Girent by Opp Po Appropriate 132:38 Office	State of New Me		Fo	orm C-103 of
<u>District I</u> – (575) 393-6161 1625 N. French Dr., Hobbs, NM 88240	Energy, Minerals and Natur	ral Resources	WELL API NO.	July 18, 2013
<u>District II</u> – (575) 748-1283 811 S. First St., Artesia, NM 88210	OIL CONSERVATION	DIVISION	30-025-52121	
<u>District III</u> – (505) 334-6178	1220 South St. Fran	icis Dr.	5. Indicate Type of Lease	
1000 Rio Brazos Rd., Aztec, NM 87410			STATE FEE 6. State Oil & Gas Lease No.	
<u>District IV</u> – (505) 476-3460 1220 S. St. Francis Dr., Santa Fe, NM	Sunta 1 0, 1 111 07	303		
37505		330703		
	OTICES AND REPORTS ON WELLS POSALS TO DRILL OR TO DEEPEN OR PLU		7. Lease Name or Unit Agreem	ent Name
DIFFERENT RESERVOIR. USE "APP	PLICATION FOR PERMIT" (FORM C-101) FO		Senile Felines 18_7 St	ate Com
PROPOSALS.) 1. Type of Well: Oil Well	Gas Well Other		8. Well Number 71H	
2. Name of Operator	0.00 (1.01)		9. OGRID Number	
XY USA INC. B. Address of Operator			16696 10. Pool name or Wildcat	
Greenway Plaza, Suite	110 Houston Taxas		RED TANK; BONE SPRIN	NG FAST
. Well Location	110, Houston, Texas		THE THINK, BOINE OF THE	10 , L/101
Unit Letter N	: 566 feet from the SOUTH	line and 181	5 feet from the WEST	line
Section 18		nge 33E	NMPM County LEA	Α
	11. Elevation (Show whether DR,		•	
	3659'			
ULL OR ALTER CASING OWNHOLE COMMINGLE ELOSED-LOOP SYSTEM OTHER: 13. Describe proposed or con of starting any proposed proposed completion or a Y USA Inc., respectfully ed below and updated C	CHANGE PLANS MULTIPLE COMPL mpleted operations. (Clearly state all p work). SEE RULE 19.15.7.14 NMAC recompletion. requests approval to amend C102 well plat. Also, see the and new VAM connection: WL, N-18-22S-33E	c. For Multiple Cor the subject we	LLING OPNS. P AND A T JOB Structure of the control	stimated date am of
oud Date:	Rig Release Dat			
nereby certify that the information	on above is true and complete to the be	est of my knowledg	e and belief.	
IGNATURE Melíssa	Guidry TITLE Regula	atory Advisor Sr.	DATE_06/12/24	
ype or print name Melissa Guid or State Use Only	dry E-mail address:	: melissa_guidry	@oxy.com PHONE: <u>713-49</u>	97-2481
PPROVED BY:	TITLE		DATE	
conditions of Approval (if any):			=	

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Phone: (575) 393-6161 Fax: (575) 393-0720 District II 811 S. First St., Artesia, NM 88210 Phone: (575) 748-1283 Fax: (575) 748-9720

1625 N. French Dr., Hobbs, NM 88240

1000 Rio Brazos Road, Aztec, NM 87410 Phone: (505) 334-6178 Fax: (505) 334-6170 District IV

1220 S. St. Francis Dr., Santa Fe, NM 87505 Phone: (505) 476-3460 Fax: (505) 476-3462

State of New Mexico Energy, Minerals & Natural Resources Department OIL CONSERVATION DIVISION 1220 South St. Francis Dr. Santa Fe, NM 87505

Page 2 of 44 Form C-102 Revised August 1, 2011 Submit one copy to appropriate District Office

■ AMENDED REPORT

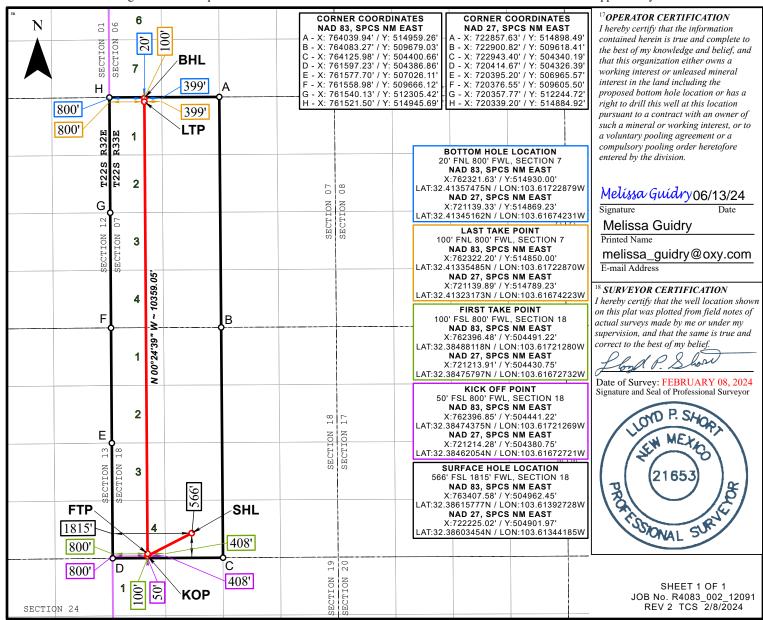
WELL LOCATION AND ACREAGE DEDICATION PLAT

¹ API Number	² Pool Code	³ Pool Name	
30-025-52121 51687		RED TANK; BONE SPRING, EAST	
⁴ Property Code	SENILE FELINE	Property Name S 18_7 STATE COM	⁶ Well Number 71H
⁷ ogrid no. 16696		Operator Name Y USA INC.	⁹ Elevation 3659'
	10 ~ ~		

¹⁰ Surface Location

	UL or lot no. N	Section 18	Township 22S	Range 33E	Lot Idn	Feet from the 566	North/South line SOUTH	Feet from the 1815	East/West line WEST	County LEA
¹¹ Bottom Hole Location If Different From S								rom Surface		
ſ	UL or lot no.	Section	Township	Range	Lot Idn	Feet from the	North/South line	Feet from the	East/West line	County
-	Ll	7	22S	33E		20	NORTH	800	WEST	LEA
ſ	12 Dedicated Acres 411 84	13 J	oint or Infill	¹⁴ Cons	olidation Code	15 Order No.				

No allowable will be assigned to this completion until all interests have been consolidated or a non-standard unit has been approved by the division.



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Oxy USA Inc. - SENILE FELINES 18_7 STATE COM 71H Drill Plan

1. Geologic Formations

TVD of Target (ft):	11270	Pilot Hole Depth (ft):	
Total Measured Depth (ft):	21584	Deepest Expected Fresh Water (ft):	871

Delaware Basin

Formation	MD-RKB (ft)	TVD-RKB (ft)	Expected Fluids
Rustler	871	871	
Salado	1587	1587	Salt
Castile	2807	2807	Salt
Delaware	4849	4848	Oil/Gas/Brine
Bell Canyon	4926	4925	Oil/Gas/Brine
Cherry Canyon	5962	5947	Oil/Gas/Brine
Brushy Canyon	7089	7056	Losses
Bone Spring	8795	8736	Oil/Gas
Bone Spring 1st	9915	9839	Oil/Gas
Bone Spring 2nd	10566	10480	Oil/Gas
Bone Spring 3rd			Oil/Gas
Wolfcamp			Oil/Gas
Penn			Oil/Gas
Strawn			Oil/Gas

^{*}H2S, water flows, loss of circulation, abnormal pressures, etc.

2. Casing Program

		V	1D	TVD					
	Hole	From	То	From	То	Csg.	Csg Wt.		
Section	Size (in)	(ft)	(ft)	(ft)	(ft)	OD (in)	(ppf)	Grade	Conn.
Surface	17.5	0	931	0	931	13.375	54.5	J-55	BTC
Intermediate	9.875	0	11693	0	11270	7.625	26.4	L-80 HC	BTC
Production	6.75	0	21584	0	11270	5.5	20	P-110	Sprint-SF

All casing strings will be tested in accordance with 43 CFR part 3170 Subpart 3172

All Casing SF Values will meet or exceed								
those below								
SF	SF	Body SF	Joint SF					
Collapse	Burst	Tension	Tension					
1.00	1.100	1.4	1.4					

	Y or N
Is casing new? If used, attach certification as required in 43 CFR 3160	Y
Does casing meet API specifications? If no, attach casing specification sheet.	Y
Is premium or uncommon casing planned? If yes attach casing specification sheet.	Y
Does the above casing design meet or exceed BLM's minimum standards?	Y
If not provide justification (loading assumptions, casing design criteria).	1
Will the intermediate pipe be kept at a minimum 1/3 fluid filled to avoid approaching	Y
the collapse pressure rating of the casing?	1
Is well located within Capitan Reef?	N
If yes, does production casing cement tie back a minimum of 50' above the Reef?	
Is well within the designated 4 string boundary.	
Is well located in SOPA but not in R-111-P?	N
If yes, are the first 2 strings cemented to surface and 3 rd string cement tied back	
500' into previous casing?	
Is well located in R-111-P and SOPA?	N
If yes, are the first three strings cemented to surface?	
Is 2 nd string set 100' to 600' below the base of salt?	
Is well located in high Cave/Karst?	N
If yes, are there two strings cemented to surface?	
(For 2 string wells) If yes, is there a contingency casing if lost circulation occurs?	
Is well located in critical Cave/Karst?	N
If yes, are there strings cemented to surface?	

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3. Cementing Program

Section	Stage	Slurry:	Sacks	Yield (ft^3/ft)	Density (lb/gal)	Excess:	тос	Placement	Description
Surface	1	Surface - Tail	973	1.33	14.8	100%	-	Circulate	Class C+Accel.
Int.	1	Intermediate 1S - Tail	584	1.68	13.2	5%	7,339	Circulate	Class C+Ret., Disper.
Int.	2	Intermediate 2S - Tail BH	1306	1.71	13.3	25%	-	Bradenhead	Class C+Accel.
Prod.	1	Production - Tail	588	1.84	13.3	25%	11,193	Circulate	Class C+Ret.

Offline Cementing Request

Oxy requests a variance to cement the 9.625" and/or 7.625" intermediate casing strings offline in accordance to the approved variance, EC Tran 461365. Please see Offline Cementing Variance attachment for further details.

Bradenhead CBL Request

Oxy requests permission to adjust the CBL requirement after bradenhead cement jobs, on 7-5/8" intermediate casings, as per the agreement reached in the OXY/BLM meeting on September 5, 2019. Please see Bradenhead CBL Variance attachment for further details.

