(DO NOT USE THIS FORM FOR PROPOSA DIFFERENT RESERVOIR. USE "APPLICA PROPOSALS.) 1. Type of Well: Oil Well G 2. Name of Operator	Energy, Minerals and Nat OIL CONSERVATION 1220 South St. Fra Santa Fe, NM 8 ES AND REPORTS ON WELL LIS TO DRILL OR TO DEEPEN OR PR	ural Resources N DIVISION uncis Dr. 17505 S LUG BACK TO A	Revised August 1, 2011 WELL API NO. 30-025-38576 AND 30-025-42139 5. Indicate Type of Lease STATE FEE 6. State Oil & Gas Lease No. V07530-0001 7. Lease Name or Unit Agreement Name Linam AGI 8. Wells Number 1 and 2 9. OGRID Number 36785				
DCP Operating Company, LP 3. Address of Operator			10. Pool name o	or Wildcat			
6900 E. Layton Ave, Suite 900, Denv	ver CO 80237		Wildcat				
4. Well Location	n the South line and 1980 feet fi	om the West line					
Section 30	Township 18S	Range 37E	NMPM	County Lea			
	11. Elevation (Show whether Di	2					
12. Check Appropriate Box to Ir	3,736 GR	enort or Other D	ata				
TEMPORARILY ABANDON	ENTION TO: PLUG AND ABANDON CHANGE PLANS MULTIPLE COMPL	REMEDIAL WOR COMMENCE DRI CASING/CEMEN	ILLING OPNS. T JOB	ALTERING CASING P AND A and Notification parameter			
13. Describe proposed or complete of starting any proposed work) proposed completion or recomp	. SEE RULE 19.15.7.14 NMAC pletion.	C. For Multiple Com	pletions: Attach v	vellbore diagram of			
for Linam AGI #1 and AGI #2 and Ro Wells This is an annual summary submittal of casing annulus pressure for Linam AGI	data as agreed to between DCP	and NMOCD relativ	e to injection pres	sure, TAG temperature and			
in October 2015. The analyses of data from both wells ha 2017 and was used exclusively until Ma #2 operated in July 2020 until AGI #1 o	ve been submitted monthly. The	e AGI #1 well was so narily to AGI #2 thro	accessfully worked	d over as planned in June Both the AGI #1 and AGI			
2021 through January 2022, after which exclusively to AGI #1 through June 202 simultaneous and switching of well use NMOCD with the required summary of to keep the approved immediate notifical	, AGI #1 and AGI #2 operated s 3. AGI #2 was used exclusively are noted in the attached annual data for the 2023 calendar year	imultaneously and by from July 2023 through summary of the data for the operation of the data.	riefly in February ough December 20 The purpose of	2022 before switching 23. The effects of the this submittal is to provide			
The summary of the data and supporting	-			. 1/01/000			
SIGNATURE Type or print name Alberto A. Gutierrez	TITLE <u>Consultant to</u> z, <u>RG</u> E-mail addres	DCP Midstream/ Gos: aag@geolex.com		<u>8 1/21/2024</u> 505-842-8000			
For State Use Only APPROVED BY:	TITLE		DA	.TE			
Conditions of Approval (if any):				Page 1 of 15			

ANALYSIS OF 2023 ANNUAL TRENDS AND REQUEST TO CONTINUE WITH APPROVED IMMEDIATE NOTIFICATION PARAMETERS FOR OPERATION OF LINAM AGI #1 AND LINAM AGI #2 (API #s 30-025-38576 AND 30-025-42139) UNDER R-12546-All

This document presents the results from the analyses of the injection parameter data collected from the Linam AGI #1 and #2 wells which serve the Linam Ranch Gas Processing Facility near Hobbs, NM. Data from the Linam AGI #1 has been collected continuously since 2012 and has been analyzed on a monthly basis by Geolex and transmitted to DCP for reporting to NMOCD as required by ACO-275 and the approved post-workover C-103. In addition, the Linam AGI #2 well was completed and brought online in October 2015. The AGI #2 well was completed in the same injection zone as the AGI #1 approximately 450 feet to the southwest of AGI #1. From the time that the AGI #2 was brought online, injection has been either into both wells simultaneously or solely into one of the two wells. AGI #2 was operated in conjunction with AGI #1 from October 2015 to January 2016 when a switch was made to operate only AGI #1 for the remainder of 2016. In May 2017, DCP switched over to injecting into AGI #2 to allow for the workover of AGI #1. The workover was completed on June 8, 2017, and AGI #1 was brought back online in July 2017 with bottom hole sensors installed. These sensors are now serving to monitor downhole and reservoir conditions since the downhole sensors in AGI #2 failed due to a lightning strike shortly after installation (2015) and will not be able to be repaired until sometime in the future when AGI #2 is worked over. In the meantime, to obtain reservoir data which would have been provided by the downhole PT sensors in AGI #2, a slick line with a pressure recorder was placed into AGI #2 and downhole pressure data are collected under both injection and non-injection conditions for the AGI #2 and AGI #1. Since that time, the downhole sensors in AGI #1 provide the reservoir data needed to evaluate the performance of the two wells. The system continued operating through 2018 with only AGI #1 active while waiting for independent flow meters to be installed/repaired in both wells so that reliable flow information would be available for each well independently. This operational mode (utilizing only AGI #1) continued through April 2019, and, to date, separate volume meters have not been installed/repaired. In May 2019, however, DCP began dividing the flow of acid gas between the two wells by using one or the other well exclusively (see Figure 3). This practice continues today with all flow having gone to AGI #1 from January 2022 through May 2023 and was switched entirely to AGI #2 for the rest of the year. Presently, surface data from both wells is being collected relative to the following parameters:

