	0.00	0.00
9.100.0	0.00	0.00	9,023.1	391.0	828.0	-315.5	0.00	0.00	0.00
9,100.0	0.00	0.00	9,023.1	391.0	828.0	-315.5 -315.5	0.00	0.00	0.00
9,300.0	0.00	0.00	9,123.1	391.0	828.0	-315.5 -315.5	0.00	0.00	0.00
9,400.0	0.00	0.00	9,323.1	391.0	828.0	-315.5	0.00	0.00	0.00
9,500.0	0.00	0.00	9,423.1	391.0	828.0	-315.5	0.00	0.00	0.00
9.600.0									
-,	0.00	0.00	9,523.1	391.0	828.0	-315.5	0.00	0.00	0.00
9,692.4	0.00	0.01	9,615.5	391.0	828.0	-315.5	0.00	0.00	0.00
9,700.0 9,725.0	0.91	180.00	9,623.1 9,648.1	390.9	828.0	-315.5	12.00	12.00	0.00
9,725.0 9,750.0	3.92 6.92	180.00 180.00	9,648.1 9,673.0	389.9 387.5	828.0 828.0	-314.4 -312.1	12.00 12.00	12.00 12.00	0.00 0.00
9,775.0	9.92	180.00	9,697.7	383.9	828.0	-308.4	12.00	12.00	0.00
9,800.0	12.92	180.00	9,722.2	378.9	828.0	-303.5	12.00	12.00	0.00
9,825.0	15.92	180.00	9,746.4	372.7	828.0	-297.3	12.00	12.00	0.00



Database: PEDM Company: Midland

Project: Lea County, NM (NAD 83 NME)

 Site:
 Amazing 19 Fed

 Well:
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 OH

Design: Plan #0.1 RT

Local Co-ordinate Reference:

TVD Reference:
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North Reference:

**Survey Calculation Method:** 

Well #402H

kn=25' @ 3677.0usft kn=25' @ 3677.0usft

Grid

sign:	FIAIT#U.TKT								
nned Survey									
Measured Depth (usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Vertical Section (usft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)
9,850.0	18.92	180.00	9,770.3	365.2	828.0	-289.9	12.00	12.00	0.00
9,875.0	21.92	180.00	9,793.7	356.5	828.0	-281.2	12.00	12.00	0.00
9,900.0	24.92	180.00	9,816.6	346.6	828.0	-271.3	12.00	12.00	0.00
9,912.8	26.46	180.00	9,828.2	341.0	828.0	-265.7	12.00	12.00	0.00
9,925.0	27.92	179.98	9,839.0	335.4	828.0	-260.2	12.00	12.00	-0.20
9,950.0 9,975.0	30.92	179.93	9,860.8 9,881.9	323.2	828.0	-248.0	12.00	12.00	-0.17
,	33.92	179.90	,	309.8	828.0	-234.6	12.00	12.00	-0.14
10,000.0	36.92	179.87	9,902.3	295.3	828.1	-220.2	12.00	12.00	-0.12
10,025.0	39.92	179.84	9,921.9	279.7	828.1	-204.7	12.00	12.00	-0.11
10,050.0	42.92	179.82	9,940.6	263.2	828.1	-188.2	12.00	12.00	-0.09
10,075.0	45.92	179.80	9,958.5	245.7	828.2	-170.8	12.00	12.00	-0.08
10,100.0	48.92	179.78	9,975.4	227.3	828.3	-152.5	12.00	12.00	-0.08
10,125.0	51.92	179.76	9,991.3	208.0	828.4	-133.3	12.00	12.00	-0.07
10,150.0	54.92	179.74	10,006.2	188.0	828.4	-113.3	12.00	12.00	-0.06
10,175.0	57.92	179.73	10,020.0	167.1	828.5	-92.5	12.00	12.00	-0.06
10,200.0	60.92	179.72	10,032.7	145.6	828.6	-71.1	12.00	12.00	-0.06
10,225.0	63.92	179.70	10,044.3	123.5	828.8	-49.0	12.00	12.00	-0.05
10,250.0	66.92	179.69	10,054.7	100.7	828.9	-26.4	12.00	12.00	-0.05
10,275.0	69.92	179.68	10,063.9	77.5	829.0	-3.2	12.00	12.00	-0.05
10,300.0	72.92	179.67	10,071.9	53.8	829.1	20.4	12.00	12.00	-0.05
10,325.0	75.92	179.66	10,078.6	29.7	829.3	44.4	12.00	12.00	-0.04
10,350.0	78.92	179.65	10,084.0	5.3	829.4	68.7	12.00	12.00	-0.04
10,375.0	81.92	179.64	10,088.2	-19.3	829.6	93.3	12.00	12.00	-0.04
10,400.0	84.92	179.63	10,091.1	-44.2	829.7	118.0	12.00	12.00	-0.04
10,425.0	87.92	179.62	10,092.6	-69.1	829.9	142.9	12.00	12.00	-0.04
10,442.4	90.00	179.61	10,092.9	-86.5	830.0	160.2	12.00	12.00	-0.04
10,500.0	90.00	179.61	10,092.9	-144.1	830.4	217.6	0.00	0.00	0.00
10,600.0	90.00	179.61	10,092.9	-244.1	831.1	317.3	0.00	0.00	0.00
10,700.0	90.00	179.61	10,092.9	-344.1	831.8	417.0	0.00	0.00	0.00
10,800.0	90.00	179.61	10,092.9	-444.1	832.5	516.6	0.00	0.00	0.00
10,900.0	90.00	179.61	10,092.9	-544.1	833.2	616.3	0.00	0.00	0.00
11,000.0	90.00	179.61	10,092.9	-644.1	833.8	715.9	0.00	0.00	0.00
11,100.0	90.00	179.61	10,092.9	-744.1	834.5	815.6	0.00	0.00	0.00
11,200.0	90.00	179.61	10,092.9	-844.1	835.2	915.3	0.00	0.00	0.00
11,300.0	90.00	179.61	10,092.9	-944.1	835.9	1,014.9	0.00	0.00	0.00
11,400.0	90.00	179.61	10,093.0	-1,044.1	836.6	1,114.6	0.00	0.00	0.00
11,500.0	90.00	179.61	10,093.0	-1,144.1	837.3	1,214.2	0.00	0.00	0.00
11,600.0	90.00	179.61	10,093.0	-1,244.1	837.9	1,313.9	0.00	0.00	0.00
11,700.0	90.00	179.61	10,093.0	-1,344.1	838.6	1,413.6	0.00	0.00	0.00
11,800.0	90.00	179.61	10,093.0	-1,444.1	839.3	1,513.2	0.00	0.00	0.00
11,900.0	90.00	179.61	10,093.0	-1,544.1	840.0	1,612.9	0.00	0.00	0.00
12,000.0	90.00	179.61	10,093.0	-1,644.1	840.7	1,712.5	0.00	0.00	0.00
12,100.0	90.00	179.61	10,093.0	-1.744.1	841.4	1,812.2	0.00	0.00	0.00
12,100.0	90.00	179.61	10,093.0	-1,744.1 -1,844.1	842.0	1,911.9	0.00	0.00	0.00
12,300.0	90.00	179.61	10,093.0	-1,944.1	842.7	2,011.5	0.00	0.00	0.00
12,400.0	90.00	179.61	10,093.0	-2,044.1	843.4	2,111.2	0.00	0.00	0.00
12,500.0	90.00	179.61	10,093.0	-2,144.1	844.1	2,210.8	0.00	0.00	0.00
12,600.0	90.00	179.61	10,093.0	-2,244.0	844.8	2,310.5	0.00	0.00	0.00
12,700.0	90.00	179.61	10,093.0	-2,244.0 -2,344.0	845.5	2,410.2	0.00	0.00	0.00
12,800.0	90.00	179.61	10,093.0	-2,444.0	846.2	2,509.8	0.00	0.00	0.00
12,900.0	90.00	179.61	10,093.0	-2,544.0	846.8	2,609.5	0.00	0.00	0.00
13,000.0	90.00	179.61	10,093.0	-2,644.0	847.5	2,709.1	0.00	0.00	0.00
13,100.0	90.00	179.61	10,093.0	-2,744.0	848.2	2,808.8	0.00	0.00	0.00



Database: Company:

Project:

PEDM Midland

Lea County, NM (NAD 83 NME)

Site: Amazing 19 Fed
Well: #402H

Wellbore: OH
Design: Plan #0.1 RT

Local Co-ordinate Reference:

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North Reference:

Survey Calculation Method:

Well #402H

kn=25' @ 3677.0usft kn=25' @ 3677.0usft

Grid

Design:	Plan #0.1 RT								
Planned Survey									
Measured Depth (usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Vertical Section (usft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)
13,300.0	90.00	179.61	10,093.0	-2,944.0	849.6	3,008.1	0.00	0.00	0.00
13,400.0	90.00	179.61	10,093.0	-3,044.0	850.3	3,107.8	0.00	0.00	0.00
13,500.0	90.00	179.61	10,093.0	-3,144.0	850.9	3,207.4	0.00	0.00	0.00
13,600.0	90.00	179.61	10,093.0	-3,244.0	851.6	3,307.1	0.00	0.00	0.00
13,700.0	90.00	179.61	10,093.0	-3,344.0	852.3	3,406.7	0.00	0.00	0.00
13,800.0	90.00	179.61	10,093.0	-3,444.0	853.0	3,506.4	0.00	0.00	0.00
13,900.0	90.00	179.61	10,093.0	-3,544.0	853.7	3,606.1	0.00	0.00	0.00
14,000.0	90.00	179.61	10,093.0	-3,644.0	854.4	3,705.7	0.00	0.00	0.00
14,100.0	90.00	179.61	10,093.0	-3,744.0	855.1	3,805.4	0.00	0.00	0.00
14,200.0	90.00	179.61	10,093.0	-3,844.0	855.7	3,905.0	0.00	0.00	0.00
14,300.0	90.00	179.61	10,093.0	-3,944.0	856.4	4,004.7	0.00	0.00	0.00
14,400.0	90.00	179.61	10,093.0	-4,044.0	857.1	4,104.4	0.00	0.00	0.00
14,500.0	90.00	179.61	10,093.0	-4,144.0	857.8	4,204.0	0.00	0.00	0.00
14,600.0	90.00	179.61	10,093.0	-4,244.0	858.5	4,303.7	0.00	0.00	0.00
14,700.0	90.00	179.61	10,093.0	-4,344.0	859.2	4,403.3	0.00	0.00	0.00
14,800.0	90.00	179.61	10,093.0	-4,444.0	859.8	4,503.0	0.00	0.00	0.00
14,900.0	90.00	179.61	10,093.0	-4,544.0	860.5	4,602.7	0.00	0.00	0.00
15,000.0	90.00	179.61	10,093.0	-4,644.0	861.2	4,702.3	0.00	0.00	0.00
15,100.0	90.00	179.61	10,093.0	-4,744.0	861.9	4,802.0	0.00	0.00	0.00
15,200.0	90.00	179.61	10,093.0	-4,844.0	862.6	4,901.6	0.00	0.00	0.00
15,300.0	90.00	179.61	10,093.0	-4,944.0	863.3	5,001.3	0.00	0.00	0.00
15,400.0	90.00	179.61	10,093.0	-5,044.0	863.9	5,101.0	0.00	0.00	0.00
15,500.0	90.00	179.61	10,093.0	-5,144.0	864.6	5,200.6	0.00	0.00	0.00
15,600.0	90.00	179.61	10,093.0	-5,244.0	865.3	5,300.3	0.00	0.00	0.00
15,700.0	90.00	179.61	10,093.0	-5,344.0	866.0	5,399.9	0.00	0.00	0.00
15,800.0	90.00	179.61	10,093.0	-5,444.0	866.7	5,499.6	0.00	0.00	0.00
15,900.0	90.00	179.61	10,093.0	-5,544.0	867.4	5,599.3	0.00	0.00	0.00
16,000.0	90.00	179.61	10,093.0	-5,644.0	868.1	5,698.9	0.00	0.00	0.00
16,100.0	90.00	179.61	10,093.0	-5,744.0	868.7	5,798.6	0.00	0.00	0.00
16,200.0	90.00	179.61	10,093.0	-5,844.0	869.4	5,898.2	0.00	0.00	0.00
16,300.0	90.00	179.61	10,093.0	-5,944.0	870.1	5,997.9	0.00	0.00	0.00
16,400.0 16,500.0	90.00 90.00	179.61 179.61	10,093.0 10,093.0	-6,044.0 -6,144.0	870.8 871.5	6,097.6 6,197.2	0.00 0.00	0.00 0.00	0.00 0.00
16,600.0	90.00	179.61	10,093.0	-6,244.0	872.2	6,296.9	0.00	0.00	0.00
16,700.0	90.00	179.61	10,093.0	-6,344.0	872.8	6,396.5	0.00	0.00	0.00
16,800.0 16,900.0	90.00 90.00	179.61 179.61	10,093.0 10,093.0	-6,443.9 -6,543.9	873.5 874.2	6,496.2 6,595.9	0.00 0.00	0.00 0.00	0.00 0.00
17,000.0	90.00	179.61	10,093.0	-6,643.9	874.2 874.9	6,695.5	0.00	0.00	0.00
•				•					
17,100.0	90.00	179.61 170.61	10,093.0 10,093.0	-6,743.9	875.6 876.3	6,795.2 6,894.8	0.00	0.00	0.00
17,200.0 17,300.0	90.00 90.00	179.61 179.61	10,093.0	-6,843.9 -6,943.9	876.3 876.9	6,894.8	0.00 0.00	0.00 0.00	0.00 0.00
17,300.0	90.00	179.61	10,093.0	-0,943.9 -7,043.9	877.6	7,094.2	0.00	0.00	0.00
17,500.0	90.00	179.61	10,093.0	-7,143.9	878.3	7,193.8	0.00	0.00	0.00
17,600.0	90.00	179.61	10,093.0	-7,243.9	879.0	7,293.5	0.00	0.00	0.00
17,800.0	90.00	179.61	10,093.0	-7,243.9 -7,343.9	879.0 879.7	7,293.5	0.00	0.00	0.00
17,800.0	90.00	179.61	10,093.0	-7,443.9	880.4	7,393.1	0.00	0.00	0.00
17,900.0	90.00	179.61	10,093.0	-7,543.9	881.1	7,592.5	0.00	0.00	0.00
18,000.0	90.00	179.61	10,093.0	-7,643.9	881.7	7,692.1	0.00	0.00	0.00
18,100.0	90.00	179.61	10,093.0	-7,743.9	882.4	7,791.8	0.00	0.00	0.00
18,200.0	90.00	179.61	10,093.0	-7,843.9	883.1	7,891.4	0.00	0.00	0.00
18,300.0	90.00	179.61	10,093.0	-7,943.9	883.8	7,991.1	0.00	0.00	0.00
18,400.0	90.00	179.61	10,093.0	-8,043.9	884.5	8,090.8	0.00	0.00	0.00
18,500.0	90.00	179.61	10,093.0	-8,143.9	885.2	8,190.4	0.00	0.00	0.00
18,600.0	90.00	179.61	10,093.0	-8,243.9	885.8	8,290.1	0.00	0.00	0.00



Database: Company: Project: PEDM

Midland Lea County, NM (NAD 83 NME)

Site: Amazing 19 Fed
Well: #402H

Wellbore: OH
Design: Plan #0.1 RT

Local Co-ordinate Reference:

TVD Reference: MD Reference: North Reference:

**Survey Calculation Method:** 

Well #402H

kn=25' @ 3677.0usft kn=25' @ 3677.0usft

Grid

lanned Survey									
Measured Depth (usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Vertical Section (usft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)
18,700.0	90.00	179.61	10,093.0	-8,343.9	886.5	8,389.7	0.00	0.00	0.00
18,800.0	90.00	179.61	10,093.0	-8,443.9	887.2	8,489.4	0.00	0.00	0.00
18,900.0	90.00	179.61	10,093.0	-8,543.9	887.9	8,589.0	0.00	0.00	0.00
19,000.0	90.00	179.61	10,093.0	-8,643.9	888.6	8,688.7	0.00	0.00	0.00
19,100.0	90.00	179.61	10,093.0	-8,743.9	889.3	8,788.4	0.00	0.00	0.00
19,200.0	90.00	179.61	10,093.0	-8,843.9	889.9	8,888.0	0.00	0.00	0.00
19,300.0	90.00	179.61	10,093.0	-8,943.9	890.6	8,987.7	0.00	0.00	0.00
19,400.0	90.00	179.61	10,093.0	-9,043.9	891.3	9,087.3	0.00	0.00	0.00
19,500.0	90.00	179.61	10,093.0	-9,143.9	892.0	9,187.0	0.00	0.00	0.00
19,600.0	90.00	179.61	10,093.0	-9,243.9	892.7	9,286.7	0.00	0.00	0.00
19,700.0	90.00	179.61	10,093.0	-9,343.9	893.4	9,386.3	0.00	0.00	0.00
19,800.0	90.00	179.61	10,093.0	-9,443.9	894.1	9,486.0	0.00	0.00	0.00
19,900.0	90.00	179.61	10,093.0	-9,543.9	894.7	9,585.6	0.00	0.00	0.00
20,000.0	90.00	179.61	10,093.0	-9,643.9	895.4	9,685.3	0.00	0.00	0.00
20,100.0	90.00	179.61	10,093.0	-9,743.9	896.1	9,785.0	0.00	0.00	0.00
20,200.0	90.00	179.61	10,093.0	-9,843.9	896.8	9,884.6	0.00	0.00	0.00
20,300.0	90.00	179.61	10,093.0	-9,943.9	897.5	9,984.3	0.00	0.00	0.00
20,377.1	90.00	179.61	10,093.0	-10,021.0	898.0	10,061.2	0.00	0.00	0.00