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4. Pressure Control Equipment

BOP installed and tested before drilling which hole?	Size?	Min. Required WP		Туре	✓	Tested to:	Deepest TVD Depth (ft) per Section:
		5M		Annular	✓	70% of working pressure	
				Blind Ram	✓		
9.875" Hole	13-5/8"	5M		Pipe Ram		250 psi / 5000 psi	11270
		JIVI		Double Ram	✓	230 psi / 3000 psi	
			Other*				
		5M	Annular		✓	100% of working pressure	
				Blind Ram			11270
6.75" Hole	13-5/8"	10M		Pipe Ram		250 psi / 10000 psi	
		I UIVI		Double Ram	√	230 μδι / Τυυυυ μδι	
			Other*				

*Specify if additional ram is utilized

BOP/BOPE will be tested by an independent service company to 250 psi low and the high pressure indicated above per 43 CFR part 3170 Subpart 3172 requirements. The System may be upgraded to a higher pressure but still tested to the working pressure listed in the table above. If the system is upgraded all the components installed will be functional and tested.

Pipe rams will be operationally checked each 24 hour period. Blind rams will be operationally checked on each trip out of the hole. These checks will be noted on the daily tour sheets. Other accessories to the BOP equipment will include a Kelly cock and floor safety valve (inside BOP) and choke lines and choke

5M Annular BOP Request

Per BLM's Memorandum No. NM-2017-008: *Decision and Rationale for a Variance Allowing the Use of a 5M Annular Preventer with a 10M BOP Stack,* Oxy requests to employ a 5M annular with a 10M BOPE stack in the pilot and lateral sections of the well and will ensure that two barriers to flow are maintained at all times. Please see Annular BOP Variance attachment for further details.

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Formation integrity test will be performed per 43 CFR part 3170 Subpart 3172.

On Exploratory wells or on that portion of any well approved for a 5M BOPE system or greater, a pressure integrity test of each casing shoe shall be performed. Will be tested in accordance with 43 CFR part 3170 Subpart 3172.

A variance is requested for the use of a flexible choke line from the BOP to Choke Manifold. See attached for specs and hydrostatic test chart.

Y Are anchors required by manufacturer?

A multibowl or a unionized multibowl wellhead system will be employed. The wellhead and connection to the BOPE will meet all API 6A requirements. The BOP will be tested per 43 CFR part 3170 Subpart 3172 after installation on the surface casing which will cover testing requirements for a maximum of 30 days. If any seal subject to test pressure is broken the system must be tested. We will test the flange connection of the wellhead with a test port that is directly in the flange. We are proposing that we will run the wellhead through the rotary prior to cementing surface casing as discussed with the BLM on October 8, 2015.

See attached schematics.

BOP Break Testing Request

Oxy requests permission to adjust the BOP break testing requirements as per the agreement reached in the OXY/BLM meeting on September 5, 2019. Please see BOP Break Testing Variance attachment for further details.

Oxy will use Cameron ADAPT wellhead system that uses an OEC top flange connection. This connection has been fully vetted and verified by API to Spec 6A and carries an API monogram.

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5. Mud Program

Section	Depth - MD		Depth -	TVD	Tymo	Weight	Vigogity	Water
Section	From (ft)	To (ft)	From (ft)	To (ft)	Type	(ppg)	Viscosity	Loss
Surface	0	931	0	931	Water-Based Mud	8.6 - 8.8	40-60	N/C
Intermediate	931	11693	931	11270	Saturated Brine-Based or Oil-Based Mud	8.0 - 10.0	35-45	N/C
Production	11693	21584	11270	11270	Water-Based or Oil- Based Mud	9.5 - 12.5	38-50	N/C

Sufficient mud materials to maintain mud properties and meet minimum lost circulation and weight increase requirements will be kept on location at all times. The following is a general list of products: Barite, Bentonite, Gypsum, Lime, Soda Ash, Caustic Soda, Nut Plug, Cedar Fiber, Cotton Seed Hulls,

What will be used to monitor the	DVT/NAD Totas (Visual Manitoring	
loss or gain of fluid?	PVT/MD Totco/Visual Monitoring	

6. Logging and Testing Procedures

Logg	ing, Coring and Testing.
Yes	Will run GR from TD to surface (horizontal well – vertical portion of hole).
res	Stated logs run will be in the Completion Report and submitted to the BLM.
No	Logs are planned based on well control or offset log information.
No	Drill stem test? If yes, explain
No	Coring? If yes, explain

Addi	tional logs planned	Interval
No	Resistivity	
No	Density	
Yes	CBL	Production string
Yes	Mud log	Bone Spring – TD
No	PEX	

7. Drilling Conditions

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Condition	Specify what type and where?
BH Pressure at deepest TVD	7326 psi
Abnormal Temperature	No
BH Temperature at deepest TVD	171°F

Pump high viscosity sweeps as needed for hole cleaning. The mud system will be monitored visually/manually as well as with an electronic PVT. The necessary mud products for additional weight and fluid loss control will be on location at all times. Appropriately weighted mud will be used to isolate potential gas, oil, and water zones until such time as casing can be cemented into place for

Hydrogen Sulfide (H2S) monitors will be installed prior to drilling out the surface shoe. If H2S is detected in concentrations greater than 100 ppm, the operator will comply with the provisions of 43 CFR part 3170 Subpart 3172. If Hydrogen Sulfide is encountered, measured values and formations will be provided to the BLM.

N H2S is present
Y H2S Plan attached

8. Other facets of operation

	Yes/No
Will the well be drilled with a walking/skidding operation? If yes, describe.	
We plan to drill the 2 well pad in batch by section: all surface sections, intermediate	Voc
sections and production sections. The wellhead will be secured with a night cap whenever	Yes
the rig is not over the well.	
Will more than one drilling rig be used for drilling operations? If yes, describe.	
Oxy requests the option to contract a Surface Rig to drill, set surface casing, and cement for	
this well. If the timing between rigs is such that Oxy would not be able to preset surface,	Yes
the Primary Rig will MIRU and drill the well in its entirety per the APD. Please see the	
attached document for information on the spudder rig.	

Total Estimated Cuttings Volume: 1735 bbls

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PRD NM DIRECTIONAL PLANS (NAD 1983) Senile Felines 18_7 Senile Felines 18_7 State Com 71H

Wellbore #1

Plan: Permitting Plan

Standard Planning Report

04 June, 2024

Planning Report

HOPSPP Database:

Company: **ENGINEERING DESIGNS**

Project: PRD NM DIRECTIONAL PLANS (NAD 1983)

Site: Senile Felines 18_7

Well: Senile Felines 18 7 State Com 71H

Wellbore: Wellbore #1 Design: Permitting Plan Local Co-ordinate Reference:

TVD Reference: MD Reference:

North Reference: **Survey Calculation Method:** Well Senile Felines 18_7 State Com 71H

RKB=25' @ 3684.00ft RKB=25' @ 3684.00ft

Grid

Minimum Curvature

Project PRD NM DIRECTIONAL PLANS (NAD 1983)

Map System: US State Plane 1983 North American Datum 1983 Geo Datum:

Map Zone: New Mexico Eastern Zone System Datum: Mean Sea Level

Using geodetic scale factor

Site Senile Felines 18_7

Site Position: Northing: 504,962.34 usft Latitude: 32.386155 From: Мар Easting: 763,528.05 usft Longitude: -103.613537

Position Uncertainty: 0.00 ft Slot Radius: 13.200 in

Well Senile Felines 18_7 State Com 71H

Well Position +N/-S 504,962.45 usf Latitude: 32.386158 0.00 ft Northing: 763,407.58 usf +E/-W 0.00 ft Easting: Longitude: -103.613928

Position Uncertainty 2.00 ft Wellhead Elevation: ft **Ground Level:** 3,659.00 ft

0.39° **Grid Convergence:**

Wellbore Wellbore #1

Model Name Declination Field Strength Magnetics Sample Date Dip Angle (°) (nT) HDGM FILE 47,510.400 6/4/2024 6.20 59.95

Design Permitting Plan

Audit Notes:

Version: Phase: **PLAN** Tie On Depth: 0.00

Vertical Section: Depth From (TVD) +N/-S +E/-W Direction (ft) (ft) (ft) (°) 353.78 0.00 0.00 0.00

Plan Survey Tool Program Date 6/4/2024

Depth From Depth To

(ft) (ft) Survey (Wellbore) **Tool Name** Remarks

0.00 21,583.69 Permitting Plan (Wellbore #1) 1

SQC_C705Mb_MWD+IFR1 +SAG+FDIR_R5

MWD+IFR1+Sag+FDIR

Plan Sections										
Measured Depth (ft)	Inclination (°)	Azimuth (°)	Vertical Depth (ft)	+N/-S (ft)	+E/-W (ft)	Dogleg Rate (°/100ft)	Build Rate (°/100ft)	Turn Rate (°/100ft)	TFO (°)	Target
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
4,300.00	0.00	0.00	4,300.00	0.00	0.00	0.00	0.00	0.00	0.00	
5,306.57	10.07	241.71	5,301.40	-41.79	-77.66	1.00	1.00	0.00	241.71	
10,746.61	10.07	241.71	10,657.71	-492.37	-914.91	0.00	0.00	0.00	0.00	
11,693.49	90.00	359.59	11,270.00	77.97	-1,015.07	10.00	8.44	12.45	117.51	
21,583.69	90.00	359.59	11,270.00	9,967.91	-1,085.99	0.00	0.00	0.00	0.00 PE	3HL (Senile

Planning Report

Database: Company: HOPSPP

ENGINEERING DESIGNS

Project: PRD NM DIRECTIONAL PLANS (NAD 1983)

Site: Senile Felines 18_7

Well: Senile Felines 18_7 State Com 71H

Wellbore: Wellbore #1

Design: Permitting Plan

Local Co-ordinate Reference:

TVD Reference: MD Reference: North Reference:

Survey Calculation Method:

Well Senile Felines 18_7 State Com 71H

RKB=25' @ 3684.00ft RKB=25' @ 3684.00ft

Grid

sigii.	remining ri								
anned Survey									
Measured Depth (ft)	Inclination (°)	Azimuth (°)	Vertical Depth (ft)	+N/-S (ft)	+E/-W (ft)	Vertical Section (ft)	Dogleg Rate (°/100ft)	Build Rate (°/100ft)	Turn Rate (°/100ft)
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
100.00	0.00	0.00	100.00	0.00	0.00	0.00	0.00	0.00	0.00
200.00	0.00	0.00	200.00	0.00	0.00	0.00	0.00	0.00	0.00
300.00	0.00	0.00	300.00	0.00	0.00	0.00	0.00	0.00	0.00
400.00	0.00	0.00	400.00	0.00	0.00	0.00	0.00	0.00	0.00
500.00	0.00	0.00	500.00	0.00	0.00	0.00	0.00	0.00	0.00
600.00	0.00	0.00	600.00	0.00	0.00	0.00	0.00	0.00	0.00
700.00	0.00	0.00	700.00	0.00	0.00	0.00	0.00	0.00	0.00
800.00	0.00	0.00	800.00	0.00	0.00	0.00	0.00	0.00	0.00
900.00	0.00	0.00	900.00	0.00	0.00	0.00	0.00	0.00	0.00
4 000 00	0.00	0.00	4 000 00	0.00	0.00	0.00	0.00	0.00	0.00
1,000.00	0.00	0.00	1,000.00	0.00	0.00	0.00	0.00	0.00	0.00
1,100.00	0.00	0.00	1,100.00	0.00	0.00	0.00	0.00	0.00	0.00
1,200.00	0.00	0.00	1,200.00	0.00	0.00	0.00	0.00	0.00	0.00
1,300.00	0.00	0.00	1,300.00	0.00	0.00	0.00	0.00	0.00	0.00
1,400.00	0.00	0.00	1,400.00	0.00	0.00	0.00	0.00	0.00	0.00
1,500.00	0.00	0.00	1,500.00	0.00	0.00	0.00	0.00	0.00	0.00
1,600.00	0.00	0.00	1,600.00	0.00	0.00	0.00	0.00	0.00	0.00
			,						
1,700.00	0.00	0.00	1,700.00	0.00	0.00	0.00	0.00	0.00	0.00
1,800.00	0.00	0.00	1,800.00	0.00	0.00	0.00	0.00	0.00	0.00
1,900.00	0.00	0.00	1,900.00	0.00	0.00	0.00	0.00	0.00	0.00
2,000.00	0.00	0.00	2,000.00	0.00	0.00	0.00	0.00	0.00	0.00
2,100.00	0.00	0.00	2.100.00	0.00	0.00	0.00	0.00	0.00	0.00
	0.00		,	0.00	0.00		0.00	0.00	
2,200.00		0.00	2,200.00			0.00			0.00
2,300.00	0.00	0.00	2,300.00	0.00	0.00	0.00	0.00	0.00	0.00
2,400.00	0.00	0.00	2,400.00	0.00	0.00	0.00	0.00	0.00	0.00
2,500.00	0.00	0.00	2,500.00	0.00	0.00	0.00	0.00	0.00	0.00
2,600.00	0.00	0.00	2,600.00	0.00	0.00	0.00	0.00	0.00	0.00
2,700.00	0.00	0.00	2,700.00	0.00	0.00	0.00	0.00	0.00	0.00
2,800.00	0.00	0.00	2,800.00	0.00	0.00	0.00	0.00	0.00	0.00
2,900.00	0.00		2,900.00	0.00	0.00		0.00	0.00	0.00
2,900.00	0.00	0.00	2,900.00	0.00	0.00	0.00	0.00	0.00	0.00
3,000.00	0.00	0.00	3,000.00	0.00	0.00	0.00	0.00	0.00	0.00
3,100.00	0.00	0.00	3,100.00	0.00	0.00	0.00	0.00	0.00	0.00
3,200.00	0.00	0.00	3,200.00	0.00	0.00	0.00	0.00	0.00	0.00
3,300.00	0.00	0.00	3,300.00	0.00	0.00	0.00	0.00	0.00	0.00
3,400.00	0.00	0.00	3,400.00	0.00	0.00	0.00	0.00	0.00	0.00
3,500.00	0.00	0.00	3,500.00	0.00	0.00	0.00	0.00	0.00	0.00
3,600.00	0.00	0.00	3,600.00	0.00	0.00	0.00	0.00	0.00	0.00
3,700.00	0.00	0.00	3,700.00	0.00	0.00	0.00	0.00	0.00	0.00
3,800.00	0.00	0.00	3,800.00	0.00	0.00	0.00	0.00	0.00	0.00
3,900.00	0.00	0.00	3,900.00	0.00	0.00	0.00	0.00	0.00	0.00
4,000.00	0.00	0.00	4,000.00	0.00	0.00	0.00	0.00	0.00	0.00
4,100.00	0.00	0.00	4,100.00	0.00	0.00	0.00	0.00	0.00	0.00
4,200.00	0.00	0.00	4,200.00	0.00	0.00	0.00	0.00	0.00	0.00
4,300.00	0.00	0.00	4,300.00	0.00	0.00	0.00	0.00	0.00	0.00
4,400.00	1.00	241.71	4,400.00	-0.41	-0.77	-0.33	1.00	1.00	0.00
4.500.00	2.00	241.71	4,499.96	-1.65	-3.07	-1.31	1.00	1.00	0.00
,									
4,600.00	3.00	241.71	4,599.86	-3.72	-6.91	-2.95 5.24	1.00	1.00	0.00
4,700.00	4.00	241.71	4,699.68	-6.61	-12.29	-5.24	1.00	1.00	0.00
4,800.00	5.00	241.71	4,799.37	-10.33	-19.20	-8.19	1.00	1.00	0.00
4,900.00	6.00	241.71	4,898.90	-14.87	-27.64	-11.79	1.00	1.00	0.00
5.000.00	7.00	241.71	4,998.26	-20.24	-37.61	-16.05	1.00	1.00	0.00
5,100.00	8.00	241.71	5,097.40	-26.42	-49.10	-20.95	1.00	1.00	0.00
5,200.00	9.00	241.71	5,196.30	-33.43	-43.10 -62.12	-26.50	1.00	1.00	0.00
5,300.00	10.00 10.07	241.71 241.71	5,294.93 5,301.40	-41.25 -41.79	-76.65 -77.66	-32.71 -33.14	1.00 1.00	1.00 1.00	0.00 0.00
5,306.57									

Planning Report

Database: Company: Project: HOPSPP

ENGINEERING DESIGNS

PRD NM DIRECTIONAL PLANS (NAD 1983)

Site: Senile Felines 18_7

Well: Senile Felines 18_7 State Com 71H

Wellbore: Wellbore #1

Design: Permitting Plan

Local Co-ordinate Reference:

TVD Reference: MD Reference: North Reference:

Survey Calculation Method:

Well Senile Felines 18_7 State Com 71H

RKB=25' @ 3684.00ft RKB=25' @ 3684.00ft

Grid

Design:	Permitting Pla	an							
Planned Survey									
Measured Depth (ft)	Inclination (°)	Azimuth (°)	Vertical Depth (ft)	+N/-S (ft)	+E/-W (ft)	Vertical Section (ft)	Dogleg Rate (°/100ft)	Build Rate (°/100ft)	Turn Rate (°/100ft)
5,400.00	10.07	241.71	5,393.39	-49.53	-92.04	-39.27	0.00	0.00	0.00
5,500.00	10.07	241.71	5,491.85	-57.81	-107.43	-45.84	0.00	0.00	0.00
5,600.00	10.07	241.71	5,590.31	-66.10	-122.82	-52.41	0.00	0.00	0.00
5,700.00	10.07	241.71	5,688.77	-74.38	-138.21	-58.97	0.00	0.00	0.00
5,800.00	10.07	241.71	5,787.24	-82.66	-153.60	-65.54	0.00	0.00	0.00
5,900.00	10.07	241.71	5,885.70	-90.94	-168.99	-72.11	0.00	0.00	0.00
6,000.00	10.07	241.71	5,984.16	-99.23	-184.38	-78.67	0.00	0.00	0.00
6,100.00	10.07	241.71	6,082.62	-107.51	-199.77	-85.24	0.00	0.00	0.00
6,200.00	10.07	241.71	6,181.08	-115.79	-215.16	-91.81	0.00	0.00	0.00
6,300.00	10.07	241.71	6,279.54	-124.07	-230.55	-98.37	0.00	0.00	0.00
6,400.00	10.07	241.71	6,378.00	-132.36	-245.94	-104.94	0.00	0.00	0.00
6,500.00	10.07	241.71	6,476.46	-140.64	-261.33	-111.51	0.00	0.00	0.00
6,600.00	10.07	241.71	6,574.92	-148.92	-276.72	-118.08	0.00	0.00	0.00
6,700.00	10.07	241.71	6,673.38	-157.21	-292.11	-124.64	0.00	0.00	0.00
6,800.00	10.07	241.71	6,771.84	-165.49	-307.50	-131.21	0.00	0.00	0.00
6,900.00	10.07	241.71	6,870.30	-173.77	-322.90	-137.78	0.00	0.00	0.00
7,000.00	10.07	241.71	6,968.77	-182.05	-338.29	-144.34	0.00	0.00	0.00
7,100.00	10.07	241.71	7,067.23	-190.34	-353.68	-150.91	0.00	0.00	0.00
7,200.00	10.07	241.71	7,165.69	-198.62	-369.07	-157.48	0.00	0.00	0.00
7,300.00	10.07	241.71	7,264.15	-206.90	-384.46	-164.04	0.00	0.00	0.00
7,400.00	10.07	241.71	7,362.61	-215.18	-399.85	-170.61	0.00	0.00	0.00
7,500.00	10.07	241.71	7,461.07	-223.47	-415.24	-177.18	0.00	0.00	0.00
7,600.00	10.07	241.71	7,559.53	-231.75	-430.63	-183.75	0.00	0.00	0.00
7,700.00	10.07	241.71	7,657.99	-240.03	-446.02	-190.31	0.00	0.00	0.00
7,800.00	10.07	241.71	7,756.45	-248.31	-461.41	-196.88	0.00	0.00	0.00
7,900.00	10.07	241.71	7,854.91	-256.60	-476.80	-203.45	0.00	0.00	0.00
8,000.00	10.07	241.71	7,953.37	-264.88	-492.19	-210.01	0.00	0.00	0.00
8,100.00	10.07	241.71	8,051.83	-273.16	-507.58	-216.58	0.00	0.00	0.00
8,200.00	10.07	241.71	8,150.30	-281.44	-522.97	-223.15	0.00	0.00	0.00
8,300.00	10.07	241.71	8,248.76	-289.73	-538.36	-229.71	0.00	0.00	0.00
8,400.00	10.07	241.71	8,347.22	-298.01	-553.75	-236.28	0.00	0.00	0.00
8,500.00	10.07	241.71	8,445.68	-306.29	-569.14	-242.85	0.00	0.00	0.00
8,600.00	10.07	241.71	8,544.14	-314.57	-584.53	-249.41	0.00	0.00	0.00
8,700.00	10.07	241.71	8,642.60	-322.86	-599.92	-255.98	0.00	0.00	0.00
8,800.00	10.07	241.71	8,741.06	-331.14	-615.31	-262.55	0.00	0.00	0.00
8,900.00 9,000.00 9,100.00 9,200.00 9,300.00	10.07 10.07 10.07 10.07 10.07	241.71 241.71 241.71 241.71 241.71	8,839.52 8,937.98 9,036.44 9,134.90 9,233.36	-339.42 -347.71 -355.99 -364.27 -372.55	-630.71 -646.10 -661.49 -676.88 -692.27	-269.12 -275.68 -282.25 -288.82 -295.38	0.00 0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00 0.00
9,400.00 9,500.00 9,600.00 9,700.00 9,800.00	10.07 10.07 10.07 10.07 10.07	241.71 241.71 241.71 241.71 241.71	9,233.36 9,331.82 9,430.29 9,528.75 9,627.21 9,725.67	-372.33 -380.84 -389.12 -397.40 -405.68 -413.97	-092.27 -707.66 -723.05 -738.44 -753.83 -769.22	-301.95 -308.52 -315.08 -321.65 -328.22	0.00 0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00 0.00 0.00
9,900.00	10.07	241.71	9,824.13	-422.25	-784.61	-334.79	0.00	0.00	0.00
10,000.00	10.07	241.71	9,922.59	-430.53	-800.00	-341.35	0.00	0.00	0.00
10,100.00	10.07	241.71	10,021.05	-438.81	-815.39	-347.92	0.00	0.00	0.00
10,200.00	10.07	241.71	10,119.51	-447.10	-830.78	-354.49	0.00	0.00	0.00
10,300.00	10.07	241.71	10,217.97	-455.38	-846.17	-361.05	0.00	0.00	0.00
10,400.00	10.07	241.71	10,316.43	-463.66	-861.56	-367.62	0.00	0.00	0.00
10,500.00	10.07	241.71	10,414.89	-471.94	-876.95	-374.19	0.00	0.00	0.00
10,600.00	10.07	241.71	10,513.35	-480.23	-892.34	-380.75	0.00	0.00	0.00
10,700.00	10.07	241.71	10,611.82	-488.51	-907.73	-387.32	0.00	0.00	0.00
10,746.61	10.07	241.71	10,657.71	-492.37	-914.91	-390.38	0.00	0.00	0.00