- Treated Acid Gas (TAG) surface injection pressure (both wells)
- TAG injection temperature (both wells)
- Annular pressure (both wells)
- Bottom Hole pressure and temperature (AGI #1 only beginning 7/2017)
- Overall total TAG flow rate from compressors

The parameters above are currently being measured in both wells in order to monitor the operations of the wells, prevent hydrate formation, and reduce corrosion potential. While improvements have been implemented in the placement of temperature controls, dehydration of TAG during compression, and other systems improvements at the AGI facility, there continue to be variations in the desired and normal

operating levels of the above-referenced parameters. Since these parameters are useful indicators and predictors of potential operational or mechanical problems in the well, various levels of alarms have been established for each of these parameters. These parameters include three which are measured directly (TAG injection pressure, TAG injection temperature, and annular pressure) and one (differential pressure) which is a calculated value (the difference between the two measured parameters of injection and annular pressure). The analyses of the long-term trends in these values have been useful in smoothing out shorter-term variations which can be observed from detailed inspection of hourly data and in the development of appropriate alarm bands for each parameter.

The Linam AGI #1 experienced a tubing leak in late 2011 which was partially addressed in a workover conducted in April/May 2012. At the beginning of 2012 (until the time of the workover) the injection parameters were reviewed, analyzed, and reported weekly to the NMOCD. Following the workover in which the tubing leak was repaired, some compromised production casing was detected immediately above the packer depth. At that time, we recommended keeping only approximately 250 psig on the annular space between the tubing and casing in AGI #1 since, with annular pressure at this level under normal operating conditions, this parameter can serve as a useful indicator of when activity should be initiated to prevent damage to the well or trigger an NMOCD shutdown and/or immediate notification requirements. Concern about this compromised casing was eliminated by stacking packers when the well was worked over again in June 2017. Data from January 2012 through December 2015 are included in our analysis, but only the post-workover data have been used to develop the recommended alarm and emergency shutdown (ESD) levels in conjunction with the requirements of NMOCD Order 12546-All, ACO-275, and the post-workover C-103.

Furthermore, a similar process has been employed on the Linam AGI #2 since it was brought online in October 2015. As described above, this well is equipped with bottom hole (just at top of packer) pressure and temperature measurement capability both inside and outside the tubing. The immediate notification parameters for both wells were developed from long-term analysis of the injection data. Initial testing of the Linam AGI #2 indicated that the pressure variations induced by flow rate and temperature fluctuations in the Linam AGI #1 are influencing the reservoir as measured in the AGI #2 location. This is to be expected as the newer well is completed in the same zone at a distance away from the initial well which we predicted would see the edge of the plume in about 7 years. The Linam AGI #1 has been injecting since 2007.

Data from the AGI #1 was continuously collected and analyzed weekly prior to the original workover in April/May 2012. This data collection, analysis, and reporting continues monthly as mandated by NMOCD. Since it is necessary to evaluate the data from both wells to know how the system is operating overall, the surface data from AGI #2 are also being collected, analyzed, and reported monthly although the reporting requirement for the AGI #2 is quarterly.

The NMOCD also requires that immediate notification parameters and levels be discussed and agreed upon with the agency and that these be periodically reviewed and updated as needed based on operational or regulatory changes. The immediate notification parameters for both wells have been approved by NMOCD and DCP requests no changes in these approved values. With this requirement in mind and for

the purpose of protecting the mechanical integrity and safety of both wells and the overall AGI facility, Geolex monitors these data under contract to DCP to prevent damage to the wells or violation of regulatory requirements or permit constraints.

Geolex has carefully and continuously assembled and analyzed the performance data and trends for the Linam AGI #1 and AGI #2 since 2012 and 2015, respectively. Several important observations can be made from analyzing this data and taking into consideration important system modifications that have occurred in the post-workover period from June 2012 through December 2023. These include the following:

- 1. AGI #1 Post-Workover MIT completed in May 2012
- 2. AGI #1 MIT test completed November 14, 2012
- 3. Bleeding of diesel from casing annular space immediately after the November 2012 AGI #1 MIT test.
- 4. AGI #1 MIT test completed April 30, 2013
- 5. Addition of diesel in annular space after April 2013 AGI #1 MIT and May 2013 plant shutdown
- 6. AGI #1 MIT test completed October 30, 2013
- 7. Failure of the VFD for the cooler on the AGI compressor from February 4 through 9, 2014.
- 8. AGI #1 MIT test completed April 30, 2014
- 9. Addition of diesel in annular space after April 2014 AGI #1 MIT
- 10. AGI #1 MIT test completed September 19, 2014
- 11. AGI #1 MIT test completed March 19, 2015
- 12. AGI #1 MIT test completed September 15, 2015
- 13. AGI #2 brought online with startup in October-November 2015 and operated until January 2016
- 14. AGI #1 MIT test completed March 22, 2016
- 15. AGI #2 MIT test completed April 1, 2016
- 16. AGI #2 TAG lines bled to flare on June 13, 2016 to remove static TAG in line when well is not operating
- 17. AGI #1 MIT test completed September 14, 2016
- 18. AGI #2 MIT test completed February 16, 2017
- 19. AGI #1 Workover completed June 8, 2017 including stacked packer, bottom hole PT gauges
- 20. AGI #1 MIT test completed June 7, 2017 after workover completion
- 21. AGI #2 MIT test completed February 15, 2018
- 22. AGI #1 MIT test completed June 19, 2018
- 23. AGI #2 MIT test completed February 15, 2019
- 24. AGI #1 MIT test completed February 15, 2019
- 25. AGI #1 MIT test completed February 4, 2020
- 26. AGI #2 MIT test completed February 4, 2020
- 27. AGI #1 MIT test completed February 9, 2021
- 28. AGI #2 MIT test completed February 9, 2021
- 29. AGI #1 MIT test completed August 12, 2021
- 30. AGI #1 MIT test completed February 14, 2022
- 31. AGI #2 MIT test completed February 14, 2022

