

# Application for Permit to Drill

# U.S. Department of the Interior Bureau of Land Management

Date Printed: 10/30/2024 01:42 PM

# **APD Package Report**

APD ID: 10400094820 Well Status: AAPD

APD Received Date: 09/29/2023 06:34 PM Well Name: POKER LAKE UNIT 30 BS

Operator: XTO PERMIAN OPERATING LLC Well Number: 209H

# APD Package Report Contents

- Form 3160-3
- Operator Certification Report
- Application Report
- Application Attachments
  - -- Well Plat: 1 file(s)
- Drilling Plan Report
- Drilling Plan Attachments
  - -- Blowout Prevention Choke Diagram Attachment: 1 file(s)
  - -- Blowout Prevention BOP Diagram Attachment: 1 file(s)
  - -- Casing Spec Documents: 2 file(s)
  - -- Casing Taperd String Specs: 2 file(s)
  - -- Casing Design Assumptions and Worksheet(s): 3 file(s)
  - -- Hydrogen sulfide drilling operations plan: 1 file(s)
  - -- Proposed horizontal/directional/multi-lateral plan submission: 1 file(s)
  - -- Other Facets: 8 file(s)
  - -- Other Variances: 4 file(s)
- SUPO Report
- SUPO Attachments
  - -- Existing Road Map: 1 file(s)
  - -- New Road Map: 1 file(s)
  - -- Attach Well map: 1 file(s)
  - -- Water source and transportation map: 1 file(s)
  - -- Well Site Layout Diagram: 1 file(s)
  - -- Recontouring attachment: 4 file(s)
  - -- Other SUPO Attachment: 2 file(s)
- PWD Report
- PWD Attachments
  - -- None

- Bond ReportBond Attachments
  - -- None

Form 3160-3 FORM APPROVED OMB No. 1004-0137 (June 2015) Expires: January 31, 2018 **UNITED STATES** DEPARTMENT OF THE INTERIOR 5. Lease Serial No. NMLC061634B BUREAU OF LAND MANAGEMENT APPLICATION FOR PERMIT TO DRILL OR REENTER 6. If Indian, Allotee or Tribe Name 7. If Unit or CA Agreement, Name and No. **|**✓ DRILL REENTER 1a. Type of work: NMNM071016X/POKER LAKE UNIT 1b. Type of Well: ✓ Oil Well Gas Well Other 8. Lease Name and Well No. 1c. Type of Completion: Hydraulic Fracturing Single Zone ✓ Multiple Zone POKER LAKE UNIT 30 BS 209H 2. Name of Operator 9. API Well No. XTO PERMIAN OPERATING LLC 30-**015-55**963 3a. Address 3b. Phone No. (include area code) 10. Field and Pool, or Exploratory WC-015 G-06 S243119/Bone Spring 6401 HOLIDAY HILL ROAD BLDG 5, MIDLAND, TX 7970 (432) 683-2277 4. Location of Well (Report location clearly and in accordance with any State requirements: \*) 11. Sec., T. R. M. or Blk. and Survey or Area SEC 30/T25S/R31E/NMP At surface SENW / 2435 FNL / 2010 FWL / LAT 32.101838 / LONG -103.819529 At proposed prod. zone SESW / 50 FSL / 2090 FWL / LAT 32.064807 / LONG -103.819419 12. County or Parish 13. State 14. Distance in miles and direction from nearest town or post office\* **EDDY** NM 15. Distance from proposed\* 16. No of acres in lease 17. Spacing Unit dedicated to this well 2010 feet location to nearest 440.0 property or lease line, ft. (Also to nearest drig. unit line, if any) 18. Distance from proposed location\* 19. Proposed Depth 20. BLM/BIA Bond No. in file to nearest well, drilling, completed, 30 feet 9774 feet / 23596 feet FED: COB000050 applied for, on this lease, ft. 22. Approximate date work will start\* 21. Elevations (Show whether DF, KDB, RT, GL, etc.) 23. Estimated duration 3379 feet 08/29/2024 45 days 24. Attachments The following, completed in accordance with the requirements of Onshore Oil and Gas Order No. 1, and the Hydraulic Fracturing rule per 43 CFR 3162.3-3 (as applicable) 1. Well plat certified by a registered surveyor. 4. Bond to cover the operations unless covered by an existing bond on file (see 2. A Drilling Plan. Item 20 above). 3. A Surface Use Plan (if the location is on National Forest System Lands, the 5. Operator certification. SUPO must be filed with the appropriate Forest Service Office). 6. Such other site specific information and/or plans as may be requested by the 25. Signature Name (Printed/Typed) Date CASSIE EVANS / Ph: (432) 682-8873 (Electronic Submission) 09/29/2023 Title Regulatory Analyst Approved by (Signature) Name (Printed/Typed) Date (Electronic Submission) 10/28/2024 CODY LAYTON / Ph: (575) 234-5959 Title Office

Assistant Field Manager Lands & Minerals Application approval does not warrant or certify that the applicant holds legal or equitable title to those rights in the subject lease which would entitle the applicant to conduct operations thereon.

Carlsbad Field Office

Conditions of approval, if any, are attached.

Title 18 U.S.C. Section 1001 and Title 43 U.S.C. Section 1212, make it a crime for any person knowingly and willfully to make to any department or agency of the United States any false, fictitious or fraudulent statements or representations as to any matter within its jurisdiction



#### **INSTRUCTIONS**

GENERAL: This form is designed for submitting proposals to perform certain well operations, as indicated on Federal and Indian lands and leases for action by appropriate Federal agencies, pursuant to applicable Federal laws and regulations. Any necessary special instructions concerning the use of this form and the number of copies to be submitted, particularly with regard to local, area, or regional procedures and practices, either are shown below or will be issued by, or may be obtained from local Federal offices.