Design Targets									
Target Name - hit/miss target - Shape	Dip Angle (°)	Dip Dir. (°)	TVD (usft)	+N/-S (usft)	+E/-W (usft)	Northing (usft)	Easting (usft)	Latitude	Longitude
KOP(Amazing 19 Fed #/ - plan hits target cen - Point		0.00	9,615.5	391.0	828.0	504,062.00	734,754.00	32° 23' 3.042 N	103° 42' 24.350 W
FTP(Amazing 19 Fed #4 - plan hits target cen - Point		0.00	9,828.2	341.0	828.0	504,012.00	734,754.00	32° 23' 2.547 N	103° 42' 24.353 W
PBHL(Amazing 19 Fed # - plan hits target cen - Point		0.00	10,093.0	-10,021.0	898.0	493,650.00	734,824.00	32° 21' 20.008 N	103° 42' 24.244 W



1500

1800-

2400

3600-

4500

4800

5400

6000

6900

7200-

7500-

7800-

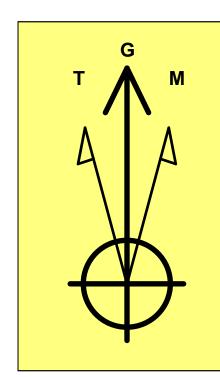
8100-

8400-

9000-

10200-

5700



Azimuths to Grid North
True North: -0.33°
Magnetic North: 6.01°

Magnetic Field Strength: 47324.6nT Dip Angle: 59.94° Date: 10/31/2023 Model: IGRF2020

To convert a Magnetic Direction to a Grid Direction, Add 6.01°
To convert a Magnetic Direction to a True Direction, Add 6.34° East
To convert a True Direction to a Grid Direction, Subtract 0.33°

Lea County, NM (NAD 83 NME)

Amazing 19 Fed #402H

Plan #0.1 RT

PROJECT DETAILS: Lea County, NM (NAD 83 NME)

Geodetic System: US State Plane 1983
Datum: North American Datum 1983
Filipsoid: GPS 1980

Ellipsoid: GRS 1980
Zone: New Mexico Eastern Zone
System Datum: Mean Sea Level

WELL DETAILS: #402H

3652.0

kn=25' @ 3677.0usft

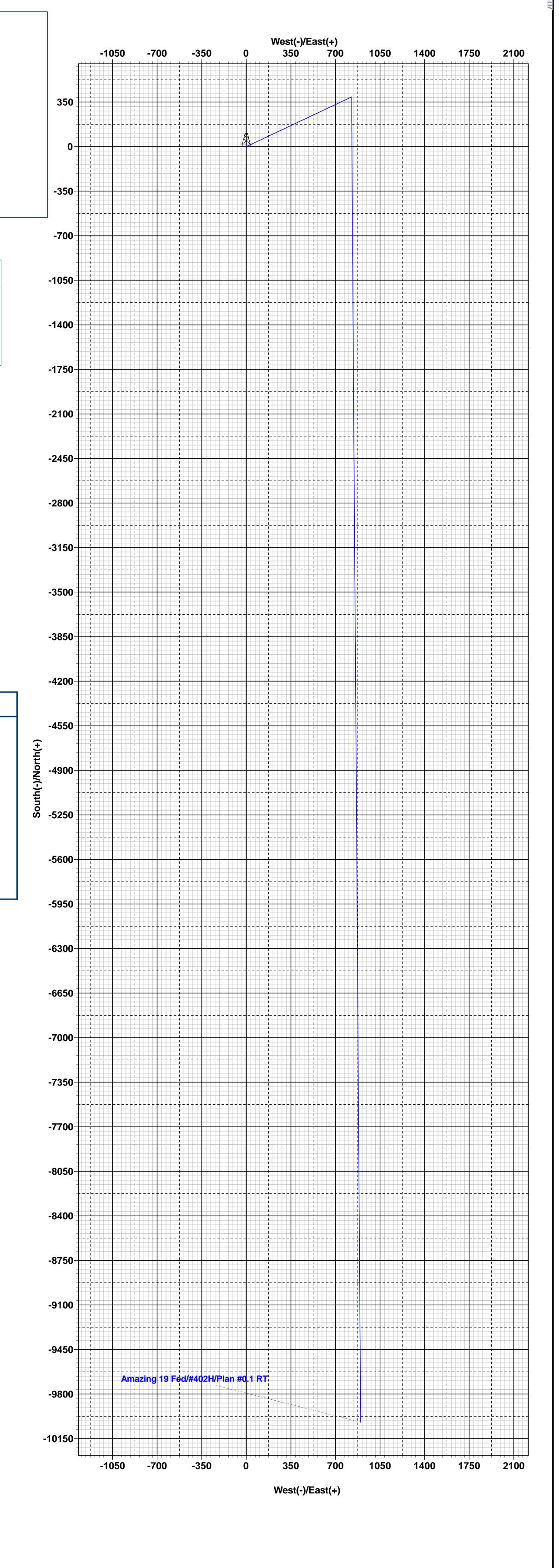
Northing Easting Latittude Longitude 503671.00 733926.00 32° 22' 59.221 N 103° 42' 34.032 W

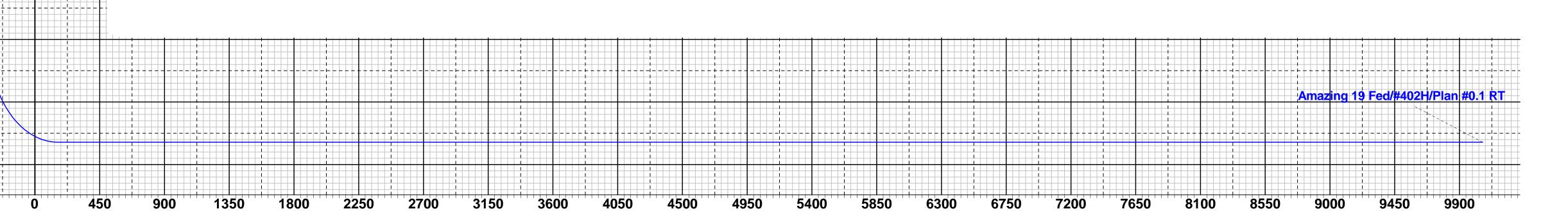
						SECT	ION DET	TAILS		
Sec	MD	Inc	Azi	TVD	+N/-S	+E/-W	Dleg	TFace	VSect	Target
1	0.0	0.00	0.00	0.0	0.0	0.0	0.00	0.00	0.0	
2	1356.0	0.00	0.00	1356.0	0.0	0.0	0.00	0.00	0.0	
3	1851.3	9.91	64.72	1848.8	18.2	38.6	2.00	64.72	-14.7	
4	6677.6	9.91	64.72	6603.2	372.8	789.4	0.00	0.00	-300.8	
5	7172.9	0.00	0.00	7096.0	391.0	828.0	2.00	180.00	-315.5	
6	9692.4	0.00	0.00	9615.5	391.0	828.0	0.00	0.00	-315.5	KOP(Amazing 19 Fed #402H)
7	9912.8	26.46	180.00	9828.2	341.0	828.0	12.00	180.00	-265.7	FTP(Amazing 19 Fed #402H)
8	10442.4	90.00	179.61	10092.9	-86.5	830.0	12.00	-0.44	160.2	
9	20377.1	90.00	179.61	10093.0	-10021.0	898.0	0.00	0.00	10061.2	PBHL(Amazing 19 Fed #402H)

CASING DETAILS

No casing data is available

WELLBORE TARGET DETAILS (MAP CO-ORDINATES) +E/-W Northing TVD +N/-S **Easting** KOP(Amazing 19 Fed #402H) FTP(Amazing 19 Fed #402H) 9615.5 391.0 504062.00 734754.00 341.0 504012.00 9828.2 734754.00 PBHL(Amazing 19 Fed #402H) 10093.0 -10021.0 493650.00 734824.00





Vertical Section at 174.88°

Lea County, NM (NAD 83 NME)
Amazing 19 Fed
#402H
OH
Plan #0.1 RT
15:52, October 31 2023

# PECOS DISTRICT DRILLING CONDITIONS OF APPROVAL

OPERATOR'S NAME: | EOG RESOURCES INCORPORATED

WELL NAME & NO.: | AMAZING 19 FED 402H

SURFACE HOLE FOOTAGE: 431'/N 1270'/E BOTTOM HOLE FOOTAGE 100'/S 440'/E

LOCATION: SECTION 19, T22S, R32E COUNTY: Lea County, New Mexico

All previous COAs still apply

COA

H2S	• Yes	O No	
Potash	None	<ul><li>Secretary</li></ul>	© R-111-P
Cave/Karst Potential	• Low	O Medium	O High
Cave/Karst Potential	© Critical		
Variance	O None	• Flex Hose	Other
Wellhead	Conventional	• Multibowl	O Both
Wellhead Variance	O Diverter		
Other	□4 String	☐ Capitan Reef	□WIPP
Other	▼ Fluid Filled	☐ Pilot Hole	☐ Open Annulus
Cementing	☐ Contingency	☐ EchoMeter	☐ Primary Cement
	Cement Squeeze		Squeeze
Special Requirements	☐ Water Disposal	□ СОМ	□ Unit
Special Requirements	☐ Batch Sundry		
Special Requirements	☑ Break Testing	☑ Offline	✓ Casing
Variance		Cementing	Clearance

#### A. CASING

NOTE: INTERMEDIATE CASING SET POINTS ADJUSTED BASED ON BLM GEOLOGY RECOMMENDATION AND ORIGINAL APD SET DEPTH

#### **Primary Casing Design:**

- 1. The **13-3/8** inch surface casing shall be set at approximately **940** feet (a minimum of 25 feet (Lea County) into the Rustler Anhydrite, above the salt, and below usable fresh water) and cemented to the surface.
  - a. If cement does not circulate to the surface, the appropriate BLM office shall be notified and a temperature survey utilizing an electronic type temperature

- survey with surface log readout will be used or a cement bond log shall be run to verify the top of the cement. Temperature survey will be run a minimum of six hours after pumping cement and ideally between 8-10 hours after completing the cement job.
- b. Wait on cement (WOC) time for a primary cement job will be a minimum of **8** hours or 500 pounds compressive strength, whichever is greater. (This is to include the lead cement)
- c. Wait on cement (WOC) time for a remedial job will be a minimum of 4 hours after bringing cement to surface or 500 pounds compressive strength, whichever is greater.
- d. If cement falls back, remedial cementing will be done prior to drilling out that string.