Planning Report

Database: Company: Project:

Site:

HOPSPP

ENGINEERING DESIGNS

PRD NM DIRECTIONAL PLANS (NAD 1983)

Senile Felines 18_7

Well: Senile Felines 18_7 State Com 71H

Wellbore: Wellbore #1

Design: Permitting Plan

Local Co-ordinate Reference:

TVD Reference:
MD Reference:
North Reference:

Survey Calculation Method:

Well Senile Felines 18_7 State Com 71H

RKB=25' @ 3684.00ft RKB=25' @ 3684.00ft

Crid

Design:	Permitting Pla	an							
Planned Survey									
Measured Depth (ft)	Inclination (°)	Azimuth (°)	Vertical Depth (ft)	+N/-S (ft)	+E/-W (ft)	Vertical Section (ft)	Dogleg Rate (°/100ft)	Build Rate (°/100ft)	Turn Rate (°/100ft)
10,800.00	8.94	273.78	10,710.40	-494.31	-923.16	-391.42	10.00	-2.11	60.07
10,900.00	13.86	320.09	10,808.59	-484.59	-938.64	-380.07	10.00	4.92	46.31
11,000.00	22.42	337.23	10,903.59	-457.75	-953.74	-351.76	10.00	8.56	17.14
11,100.00	31.80	344.93	10,992.54	-414.62	-968.00	-307.33	10.00	9.38	7.70
11,200.00	41.45	349.36	11,072.71	-356.50	-981.00	-248.15	10.00	9.65	4.43
11,300.00	51.22	352.35	11,141.68	-285.16	-992.34	-176.00	10.00	9.77	2.99
11,400.00	61.04	354.61	11,197.35	-202.77	-1,001.66	-93.08	10.00	9.82	2.26
11,500.00	70.89	356.47	11,238.03	-111.82	-1,008.70	-1.92	10.00	9.85	1.87
11,600.00	80.77	358.13	11,262.48	-15.10	-1,013.23	94.73	10.00	9.87	1.65
11,693.49	90.00	359.59	11,270.00	77.97	-1,015.07	187.45	10.00	9.88	1.56
11,700.00	90.00	359.59	11,270.00	84.48	-1,015.12	193.93	0.00	0.00	0.00
11,800.00	90.00	359.59	11,270.00	184.48	-1,015.84	293.41	0.00	0.00	0.00
11,900.00	90.00	359.59	11,270.00	284.47	-1,016.56	392.90	0.00	0.00	0.00
12,000.00	90.00	359.59	11,270.00	384.47	-1,017.27	492.39	0.00	0.00	0.00
12,100.00	90.00	359.59	11,270.00	484.47	-1,017.99	591.87	0.00	0.00	0.00
12,200.00	90.00	359.59	11,270.00	584.47	-1,018.71	691.36	0.00	0.00	0.00
12,300.00	90.00	359.59	11,270.00	684.46	-1,019.42	790.85	0.00	0.00	0.00
12,400.00	90.00	359.59	11,270.00	784.46	-1,020.14	890.33	0.00	0.00	0.00
12,500.00	90.00	359.59	11,270.00	884.46	-1,020.86	989.82	0.00	0.00	0.00
12,600.00	90.00	359.59	11,270.00	984.46	-1,021.57	1,089.31	0.00	0.00	0.00
12,700.00	90.00	359.59	11,270.00	1,084.45	-1,022.29	1,188.80	0.00	0.00	0.00
12,800.00	90.00	359.59	11,270.00	1,184.45	-1,023.01	1,288.28	0.00	0.00	0.00
12,900.00	90.00	359.59	11,270.00	1,284.45	-1,023.73	1,387.77	0.00	0.00	0.00
13,000.00	90.00	359.59	11,270.00	1,384.45	-1,024.44	1,487.26	0.00	0.00	0.00
13,100.00	90.00	359.59	11,270.00	1,484.44	-1,025.16	1,586.74	0.00	0.00	0.00
13,200.00	90.00	359.59	11,270.00	1,584.44	-1,025.88	1,686.23	0.00	0.00	0.00
13,300.00	90.00	359.59	11,270.00	1,684.44	-1,026.59	1,785.72	0.00	0.00	0.00
13,400.00	90.00	359.59	11,270.00	1,784.43	-1,027.31	1,885.20	0.00	0.00	0.00
13,500.00	90.00	359.59	11,270.00	1,884.43	-1,028.03	1,984.69	0.00	0.00	0.00
13,600.00	90.00	359.59	11,270.00	1,984.43	-1,028.74	2,084.18	0.00	0.00	0.00
13,700.00	90.00	359.59	11,270.00	2,084.43	-1,029.46	2,183.66	0.00	0.00	0.00
13,800.00	90.00	359.59	11,270.00	2,184.42	-1,030.18	2,283.15	0.00	0.00	0.00
13,900.00	90.00	359.59	11,270.00	2,284.42	-1,030.90	2,382.64	0.00	0.00	0.00
14,000.00	90.00	359.59	11,270.00	2,384.42	-1,031.61	2,482.12	0.00	0.00	0.00
14,100.00	90.00	359.59	11,270.00	2,484.42	-1,032.33	2,581.61	0.00	0.00	0.00
14,200.00	90.00	359.59	11,270.00	2,584.41	-1,033.05	2,681.10	0.00	0.00	0.00
14,300.00	90.00	359.59	11,270.00	2,684.41	-1,033.76	2,780.59	0.00	0.00	0.00
14,400.00	90.00	359.59	11,270.00	2,784.41	-1,034.48	2,880.07	0.00	0.00	0.00
14,500.00	90.00	359.59	11,270.00	2,884.41	-1,035.20	2,979.56	0.00	0.00	0.00
14,600.00	90.00	359.59	11,270.00	2,984.40	-1,035.92	3,079.05	0.00	0.00	0.00
14,700.00	90.00	359.59	11,270.00	3,084.40	-1,036.63	3,178.53	0.00	0.00	0.00
14,800.00	90.00	359.59	11,270.00	3,184.40	-1,037.35	3,278.02	0.00	0.00	0.00
14,900.00	90.00	359.59	11,270.00	3,284.40	-1,038.07	3,377.51	0.00	0.00	0.00
15,000.00	90.00	359.59	11,270.00	3,384.39	-1,038.78	3,476.99	0.00	0.00	0.00
15,100.00	90.00	359.59	11,270.00	3,484.39	-1,039.50	3,576.48	0.00	0.00	0.00
15,200.00	90.00	359.59	11,270.00	3,584.39	-1,040.22	3,675.97	0.00	0.00	0.00
15,300.00	90.00	359.59	11,270.00	3,684.39	-1,040.93	3,775.45	0.00	0.00	0.00
15,400.00	90.00	359.59	11,270.00	3,784.38	-1,041.65	3,874.94	0.00	0.00	0.00
15,500.00	90.00	359.59	11,270.00	3,884.38	-1,042.37	3,974.43	0.00	0.00	0.00
15,600.00	90.00	359.59	11,270.00	3,984.38	-1,043.09	4,073.91	0.00	0.00	0.00
15,700.00	90.00	359.59	11,270.00	4,084.38	-1,043.80	4,173.40	0.00	0.00	0.00
15,800.00	90.00	359.59	11,270.00	4,184.37	-1,044.52	4,272.89	0.00	0.00	0.00
15,900.00	90.00	359.59	11,270.00	4,284.37	-1,045.24	4,372.37	0.00	0.00	0.00
16,000.00	90.00	359.59	11,270.00	4,384.37	-1,045.95	4,471.86	0.00	0.00	0.00
16,100.00	90.00	359.59	11,270.00	4,484.37	-1,046.67	4,571.35	0.00	0.00	0.00

Planning Report

Database: Company: Project:

Site:

HOPSPP

ENGINEERING DESIGNS

PRD NM DIRECTIONAL PLANS (NAD 1983)

Senile Felines 18_7

Well: Senile Felines 18_7 State Com 71H

Wellbore: Wellbore #1 Local Co-ordinate Reference:

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Survey Calculation Method:

Well Senile Felines 18_7 State Com 71H

RKB=25' @ 3684.00ft RKB=25' @ 3684.00ft

libore: sign:	Permitting Pla	an							
anned Survey									
Measured Depth (ft)	Inclination (°)	Azimuth (°)	Vertical Depth (ft)	+N/-S (ft)	+E/-W (ft)	Vertical Section (ft)	Dogleg Rate (°/100ft)	Build Rate (°/100ft)	Turn Rate (°/100ft)
16,200.00	90.00	359.59	11,270.00	4,584.36	-1,047.39	4,670.84	0.00	0.00	0.00
16,300.00	90.00	359.59	11,270.00	4,684.36	-1,048.10	4,770.32	0.00	0.00	0.00
16,400.00	90.00	359.59	11,270.00	4,784.36	-1,048.82	4,869.81	0.00	0.00	0.00
16,500.00 16,600.00	90.00 90.00	359.59 359.59	11,270.00 11,270.00	4,884.36 4,984.35	-1,049.54 -1,050.26	4,969.30 5,068.78	0.00 0.00	0.00 0.00	0.00 0.00
16,700.00	90.00	359.59	11,270.00	5.084.35	,		0.00	0.00	0.00
16,800.00	90.00	359.59	11,270.00	5,084.35	-1,050.97 -1,051.69	5,168.27 5,267.76	0.00	0.00	0.00
16,900.00	90.00	359.59	11,270.00	5,284.34	-1,051.09	5,367.24	0.00	0.00	0.00
17,000.00	90.00	359.59	11,270.00	5,384.34	-1,052.41	5,367.24	0.00	0.00	0.00
17,100.00	90.00	359.59	11,270.00	5,484.34	-1,053.12	5,566.22	0.00	0.00	0.00
17,200.00	90.00	359.59	11,270.00	5,584.34	-1,054.56	5,665.70	0.00	0.00	0.00
17,300.00	90.00	359.59	11,270.00	5,684.33	-1,055.27	5,765.19	0.00	0.00	0.00
17,400.00	90.00	359.59	11,270.00	5,784.33	-1,055.99	5,864.68	0.00	0.00	0.00
17,500.00	90.00	359.59	11,270.00	5,884.33	-1,056.71	5,964.16	0.00	0.00	0.00
17,600.00	90.00	359.59	11,270.00	5,984.33	-1,057.43	6,063.65	0.00	0.00	0.00
17.700.00	90.00	359.59	11,270.00	6,084.32	-1.058.14	6,163.14	0.00	0.00	0.00
17,800.00	90.00	359.59	11,270.00	6,184.32	-1,058.86	6,262.62	0.00	0.00	0.00
17,900.00	90.00	359.59	11,270.00	6.284.32	-1.059.58	6,362.11	0.00	0.00	0.00
18,000.00	90.00	359.59	11,270.00	6,384.32	-1,060.29	6,461.60	0.00	0.00	0.00
18,100.00	90.00	359.59	11,270.00	6,484.31	-1,061.01	6,561.09	0.00	0.00	0.00
18,200.00	90.00	359.59	11,270.00	6,584.31	-1,061.73	6,660.57	0.00	0.00	0.00
18,300.00	90.00	359.59	11,270.00	6,684.31	-1,062.44	6,760.06	0.00	0.00	0.00
18,400.00	90.00	359.59	11,270.00	6,784.31	-1,063.16	6,859.55	0.00	0.00	0.00
18,500.00	90.00	359.59	11,270.00	6,884.30	-1,063.88	6,959.03	0.00	0.00	0.00
18,600.00	90.00	359.59	11,270.00	6,984.30	-1,064.60	7,058.52	0.00	0.00	0.00
18,700.00	90.00	359.59	11,270.00	7,084.30	-1,065.31	7,158.01	0.00	0.00	0.00
18,800.00	90.00	359.59	11,270.00	7,184.30	-1,066.03	7,257.49	0.00	0.00	0.00
18,900.00	90.00	359.59	11,270.00	7,284.29	-1,066.75	7,356.98	0.00	0.00	0.00
19,000.00	90.00	359.59	11,270.00	7,384.29	-1,067.46	7,456.47	0.00	0.00	0.00
19,100.00	90.00	359.59	11,270.00	7,484.29	-1,068.18	7,555.95	0.00	0.00	0.00
19,200.00	90.00	359.59	11,270.00	7,584.29	-1,068.90	7,655.44	0.00	0.00	0.00
19,300.00	90.00	359.59	11,270.00	7,684.28	-1,069.62	7,754.93	0.00	0.00	0.00
19,400.00	90.00	359.59	11,270.00	7,784.28	-1,070.33	7,854.41	0.00	0.00	0.00
19,500.00	90.00	359.59	11,270.00	7,884.28	-1,071.05	7,953.90	0.00	0.00	0.00
19,600.00	90.00	359.59	11,270.00	7,984.28	-1,071.77	8,053.39	0.00	0.00	0.00
19,700.00	90.00	359.59	11,270.00	8,084.27	-1,072.48	8,152.87	0.00	0.00	0.00
19,800.00	90.00	359.59	11,270.00	8,184.27	-1,073.20	8,252.36	0.00	0.00	0.00
19,900.00	90.00	359.59	11,270.00	8,284.27	-1,073.92	8,351.85	0.00	0.00	0.00
20,000.00	90.00	359.59	11,270.00	8,384.27	-1,074.63	8,451.34	0.00	0.00	0.00
20,100.00	90.00	359.59	11,270.00	8,484.26	-1,075.35	8,550.82	0.00	0.00	0.00
20,200.00	90.00	359.59	11,270.00	8,584.26	-1,076.07	8,650.31	0.00	0.00	0.00
20,300.00	90.00	359.59	11,270.00	8,684.26	-1,076.79	8,749.80	0.00	0.00	0.00
20,400.00	90.00	359.59	11,270.00	8,784.26	-1,077.50	8,849.28	0.00	0.00	0.00
20,500.00	90.00	359.59	11,270.00	8,884.25	-1,078.22	8,948.77	0.00	0.00	0.00
20,600.00	90.00	359.59	11,270.00	8,984.25	-1,078.94	9,048.26	0.00	0.00	0.00
20,700.00	90.00	359.59	11,270.00	9,084.25	-1,079.65	9,147.74	0.00	0.00	0.00
20,800.00	90.00	359.59	11,270.00	9,184.24	-1,080.37	9,247.23	0.00	0.00	0.00
20,900.00	90.00	359.59	11,270.00	9,284.24	-1,081.09	9,346.72	0.00	0.00	0.00
21,000.00	90.00	359.59	11,270.00	9,384.24	-1,081.80	9,446.20	0.00	0.00	0.00
21,100.00	90.00	359.59	11,270.00	9,484.24	-1,082.52	9,545.69	0.00	0.00	0.00
21,200.00	90.00	359.59	11,270.00	9,584.23	-1,083.24	9,645.18	0.00	0.00	0.00
21,300.00	90.00	359.59	11,270.00	9,684.23	-1,083.96	9,744.66	0.00	0.00	0.00
21,400.00	90.00	359.59	11,270.00	9,784.23	-1,084.67	9,844.15	0.00	0.00	0.00
21,500.00	90.00	359.59	11,270.00	9,884.23	-1,085.39	9,943.64	0.00	0.00	0.00
21,583.69	90.00	359.59	11,270.00	9,967.91	-1,085.99	10,026.90	0.00	0.00	0.00

Planning Report

Database: HOPSPP

Company: ENGINEERING DESIGNS

Project: PRD NM DIRECTIONAL PLANS (NAD 1983)

Site: Senile Felines 18_7

Well: Senile Felines 18_7 State Com 71H

Wellbore: Wellbore #1

Design: Permitting Plan

Local Co-ordinate Reference:

TVD Reference:
MD Reference:
North Reference:

Survey Calculation Method:

Well Senile Felines 18_7 State Com 71H

RKB=25' @ 3684.00ft RKB=25' @ 3684.00ft

Grid

Design Targets									
Target Name - hit/miss target - Shape	Dip Angle (°)	Dip Dir. (°)	TVD (ft)	+N/-S (ft)	+E/-W (ft)	Northing (usft)	Easting (usft)	Latitude	Longitude
KOP (Senile Felines - plan misses targe - Point	0.00 t center by 25		11,270.00 221.97ft MD	-521.25 (11088.90 T	-1,010.77 VD, -341.89 i	504,441.22 N, -983.65 E)	762,396.85	32.384744	-103.617213
PBHL (Senile Felines - plan hits target ce - Point	0.00 nter	0.00	11,270.00	9,967.91	-1,085.99	514,930.00	762,321.63	32.413575	-103.617229
FTP (Senile Felines - plan misses targe - Point	0.00 t center by 22		11,270.00 257.77ft MD	-471.25 (11114.06 T	-1,011.14 VD, -316.77 i	504,491.22 N, -987.78 E)	762,396.48	32.384881	-103.617213

Formations							
	Measured Depth (ft)	Vertical Depth (ft)	Name	Lithology	Dip (°)	Dip Direction (°)	
	871.00	871.00	RUSTLER				
	1,587.00	1,587.00	SALADO				
	2,807.00	2,807.00	CASTILE				
	4,848.84	4,848.00	DELAWARE				
	4,926.25	4,925.00	BELL CANYON				
	5,962.26	5,947.00	CHERRY CANYON				
	7,088.60	7,056.00	BRUSHY CANYON				
	8,794.86	8,736.00	BONE SPRING				
	9,915.10	9,839.00	BONE SPRING 1ST				
	10,566.12	10,480.00	BONE SPRING 2ND				

Plan Annota	itions				
	Measured	Vertical	Local Coor	dinates	
	Depth (ft)	Depth (ft)	+N/-S (ft)	+E/-W (ft)	Comment
	4,300.00	4,300.00	0.00	0.00	Build 1°/100'
	5.306.57	5.301.40	-41.79	-77.66	Hold 10° Tangent
	10,746.61	10,657.71	-492.37	-914.91	KOP, Build 10°/100'
	11,693.49	11,270.00	77.97	-1,015.07	Landing Point
	21,583.69	11,270.00	9,967.91	-1,085.99	TD at 21583.69' MD



CONNECTION DATA SHEET



PIPE BODY PROPERTIES

Nominal OD	5.500	in.
Nominal ID	4.778	in.
Nominal Wall Thickness	0.361	in.
Minimum Wall Thickness	87.5	%
Nominal Weight (API)	20.00	lb/ft
Plain End Weight	19.83	lb/ft
Drift	4.653	in.
Grade Type	Controlle	ed Yield
Grade Type Minimum Yield Strength	Controlle	ed Yield <i>ksi</i>
Minimum Yield Strength	110	ksi
Minimum Yield Strength Maximum Yield Strength	110 125	ksi ksi
Minimum Yield Strength Maximum Yield Strength Minimum Ultimate Tensile Strength	110 125 140	ksi ksi ksi

CONNECTION PROPERTIES

Connection Type	Semi-Pr	emium Integral Semi-Flu
Nominal Connection OD	5.783	in.
Nominal Connection ID	4.718	in.
Make-up Loss	5.965	in.
Tension Efficiency	90	% Pipe Body
Compression Efficiency	90	% Pipe Body
Internal Pressure Efficiency	100	% Pipe Body
External Pressure Efficiency	100	% Pipe Body

JOINT PERFORMANCES

Tension Strength	577	klb
Compression Strength	577	klb
Internal Pressure Resistance	12,640	psi
External Pressure Resistance	11,110	psi
Maximum Bending, Structural	78	°/100 ft
Maximum Bending, with Sealability(1)	30	°/100 ft