ITEM I: If the proposal is to redrill to the same reservoir at a different subsurface location or to a new reservoir, use this form with appropriate notations. Consult applicable Federal regulations concerning subsequent work proposals or reports on the well.

ITEM 4: Locations on Federal or Indian land should be described in accordance with Federal requirements. Consult local Federal offices for specific instructions.

ITEM 14: Needed only when location of well cannot readily be found by road from the land or lease description. A plat, or plats, separate or on the reverse side, showing the roads to, and the surveyed location of, the wen, and any other required information, should be furnished when required by Federal agency offices.

ITEMS 15 AND 18: If well is to be, or has been directionany drilled, give distances for subsurface location of hole in any present or objective productive zone.

ITEM 22: Consult applicable Federal regulations, or appropriate officials, concerning approval of the proposal before operations are started.

ITEM 24: If the proposal will involve hydraulic fracturing operations, you must comply with 43 CFR 3162.3-3, including providing information about the protection of usable water. Operators should provide the best available information about all formations containing water and their depths. This information could include data and interpretation of resistivity logs run on nearby wells. Information may also be obtained from state or tribal regulatory agencies and from local BLM offices.

# NOTICES

The Privacy Act of 1974 and regulation in 43 CFR 2.48(d) provide that you be furnished the following information in connection with information required by this application.

AUTHORITY: 30 U.S.C. 181 et seq., 25 U.S.C. 396; 43 CFR 3160

PRINCIPAL PURPOSES: The information will be used to: (1) process and evaluate your application for a permit to drill a new oil, gas, or service wen or to reenter a plugged and abandoned well; and (2) document, for administrative use, information for the management, disposal and use of National Resource Lands and resources including (a) analyzing your proposal to discover and extract the Federal or Indian resources encountered; (b) reviewing procedures and equipment and the projected impact on the land involved; and (c) evaluating the effects of the proposed operation on the surface and subsurface water and other environmental impacts.

ROUTINE USE: Information from the record and/or the record win be transferred to appropriate Federal, State, and local or foreign agencies, when relevant to civil, criminal or regulatory investigations or prosecution, in connection with congressional inquiries and for regulatory responsibilities.

EFFECT OF NOT PROVIDING INFORMATION: Filing of this application and disclosure of the information is mandatory only if you elect to initiate a drilling or reentry operation on an oil and gas lease.

The Paperwork Reduction Act of 1995 requires us to inform you that:

The BLM conects this information to anow evaluation of the technical, safety, and environmental factors involved with drilling for oil and/or gas on Federal and Indian oil and gas leases. This information will be used to analyze and approve applications. Response to this request is mandatory only if the operator elects to initiate drilling or reentry operations on an oil and gas lease. The BLM would like you to know that you do not have to respond to this or any other Federal agency-sponsored information collection unless it displays a currently valid OMB control number.

**BURDEN HOURS STATEMENT:** Public reporting burden for this form is estimated to average 8 hours per response, including the time for reviewing instructions, gathering and maintaining data, and completing and reviewing the form. Direct comments regarding the burden estimate or any other aspect of this form to U.S. Department of the Interior, Bureau of Land Management (1004-0137), Bureau Information Conection Clearance Officer (WO-630), 1849 C Street, N.W., Mail Stop 401 LS, Washington, D.C. 20240.

(Form 3160-3, page 2)

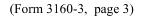
# **Additional Operator Remarks**

## **Location of Well**

0. SHL: SENW / 2435 FNL / 2010 FWL / TWSP: 25S / RANGE: 31E / SECTION: 30 / LAT: 32.101838 / LONG: -103.819529 ( TVD: 0 feet, MD: 0 feet ) PPP: SENW / 2435 FNL / 2090 FWL / TWSP: 25S / RANGE: 31E / SECTION: 30 / LAT: 32.101838 / LONG: -103.81927 ( TVD: 9774 feet, MD: 10200 feet ) BHL: SESW / 50 FSL / 2090 FWL / TWSP: 26S / RANGE: 31E / SECTION: 6 / LAT: 32.064807 / LONG: -103.819419 ( TVD: 9774 feet, MD: 23596 feet )

# **BLM Point of Contact**

Name: MARIAH HUGHES Title: Land Law Examiner Phone: (575) 234-5972 Email: mhughes@blm.gov



# **Review and Appeal Rights**

A person contesting a decision shall request a State Director review. This request must be filed within 20 working days of receipt of the Notice with the appropriate State Director (see 43 CFR 3165.3). The State Director review decision may be appealed to the Interior Board of Land Appeals, 801 North Quincy Street, Suite 300, Arlington, VA 22203 (see 43 CFR 3165.4). Contact the above listed Bureau of Land Management office for further information.