### Intermediate casing must be kept fluid filled to meet BLM minimum collapse requirement in Design A.

2. The 9-5/8 inch intermediate casing shall be set at approximately 4,452 feet TVD. Cement excess < 25% CFO recommendation. Please review cement volumes to achieve below mentioned tie-back. The minimum required fill of cement behind the 9-5/8 inch intermediate casing is:

#### **Option 1 (Single Stage):**

- Cement to surface. If cement does not circulate see B.1.a, c-d above.
- 3. The **5-1/2** inch production casing shall be set at approximately **20,377** feet. The minimum required fill of cement behind the **5-1/2** inch production casing is:

#### **Option 1 (Single Stage):**

• Cement should tie-back at least **200 feet** into previous casing string. Operator shall provide method of verification.

#### **Alternate Casing Design:**

- 1. The **10-3/4** inch surface casing shall be set at approximately **940** feet (a minimum of 25 feet (Lea County) into the Rustler Anhydrite, above the salt, and below usable fresh water) and cemented to the surface.
  - e. If cement does not circulate to the surface, the appropriate BLM office shall be notified and a temperature survey utilizing an electronic type temperature survey with surface log readout will be used or a cement bond log shall be run to verify the top of the cement. Temperature survey will be run a minimum of six hours after pumping cement and ideally between 8-10 hours after completing the cement job.
  - f. Wait on cement (WOC) time for a primary cement job will be a minimum of 8

- **hours** or 500 pounds compressive strength, whichever is greater. (This is to include the lead cement)
- g. Wait on cement (WOC) time for a remedial job will be a minimum of 4 hours after bringing cement to surface or 500 pounds compressive strength, whichever is greater.
- h. If cement falls back, remedial cementing will be done prior to drilling out that string.

### Intermediate casing must be kept fluid filled to meet BLM minimum collapse requirement in Design B.

2. The **8-5/8** inch intermediate casing shall be set at approximately **4,452** feet TVD. The minimum required fill of cement behind the **8-5/8** inch intermediate casing is:

#### **Option 1 (Single Stage):**

- Cement to surface. If cement does not circulate see B.1.a, c-d above.
- 3. The **5-1/2** inch production casing shall be set at approximately **20,377** feet. The minimum required fill of cement behind the **5-1/2** inch production casing is:

#### **Option 1 (Single Stage):**

a. Cement should tie-back at least **200 feet** into previous casing string. Operator shall provide method of verification.

#### B. SPECIAL REQUIREMENT (S)

#### (Note: For a minimum 5M BOPE or less (Utilizing a 10M BOPE system) BOPE Break Testing Variance

- BOPE Break Testing is ONLY permitted for 5M BOPE or less. (Annular preventer must be tested to a minimum of 70% of BOPE working pressure and shall be higher than the MASP)
- BOPE Break Testing is NOT permitted to drilling the production hole section.
- Variance only pertains to the intermediate hole-sections and no deeper than the Bone Springs formation.
- While in transfer between wells, the BOPE shall be secured by the hydraulic carrier or cradle.
- Any well control event while drilling require notification to the BLM Petroleum Engineer (575-706-2779) prior to the commencement of any BOPE Break Testing operations.
- A full BOPE test is required prior to drilling the first deep intermediate hole section. If any subsequent hole interval is deeper than the first, a full BOPE test will be required. (200' TVD tolerance between intermediate shoes is allowable).
- The BLM is to be contacted (575-689-5981 Lea County) 4 hours prior to BOPE tests.
- As a minimum, a full BOPE test shall be performed at 21-day intervals.

- In the event any repairs or replacement of the BOPE is required, the BOPE shall test as per 43 CFR part 3170 Subpart 3172.
- If in the event break testing is not utilized, then a full BOPE test would be conducted.

#### **Offline Cementing**

OK for surface and intermediate intervals. Notify the BLM prior to the commencement of any offline cementing procedure.

#### **Casing Clearance:**

- Salt annular clearance variance in place
- Overlap clearance OK in the production interval

Operator shall clean up cycles until wellbore is clear of cuttings and any large debris, ensure cutting sizes are adequate "coffee ground or less" before cementing.

#### **GENERAL REQUIREMENTS**

The BLM is to be notified in advance for a representative to witness:

- a. Spudding well (minimum of 24 hours)
- b. Setting and/or Cementing of all casing strings (minimum of 4 hours)
- c. BOPE tests (minimum of 4 hours)
  - ⊠ Eddy County

**EMAIL** or call the Carlsbad Field Office, 620 East Greene St., Carlsbad, NM 88220,

**BLM\_NM\_CFO\_DrillingNotifications@BLM.GOV** (575) 361-2822

- ✓ Lea CountyCall the Hobbs Field Station, 414 West Taylor, Hobbs NM 88240, (575) 689-5981
- 1. Unless the production casing has been run and cemented or the well has been properly plugged, the drilling rig shall not be removed from over the hole without prior approval.
  - a. In the event the operator has proposed to drill multiple wells utilizing a skid/walking rig. Operator shall secure the wellbore on the current well, after installing and testing the wellhead, by installing a blind flange of like pressure rating to the wellhead and a pressure gauge that can be monitored while drilling is performed on the other well(s).
  - b. When the operator proposes to set surface casing with Spudder Rig
    - Notify the BLM when moving in and removing the Spudder Rig.

- Notify the BLM when moving in the 2<sup>nd</sup> Rig. Rig to be moved in within 90 days of notification that Spudder Rig has left the location.
- BOP/BOPE test to be conducted per **43 CFR part 3170 Subpart 3172** as soon as 2nd Rig is rigged up on well.
- 2. Floor controls are required for 3M or Greater systems. These controls will be on the rig floor, unobstructed, readily accessible to the driller and will be operational at all times during drilling and/or completion activities. Rig floor is defined as the area immediately around the rotary table; the area immediately above the substructure on which the draw works are located, this does not include the dog house or stairway area.
- 3. The record of the drilling rate along with the GR/N well log run from TD to surface (horizontal well vertical portion of hole) shall be submitted to the BLM office as well as all other logs run on the borehole 30 days from completion. If available, a digital copy of the logs is to be submitted in addition to the paper copies. The Rustler top and top and bottom of Salt are to be recorded on the Completion Report.

#### A. CASING

- 1. Changes to the approved APD casing program need prior approval if the items substituted are of lesser grade or different casing size or are Non-API. The Operator can exchange the components of the proposal with that of superior strength (i.e. changing from J-55 to N-80, or from 36# to 40#). Changes to the approved cement program need prior approval if the altered cement plan has less volume or strength or if the changes are substantial (i.e. Multistage tool, ECP, etc.). The initial wellhead installed on the well will remain on the well with spools used as needed.
- 2. Wait on cement (WOC) for Potash Areas: After cementing but before commencing any tests, the casing string shall stand cemented under pressure until both of the following conditions have been met: 1) cement reaches a minimum compressive strength of 500 psi for all cement blends, 2) until cement has been in place at least 24 hours. WOC time will be recorded in the driller's log. The casing intergrity test can be done (prior to the cement setting up) immediately after bumping the plug.
- 3. Wait on cement (WOC) for Water Basin: After cementing but before commencing any tests, the casing string shall stand cemented under pressure until both of the following conditions have been met: 1) cement reaches a minimum compressive strength of 500 psi at the shoe, 2) until cement has been in place at least 8 hours. WOC time will be recorded in the driller's log. See individual casing strings for details regarding lead cement slurry requirements. The casing integrity test can be done (prior to the cement setting up) immediately after bumping the plug.
- 4. Provide compressive strengths including hours to reach required 500 pounds compressive strength prior to cementing each casing string. Have well specific cement details onsite prior to pumping the cement for each casing string.