- 32. AGI #1 MIT test completed August 17, 2022
- 33. AGI #1 MIT test completed February 14, 2023
- 34. AGI #2 MIT test completed February 14, 2023
- 35. AGI #1 MIT test completed November 1, 2023

The following trends have been observed in the AGI well data and are reflected in Figures 1-4:

- TAG injection pressure, which was on a slight increasing trend due to slightly increasing average
 temperature of injected TAG, began to level off due to temperature decreases in 2017. This trend
 continued over the last six months of 2018 until flow began cycling between AGI #1 and AGI #2
 in May 2019. The TAG injection pressure and rate has been more variable since 2016 due to inlet
 flow variations.
- 2. AGI #1 was used exclusively following the workover from July 2017 through April 2019. Beginning in May 2019, the flow of TAG was split between the two wells with either one or the other being used with simultaneous operation occurring for only brief periods of time, if at all (Figure 3).
- 3. The TAG injection temperature is significantly lower during periods of low flow or no flow when the other well is being used.
- 4. Pressure in the casing annulus has been consistently tracked; the correlative behavior of annular pressure with flowrate, injection pressure, and temperature confirms both wells have good integrity and are functioning as expected (Figures 1 and 2). The injection temperature is the largest influencer of this parameter under normal conditions.
- 5. The pressure differential between the casing annulus and the TAG injection pressure clearly indicates that no communication currently exists between the tubing and the casing annulus.
- 6. The generally low annular pressures observed, especially in recent years, indicate that the production casing and cement continue to have good integrity.
- 7. TAG injection temperatures can now be lower due to the improvement of water reduction in compression which reduces the potential for hydrate formation at lower temperatures. This has allowed for relatively lower injection temperatures from 2018 to 2023 in AGI #1 and, generally, more stable operational temperatures in AGI #2.
- 8. The behavior of the reservoir in terms of pressure and temperature when switching between wells clearly demonstrates that the bottom hole sensors in AGI #1 are sufficient for recording reservoir conditions in both wells (Figure 4).
- The behavior of the reservoir in response to injection demonstrates that the reservoir is not
 pressuring up significantly and responds quickly to reduction of pressure upon cessation of
 injection.

There is no current indication of the reservoir being pressured up to any significant degree by the injection from Linam AGI #1. This was confirmed during the drilling and testing of AGI #2. Upon startup from any shutdown that lasts more than 6-8 hours it is critical to inject methanol along with the TAG for the initial startup period to prevent the formation of hydrates. While this may no longer be necessary due to the changes which were made in the water removal efficiency of the AGI compressor system, it is a good preventative measure. Prior to the increased water removal efficiency, this effect was observed in the period of March 2013 when hydrate formation during one of these events caused a spike

in TAG injection pressure of approximately 35% over normal pressures due to partial blockage of the injection line and tubing created by hydrate formation. This persisted for several hours until the situation was alleviated by the stabilization of the compressor and the simultaneous injection of methanol to cause the hydrates to be reabsorbed into the TAG. Subsequently, injection pressures and temperatures returned to normal.

It is also critical to maintain temperature control on the injected TAG and to avoid rapid temperature or pressure fluctuations during periods when power failures or other mechanical failures may occur. The extensive and wide variation in TAG injection temperatures resulted in the formation of free water and corrosion within the tubing resulting in a tubing leak which had to be repaired in April/May 2012. Temperature control changes were implemented and helped to significantly control downward swings in temperature and prevent the formation of hydrates. However, in February 2014, there was a failure in the VFD for the cooler on the AGI compressor which persisted for five days. During this time, the TAG temperature increased to at least 150 °F and resulted in a dramatic increase in the annular pressure due to the heating of the diesel fluid in the annular space. TAG temperature as well as annular pressure returned to the normal range once the VFD on the cooler was repaired. The significant spread between TAG injection pressure and the annular pressure maintained even during this heating episode confirms the continued integrity of the well, packer, casing, and tubing. However, the rise in annular pressure has the potential to damage the integrity of the compromised casing in the well and should be avoided in subsequent operations. In response to these issues, DCP undertook and successfully completed a project in 2015 to address the temperature fluctuations resulting from compression controls and to increase the efficiency of water removal to the point where all free water is removed from the TAG prior to injection. This significantly reduces hydrate formation potential in the entire system regardless of temperature variations. This has provided for lower average injection temperatures observed without resulting in hydrate formation.

In October 2015, AGI #2 began operating in a startup mode, switching operation back and forth with AGI #1. This effect is reflected in the trend data shown in Figure 2. Due to a volume meter sensor failure and configuration issues, only total flow to the AGI system can be reliably measured through 2019. For 2021, AGI #1 operated exclusively from January through February with AGI #2 operating the remainder of the year and through February 2022, after which, AGI #1 was operated exclusively through June 2023. AGI #2 was operated exclusively from July 2023 through December 2023. On the rare occasion that both wells are in operation simultaneously, this typically occurs only briefly. See Figure 3 for total flowrate and flowrate of both the AGI #1 and AGI #2 wells.