	F			ew Mexico	D	4	Revised July 9, 2024			
Submit Electronically	Ene		Minerals & Natu		-	nt			Initial Submittal	
ia OCD Permitting		U	IL CONSERV <i>A</i>	ATION DIVISI	ION		Submitta		Amended Report	
							Type:	-	As Drilled	
						As Drilled				
API Number	Pool Code	05051	WELL LOCATION Pool Nam	INFORMATION WILDER	-015 S2	2 <mark>630</mark> (	0 <mark>10</mark> ;	Во	ne Spring	
30-015 <u>-55963</u> Property Code	Property Name				.5 G-00 S2	(43119;		Sprii Well Ni		
327328 ORGID No.	Operator Name		ER LAKE UN <b>I</b> T 30 BS ————————————————————————————————————				(		Level Elevation	
373075 Surface Owner:	 Fee □ Tribal <b>X</b>			Mineral Owner:	State   Fee	☐ Tribal	I ☑ Feder	3,379	<b>,</b>	
			Surface	Location			Д			
UL Section Townsh F 30 25 S	.   -	Lot	Ft. from N/S 2,435' FNL	Ft. from E/W 2,010' FWL	Latitude 32.10183		ngitude 103.819	529	County EDDY	
		Bottom Hol								
UL Section Townsh N 6 26 S		Lot	Ft. from N/S 50' FSL	Ft. from E/W 2,090' FWL	Latitude 32.06480		ngitude 103.819	419	County EDDY	
Dedicated Acres Infill or I	Defining Well	Definin	g Well API	Overlapping Spacing U	Unit (Y/N)	Consolidat U	tion Code			
Order Numbers.				Well setbacks are unde	er Common Ow		ĭ Yes □	] No		
			Kick Off	Point (KOP)						
UL Section Townsh	.   -	Lot	Ft. from N/S	Ft. from E/W	Latitude		ngitude		County	
F 30 25 S	31 E		2,435' FNL	2,010' FWL	32.10183	8 -	103.819	529	EDDY	
UL Section Townsh	in Dance	Lot	Ft. from N/S	Point (FTP) Ft. from E/W	Latitude	т.	ngitude		County	
F 30 25 S		LUC	2,435' FNL	2,090' FWL	32.10083		ngitude -103.8192	270	EDDY	
и с	D	т		Point (LTP)	T arises 1		mair- 7		Count	
UL Section Townsh N 6 26 S	.   -	Lot	Ft. from N/S 100' FSL	Ft. from E/W 2,090' FWL	Latitude 32.06494				County EDDY	
Unitized Area or Area of Unifo	rm Interest N=071016X	Spacin	g Unit Type 🔀 Horizon	ntal  Vertical	Grou	nd Floor E	levation:	3,379'		
OPERATOR CERTIFIC	CATIONS			SURVEYOR CERTIFICATIONS						
I hereby certify that the informa best of my knowledge and belief				I hereby certify that the well location shown on this plat was plotted from field notes of actual surveys made by me or under my supervision, and that the same						
interest or unleased mineral inte location or has a right to drill th	erest in the land in his well at this loca	cluding thation purs	ne proposed bottom hole want to a contract with	is true and correct	to the best of m	ıy belief. HONAL SURVI	EYOR NO.	,		
an owner of such a mineral or w agreement or a compulsory poo				21209, DO HEREBY CERTIFY THAT THIS SURVEY PLAT AND THE ACTUAL SURVEY ON THE GROUND UPON WHICH IT IS BASED WERE PERFORMED BY ME OR UNDER MY DIRECT SUPERVISION; THAT I AM RESPONSIBLE FOR THIS SURVEY, THAT THIS SURVEY MEETS THE MINIMUM STANDARDS FOR SURVEYING IN NEW MEETS.						
If this well is a horizontal well, the consent of at least one lesse				MEXICO, AND THAT IS TO MY KNOWLEDGE AND BE	RUE AND CORREC	T TO THE B	BEST OF	1	" 1/Co	
interest in each tract (in the tars completed interval will be locate division.	get pool or formati	ion) in wh	ich any part of the well's		M		-		21209	
	1) pin	12/13	/2024	TIM C. PAPPAS REGISTERED PROFESSION STATE OF NEW MEXICO	NAL LAND SURVEY NO. 21209	ror .	\3	OFFISS	ONAL SURVEY	
Samouthal	· · · ·	Date	·	Signature and Seal o	of Professional S	Surveyor				
	I									
	1			-						
Signature Samantha Weis				Certificate Number	Da	ate of Surv	ey			
Signature Samantha Weis Printed Name samantha.r.bartnik@exxoni				Certificate Number		ate of Surv 6/11/20	•			

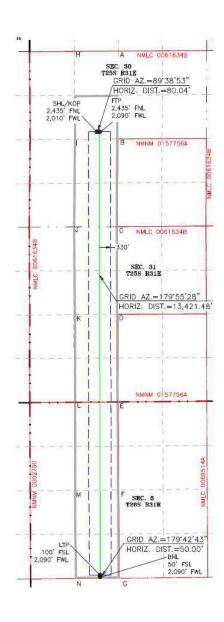


#### ACREAGE DEDICATION PLATS

This grid represents a standard section. You may superimpose a non-standard section, or a larger area, over this grid. Operators must outline the dedicated acreage in a red box, clearly show the well surface location and bottom hole location, if it is directionally drilled, with the dimensions from the section lines in the cardinal directions. If this is a horizontal wellbore show on this plat the location of the First Take Point and Last Take Point, and the point within the Completed interval (other than the First Take Point or Last Take Point) that is the closest to any outer boundary of the tract.

Surveyors shall use the latest United States government survey or dependent resurvey. Well locations will be in reference to the New Mexico Principal Meridian. If the land is not surveyed, contact the OCD Engineering Bureau. Independent subdivision surveys will not be acceptable.