- 5. No pea gravel permitted for remedial or fall back remedial without prior authorization from the BLM engineer.
- 6. On that portion of any well approved for a 5M BOPE system or greater, a pressure integrity test of each casing shoe shall be performed. Formation at the shoe shall be tested to a minimum of the mud weight equivalent anticipated to control the formation pressure to the next casing depth or at total depth of the well. This test shall be performed before drilling more than 20 feet of new hole.
- 7. If hardband drill pipe is rotated inside casing, returns will be monitored for metal. If metal is found in samples, drill pipe will be pulled and rubber protectors which have a larger diameter than the tool joints of the drill pipe will be installed prior to continuing drilling operations.
- 8. Whenever a casing string is cemented in the R-111-P potash area, the NMOCD requirements shall be followed.
- B. PRESSURE CONTROL
- 1. All blowout preventer (BOP) and related equipment (BOPE) shall comply with well control requirements as described in 43 CFR part 3170 Subpart 3172 and API STD 53 Sec. 5.3.
- 2. If a variance is approved for a flexible hose to be installed from the BOP to the choke manifold, the following requirements apply: The flex line must meet the requirements of API 16C. Check condition of flexible line from BOP to choke manifold, replace if exterior is damaged or if line fails test. Line to be as straight as possible with no hard bends and is to be anchored according to Manufacturer's requirements. The flexible hose can be exchanged with a hose of equal size and equal or greater pressure rating. Anchor requirements, specification sheet and hydrostatic pressure test certification matching the hose in service, to be onsite for review. These documents shall be posted in the company man's trailer and on the rig floor.
- 3. 5M or higher system requires an HCR valve, remote kill line and annular to match. The remote kill line is to be installed prior to testing the system and tested to stack pressure.
- 4. If the operator has proposed a multi-bowl wellhead assembly in the APD. The following requirements must be met:
  - a. Wellhead shall be installed by manufacturer's representatives, submit documentation with subsequent sundry.

- b. If the welding is performed by a third party, the manufacturer's representative shall monitor the temperature to verify that it does not exceed the maximum temperature of the seal.
- c. Manufacturer representative shall install the test plug for the initial BOP test.
- d. Whenever any seal subject to test pressure is broken, all the tests in 43 CFR part 3170 Subpart 3172 must be followed.
- e. If the cement does not circulate and one inch operations would have been possible with a standard wellhead, the well head shall be cut off, cementing operations performed and another wellhead installed.
- 5. The appropriate BLM office shall be notified a minimum of 4 hours in advance for a representative to witness the tests.
  - a. In a water basin, for all casing strings utilizing slips, these are to be set as soon as the crew and rig are ready and any fallback cement remediation has been done. The casing cut-off and BOP installation can be initiated four hours after installing the slips, which will be approximately six hours after bumping the plug. For those casing strings not using slips, the minimum wait time before cut-off is eight hours after bumping the plug. BOP/BOPE testing can begin after cut-off or once cement reaches 500 psi compressive strength (including lead cement), whichever is greater. However, if the float does not hold, cut-off cannot be initiated until cement reaches 500 psi compressive strength (including lead when specified).
  - b. In potash areas, for all casing strings utilizing slips, these are to be set as soon as the crew and rig are ready and any fallback cement remediation has been done. For all casing strings, casing cut-off and BOP installation can be initiated at twelve hours after bumping the cement plug. The BOPE test can be initiated after bumping the cement plug with the casing valve open. (only applies to single stage cement jobs, prior to the cement setting up.)
  - c. The tests shall be done by an independent service company utilizing a test plug not a cup or J-packer and can be initiated immediately with the casing valve open. The operator also has the option of utilizing an independent tester to test without a plug (i.e. against the casing) pursuant to **43 CFR part 3170 Subpart 3172** with the pressure not to exceed 70% of the burst rating for the casing. Any test against the casing must meet the WOC time for water basin (8 hours) or potash (24 hours) or 500 pounds compressive strength, whichever is greater, prior to initiating the test (see casing segment as lead cement may be critical item).
  - d. The test shall be run on a 5000 psi chart for a 2-3M BOP/BOP, on a 10000 psi chart for a 5M BOP/BOPE and on a 15000 psi chart for a 10M BOP/BOPE. If a linear chart is used, it shall be a one hour chart. A circular chart shall

have a maximum 2 hour clock. If a twelve hour or twenty-four hour chart is used, tester shall make a notation that it is run with a two hour clock.

- e. The results of the test shall be reported to the appropriate BLM office.
- f. All tests are required to be recorded on a calibrated test chart. A copy of the BOP/BOPE test chart and a copy of independent service company test will be submitted to the appropriate BLM office.
- g. The BOP/BOPE test shall include a low pressure test from 250 to 300 psi. The test will be held for a minimum of 10 minutes if test is done with a test plug and 30 minutes without a test plug. This test shall be performed prior to the test at full stack pressure.
- h. BOP/BOPE must be tested by an independent service company within 500 feet of the top of the Wolfcamp formation if the time between the setting of the intermediate casing and reaching this depth exceeds 20 days. This test does not exclude the test prior to drilling out the casing shoe as per 43 CFR part 3170 Subpart 3172.

#### C. DRILLING MUD

Mud system monitoring equipment, with derrick floor indicators and visual and audio alarms, shall be operating before drilling into the Wolfcamp formation, and shall be used until production casing is run and cemented.

#### D. WASTE MATERIAL AND FLUIDS

All waste (i.e. drilling fluids, trash, salts, chemicals, sewage, gray water, etc.) created as a result of drilling operations and completion operations shall be safely contained and disposed of properly at a waste disposal facility. No waste material or fluid shall be disposed of on the well location or surrounding area.

Porto-johns and trash containers will be on-location during fracturing operations or any other crew-intensive operations.

**KPI** 11/21/2023



#### **Break-test BOP & Offline Cementing:**

EOG Resources Inc. (EOG) respectfully requests a variance from the minimum standards for well control equipment testing of ECFR Title 43 Part 3172.6(b)(9)(iv) to allow a testing schedule of the blow out preventer (BOP) and blow out prevention equipment (BOPE) along with Batch Drilling & Offline cement operations to include the following:

- Full BOPE test at first installation on the pad.
- Full BOPE test every 21 days.
- This test will be conducted for 5M rated hole intervals only.
- Each rig requesting the break-test variance is capable of picking up the BOP without damaging components using winches, following API Standard 53, Well Control Equipment Systems for Drilling Wells (Fifth edition, December 2018, Annex C. Table C.4) which recognizes break testing as an acceptable practice.
- Function tests will be performed on the following BOP elements:
  - Annular **à** during each full BOPE test
  - Upper Pipe Rams **à** On trip ins where FIT required
  - Blind Rams **à** Every trip
  - Lower Pipe Rams à during each full BOPE test
- Break testing BOP and BOPE coupled with batch drilling operations and option to offline cement and/or remediate (if needed) any surface or intermediate sections, according to attached offline cementing support documentation.
- After the well section is secured, the BOP will be disconnected from the wellhead and walked with the rig to another well on the pad.
- TA cap will also be installed per Wellhead vendor procedure and pressure inside the
  casing will be monitored via the valve on the TA cap as per standard batch drilling
  ops.

Blind Rams

Roadside Kill

Test plug

# **Break Test Diagram (HCR valve)**

### Steps

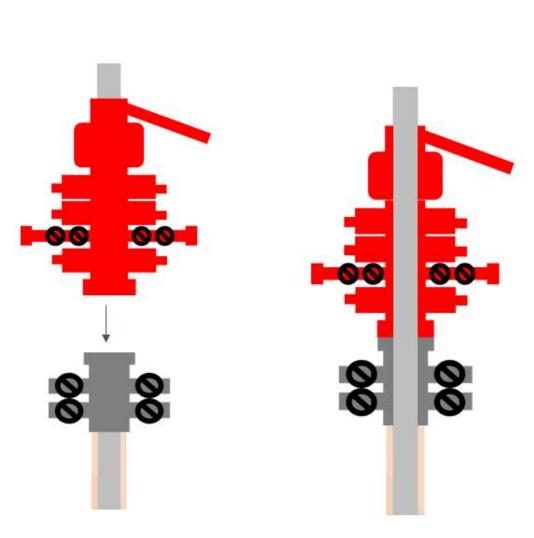
Pressure

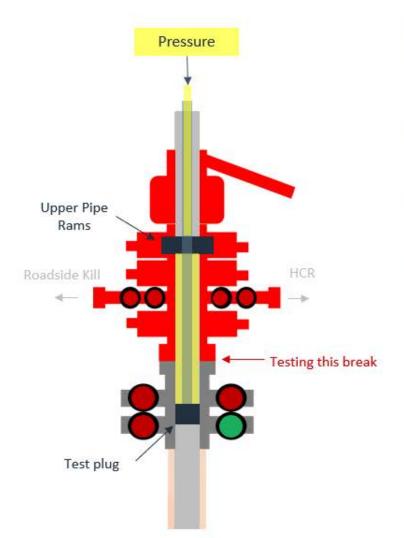
HCR

Testing this break

- 1. Set plug in wellhead (lower barrier)
- 2. Close Blind Rams (upper barrier)
- 3. Close roadside kill
- 4. Open HCR (pressure application)
- 5. Open wellhead valves below test plug to ensure if leak past test plug, pressure won't be applied to wellbore
- 6. Tie BOP testers high pressure line to main choke manifold crown valve
- 7. Pressure up to test break
- 8. Bleed test pressure from BOP testing unit

# **Break Test Diagram (Test Joint)**





#### Steps

- Set plug in with test joint wellhead (lower barrier)
- 2. Close Upper Pipe Rams (upper barrier)
- 3. Close roadside kill
- 4. Close HCR
- Open wellhead valves below test plug to ensure if leak past test plug, pressure won't be applied to wellbore
- Tie BOP testers high pressure line to top of test joint
- 7. Pressure up to test break
- Bleed test pressure from BOP testing unit