(1) Sealability rating demonstrated as per API RP 5C5 / ISO 13679



4,500 **MIN**

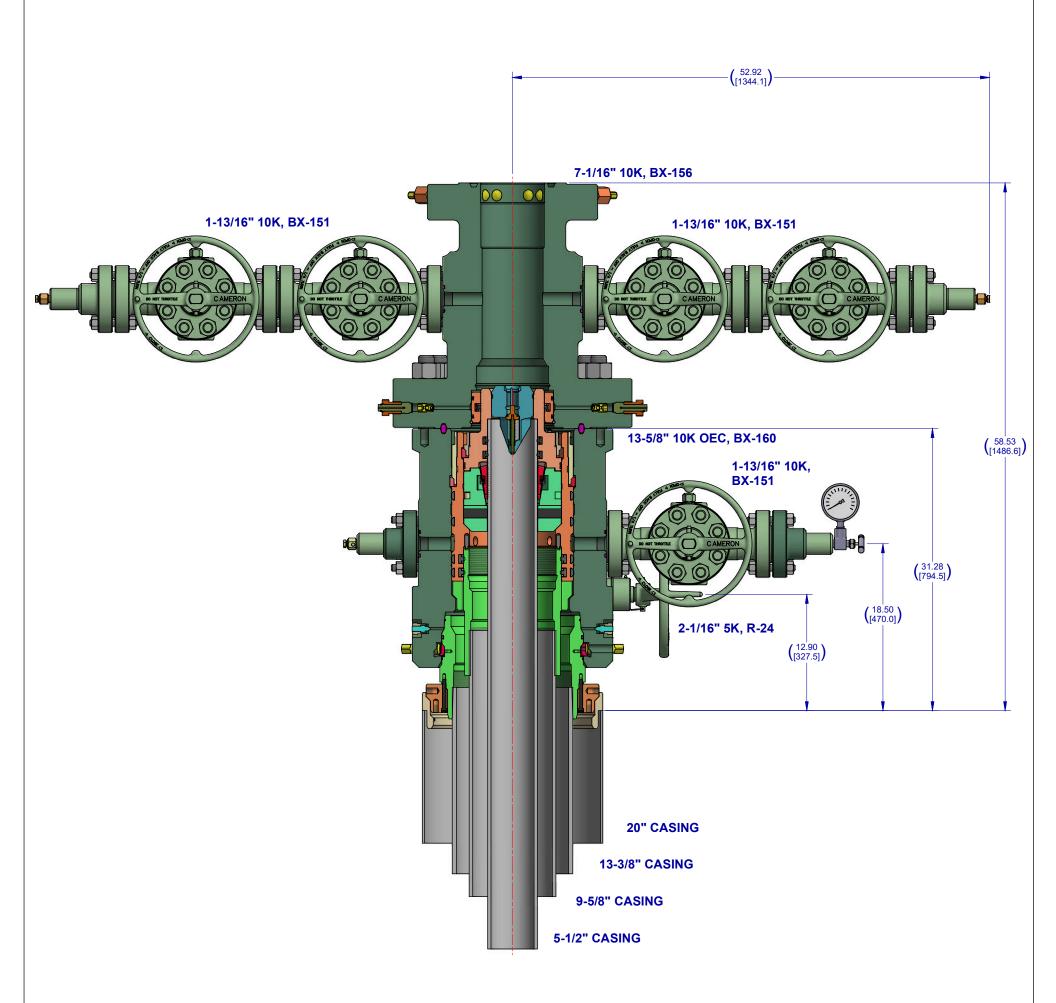
15,750 **MAX**

(2) MTS: Maximum Torque with Sealability.

BOOST YOUR EFFICIENCY, REDUCE COSTS AND ENSURE 100% WELL INTEGRITY WITH VAM® FIELD SERVICE

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Notes:

1. THIS IS A PROPOSAL DRAWING AND DIMENSIONS SHOWN ARE SUBJECT TO CHANGE DURING THE FINAL DESIGN PROCESS.

2. DIGITALLY ENABLED SOLUTIONS, CHOKES AND ESD'S AVAILABLE ON REQUEST

CONFIDENTIAL				
DO NOT SC	ALE		CAMFRON	SURFACE
DRAWN BY:	DATE			SYSTEMS
D. GOTTUNG	18 Feb 22		A Schlumberger Company	2.2.2
CHECKED BY:	DATE			•
D. GOTTUNG	18 Feb 22		OXY 13-5/8" 10K AE	APT
APPROVED BY:	DATE	ĺ	16" X 10-3/4" X 7-5/8"	X 5-1/2"
D. GOTTUNG	18 Feb 22		.0 % .0 3/4 % 1 0/0	
5.068 LBS INITIAL USE B/M:		SHEET	00 050404 04	AO REV:
3.748 KG		1 of 1	SD-053434-94	-12 01
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5M Annluar BOP Variance Request

Per BLM's Memorandum No. NM-2017-008: *Decision and Rationale for a Variance Allowing the Use of a 5M Annular Preventer with a 10M BOP Stack*, Oxy requests to employ a 5M annular with a 10M BOPE stack in the pilot and lateral sections of the well and will ensure that two barriers to flow are maintained at all times. Please see Well Control Plan below.

Oxy Well Control Plan

A. Component and Preventer Compatibility Table

The table below, which covers the drilling and casing of the >5M MASP portion of the well, outlines the tubulars and the compatible preventers in use. This table, combined with the mud program, documents that two barriers to flow can be maintained at all times, independent of the rating of the annular preventer.

Pilot hole and Lateral sections, 10M requirement

Component	OD	Preventer	RWP
Drillpipe	4-1/2"-5"	Lower 3-1/2 - 5-1/2" VBR	10M
		Upper 3-1/2 - 5-1/2" VBR	
HWDP	4-1/2"-5"	Lower 3-1/2 - 5-1/2" VBR	10M
		Upper 3-1/2 - 5-1/2" VBR	
Drill collars and MWD tools	4-3/4" – 5-1/2"	Lower 3-1/2 - 5-1/2" VBR	10M
		Upper 3-1/2 - 5-1/2" VBR	
Mud Motor	4-3/4"	Lower 3-1/2 - 5-1/2" VBR	10M
		Upper 3-1/2 - 5-1/2" VBR	
Production casing	5-1/2"	Lower 3-1/2 - 5-1/2" VBR	10M
		Upper 3-1/2 - 5-1/2" VBR	
ALL	0" - 13-5/8"	Annular	5M
Open-hole	6-3/4"	Blind Rams	10M

VBR = Variable Bore Ram. Compatible range listed in chart.

HWDP = Heavy Weight Drill Pipe

MWD = Measurement While Drilling

B. Well Control Procedures

Well control procedures are specific to the rig equipment and the operation at the time the kick occurs. Below are the minimal high-level tasks prescribed to assure a proper shut-in while drilling, tripping, running casing, pipe out of the hole (open hole), and moving the Bottom Hole Assembly (BHA) through the Blowout Preventers (BOP). The pressure at which control is swapped from the annular to another compatible ram will occur when the anticipated pressure is approaching or envisioned to exceed 70% of the 5M annular Rated Working Pressure (RWP) or 3500 PSI.

General Procedure While Drilling

- 1. Sound alarm (alert crew)
- 2. Space out drill string
- 3. Shut down pumps (stop pumps and rotary)
- 4. Shut-in Well (uppermost applicable BOP, typically annular preventer first. The Hydraulic Control Remote (HCR) valve and choke will already be in the closed position).
- 5. Confirm shut-in
- 6. Notify tool pusher/company representative
- 7. Read and record the following:
 - a. SIDPP and SICP
 - b. Pit gain
 - c. Time
- 8. Regroup and identify forward plan
- 9. If pressure has built or expected to reach 70% of the annular RWP during kill operations, crew will reconfirm spacing and swap to the upper pipe ram

General Procedure While Tripping

- 1. Sound alarm (alert crew)
- 2. Stab full opening safety valve and close
- 3. Space out drill string
- 4. Shut-in (uppermost applicable BOP, typically annular preventer first. The HCR and choke will already be in the closed position)
- 5. Confirm shut-in
- 6. Notify tool pusher/company representative
- 7. Read and record the following
 - a. SIDPP and SICP
 - b. Pit gain
 - c. Time
 - d. Regroup and identify forward plan
 - e. If pressure has built or is anticipated during the kill to reach the RWP of the annular preventer, confirm spacing and swap to the upper pipe ram

General Procedure While Running Casing

- 1. Sound alarm (alert crew)
- 2. Stab crossover and full opening safety valve and close
- 3. Space out string
- 4. Shut-in (uppermost applicable BOP, typically annular preventer first. The HCR and choke will already be in the closed position).
- 5. Confirm shut-in
- 6. Notify tool pusher/company representative
- 7. Read and record the following:
 - a. SIDPP and SICP
 - b. Pit gain
 - c. Time
 - d. Regroup and identify forward plan.
 - e. If pressure has built or is anticipated during the kill to reach the RWP of the annular preventer, confirm spacing and swap to compatible pipe ram.

General Procedure With No Pipe In Hole (Open Hole)

- 1. Sound alarm (alert crew)
- 2. Shut-in with blind rams or BSR. (The HCR and choke will already be in the closed position)
- 3. Confirm shut-in
- 4. Notify tool pusher/company representative
- 5. Read and record the following:
 - a. SICP
 - b. Pit gain
 - c. Time
- 6. Regroup and identify forward plan

General Procedures While Pulling BHA thru Stack

- 1. PRIOR to pulling last joint of drill pipe thru the stack.
 - a. Perform flow check, if flowing:
 - b. Sound alarm (alert crew)
 - c. Stab full opening safety valve and close
 - d. Space out drill string with tool joint just beneath the upper pipe ram
 - e. Shut-in using upper pipe ram. (The HCR and choke will already be in the closed position)
 - f. Confirm shut-in
 - g. Notify tool pusher/company representative
 - h. Read and record the following:
 - i. SIDPP and SICP
 - ii. Pit gain
 - iii. Time
 - iv. Regroup and identify forward plan
- 2. With BHA in the stack and compatible ram preventer and pipe combo immediately available.
 - a. Sound alarm (alert crew)
 - b. Stab crossover and full opening safety valve and close
 - c. Space out drill string with upset just beneath the compatible pipe ram
 - d. Shut-in using compatible pipe ram. (The HCR and choke will already be in the closed position.)
 - e. Confirm shut-in
 - f. Notify tool pusher/company representative
 - g. Read and record the following:
 - i. SIDPP and SICP
 - ii. Pit gain
 - iii. Time
 - iv. Regroup and identify forward plan
- 3. With BHA in the stack and NO compatible ram preventer and pipe combo immediately available.

- a. Sound alarm (alert crew)
- b. If possible to pick up high enough, pull string clear of the stack and follow "Open Hole" scenario
- c. If impossible to pick up high enough to pull the string clear of the stack
- d. Stab crossover, make up one joint/stand of drill pipe, and full opening safety valve and close
- e. Space out drill string with tool joint just beneath the upper pipe ram
- f. Shut-in using upper pipe ram. (The HCR and choke will already be in the closed position)
- g. Confirm shut-in
- h. Notify tool pusher/company representative
- i. Read and record the following:
 - i. SIDPP and SICP
 - ii. Pit gain
 - iii. Time
- j. Regroup and identify forward plan

BOP Break Testing Request

Oxy requests permission to adjust the BOP break testing requirements as per the agreement reached in the OXY/BLM meeting on September 5, 2019.

BOP break test under the following conditions:

- After a full BOP test is conducted
- When skidding to drill an intermediate section where ICP is set into the third Bone Spring or shallower.
- When skidding to drill a production section that does not penetrate into the third Bone Spring or deeper.

If the kill line is broken prior to skid, two tests will be performed.

- 1) Wellhead flange, co-flex hose, kill line connections and upper pipe rams
- 2) Wellhead flange, HCR valve, check valve, upper pipe rams

If the kill line is not broken prior to skid, only one test will be performed.

1) Wellhead flange, co-flex hose, check valve, upper pipe rams

See supporting information below:

Subject: Request for a Variance Allowing Break Testing of a Blowout Preventer Stack

OXY USA Inc. (OXY) requests a variance to allow break testing of the Blowout Preventer (BOP) stack when skidding a drilling rig between wells on multi-well pads. This practice entails retesting only the connections of the **BOP** stack that have been disconnected during this operation and not a complete **BOP** test.

Background

43 CFR part 3170 Subpart 3172 states that a **BOP** test must be performed whenever any seal subject to test pressure is broken. The current interpretation of the Bureau of Land Management (BLM) is this requires a complete **BOP** test and not just a test of the affected component. 43 CFR part 3170 Subpart 3172, Section I.D.2. states, "Some situations may exist either on a well-by-well basis or field-wide basis whereby it is commonly accepted practice to vary a particular minimum standard(s) established in this Order. This situation can be resolved by requesting a variance...". OXY feels the practice of break testing the **BOP** stack is such a situation. Therefore, as per 43 CFR part 3170 Subpart 3172, Section IV., OXY submits this request for the variance.