SHL/KOF	(NAD83 NME)		LTP (N	AD83 NME)
Y =	401,164.32		Y =	387,743.39
X =	700,435.51		X =	700,533.23
LAT. =	32.101838 °N		LAT. =	32.064944 °N
LONG. =	103.819529 °W		LONG, =	103.819420 °W
FTP (I	NAD83 NME)		BHL (	NAD83 NME)
Y =	401,164.87		Y =	387,693.39
X =	700,515.51		X =	700,533.48
LAT. =	32.101838 °N		LAT. =	32.064807 °N
LONG, =	103.819270 °W		LONG. =	103.819419 °V
	CORNER COORD	INA	TES (NAD8	NME)
A - Y =	400,933.82 N		X =	699,752.46 E
B - Y =	400,944.65 N		X =	701,070.69 E
C - Y =		,	X =	699,727.46 E
D - Y =			X =	701,058.38 E
E - Y =	395,624.57 N	,	X =	699,742.56 E
F - Y =	395,633.71 N		X =	701,071.07 E
G - Y =	Taken was a visit of	950 1863	X =	699,750.06 E
H - Y =			X =	701,083.78 E
I - Y =	390,300.25 N		X =	699,767.38 E
J - Y =	390,312.08 N	E)	X =	701,099.41 E
K - Y =	207 625 04 41		X =	699,784.70 E
L-Y=	387,649.18 N		X =	701,115.03 E
SHL/KOF	(NAD27 NME)		LTP (N	AD27 NME)
Y =	401,106.38		Y =	387,685.82
X =	659,249.96		X =	659,347.19
LAT. =	32.101713 °N		LAT. =	32.064820 °N
LONG. =	103.819049 °W		LONG. =	103.818942 °V
FTP (	NAD27 NME)		BHL (	NAD27 NME)
Y =	401,106.98		Y =	387,635.82
X =	659,329.96		X =	659,347.49
LAT. =	32.101714 °N		LAT, =	32.064682 °N
LONG. =	103.818791 °W		LONG. =	103.818942 °W
	CORNER COORD	INA	TES (NAD27	NME)
A - Y =	400,875.90 N	(A)	X =	658,566.93 E
B - Y =	400,886.74 N	,	X =	659,885.13 E
C - Y =	398,220.62 N	,	X =	658,541.83 E
D ~ Y =				659,872.73 E
E - Y =	205 555 70 11	***	X =	658,556.84 E
F - Y =			X =	659,885.33 E
G - Y =	392,906.39 N		X =	
H - Y =	392,917.03 N	ě.	X =	659,897.94 E
[ - Y =			X =	658,581.47 E
J - Y =			X =	659,913.47 E
K - Y =	387,578.36 N	,	X =	658,598.70 E

# State of New Mexico Energy, Minerals and Natural Resources Department

Submit Electronically Via E-permitting

Oil Conservation Division 1220 South St. Francis Dr. Santa Fe, NM 87505

# NATURAL GAS MANAGEMENT PLAN

This Natural Gas Management Plan must be submitted with each Application for Permit to Drill (APD) for a new or recompleted well.

# Section 1 – Plan Description Effective May 25, 2021

I. Operator:	<u>X7</u>	O Permian	Operating,	LLC	OGRID:	373075	Date:	09 / 24 / 2	024_
II. Type: ⊠ Ori	ginal 🗆	Amendmei	nt due to □	19.15.27.9.D	(6)(a) NMAC	□ 19.15.27.9.D	0(6)(b) NMAC	☐ Other.	
If Other, please d	escribe:								
III. Well(s): Pro- be recompleted fi							wells propose	d to be drilled	or proposed to
•									
Well Name	API	ULSTR	Footages	Anticipated Oil BBL/D	3 yr Anticipated decline Oil BBL/D	Anticipated Gas MCF/D	3 yr Anticipated decline Gas MCF/D	Anticipated Produced Water BBL/D	3 yr Anticipated decline Water BBL/D
POKER LAKE	TBD	30 T25S	2435 FNL,	1.000	200	2 250	000	2.750	400
UNIT 30 BS 108H POKER LAKE	TBD	R31E 30 T25S	455 FWL 2435 FNL,	1,900	200	3,250	900	3,750	400
UNIT 30 BS 109H	155	R31E	485 FWL	1,900	200	3,250	900	3,750	400
POKER LAKE	TBD	30 T25S	2435 FNL,						
UNIT 30 BS 110H	TDD	R31E	515 FWL	1,900	200	3,250	900	3,750	400
POKER LAKE UNIT 30 BS 208H	TBD	30 T25S R31E	2435 FNL, 1980 FWL	1,900	200	3,250	900	3,750	400
POKER LAKE	TBD	30 T25S	2435 FNL,	1,500	200	3,230	700	3,730	100
UNIT 30 BS 209H		R31E	2010 FWL	1,900	200	3,250	900	3,750	400
POKER LAKE	TBD	30 T25S	2435 FNL,						
UNIT 30 BS 210H		R31E	2040 FWL	1,900	200	3,250	900	3,750	400
POKER LAKE	TBD	30 T25S	2435 FNL,	1,900	200	2 250	900	2 750	400
UNIT 30 BS 308H POKER LAKE	TBD	R31E 30 T25S	1979 FEL 2435 FNL,	1,900	200	3,250	900	3,750	400
UNIT 30 BS 309H	155	R31E	1949 FEL	1,900	200	3,250	900	3,750	400
POKER LAKE	TBD	30 T25S	2435 FNL,	ĺ				ĺ	
UNIT 30 BS 310H		R31E	1919 FEL	1,900	200	3,250	900	3,750	400
POKER LAKE	TBD	30 T25S	2435 FNL,	1.000	200	2.250	000	2.750	400
UNIT 30 BS 408H POKER LAKE	TBD	R31E 30 T25S	659 FEL 2435 FNL,	1,900	200	3,250	900	3,750	400
UNIT 30 BS 409H	160	R31E	629 FEL	1,900	200	3,250	900	3,750	400
POKER LAKE	TBD	30 T25S	2435 FNL,	1,500	200	3,230	300	3,730	100
UNIT 30 BS 410H		R31E	599 FEL	1,900	200	3,250	900	3,750	400
IV. Central Deli	very Poi	nt Name:_		PLU 30 B	S CTB		[See 19	2.15.27.9(D)(1)	NMAC]
V. Anticipated S	chedule	: Provide th	e following	information	for each new o	r recompleted v	well or set of v	vells proposed	to be drilled o