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#### **Cement Program**

1. No changes to the cement program will take place for offline cementing.

#### **Summarized Operational Procedure for Intermediate Casing**

- 1. Run casing as per normal operations. While running casing, conduct negative pressure test and confirm integrity of the float equipment back pressure valves.
  - a. Float equipment is equipped with two back pressure valves rated to a minimum of 5,000 psi.
- 2. Land production casing on mandrel hanger through BOP.
  - a. If casing is unable to be landed with a mandrel hanger, then the casing will be cemented online.
- 3. Break circulation and confirm no restrictions.
  - a. Ensure no blockage of float equipment and appropriate annular returns.
  - b. Perform flow check to confirm well is static.
- 4. Set pack-off
  - a. If utilizing a fluted/ported mandrel hanger, ensure well is static on the annulus and inside the casing by filling the pipe with kill weight fluid, remove landing joint, and set annular packoff through BOP. Pressure test to 5,000 psi for 10 min.
  - b. If utilizing a solid mandrel hanger, ensure well is static on the annulus and inside the casing by filling the pipe with kill weight fluid. Pressure test seals to 5,000 psi for 10 min. Remove landing joint through BOP.
- 5. After confirmation of both annular barriers and the two casing barriers, install TA plug and pressure test to 5,000 psi for 10 min. Notify the BLM with intent to proceed with nipple down and offline cementing.
  - a. Minimum 4 hrs notice.
- 6. With the well secured and BLM notified, nipple down BOP and secure on hydraulic carrier or cradle.
  - a. Note, if any of the barriers fail to test, the BOP stack will not be nippled down until after the cement job has concluded and both lead and tail slurry have reached 500 psi.
- 7. Skid/Walk rig off current well.
- 8. Confirm well is static before removing TA Plug.
  - a. Cementing operations will not proceed until well is under control. (If well is not static, notify BLM and proceed to kill)
  - b. Casing outlet valves will provide access to both the casing ID and annulus. Rig or third party pump truck will kill well prior to cementing.
  - c. Well control plan can be seen in Section B, Well Control Procedures.
  - d. If need be, rig can be moved back over well and BOP nippled back up for any further remediation.



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- e. Diagram for rig positioning relative to offline cementing can be seen in Figure 4.
- 9. Rig up return lines to take returns from wellhead to pits and rig choke.
  - a. Test all connections and lines from wellhead to choke manifold to 5,000 psi high for 10 min.
  - b. If either test fails, perform corrections and retest before proceeding.
  - c. Return line schematics can be seen in Figure 3.
- 10. Remove TA Plug from the casing.
- 11. Install offline cement tool.
  - a. Current offline cement tool schematics can be seen in Figure 1 (Cameron) and Figure 2 (Cactus).
- 12. Rig up cement head and cementing lines.
  - a. Pressure test cement lines against cement head to 80% of casing burst for 10 min.
- 13. Break circulation on well to confirm no restrictions.
  - a. If gas is present on circulation, well will be shut in and returns rerouted through gas buster.
  - b. Max anticipated time before circulating with cement truck is 6 hrs.
- 14. Pump cement job as per plan.
  - a. At plug bump, test casing to 0.22 psi/ft or 1500 psi, whichever is greater.
  - b. If plug does not bump on calculated, shut down and wait 8 hrs or 500 psi compressive strength, whichever is greater before testing casing.
- 15. Confirm well is static and floats are holding after cement job.
  - a. With floats holding and backside static:
    - i. Remove cement head.
  - b. If floats are leaking:
    - i. Shut-in well and WOC (Wait on Cement) until tail slurry reaches 500 psi compressive strength and the casing is static prior to removing cement head.
  - c. If there is flow on the backside:
    - i. Shut in well and WOC until tail slurry reaches 500 psi compressive strength. Ensure that the casing is static prior to removing cement head.
- 16. Remove offline cement tool.
- 17. Install night cap with pressure gauge for monitoring.
- 18. Test night cap to 5,000 psi for 10 min.



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#### **Example Well Control Plan Content**

#### A. Well Control Component Table

The table below, which covers the cementing of the <u>5M MASP (Maximum Allowable Surface Pressure) portion of the well</u>, outlines the well control component rating in use. This table, combined with the mud program, documents that two barriers to flow can be maintained at all times, independent of the BOP nippled up to the wellhead.

Intermediate hole section, 5M requirement

Component	RWP
Pack-off	10M
Casing Wellhead Valves	10M
Annular Wellhead Valves	5M
TA Plug	10M
Float Valves	5M
2" 1502 Lo-Torque Valves	15M

#### **B.** Well Control Procedures

Well control procedures are specific to the rig equipment and the operation at the time the kick occurs. Below are the minimal high-level tasks prescribed to assure a proper shut-in while circulating and cementing through the Offline Cement Adapter.

#### **General Procedure While Circulating**

- 1. Sound alarm (alert crew).
- 2. Shut down pumps.
- 3. Shut-in Well (close valves to rig pits and open valve to rig choke line. Rig choke will already be in the closed position).
- 4. Confirm shut-in.
- 5. Notify tool pusher/company representative.

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- 6. Read and record the following:
  - a. SICP (Shut in Casing Pressure) and AP (Annular Pressure)
  - b. Pit gain
  - c. Time
  - d. Regroup and identify forward plan to continue circulating out kick via rig choke and mud/gas separator. Circulate and adjust mud density as needed to control well.

#### **General Procedure While Cementing**

- 1. Sound alarm (alert crew).
- 2. Shut down pumps.
- 3. Shut-in Well (close valves to rig pits and open valve to rig choke line. Rig choke will already be in the closed position).
- 4. Confirm shut-in.
- 5. Notify tool pusher/company representative.
- 6. Open rig choke and begin pumping again taking returns through choke manifold and mud/gas separator.
- 7. Continue to place cement until plug bumps.
- 8. At plug bump close rig choke and cement head.
- 9. Read and record the following
  - a. SICP and AP
  - b. Pit gain
  - c. Time
  - d. Shut-in annulus valves on wellhead

#### **General Procedure After Cementing**

- 1. Sound alarm (alert crew).
- 2. Shut-in Well (close valves to rig pits and open valve to rig choke line. Rig choke will already be in the closed position).
- 3. Confirm shut-in.
- 4. Notify tool pusher/company representative.
- 5. Read and record the following:
  - a. SICP and AP
  - b. Pit gain
  - c. Time
  - d. Shut-in annulus valves on wellhead

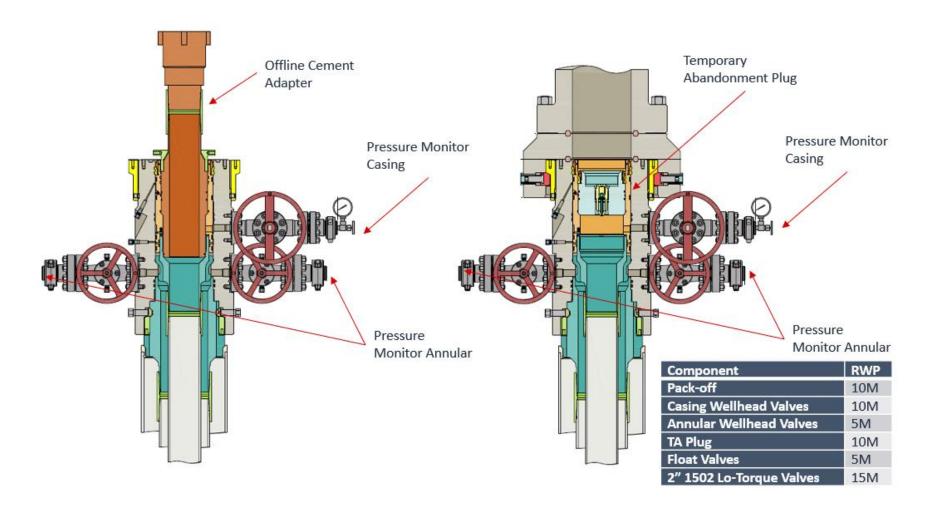
2/24/2022

Figure 1: Cameron TA Plug and Offline Adapter Schematic



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Figure 2: Cactus TA Plug and Offline Adapter Schematic



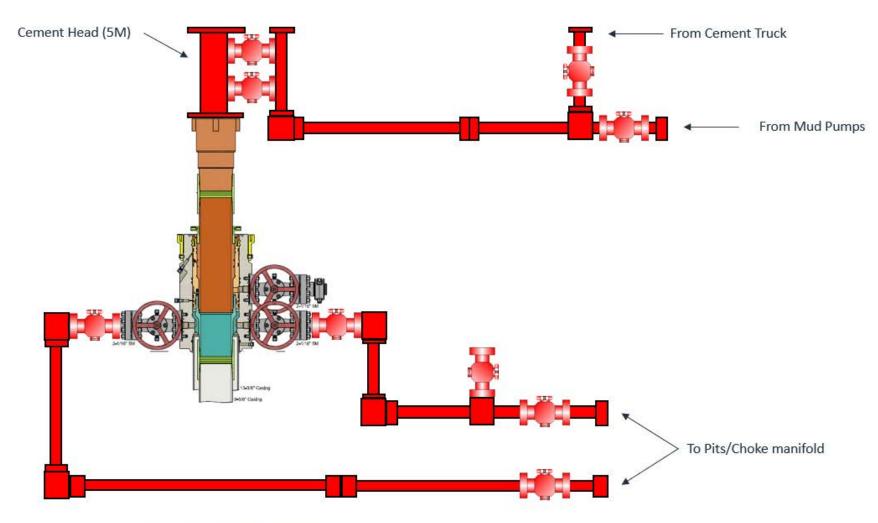
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Offline Intermediate Cementing Procedure