REVIEW OF STATISTICAL ANALYSIS OF INJECTION PARAMETERS, DEVELOPMENT OF AND REQUEST TO CONTINUE WITH APPROVED IMMEDIATE NOTIFICATION PARAMETERS (API #s 30-025-38576 AND 30-025-42139) UNDER R-12546-All

The statistical analyses of the injection parameter data were initially conducted for the purpose of establishing normal operating levels for the parameters that are automatically monitored. Several data filtering steps were undertaken to take the hourly data, which forms the basis of the analysis, in order to smooth out variability and to account for the physical changes in the well and its operation after the repair of the tubing leak and the workover completed in May 2012. Because the configuration of the well changed dramatically after the workover, only data after the well had stabilized post-workover were used in this analysis. Additionally, in June 2017 during a workover, AGI #1 was equipped with a stacked packer configuration. The bottom hole pressure and temperature sensors installed during the 2017 workover of AGI #1 have been providing excellent data, as shown in Figure 4. During 2018, communication issues between the Halliburton BHPT panel and the plant DCS system were corrected. BHPT readings had been inaccurately reported from November 2017 to June 2018 until this issue was detected. In 2018, for the period affected, we downloaded the data directly from the Halliburton panel and corrected the values. A C-103 was submitted with these corrections in July 2018. The corrected values are used in this analysis. No problems with BHPT readings occurred from 2019 through 2023. It is clear from the variation in these parameters when flow is switched between wells that the conditions measured in the BHPT gauge in AGI #1 reflect the values in the reservoir which would be very similar to AGI #2 if the BHPT gauges in the well were operational.

All the data are summarized in Table 1 and the calculated statistical parameters of arithmetic mean and standard deviation were used to establish base levels and variability for each parameter. The results of these analyses resulted in the immediate notification parameters which were approved both for AGI #2 and the parameters required under ACO-275 for AGI #1.

Based on the analysis of observed trends, the immediate notification parameters which were approved for AGI #1 and the parameters previously approved for AGI# 2 and continued through 2023 remain appropriate to continue through 2024. This is DCPs request and the approved immediate notification parameters are detailed below:

The approved immediate notification parameters for Linam AGI #1 are summarized below:

- 1. Exceedance of the approved MAOP of 2,644 psig for a period greater than two hours.
- 2. Failure of a mechanical integrity test (MIT) of the well.
- 3. Confirmation of any condition that indicates a tubing, packer or casing leak.
- 4. Any increase of the annular pressure to a value that is greater than 1,200 psig
- 5. Any instance in which differential pressure between the injection tubing and injection tubing annulus is less than 100 psig.
- 6. Any release of H₂S at the well which results in an activation of the facility's approved Rule 11 H₂S contingency plan.
- 7. Any workover or maintenance activity that requires intrusive work in the well.

The approved immediate notification parameters for the Linam AGI #2 are summarized below:

- 1. Exceedance of the approved MAOP of 2,644 psig for a period greater than two hours.
- 2. Failure of a mechanical integrity test (MIT) of the well.
- 3. Confirmation of any condition that indicates a tubing, packer or casing leak.
- 4. Any increase of the annular pressure to a value that is more than 80% of the injection pressure.
- 5. Any release of H₂S at the well which results in an activation of the facility's approved Rule 11 H₂S contingency plan.
- 6. Any workover or maintenance activity that requires intrusive work in the well.

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 TABLE 1 SUMMARY DATA ANALYSIS OF LINAM AGI #1 AND AGI #2 TRENDS FOR JANUARY 2012 THROUGH DECEMBER 2023