TD Reached

Date

TBD

Completion

Commencement Date

TBD

**Initial Flow** 

Back Date

TBD

Page 1 of 6

First Production

Date

TBD

Well Name

POKER LAKE UNIT

30 BS 108H

proposed to be recompleted from a single well pad or connected to a central delivery point.

API

TBD

Spud Date

TBD

POKER LAKE UNIT	<b>TBD</b>	<u>TBD</u>	<u>TBD</u>	<u>TBD</u>	<u>TBD</u>	<u>TBD</u>
30 BS 109H						
POKER LAKE UNIT	<b>TBD</b>	<u>TBD</u>	<u>TBD</u>	<u>TBD</u>	<u>TBD</u>	<u>TBD</u>
30 BS 110H						
POKER LAKE UNIT	<u>TBD</u>	<u>TBD</u>	<u>TBD</u>	<u>TBD</u>	<u>TBD</u>	<u>TBD</u>
30 BS 208H						
POKER LAKE UNIT	<b>TBD</b>	<u>TBD</u>	<u>TBD</u>	<u>TBD</u>	<u>TBD</u>	<u>TBD</u>
30 BS 209H						
POKER LAKE UNIT	<b>TBD</b>	<u>TBD</u>	<u>TBD</u>	<u>TBD</u>	<u>TBD</u>	<u>TBD</u>
30 BS 210H						
POKER LAKE UNIT	<u>TBD</u>	<u>TBD</u>	<u>TBD</u>	<u>TBD</u>	<u>TBD</u>	<u>TBD</u>
30 BS 308H						
POKER LAKE UNIT	<u>TBD</u>	<u>TBD</u>	<u>TBD</u>	<u>TBD</u>	<u>TBD</u>	<u>TBD</u>
30 BS 309H						
POKER LAKE UNIT	<b>TBD</b>	<u>TBD</u>	<u>TBD</u>	<u>TBD</u>	<u>TBD</u>	<u>TBD</u>
30 BS 310H						
POKER LAKE UNIT	<b>TBD</b>	<u>TBD</u>	<u>TBD</u>	<u>TBD</u>	<u>TBD</u>	<u>TBD</u>
30 BS 408H						
POKER LAKE UNIT	<u>TBD</u>	<u>TBD</u>	<u>TBD</u>	<u>TBD</u>	<u>TBD</u>	<u>TBD</u>
30 BS 409H						
POKER LAKE UNIT	<u>TBD</u>	<u>TBD</u>	<u>TBD</u>	<u>TBD</u>	<u>TBD</u>	<u>TBD</u>
30 BS 410H						

VI. Separation Equipment: ⊠ Attach a complete description of how Operator will size separation equipment to optimize gas capture.

VII. Operational Practices: ⊠ Attach a complete description of the actions Operator will take to comply with the requirements of Subsection A through F of 19.15.27.8 NMAC.

VIII. Best Management Practices: 

Attach a complete description of Operator's best management practices to minimize venting during active and planned maintenance.

# Section 2 – Enhanced Plan EFFECTIVE APRIL 1, 2022

Beginning April 1, 2022, an operator that is not in compliance with its statewide natural gas capture requirement for the applicable reporting area must complete this section.

☑ Operator certifies that it is not required to complete this section because Operator is in compliance with its statewide natural gas capture requirement for the applicable reporting area.

# IX. Anticipated Natural Gas Production:

Well	API	Anticipated Average Natural Gas Rate MCF/D	Anticipated Volume of Natural Gas for the First Year MCF

# X. Natural Gas Gathering System (NGGS):

for which confidentiality is asserted and the basis for such assertion.

Operator	System	ULSTR of Tie-in	Anticipated Gathering Start Date	Available Maximum Daily Capacity of System Segment Tie-in

production operatio	ns to the existing or pla	nned interconnect of	* * * * * * * * * * * * * * * * * * * *	nticipated pipeline route(s) connecting the em(s), and the maximum daily capacity of nected.
	y. The natural gas gather from the well prior to t	<b>.</b>	1 ,	gather 100% of the anticipated natural gas
	-	•	9 ()	ted to the same segment, or portion, of the n line pressure caused by the new well(s).
☐ Attach Operator	's plan to manage prod	uction in response to t	the increased line pressure.	
	• •	• 1		SA 1978 for the information provided in full description of the specific information