Supporting Rationale

43 CFR part 3170 Subpart 3172 became effective on December 19, 1988, and has remained the standard for regulating BLM onshore drilling operations for almost 30 years. During this time there have been significant changes in drilling technology. **BLM** continues to use the variance request process to allow for the use of modern technology and acceptable engineering practices that have arisen since 43 CFR part 3170 Subpart 3172 was originally released. The drilling rig fleet OXY utilizes in New Mexico was built with many modern upgrades. One of which allows the rigs to skid between wells on multi-well pads. A part of this rig package is a hydraulic winch system which safely installs and removes the BOP from the wellhead and carries it during skidding operations. This technology has made break testing a safe and reliable procldure.

American Petroleum Institute (API) standards, specifications and recommended practices are considered industry standards and are consistently utilized and referenced by the industry. 43 CFR part 3170 Subpart 3172 recognized API Recommended Practices (RP) 53 in its original development. API Standard 53,

Blowout Prevention Equipment Systems for Drilling Wells (Fourth Edition, November 2012, Addendum 1, July 2016) recognizes break testing as an acceptable practice. Specifically, API Standard 53, Section 6.5.3.4.1.b states "Pressure tests on the well control equipment shall be conducted after the disconnection or repair of any pressure containment seal in the **BOP** stack, choke line, kill line, choke manifold, or wellhead assembly but limited to the affected component."

The Bureau of Safety and Environmental Enforcement (BSEE), Department of Interior, has also utilized the API standards, specifications and best practices in the development of its offshore oil and gas regulations and incorporates them by reference within its regulations. BSEE issued new offshore regulations under 30 CFR Part 250, *Oil and Gas and Sulphur Operations in the Outer Continental Shelf - Blowout Preventer Systems and Well Control*, which became effective on July 28, 2016. Section 250.737(d.1) states "Follow the testing requirements of API Standard 53". In addition, Section 250.737(d.8) has adopted language from **API** Standard 53 as it states "Pressure test affected **BOP** components following the disconnection or repair of any well-pressure containment seal in the wellhead or **BOP** stack assembly".

Break testing has been approved by the BLM in the past. See the Appendix for a Sundry Notice that was approved in 2015 by the Farmington Field Office. This approval granted permission for the operator to break test when skidding its Aztec 1000 rig on multi-well pads.

Oxy feels break testing and our current procedures meet the intent of 43 CFR part 3170 Subpart 3172 and often exceed it. We have not seen any evidence that break testing results in more components failing tests than seen on full BOP tests. As skidding operations take place within the 30-day full BOPE test window, the BOP shell and components such as the pipe rams and check valve get tested to the full rated working pressure more often. Therefore, there are more opportunities to ensure components are in good working order. Also, Oxy's standard requires complete BOP tests more often than that of 43 CFR part 3170 Subpart 3172. In addition to function testing the annular at least weekly and the pipe and blind rams on each trip, Oxy also performs a choke drill prior to drilling out every casing shoe. As a crew's training is a vital part of well control, this procedure to simulate step one of the Driller's Method exceeds the requirements of 43 CFR part 3170 Subpart 3172.

Procedures

- 1) OXY to submit the break testing plan in the APD or Sundry Notice (SN) and receive approval prior to implementing (See Appendix for examples)
- 2) OXY would perform BOP break testing on multi-well pads where multiple intermediate sections can be drilled and cased within the 30-day BOP test window
- 3) After performing a complete BOP test on the first well and drilling and casing the hole section, three breaks would be made on the BOP.
 - > Between the check valve and the kill line
 - ➤ Between the HCR valve and the co-flex hose or the co-flex hose and the manifold
 - > Between the BOP flange and the wellhead
- 4) The BOP is then lifted and removed from the wellhead by the hydraulic winch system
- 5) After skidding to the next well, the BOP is moved to the wellhead by the hydraulic winch system and installed
- 6) The choke line and kill line are reconnected
- 7) A test plug is installed in the wellhead with a joint of drill pipe and the internal parts of the check valve are removed
- 8) A shell teit is performed against the upper pipe rams testing all thlee breaks
- 9) The internal parts of the check valve are reinstalled and the HCR valve is closed. A second test is performed on them
- 10) These tests consist of a 250 psi low test and a high test to the value submitted in the APD or SN (e.g., 5000 psi)
- Perform a function test of components not pressure tested to include the lower pipe rams, the blind rams and the annular
- 12) If this were a three well pad, the same three breaks on the BOP would be made and steps 4 through 11 would be repeated
- 13) A second break test would only be done if the third hole section could be completed within the 30-day BOP test window
- 14) If a second break test is performed, additional components that were not tested on the initial break test will be tested on this break test

Notes:

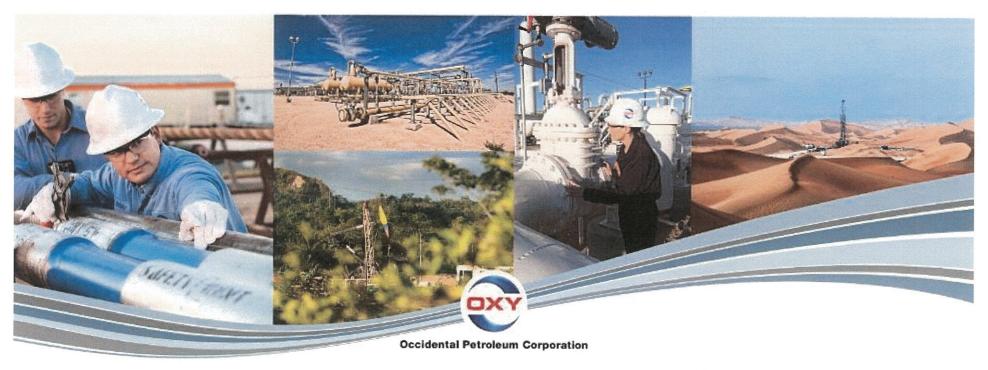
- a. If any parts of the BOP are changed out or any additional breaks are made during the skidding operation, these affected components would also be tested as in step 10.
- b. As the choke manifold remains stationary during the skidding operation and the only break to the manifold is tested in step 8 above, no further testing of the manifold is done until the next full BOP test.

Summary

OXY requests a variance to allow break testing of the BOP stack when skidding drilling rigs between wells on multi-well pads. API standards, specifications and recommended practices are considered industry standards and are consistently utilized and referenced by the industry and the BLM. API Standard 53 recognizes break testing as an acceptable practice and BSEE adopted language from this standard into its newly created 30 CFR Part 250 which also supports break testing. Due to this, OXY feels this request meets the intent of 43 CFR part 3170

REQUEST FOR A VARIANCE TO BREAK TEST THE BOP

Permian Resources New Mexico



Request for Variance

OXY USA Inc. (OXY) requests a variance to allow break testing of the Blowout Preventer (BOP) stack when skidding a drilling rig between wells on multi-well pads

- This practice entails retesting only the connections of the BOP stack that have been disconnected during this operation and not a complete BOP test.
- As the choke manifold remains stationary during the skidding operation and the only break to the manifold is tested, no further testing of the manifold is done until the next full BOP test.
- This request is being made as per Section IV of the Onshore Oil and Gas Order (OOGO) No. 2

Rationale for Allowing BOP Break Testing

American Petroleum Institute (API) standards, specifications and recommended practices are considered industry standards and are consistently utilized and referenced by the industry

- (Fourth Edition, November 2012, Addendum 1, July 2016) recognizes break API Standard 53, Blowout Prevention Equipment Systems for Drilling Wells testing as an acceptable practice.
- Specifically, API Standard 53, Section 6.5.3.4.1.b states "Pressure tests on the well control equipment shall be conducted after the disconnection or repair of any pressure containment seal in the BOP stack, choke line, kill line, choke manifold, or wellhead assembly but limited to the affected component."



Rationale for Allowing BOP Break Testing

Interior, has also utilized the API standards, specifications and best practices in the The Bureau of Safety and Environmental Enforcement (BSEE), Department of development of its offshore oil and gas regulations and incorporates them by reference within its regulations.

- BSEE issued new offshore regulations in July 2016 under 30 CFR Part 250, Oil Preventer Systems and Well Control. Within these regulations is language and Gas and Sulphur Operations in the Outer Continental Shelf - Blowout adopted from API Standard 53 which also supports break testing.
- components following the disconnection or repair of any well-pressure Specifically, Section 250.737(d.8) states "Pressure test affected BOP containment seal in the wellhead or BOP stack assembly."



Rationale for Allowing BOP Break Testing

Break testing has been approved by the BLM in the past

- The Farmington Field Office approved a Sundry Notice (SN) to allow break testing
- This SN granted permission for the operator to break test when skidding its Aztec 1000 rig on multi-well pads

Oxy feels break testing and our current procedures meet or exceed the intent of OOGO

- BOP shell and components such as the pipe rams and check valve get tested to As skidding operations take place within the 30-day full BOPE test window, the the full rated working pressure more often
- Oxy's standard requires complete BOP tests more often than that of OOGO No. 2
- training is a vital part of well control, this procedure to simulate step one of the - Oxy performs a choke drill prior to drilling out every casing shoe. As a crew's Driller's Method exceeds the requirements of OOGO No. 2



Break Testing Procedures

- 1) OXY to submit the break testing plan in the APD or Sundry Notice (SN) and receive approval prior to implementing
- OXY would perform BOP break testing on multi-well pads where multiple intermediate sections can be drilled and cased within the full BOP test window 5
- After performing a complete BOP test on the first well and drilling and casing the hole section, three breaks would be made on the BOP. 3
 - Between the check valve and the kill line
- Between the HCR valve and the co-flex hose or the co-flex hose and the manifold
 - Between the BOP flange and the wellhead
- The BOP is then lifted and removed from the wellhead by the hydraulic winch system 4
- After skidding to the next well, the BOP is moved to the wellhead by the hydraulic winch system and installed 2
- 6) The choke line and kill line are reconnected
- 7) A test plug is installed in the wellhead with a joint of drill pipe and the internal parts of the check valve are removed