DCP MIDSTREAM LINAM RANCH AGI #1 AND #2 CUMULATIVE INJECTION DATA

						AGI #1 Surface								AGI #2 Surface	Total CO2	
		AGI #1 Surface	AGI #1 TAG	AGI #1 Surface		Injection/Casing Annular	AGI #1 Average	AGI #1 Average	AGI #2 Surface TAG	AGI #2 Surface Casing	AGI #2 Surface TAG	AGI #1		Injection/Casing	Sequestered per	
		TAG Injection	Injection	Casing Annulus	Total Flowrate	Pressure Differential	Bottom Hole	Bottom Hole	Injection Pressure	Annulus Pressure	Injection	Flowrate	AGI #2 Flowrate	Annular Pressure	month (Metric	
Mont	h Ended		Temperature (°F)		(MSCFPH)	(psig)	Pressure (psig)	Temperature (°F)	(psig)	(psig)	Temperature (°F)	(MSCFPH)	(MSCFPH)	Differential (psig)	Ton)	Notes
January	2012 Jan				-			, , ,	11 07	11 07	, ,	N/A	()	,	No Flow Data Available
February	2012 Feb											N/A	()		No Flow Data Available
March	2012 Mar	-12 147			N/A	429						N/A	()		No Flow Data Available
April	2012 Apr											N/A)		No Flow Data Available
May	2012 May											120)	3693	
June	2012 Jun											113)		Plant Workover and Shutdown
July	2012 Jul											148)	4562	
August	2012 Aug											137)	4218	
September	2012 Sep											152)	4547	
October November	2012 Oct 2012 Nov											167 191)	5150	November 14, 2012 MIT Test
December	2012 Nov											155)	4775	
January	2012 Dec											151)	4664	
February	2013 Feb											174)	4845	
March	2013 Mar											179)	5514	
April	2013 Apr											178)		April 30, 2013 MIT Test
May	2013 May	-13 151										154)	4753	
June	2013 Jun											166	()	4957	
July	2013 Jul				177	1375						177	()	5461	
August	2013 Aug	-13 156	5 12							ļ		171			5291	
September	2013 Sep											179			5343	
October	2013 Oct											174	(October 30, 2013 MIT Test
November	2013 Nov											171	()	5103	
December	2013 Dec											175			5414	
January	2014 Jan									-		166			5131	
February	2014 Feb											182			5083	
March	2014 Mar 2014 Apr								-	-	1	162		,	5011	April 30, 2014 MIT Test
April May	2014 Apr 2014 May									-		175 170		1	5242	
June	2014 Iviay 2014 Jun											162)	4844	
July	2014 Juli											167)	5144	
August	2014 Aug											161)	4971	
September	2014 Sep											158)		September 19, 2014 MIT Test
October	2014 Oct											170)	5241	
November	2014 Nov											158)	4716	
December	2014 Dec											168)	5173	
January	2015 Jan	-15 163	1 12	.5 180	151	1451						151	()	4666	
February	2015 Feb				161	1407						161	()	4491	
March	2015 Mar				161	. 1357	1					161	()	4984	March 19, 2015 MIT Test
April	2015 Apr											163	()	4869	
May	2015 May											159	()	4911	
June	2015 Jun											152)	4531	
July	2015 Jul											154)	4746	
August	2015 Aug											131)	4048	
September October	2015 Sep 2015 Oct											163 160				September 15, 2015 MIT Test AGI #2 Operations Began October 2015
November	2015 Nov				164				1430	394	1 109			103		AGI #1 & #2 both in use
December	2015 Dec								1498					100		AGI #1 & #2 both in use
January	2016 Jan								1094		77			109		AGI #2 not in use
February	2016 Feb								1603) 49			160		AGI #2 not in use
March	2016 Mar								1679		1 58			167		AGI #2 not in use
April	2016 Apr	-16 168	2 11			1400			1688	1	63			168	7 4304	AGI #2 not in use
May	2016 May	-16 167	8 11	.6 250	185	1428			1685	1	1 70	185	(168	4 5714	AGI #2 not in use
																AGI #2 not in use. TAG trapped in blocked off section of AGI #2
June	2016 Jun								2	. 1	L 81		(<u> </u>	1 5709	
July	2016 Jul									. 1	1 88					AGI #2 not in use
August	2016 Aug	-16 171							3	1	1 78					AGI #2 not in use
September	2016 Sep								3	1	1 73					AGI #2 not in use
October	2016 Oct							ļ	1 2	. L	68)		AGI #2 not in use
November	2016 Nov								1		54					AGI #2 not in use
December	2016 Dec								1		43					AGI #2 not in use
January	2017 Jan										45					AGI #2 not in use
February	2017 Feb	-17 175	0 11	.9 958	186	791	1		10	278	54	186	-	-26	, 5189	AGI #2 not in use
	1				1											Both wells used; #2 flow meter not functioning. AGI #1 for entire
March	2017 Mar	-17 170	8 11	.4 782	186	927	.		1701	373	3 104	175	14	132	7	month and AGI #2 only from 3-13 to 3-16 and 3-21 to 3-31
IVIGICII	ZUI/ IVIAI	1/0	11	/82	. 180	927	1		1701	3/3	, 102	1/3	1.	. 132	, 5745	Both wells used. Flow meter for #2 not working. TAG routed to #1
	1				1											well exclusively, both wells simultaneously and #2 well exclusively.
						1										All TAG routed to #2 from 4-26 onward in anticipation of
April	2017 Apr	-17 165	1 10	15 418	194	1234			1862	296	100	153	41	156	6 5798	workover of #1 well.
	2027 Apr			410	154	1234			1802	250	100		4.	150	3730	Both wells used. #2 Flow Meter not working. TAG Routed to AGI
						1										#2 save for 19 hour period from 5-17 to 5-18 when it was routed
						1										to AGI #1. AGI #1 workover 5-22 thru 6-8. AGI #2 experienced
	1				1											mechanical blockage resulting in both wells being shut down from
May	2017 May	-17 159	6 10	203	155	1390			1842	66	104	49	150	177	2 4787	5-25 to 5-31.
										-						
						1										Both wells used. #2 used from 6-2 through 6-15. Workover of #1
						1										completed 6-8 and sucessful MIT performed 6-8; #1 back online 6-
						1										15. #1 and #2 used simultaneously from 6-15 to 6-30.
						1										Mechanical Problem with flow meter for #2 well. Only total flow
						1										can be measured; no way to differentiate between #1 and #2
	2017 Jun	-17 143	οI c	9 429	147	1010	ıl.	I	1838	tl 1	113	40	107	183	7 4394	when they are used together.