# Section 3 - Certifications Effective May 25, 2021

<b>Effective May 25, 2021</b>
Operator certifies that, after reasonable inquiry and based on the available information at the time of submittal:
☑ Operator will be able to connect the well(s) to a natural gas gathering system in the general area with sufficient capacity to transport one hundred percent of the anticipated volume of natural gas produced from the well(s) commencing on the date of first production, taking into account the current and anticipated volumes of produced natural gas from other wells connected to the pipeline gathering system; or
Operator will not be able to connect to a natural gas gathering system in the general area with sufficient capacity to transport one hundred percent of the anticipated volume of natural gas produced from the well(s) commencing on the date of first production, taking into account the current and anticipated volumes of produced natural gas from other wells connected to the pipeline gathering system. <i>If Operator checks this box, Operator will select one of the following:</i>
<b>Well Shut-In.</b> □ Operator will shut-in and not produce the well until it submits the certification required by Paragraph (4) of Subsection D of 19.15.27.9 NMAC; or
Venting and Flaring Plan. □ Operator has attached a venting and flaring plan that evaluates and selects one or more of the potential alternative beneficial uses for the natural gas until a natural gas gathering system is available, including:  (a) power generation on lease; (b) power generation for grid; (c) compression on lease; (d) liquids removal on lease; (e) reinjection for underground storage; (f) reinjection for temporary storage; (g) reinjection for enhanced oil recovery; (h) fuel cell production; and (i) other alternative beneficial uses approved by the division.

# **Section 4 - Notices**

- 1. If, at any time after Operator submits this Natural Gas Management Plan and before the well is spud:
- (a) Operator becomes aware that the natural gas gathering system it planned to connect the well(s) to has become unavailable or will not have capacity to transport one hundred percent of the production from the well(s), no later than 20 days after becoming aware of such information, Operator shall submit for OCD's approval a new or revised venting and flaring plan containing the information specified in Paragraph (5) of Subsection D of 19.15.27.9 NMAC; or
- (b) Operator becomes aware that it has, cumulatively for the year, become out of compliance with its baseline natural gas capture rate or natural gas capture requirement, no later than 20 days after becoming aware of such information, Operator shall submit for OCD's approval a new or revised Natural Gas Management Plan for each well it plans to spud during the next 90 days containing the information specified in Paragraph (2) of Subsection D of 19.15.27.9 NMAC, and shall file an update for each Natural Gas Management Plan until Operator is back in compliance with its baseline natural gas capture rate or natural gas capture requirement.
- 2. OCD may deny or conditionally approve an APD if Operator does not make a certification, fails to submit an adequate venting and flaring plan which includes alternative beneficial uses for the anticipated volume of natural gas produced, or if OCD determines that Operator will not have adequate natural gas takeaway capacity at the time a well will be spud.

I certify that, after reasonable inquiry, the statements in and attached to this Natural Gas Management Plan are true and correct to the best of my knowledge and acknowledge that a false statement may be subject to civil and criminal penalties under the Oil and Gas Act.

Signature: Gamantha Weis
Printed Name: Samantha Weis
Title: Permitting Advisor
E-mail Address: samantha.r.bartnik@exxonmobil.com
Date: 11/4/2024
Phone: +1-832-625-7361
OIL CONSERVATION DIVISION
(Only applicable when submitted as a standalone form)
Approved By:
Title:
Approval Date:
Conditions of Approval:

# VI. Separation Equipment:

XTO Permian Operating LLC. utilizes a "stage separation" process in which oil and gas separation is carried out through a series of separators operating at successively reduced pressures. Hydrocarbon liquids are produced into a high-pressure inlet separator, then carried through one or more lower pressure separation vessels before entering the storage tanks. The purpose of this separation process is to attain maximum recovery of liquid hydrocarbons from the fluids and allow maximum capture of produced gas into the sales pipeline. XTO utilizes a series of Low-Pressure Compression units to capture gas off the staged separation and send it to the sales pipeline. This process minimizes the amount of flash gas that enters the end-stage storage tanks that is subsequently vented or flared.

# VII. Operational Practices

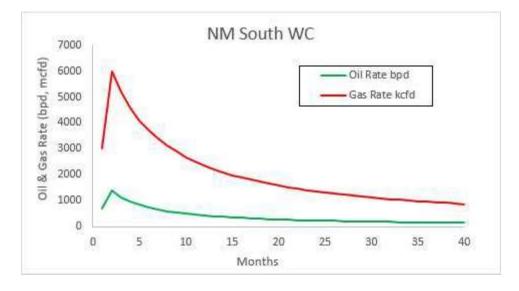
XTO Permian Operating LLC will employ best management practices and control technologies to maximize the recovery and minimize waste of natural gas through venting and flaring.

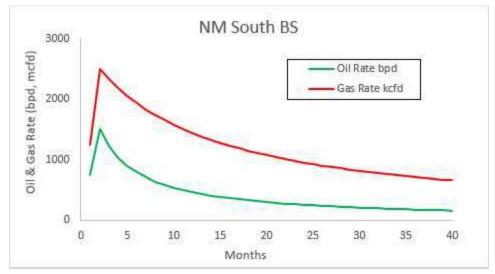
- During drilling operations, XTO will utilize flares to capture and control natural gas, where technically feasible. If flaring is deemed technically in-feasible, XTO will employ best management practices to minimize or reduce venting to the extent possible.
- During completions operations, XTO will utilize Green Completion methods to capture gas produced during well completions that is otherwise vented or flared. If capture is technically infeasible, flares will be used to control flow back fluids entering into frac tanks during initial flowback. Upon indication of first measurable hydrocarbon volumes, XTO Permian Operating LLCwill turn operations to onsite separation vessels and flow to the gathering pipeline.
- During production operations, XTO Permian Operating LLC will take every practical effort to minimize waste of natural gas through venting and flaring by:
  - Designing and constructing facilities in a manner consistent to achieve maximum capture and control of hydrocarbon liquids & produced gas
  - Utilizing a closed-loop capture system to collect, and route produced gas to sales line via low pressure compression, or to a flare/combustor
  - Flaring in lieu of venting, where technically feasible
  - Utilizing auto-ignitors or continuous pilots, with thermocouples connected to Scada, to quickly detect and resolve issues related to malfunctioning flares/combustors
  - Employ the use of automatic tank gauging to minimize storage tank venting during loading events
  - Installing air-driven or electric-driven pneumatics & combustion engines, where technically feasible to minimize venting to the atmosphere
  - Confirm equipment is properly maintained and repaired through a preventative maintenance and repair program to ensure equipment meets all manufacturer specifications

• Conduct and document AVO inspections on the frequency set forth in Part 27 to detect and repair any onsite leaks as quickly and efficiently as is feasible.