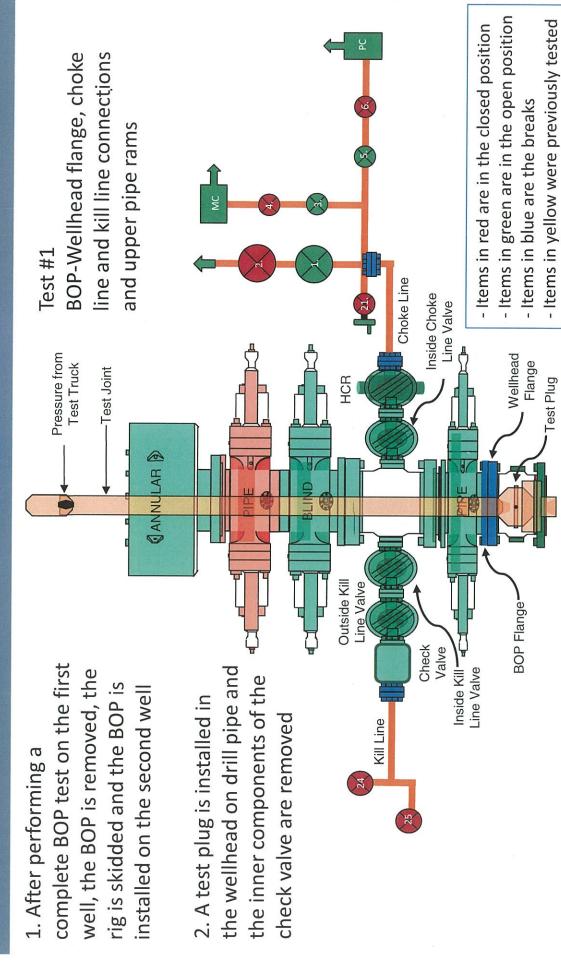


Break Testing Procedures

- 8) A shell test is performed against the upper pipe rams testing all three breaks
- 9) The internal parts of the check valve are reinstalled and the HCR valve is closed. A second test is performed on them
- 10)These tests consist of a 250 psi low test and a high test to the value submitted in the APD or SN (e.g., 5000 psi)
- 11) Perform a function test of components not pressure tested to include the lower pipe rams, the blind rams and the annular
- 12) If this were a three well pad, the same three breaks on the BOP would be made and steps 4 through 11 would be repeated
- 13) A second break test would only be done if the third hole section could be completed within the 30-day BOP test window
- 14) If a second break test is performed, additional components that were not tested on the first break test will be tested

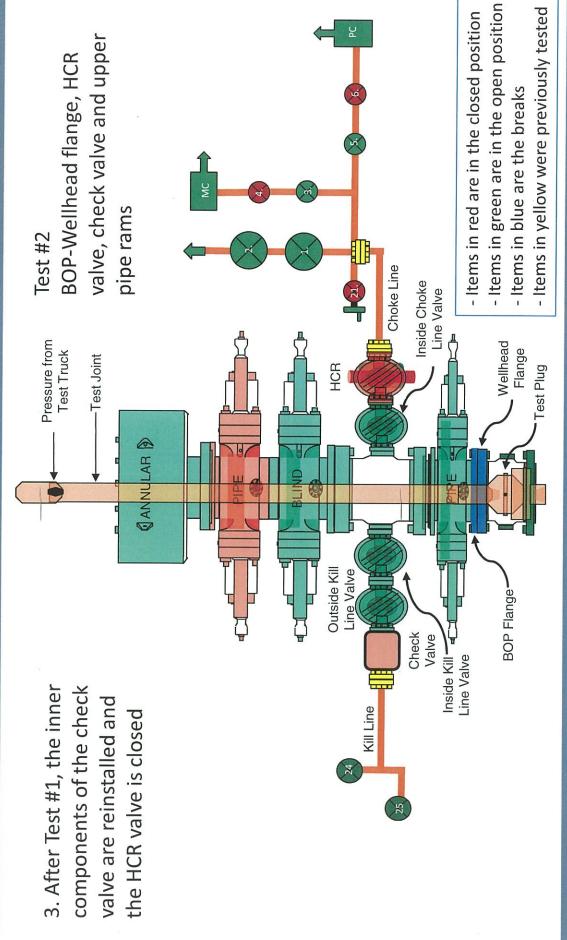


Break Testing Procedures and Tests



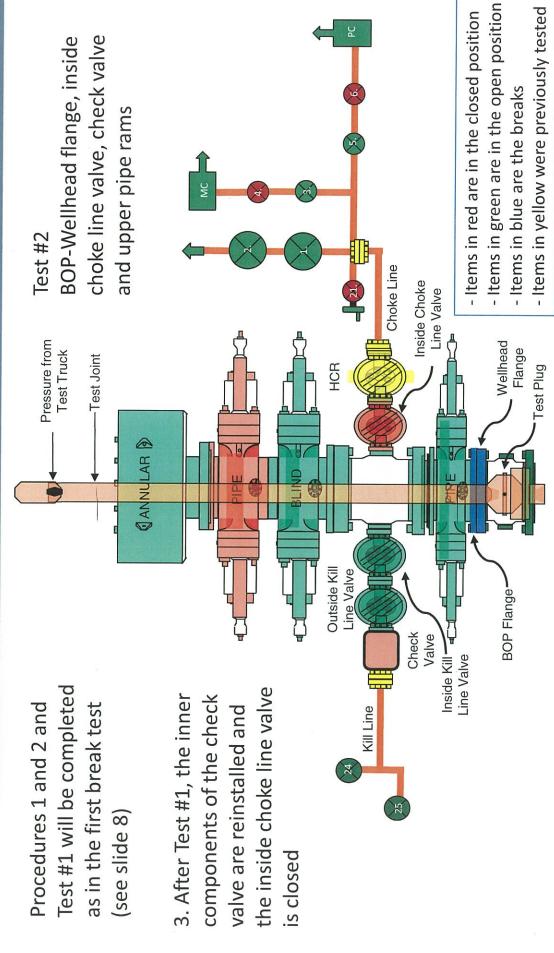


Break Testing Procedures and Tests





Second Break Testing Procedures and Tests



=

BOP standing in its carrier



Hydraulic winch system which moves the BOP from its carrier to the wellhead

BOP Handling System

12

Wellhead

BOP Handling System

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system moving the BOP over to the wellhead

Hydraulic winch

Summary for Variance Request for Break Testing

- API standards, specifications and recommended practices are considered industry standards
- OOGO No. 2 recognized API Recommended Practices (RP) 53 in its original development
- API Standard 53 recognizes break testing as an acceptable practice
- standards, specifications and best practices in the development of its offshore The Bureau of Safety and Environmental Enforcement has utilized API oil and gas regulations
- API Standard 53 recognizes break testing as an acceptable practice
- OXY feels break testing meets the intent of OOGO No. 2 to protect public health and safety and the environment



Bradenhead Cement CBL Variance Request

Oxy requests permission to adjust the CBL requirement after bradenhead cement jobs, on 7-5/8" intermediate casings, as per the agreement reached in the OXY/BLM meeting on September 5, 2019.

Three string wells:

- CBL will be required on one well per pad
- If the pumped volume of cement is less than permitted in the APD, BLM will be notified and a CBL may be run
- Echometer will be used after bradenhead cement job to determine TOC before pumping top-out cement

Four string wells:

- CBL is not required
- If the pumped volume of cement is less than permitted in the APD, BLM will be notified and a CBL may be run
- Echometer will be used after bradenhead cement job to determine TOC before pumping top-out cement

Offline Cementing Variance Request

Oxy requests a variance to cement the 9.625" and/or 7.625" intermediate casing strings offline in accordance to the approved variance, EC Tran 461365.

1. Cement Program

No changes to the cement program will take place for offline cementing.

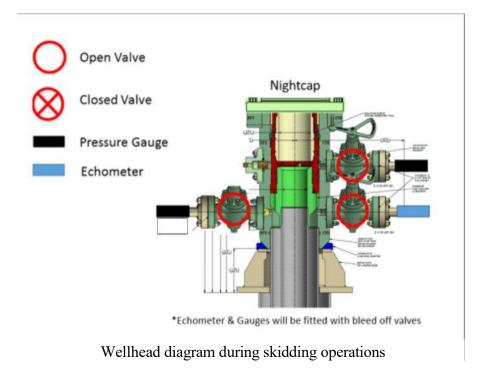
2. Offline Cementing Procedure

The operational sequence will be as follows:

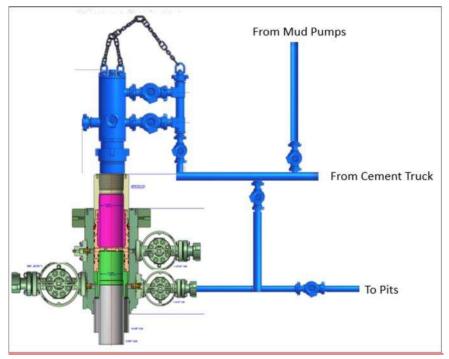
- 1. Run casing as per normal operations. While running casing, conduct negative pressure test and confirm integrity of the float equipment (float collar and shoe)
- 2. Land casing with mandrel
- 3. Fill pipe with kill weight fluid, do not circulate through floats and confirm well is static
- 4. Set annular packoff shown below and pressure test to confirm integrity of the seal. Pressure ratings of wellhead components and valves is 5,000 psi

Annular packoff with both external and internal seals





- 5. After confirmation of both annular barriers and internal barriers, nipple down BOP and install cap flange.
 - a. If any barrier fails to test, the BOP stack will not be nippled down until after the cement job is completed with cement 500ft above the highest formation capable of flow with kill weight mud above or after it has achieved 50 psi compressive strength if cannot be verified.
- 6. Skid rig to next well on pad.
- 7. Confirm well is static before removing cap flange, flange will not be removed and offline cementing operations will not commence until well is under control. If well is not static, casing outlet valves will provide access to both the casing ID and annulus. Rig or third party pump truck will kill well prior to cementing or nippling up for further remediation.
 - a. Well Control Plan
 - i. The Drillers Method will be the primary well control method to regain control of the wellbore prior to cementing, if wellbore conditions do not permit the drillers method other methods of well control may be used
 - ii. Rig pumps or a $3^{\rm rd}$ party pump will be tied into the upper casing valve to pump down the casing ID
 - iii. A high pressure return line will be rigged up to lower casing valve and run to choke manifold to control annular pressure
 - iv. Once influx is circulated out of the hole, kill weight mud will be circulated
 - v. Well will be confirmed static
 - vi. Once confirmed static, cap flange will be removed to allow for offline cementing operations to commence
- 8. Install offline cement tool
- 9. Rig up cement equipment



Wellhead diagram during offline cementing operations

- 10. Circulate bottoms up with cement truck
 - a. If gas is present on bottoms up, well will be shut in and returns rerouted through gas buster to handle entrained gas
 - b. Max anticipated time before circulating with cement truck is 6 hrs
- 11. Perform cement job taking returns from the annulus wellhead valve
- 12. Confirm well is static and floats are holding after cement job
- 13. Remove cement equipment, offline cement tools and install night cap with pressure gauge for monitoring.

Sante Fe Main Office Phone: (505) 476-3441

General Information Phone: (505) 629-6116

pkautz

None

Online Phone Directory https://www.emnrd.nm.gov/ocd/contact-us

State of New Mexico Energy, Minerals and Natural Resources Oil Conservation Division 1220 S. St Francis Dr. Santa Fe, NM 87505

CONDITIONS

Action 353867

10/29/2024

CONDITIONS

	CONDITIONS
Operator:	OGRID:
OXY USA INC	16696
P.O. Box 4294	Action Number:
Houston, TX 772104294	353867
	Action Type:
	[C-103] NOI Change of Plans (C-103A)
CONDITIONS	
Created Condition	Condition Date
Ву	