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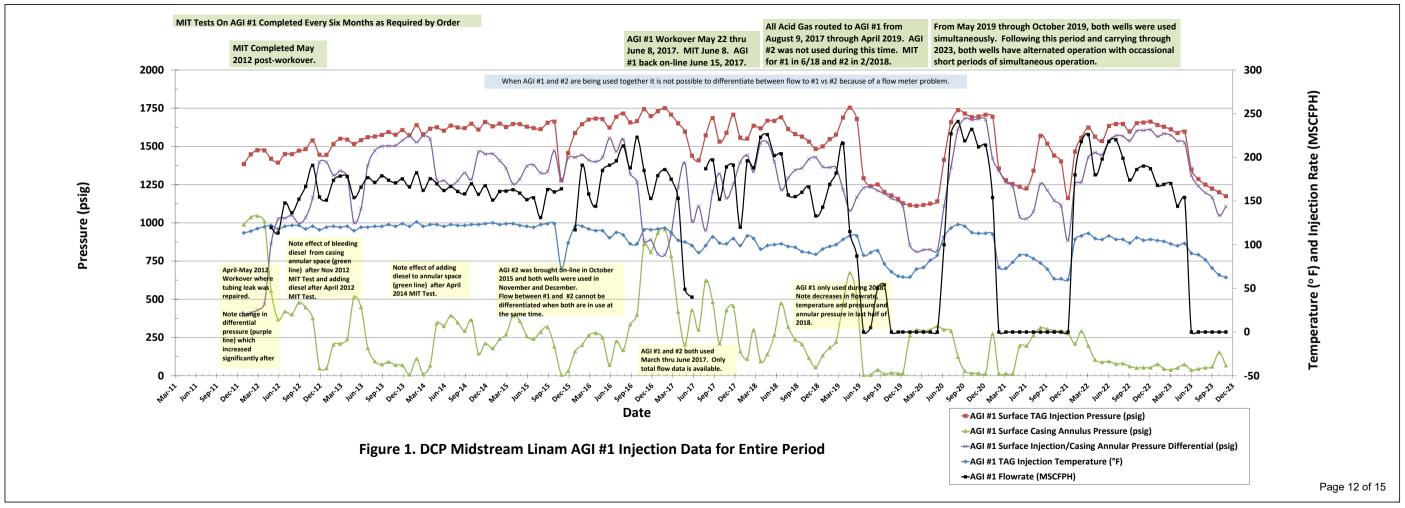
Мо	onth En	nded			AGI #1 TAG Injection Temperature (°F)	AGI #1 Surface Casing Annulus Pressure (psig)	Total Flowrate	AGI #1 Surface Injection/Casing Annular Pressure Differential (psig)	AGI #1 Average Bottom Hole Pressure (psig) Temperature (°F)	AGI #2 Surface TAG Injection Pressure (psig)	AGI #2 Surface Casing Annulus Pressure (psig)	AGI #2 Surface TAG Injection Temperature (°F)	AGI #1 Flowrate AGI #2 Flowrate (MSCFPH)	AGI #2 Surface Injection/Casing Annular Pressure Differential (psig)	Total CO2 Sequestered per month (Metric Ton) Notes Both wells used. Annular Pressure Meter for AGI #2
July	20	017	Jul-17	1409	91	. 302	171	1108	4392 1	37 181	0 sensor error	10	2	n/a	malfunctioning for month of July. Mechanical problem with flow meter for #2 well persists. Bottomhole sensors added to #1 Well as part of workover completed in June and began recording data 5281 on 7-20-17
August			Aug-17	1572		621								0 106	Both wells used. Mechanical problem with flow meter for #2 well persists. Only total flow data available. Annular Pressure meter for AGI #2 back in service 8-11-17. Annular Pressure and differential pressure readings are for period 8-11-17 through 8-31
September	20	017	Sep-17	1685	109	482	197	1203	4578 1	35 126	7 134	4 7	7 197 (113	Only AGI #1 used. Entire plant shut down from Sept 19 to Sept 30th for a scheduled turnaround. Data available only for first 19 5888 days of September Plant shutdown 9-19 through 10-3 for a turnaround. Only AGI #1
October	20	:017	Oct-17	1531	102	211	152	1321	4250 1	36 87.	2 9:	7 6	3 152	77	used during remainder of month. Major software upgrade in DCS.
November December			Nov-17 Dec-17	1589 1707	101 107	428			4080 1 4080 1	36 101 36 110		<u> </u>	6 189 4 191	93	
January		017	Jan-18	1557		160				33 70			† †	5 103	'
February			Feb-18	1551					1	31 78			5 250	52	'
March April		018	Mar-18 Apr-18	1635 1618		300			1	93 31 115			0 100	93	
May	20	018	May-18	1668	99	141	226	1527	4646 1	31 112	0 198	8 7	9 226 (92	21 6980 Only AGI #1 in use.
June		018	Jun-18 Jul-18	1667 1690		1			•	32 106 32 108				90	
July August		018	Jul-18 Aug-18	1690 1614		321			1				2 157	90	'
September	20	018	Sep-18	1581	97	237	155	1345	4534 1	30 89	8 154	4 7	2 155	74	14 4633 Only AGI #1 in use.
October November			Oct-18	1564 1531		206				30 83 29 114			100	0 69	
			Nov-18		91	55							1	103	
December		018	Dec-18	1483 1500	89	133	133					3	9 133 (0 85	
January		019	Jan-19 Feb-19	1500	95	133			4487 1			9		72	
February		019	Mar-19	1547	100	222			4511 1				8 187	16	
March					100								2 216		
April		019	Apr-19	1689 1753	106	673	216	1217 1080	4577 1 4516 1				210	21	
May			May-19	1/53	110	513	-								
June		019	Jun-19 Jul-19	1680	110	513	199 207	1167 1228						7 148	
August			Aug-19	1292	91	5	182			38 155					
September			Sep-19	1251	91	38	169		4171 1						
October			Oct-19	1202	93	38									
November			Nov-19	1179		19	204					3			
December		019	Dec-19	1179		15				38 149					
		020	Jan-20	1128	64	15	188		4096 1					1	
January					63	252									
February		020	Feb-20	1116		262				38 146					
March			Mar-20	1111		300				38 150		9 10		1	
May			Apr-20 May-20	1117 1126		294				38 151: 38 150		5 10 0 10			
Iviay														1	
June			Jun-20	1140		323				38 150					
August		020	Jul-20	1412 1658						39 140 41 111				9 130	·
August			Aug-20												
September			Sep-20	1737						43 112				90	
October			Oct-20	1715 1692						42 115 40 118				103	
November			Nov-20												
December			Dec-20	1696						38 122				108	
January			Jan-21	1707									1 214 (110	
February			Feb-21	1694						36 123				71	
March			Mar-21	1355		14				38 164				1	
Aprii			Apr-21	1279		14				38 162					
May			May-21	1254		15				39 160					
June			Jun-21	1236		196									
July		021	Jul-21	1225		196									
August			Aug-21	1341		266				39 155				1	
September			Sep-21	1569		314				39 155					
October	20	021	Oct-21	1518	72	305	224	1213	4140 1	157	4 30	2 11	4 0 224	127	72 6918