VIII. Best Management Practices during Maintenance

XTO Permian Operating LLC. will utilize best management practices to minimize venting during active and planned maintenance activities. XTO is operating under guidance that production facilities permitted under NOI permits have no provisions to allow high pressure flaring and high-pressure flaring is only allowed in disruption scenarios so long as the duration is less than eight hours. When technically feasible, flaring during maintenance activities will be utilized in lieu of venting to the atmosphere. XTO will work with third-party operators during scheduled maintenance of downstream pipeline or processing plants to address those events ahead of time to minimize venting. Actions considered include identifying alternative capture approaches or planning to temporarily reduce production or shut in the well to address these circumstances.





U.S. Department of the Interior BUREAU OF LAND MANAGEMENT

# Drilling Plan Data Report

Submission Date: 09/29/2023

**Operator Name: XTO PERMIAN OPERATING LLC** 

Well Name: POKER LAKE UNIT 30 BS

Well Name: POKER LAKE UNIT 30 BS

Well Type: OIL WELL

APD ID: 10400094820

Well Number: 209H

Well Work Type: Drill

Highlighted data reflects the most recent changes

**Show Final Text** 

# **Section 1 - Geologic Formations**

Formation ID	Formation Name Elevation True Vertical Measured Depth Lithologies		Lithologies	Mineral Resources	Producing Formatio		
14396375	QUATERNARY	3379	0	0	ALLUVIUM	USEABLE WATER	N
14396376	RUSTLER	2404	975	975	ANHYDRITE, SANDSTONE	USEABLE WATER	N
14396377	SALADO 20		1302	1302 SALT		NONE	N
14396378	BASE OF SALT	-584	3963	3963	SALT	NONE	N
14396379	DELAWARE	-794	4173	4173	LIMESTONE, SANDSTONE	NATURAL GAS, OIL, OTHER: Produced Water	N
14396380	BONE SPRING	-4620	7999	7999	LIMESTONE, SANDSTONE	NATURAL GAS, OIL, OTHER : Produced Water	Y
14396381	BONE SPRING 1ST	-5572	8951	8951	LIMESTONE, SANDSTONE	NATURAL GAS, OIL, OTHER : Produced Water	Y
14396382	BONE SPRING 2ND	-6295	9674	9674	LIMESTONE, SANDSTONE	NATURAL GAS, OIL, OTHER : Produced Water	Y

# **Section 2 - Blowout Prevention**

Pressure Rating (PSI): 5M Rating Depth: 9774

**Equipment:** Once the permanent WH is installed on the surface casing, the blow out preventer equipment (BOP) will consist of a 5M Hydril and a 5M Double Ram BOP. XTO will use a Multi-Bowl system which is attached.

# Requesting Variance? YES

Variance request: A variance is requested to allow use of a flex hose as the choke line from the BOP to the Choke Manifold. If this hose is used, a copy of the manufacturer's certification and pressure test chart will be kept on the rig. Attached is an example of a certification and pressure test chart. The manufacturer does not require anchors. XTO requests a variance to be able to batch drill this well if necessary. In doing so, XTO will set casing and ensure that the well is cemented properly (unless approval is given for offline cementing) and the well is static. With floats holding, no pressure on the csg annulus, and the installation of a 10K TA cap as per Cactus recommendations, XTO will contact the BLM to skid the rig to drill the remaining wells on the pad. Once surface and both intermediate strings are all completed, XTO will begin drilling the production hole on each of the wells. A variance is requested to ONLY test broken pressure seals on the BOP equipment when moving from wellhead to wellhead which is in compliance with API Standard 53. API standard 53 states, that for pad drilling operation, moving from one wellhead to another within 21 days, pressure testing is required for pressure-containing and pressure-controlling connections when the integrity of a pressure seal is broken. We will request permission to ONLY retest broken pressure seals if the following conditions are met: 1. After a

Well Name: POKER LAKE UNIT 30 BS Well Number: 209H

full BOP test is conducted on the first well on the pad 2. When skidding to drill an intermediate section that does not penetrate into the Wolfcamp.

**Testing Procedure:** All BOP testing will be done by an independent service company. Operator will test as per 43 CFR 3172.