2/24/2022

Figure 3: Back Yard Rig Up



\*\*\* All Lines 10M rated working pressure

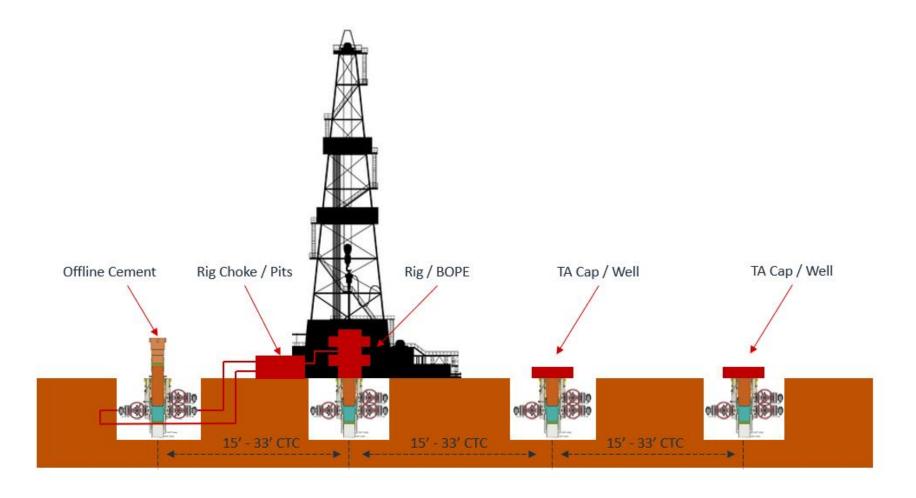
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Offline Intermediate Cementing Procedure

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Figure 4: Rig Placement Diagram



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# Salt Section Annular Clearance Variance Request

**Daniel Moose** 

# **Current Design (Salt Strings)**

## **0.422"** Annular clearance requirement

- Casing collars shall have a minimum clearance of 0.422 inches on all sides in the hole/casing annulus, with recognition that variances can be granted for justified exceptions.
- 12.25" Hole x 9.625"40# J55/HCK55 LTC Casing
  - 1.3125" Clearance to casing OD
  - 0.8125" Clearance to coupling OD
- 9.875" Hole x 8.75" 38.5# P110 Sprint-SF Casing
  - 0.5625" Clearance to casing OD
  - 0.433" Clearance to coupling OD

## **Annular Clearance Variance Request**

EOG request permission to allow deviation from the 0.422" annulus clearance requirement for the intermediate (salt) section from Onshore Order #2 under the following conditions:

- The variance is not applicable within the Potash Boundaries or Capitan Reef areas.
- Operator takes responsibility to get casing to set point in the event that the clearance causes stuck pipe issues

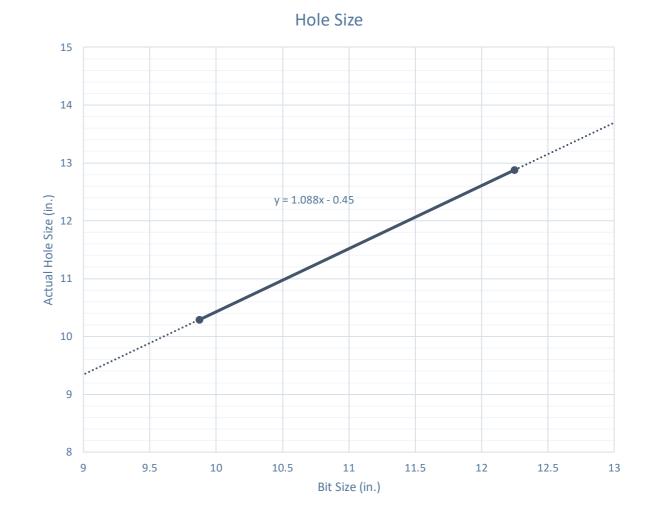
## **Volumetric Hole Size Calculation**

## **Hole Size Calculations Off Cement Volumes**

- Known volume of cement pumped
- Known volume of cement returned to surface
- Must not have had any losses
- Must have bumped plug

## **Average Hole Size**

- 12.25" Hole
  - 12.88" Hole
    - 5.13% diameter increase
    - 10.52% area increase
  - 0.63" Average enlargement
  - 0.58" Median enlargement
  - 179 Well Count
- 9.875" Hole
  - 10.30" Hole
    - 4.24% diameter increase
    - 9.64% area increase
  - 0.42" Average enlargement
  - 0.46" Median enlargement
  - 11 Well Count

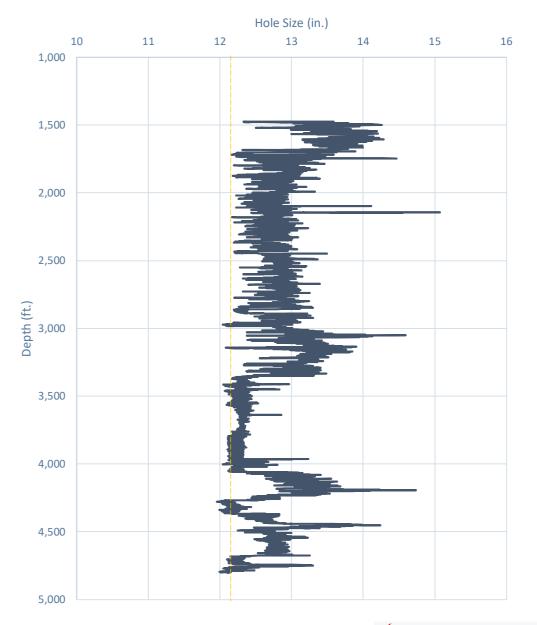


### Modelo 10 Fed Com #501H

# Caliper Hole Size (12.25")

## **Average Hole Size**

- 12.25" Bit
  - 12.76" Hole
    - 4.14% diameter increase
    - 8.44% area increase
  - 0.51" Average enlargement
  - 0.52" Median enlargement
  - Brine

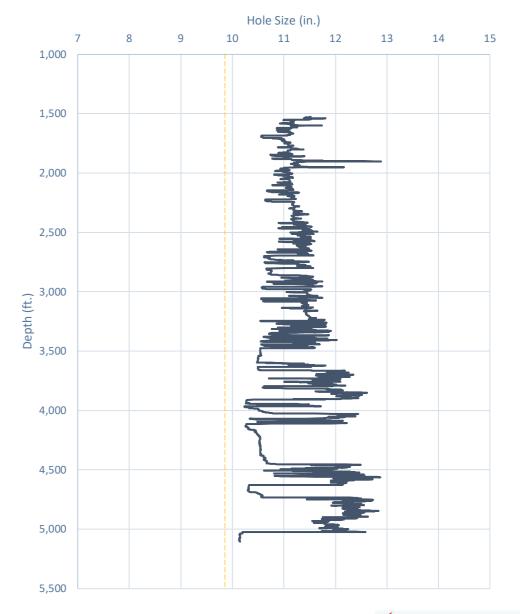


# Caliper Hole Size (9.875")

## **Average Hole Size**

- 9.875" Hole
  - 11.21" Hole
    - 13.54% diameter increase
    - 28.92% area increase
  - 1.33" Average enlargement
  - 1.30" Median enlargement
  - EnerLite

## Whirling Wind 11 Fed Com #744H



# **Design A**

# Proposed 11" Hole with 9.625" 40# J55/HCK55 LTC Casing

- 11" Bit + 0.52" Average hole enlargement = 11.52" Hole Size
  - 0.9475" Clearance to casing OD

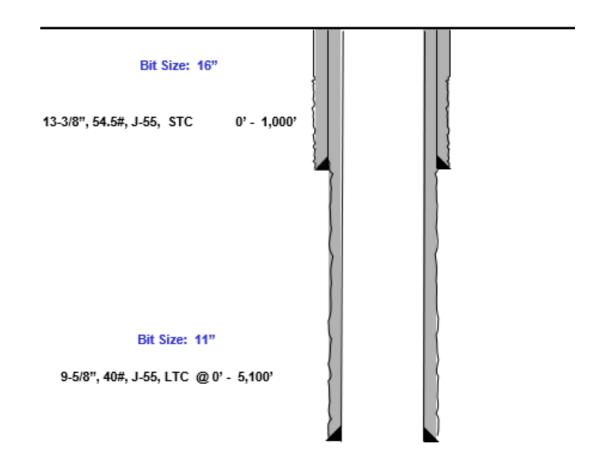
$$=\frac{11.52-9.625}{2}$$

• 0.4475" Clearance to coupling OD

$$=\frac{11.52-10.625}{2}$$

- Previous Shoe 13.375" 54.5# J55 STC
  - 0.995" Clearance to coupling OD (~1,200' overlap)

$$=\frac{12.615-10.625}{2}$$



## **Design B**

# Proposed 9.875" Hole with 8.625" 32# J55/P110 BTC-SC Casing

- 9.875" Bit + 0.42" Average hole enlargement = 10.295" Hole Size
  - 0.835" Clearance to casing OD