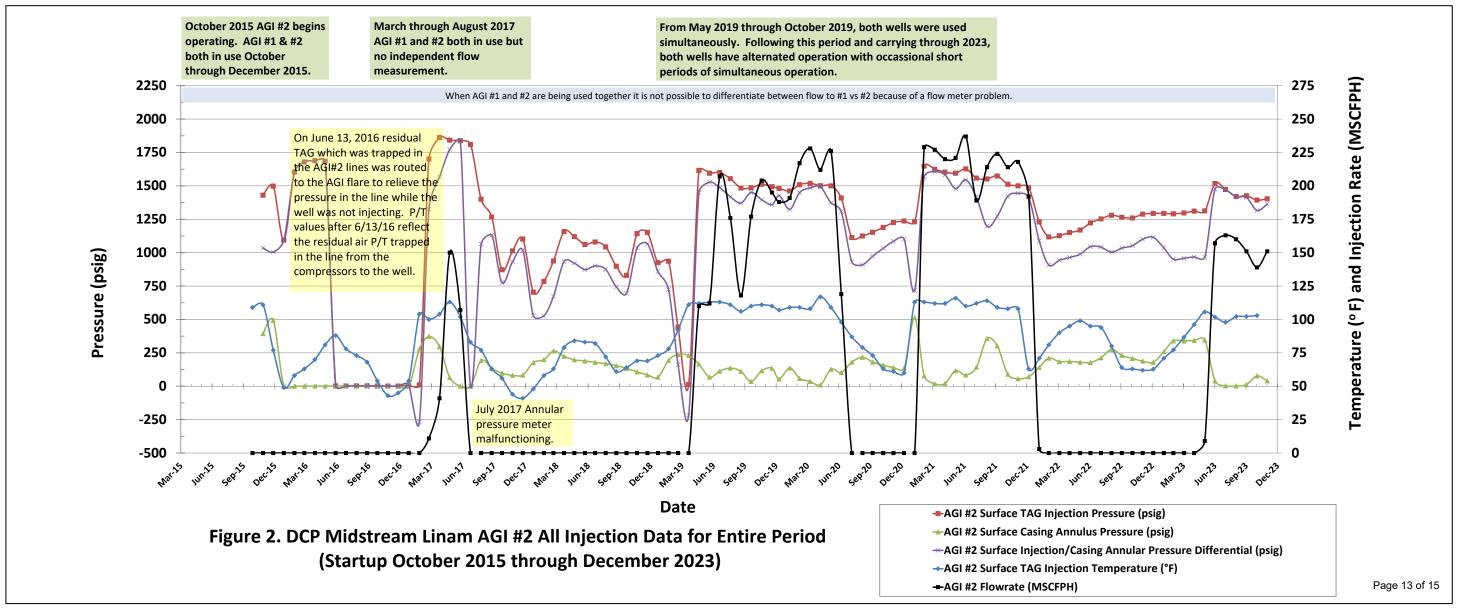
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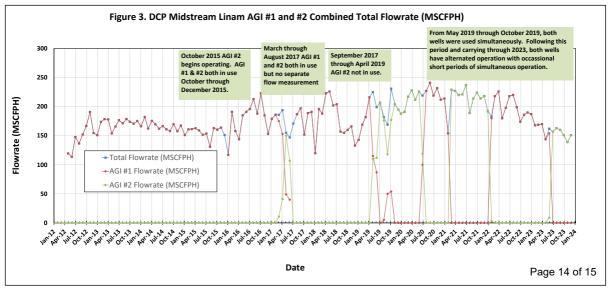
м	onth Ende	d	AGI #1 Surface AGI #1 TAG TAG Injection Injection Pressure (psig) Temperature (°	AGI #1 Surface Casing Annulus) Pressure (psig)	Total Flowrate (MSCFPH)	AGI #1 Surface Injection/Casing Annular Pressure Differential (psig)	Bottom Hole	AGI #1 Average Bottom Hole Temperature (°F)	AGI #2 Surface TAG Injection Pressure (psig)	AGI #2 Surface Casing Annulus Pressure (psig)	AGI #2 Surface TAG Injection Temperature (°F)	AGI #1 Flowrate (MSCFPH)		AGI #2 Surface Injection/Casing Annular Pressure Differential (psig)	Total CO2 Sequestered per month (Metric Ton) Notes
November	2021	Nov-21	1440	61 295	214	1145	4133	139	151	2 90	0 10	0	214	1422	6396
December	2021	Dec-21	1402	61 291	1 218	1111	4129	139	150	0 50	6 10	3 0	218	1444	4 6733
January	2022	Jan-22	1162	60 278	192	. 885	4116	139	148	7:	1 10	3 0	192	1415	5930
February	2022	Feb-22	1466	106 210	183	1256	4262	134	123	0 143	2 6	180	3	1089	5105 Flow switched to AGI #1 on 2/1/2022
March	2022	Mar-22	1557	110 292	2 218	1265	4319	136	111	8 210	7:	218	C	908	6733
April	2022	Apr-22	1623	113 195	226	1429	4361	138	112	7 184	4 8:	226	c	943	3 6755
May	2022	May-22	1563	107 104	1 180	1459	4334	137	115	0 186	6 90	180	o	964	5559
June	2022	Jun-22	1535	106 89	198	1446	4328	135	116	9 180	9:	198	C	989	5918
July	2022	Jul-22	1633	110 94	1 218	1538	4417	136	122	3 178	8 9	218	C	1045	6733
August	2022	Aug-22	1647	106 77	7 220	1570	4478	135	125	3 21:	3 9:	220	C	1041	1 6795
September	2022	Sep-22	1647	106 80	199	1567	4499	134	128	0 270	6 9	199	C	1004	5948
October	2022	Oct-22	1598	102 61	1 174	1537	7 4493	132	126	5 23:	1 80	174	C	1034	5374
November	2022	Nov-22	1652	108 51	1 186	1601	4508	134	126	208	8 6-	186	O	1052	2 5559
December	2022	Dec-22	1656	105 53	190	1604	4539	133	128	8 188	8 6:	190	O	1100	5868
January	2023	Jan-23	1662	106 53	187	1609	4549	133	129	4 179	9 6	187	O	1115	5 5557
February	2023	Feb-23	1640	105 75	168	1565	4533	133	129	4 258	8 6	168	C	1036	4669
March	2023	Mar-23	1628	104 45	169	1583	4536	132	129	1 339	9 7:	169	C	951	5210
April	2023	Apr-23	1612	101 39	170	1572	4534	131	129	7 339	9 7	7 170	C	958	5083
May	2023	May-23	1587	99 52	144	1535	4511	132	131	1 34	8	7 144	C	968	4243
June	2023	Jun-23	1597	101 73	162	1523	4509	132	131	34	6 9	5 154	g	966	4863
July	2023	Jul-23	1349	90 37	7 157	1312	4331	137	151	7 40	100	0	157	1476	4864
August	2023	Aug-23	1286	88 45	163	1241	4260	138	147	3	3 10	0	163	1470	5005
September	2023	Sep-23	1250	83 53	3 160	1197	4226	138	142	0	2 9	0	160	1418	3 4749
October	2023	Oct-23	1224	73 60	151	1164	4190	138	142	6 1	2 10	2 0	151	1414	4 4483
November	2023	Nov-23	1199	65 152	139	1048	4162	138	139	4 7	7 10:	0	139	1316	5 4148
December	2023	Dec-23	1174	63 67	7 151	1107	4136	138	140.	3 4:	1 10	0	151	1363	3 4658
Average for 2	023		1434 192	90 63					136	9 169		, 00	78	220	
Standard Dev	riation 2023			_			100								
Average for I	Average for Entire Period		1526.7 1	04.9 254.5	180.8	1271.6	4351.1	135.6	1201.	2 141.8	8 86.:	135.7	43.8	1050.5	5 5477
Standard Dev				17.8 231.6	28.5	257.6	173.6	3.4	478.	5 115.:	1 21.	74.5	80.1		
OPERATI	NG CONS	TRAINT	BASED ON NMOCC ORDER A	ND ACO-275										Total for 2023 ¹ (metric ton	57530
MAOP in NM	OCC Order is	2,644 psig											Tota	for Entire Period ² (metric ton	766811
													2023 Car	bon credit in USD (at \$85/ton	\$ 4,890,074.66