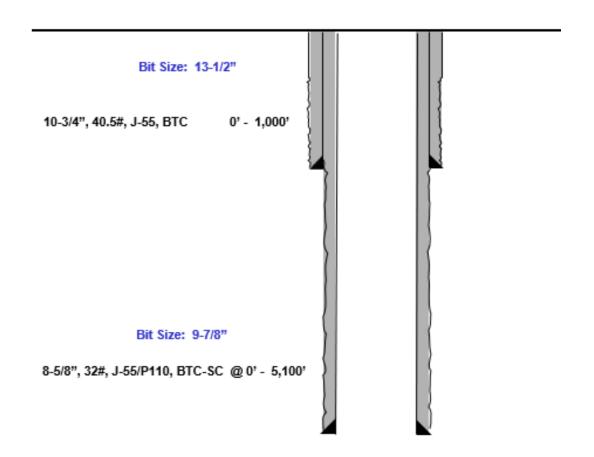
$$=\frac{10.295-8.625}{2}$$

• 0.585" Clearance to coupling OD

$$=\frac{10.295-9.125}{2}$$

- Previous Shoe 10.75" 40.5# J55 STC
  - 0.4625" Clearance to coupling OD (~1,200' overlap)

$$=\frac{10.05-9.125}{2}$$



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# Index

# **Casing Spec Sheets**

## PERFORMANCE DATA

API LTC 9.625 in 40.00 lbs/ft K55 HC Technical Data Sheet

Tubular Parameters					
Size	9.625	in	Minimum Yield	55	ksi
Nominal Weight	40.00	lbs/ft	Minimum Tensile	95	ksi
Grade	K55 HC		Yield Load	629	kips
PE Weight	38.94	lbs/ft	Tensile Load	1088	kips
Wall Thickness	0.395	in	Min. Internal Yield Pressure	3,950	psi
Nominal ID	8.835	in	Collapse Pressure	3600	psi
Drift Diameter	8.750	in		•	1

Connection Parameters				
Connection OD	10.625	in		
Coupling Length	10.500	in		
Threads Per Inch	8	tpi		
Standoff Thread Turns	3.50	turns		
Make-Up Loss	4.750	in		
Min. Internal Yield Pressure	3,950	psi		

11.454

## Pipe Body and API Connections Performance Data

13.375 54.50/0.380 J55 PDF

New Search »

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USC	Metric

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Mechanical Properties	Ptpe	втс	LTC	STC	
Minimum Yield Strength	55,000	-	-	-	psi
Maximum Yield Strength	80,000	-	-	-	psi
Minimum Tensile Strength	75,000	-	-	-	psi
Dimensions	Ptpe	втс	LTC	STC	
Outside Diameter	13.375	14.375	-	14.375	in.
Wall Thickness	0.380	-	-	-	in.
Inside Diameter	12.615	12.615	-	12.615	in.
Standard Drift	12.459	12.459	-	12.459	in.
Alternate Drift	-	-	-	-	in.
Nominal Linear Weight, T&C	54.50	-	-	-	lbs/ft
Plain End Weight	52.79	-	-	-	lbs/ft
Performance	Pipe	втс	LTC	STC	
Minimum Collapse Pressure	1,130	1,130	-	1,130	psi
Minimum Internal Yield Pressure	2,740	2,740	-	2,740	psi
Minimum Pipe Body Yield Strength	853.00	-	-	-	1000 lbs
Joint Strength		909	-	514	1000 lbs
Reference Length	-	11,125	-	6,290	ft
Make-Up Data	Ptpe	втс	LTC	STC	
Make-Up Loss	-	4.81	-	3.50	in.
Minimum Make-Up Torque	-	-	-	3,860	ft-lbs
Maximum Make-Up Torque		-	-	6,430	ft-lbs

Nom. Pipe Body Area

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5,250

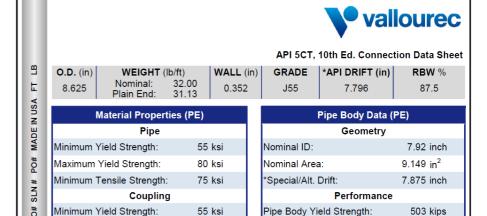
ft-lbs

# **Casing Spec Sheets**

#### Pipe Body and API Connections Performance Data

10.750 40.50/0.350 J55 PDF

New Search » « Back to Previous List USC Metric 6/8/2015 10:14:05 AM BTC LTC Ptpe STC **Mechanical Properties** Minimum Yield Strength 55,000 psi Maximum Yield Strength 80,000 Minimum Tensile Strength 75,000 psi BTC LTC Pipe STC 11.750 Outside Diamete 10.750 11.750 in. Wall Thickness 0.350 Inside Diameter 10.050 10.050 10.050 Standard Drift 9.894 9.894 in. Alternate Drift in. 40.50 Nominal Linear Weight, T&C lbs/ft 38.91 lbs/ft Plain End Weight Performance Ptpe BTC STC 1.580 1,580 Minimum Collapse Pressure psi Minimum Internal Yield Pressure 3.130 3.130 3.130 629.00 Minimum Pipe Body Yield Strength 1000 lbs 700 420 Joint Strength 1000 lbs Reference Length 11,522 6,915 BTC Make-Up Data Ptpe STC 4.81 Make-Up Loss 3.50 in. Minimum Make-Up Torque 3,150 ft-lbs



80 ksi

75 ksi

Coupling OD: 9.625"						
STC Performa	STC Performance					
STC Internal Pressure:	3,930	psi				
STC Joint Strength:	372	kips				
LTC Performa	ınce					
LTC Internal Pressure:	3,930	psi				
LTC Joint Strength:	417	kips				
SC-BTC Performance - Cp	olg OD =	9.125"				
BTC Internal Pressure:	3,930	psi				
BTC Joint Strength:	503	kips				
*	Alt Drift will	ho ucod un				

**API Connection Data** 

Maximum Yield Strength:

Minimum Tensile Strength:

A

S2L2

S

8.625

STAR

VALLOUREC

API Connection Torque					
	9	STC Tor	que (ft-lb	s)	
Min:	2,793	Opti:	3,724	Max:	4,655
LTC Torque (ft-lbs)					
Min:	3,130	Opti:	4,174	Max:	5,217
BTC Torque (ft-lbs)					
follow API guidelines regarding positional make up					

2,530 psi

3,930 psi

\*Alt. Drift will be used unless API Drift is specified on order.

Collapse Resistance:

Internal Yield Pressure:

(API Historical)

\*\*If above API connections do not suit your needs, VAM® premium connections are available up to 100% of pipe body ratings.

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Maximum Make-Up Torque



## **Amazing 19 Fed Package**

Wells in package:	Tgt TVD
Jefe 29 Fed Com #102H	8,818
Jefe 29 Fed Com #103H	8,818
Jefe 29 Fed Com #104H	8,818
Jefe 29 Fed Com #105H	8,818
Jefe 29 Fed Com #106H	8,818
Jefe 29 Fed Com #107H	8,818
Jefe 29 Fed Com #108H	8,818
Jefe 29 Fed Com #201H	8,907
Jefe 29 Fed Com #202H	8,907
Jefe 29 Fed Com #203H	8,907
Jefe 29 Fed Com #204H	9,094
Jefe 29 Fed Com #205H	9,094
Jefe 29 Fed Com #206H	9,094
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Jefe 29 Fed Com #214H	8,907
Jefe 29 Fed Com #215H	8,907
Jefe 29 Fed Com #301H	9,499
Jefe 29 Fed Com #302H	9,499
Jefe 29 Fed Com #303H	9,499
Jefe 29 Fed Com #304H	9,499
Jefe 29 Fed Com #305H	9,499
Jefe 29 Fed Com #306H	9,499
Jefe 29 Fed Com #581H	10,960
Jefe 29 Fed Com #582H	10,960
Jefe 29 Fed Com #584H	10,960
Jefe 29 Fed Com #586H	10,960

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1625 N. French Dr., Hobbs, NM 88240
Phone: (575) 393-6161 Fax: (575) 393-0720

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District III 1000 Rio Brazos Rd., Aztec, NM 87410 Phone:(505) 334-6178 Fax:(505) 334-6170

1220 S. St Francis Dr., Santa Fe, NM 87505 Phone:(505) 476-3470 Fax:(505) 476-3462

**State of New Mexico Energy, Minerals and Natural Resources Oil Conservation Division** 1220 S. St Francis Dr. **Santa Fe, NM 87505** 

CONDITIONS

Action 288698

#### **CONDITIONS**

Operator:	OGRID:
EOG RESOURCES INC	7377
P.O. Box 2267	Action Number:
Midland, TX 79702	288698
	Action Type:
	[C-103] NOI Change of Plans (C-103A)

#### CONDITIONS

Created By	Condition	Condition Date
pkautz	None	12/27/2023