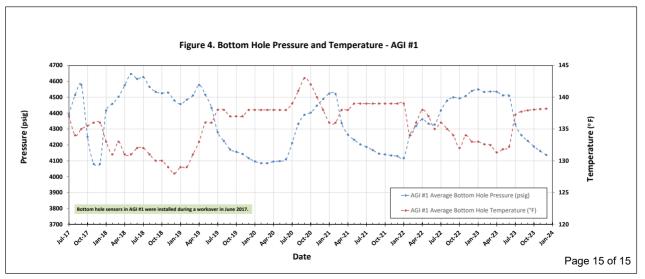
 $^{^{\}mathrm{1}}$ - Based on data from Ron Tabery, 180- day trend from 4/4/23

² - Assumes a stream of 80% CO2









District I
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District III 1000 Rio Brazos Rd., Aztec, NM 87410 Phone:(505) 334-6178 Fax:(505) 334-6170

1220 S. St Francis Dr., Santa Fe, NM 87505 Phone:(505) 476-3470 Fax:(505) 476-3462

State of New Mexico Energy, Minerals and Natural Resources Oil Conservation Division 1220 S. St Francis Dr. **Santa Fe, NM 87505**

CONDITIONS

Action 319241

CONDITIONS

Operator:	OGRID:
DCP OPERATING COMPANY, LP	36785
6900 E. Layton Ave	Action Number:
Denver, CO 80237	319241
	Action Type:
	[C-103] Sub. General Sundry (C-103Z)

CONDITIONS

Created By		Condition Date
anthony.harris	None	3/4/2024