**Choke Diagram Attachment:** 

PLU\_30\_BS\_5MCM\_20240808101330.pdf

**BOP Diagram Attachment:** 

PLU\_30\_BS\_5MBOP\_20240808101400.pdf

# **Section 3 - Casing**

Casing ID	String Type	Hole Size	Csg Size	Condition	Standard	Tapered String	Top Set MD	Bottom Set MD	Top Set TVD	Bottom Set TVD	Top Set MSL	Bottom Set MSL	Calculated casing length MD	Grade	Weight	Joint Type	Collapse SF	Burst SF	Joint SF Type	Joint SF	Body SF Type	Body SF
1	SURFACE	12.2 5	9.625	NEW	API	N	0	1075	0	1075	3379	2304	1075	J-55	40	BUTT	5.28	1.57	DRY	14.6 5	DRY	14.6 5
2	INTERMED IATE	8.75	7.625	NEW	API	Υ	0	8850	0	8827	0	-5448	8850	L-80	29.7	FJ	2.26	1.86	DRY	2.82	DRY	2.82
	PRODUCTI ON	6.75	5.5	NEW	NON API	Υ	0	23596	0	9774	0	-6395	23596	P- 110		OTHER - TalonHTQ/F reedomHTQ	2.49	1.21	DRY	4.93	DRY	4.93

1.0	CIDA	. Attac	hmonte
va	SILIC	ı Allac	hments

Casing ID:	1	Strina	SURFACE

**Inspection Document:** 

**Spec Document:** 

**Tapered String Spec:** 

Casing Design Assumptions and Worksheet(s):

PLU\_30\_BS\_209H\_Csg\_20230926140717.pdf

Well Name: POKER LAKE UNIT 30 BS Well Number: 209H

# **Casing Attachments**

Casing ID: 2

String

**INTERMEDIATE** 

**Inspection Document:** 

**Spec Document:** 

**Tapered String Spec:** 

PLU\_30\_BS\_209H\_Csg\_20230926140818.pdf

**Casing Design Assumptions and Worksheet(s):** 

PLU 30 BS 209H Csg 20230926141156.pdf

Casing ID: 3

String

**PRODUCTION** 

**Inspection Document:** 

**Spec Document:** 

Freedom\_Semi\_Premium\_5.5000\_23.0000\_0.4150\_\_P110\_RY\_20240905074852.pdf
Talon\_Semiflush\_HTQ\_RD\_5.5000\_23.0000\_0.4150\_\_P110\_RY\_20240905074853.pdf

**Tapered String Spec:** 

PLU\_30\_BS\_209H\_Csg\_20230926140337.pdf

Casing Design Assumptions and Worksheet(s):

PLU\_30\_BS\_209H\_Csg\_20230926140450.pdf

# **Section 4 - Cement**

String Type	Lead/Tail	Stage Tool Depth	Тор МD	Bottom MD	Quantity(sx)	Yield	Density	Cu Ft	Excess%	Cement type	Additives
SURFACE	Lead		0	1075	250	1.87	12.9	467.5	100	EconoCem- HLTRRC	NA
SURFACE	Tail		0	1075	130	1.35	14.8	175.5	100	Class C	2% CaCl
INTERMEDIATE	Lead		0	6450	210	1.35	14.8	283.5	100	Class C	NA
INTERMEDIATE	Tail		6450	8850	730	1.33	14.8	970.9	100	Class C	NA

Well Name: POKER LAKE UNIT 30 BS Well Number: 209H

String Type	Lead/Tail	Stage Tool Depth	Top MD	Bottom MD	Quantity(sx)	Yield	Density	Cu Ft	Excess%	Cement type	Additives
PRODUCTION	Lead		8550	9250	20	2.69	11.5	53.8	30	NeoCem	NA
PRODUCTION	Tail		0	2359 6	1030	1.51	13.2	1555. 3	30	VersaCem	NA

# **Section 5 - Circulating Medium**

Mud System Type: Closed

Will an air or gas system be Used? NO

Description of the equipment for the circulating system in accordance with Onshore Order #2:

Diagram of the equipment for the circulating system in accordance with Onshore Order #2:

**Describe what will be on location to control well or mitigate other conditions:** The necessary mud products for weight addition and fluid loss control will be on location at all times.

Describe the mud monitoring system utilized: Spud with fresh water/native mud. Drill out from under surface casing with Saturated Salt solution. Saturated Salt mud will be used while drilling through the salt formation. Use fibrous materials as needed to control seepage and lost circulation. Pump viscous sweeps as needed for hole cleaning. Pump speed will be recorded on a daily drilling report after mudding up. A Pason or Totco will be used to detect changes in loss or gain of mud volume. A mud test will be performed every 24 hours to determine: density, viscosity, strength, filtration and pH as necessary. Use available solids controls equipment to help keep mud weight down after mud up. Rig up solids control equipment to operate as a closed loop system.

# **Circulating Medium Table**

Top Depth	Bottom Depth	Mud Type	Min Weight (lbs/gal)	Max Weight (lbs/gal)	Density (lbs/cu ft)	Gel Strength (lbs/100 sqft)	ЬН	Viscosity (CP)	Salinity (ppm)	Filtration (cc)	Additional Characteristics
1075	4173	SALT SATURATED	10.5	11							
8850	2359 6	OIL-BASED MUD	11.5	12							
0	1075	WATER-BASED MUD	8.7	9.2							fresh water or native water
4173	8850	OTHER : BDE/OBM	9	9.5							

Well Name: POKER LAKE UNIT 30 BS Well Number: 209H

# Section 6 - Test, Logging, Coring

### List of production tests including testing procedures, equipment and safety measures:

Mud Logger: Mud Logging Unit (2 man) below intermediate casing.

Open hole logging will not be done on this well.

List of open and cased hole logs run in the well:

GAMMA RAY LOG, DIRECTIONAL SURVEY, CEMENT BOND LOG, MEASUREMENT WHILE DRILLING, MUD

LOG/GEOLOGICAL LITHOLOGY LOG, Coring operation description for the well:

No coring is planned for the well.

# **Section 7 - Pressure**

Anticipated Bottom Hole Pressure: 6099 Anticipated Surface Pressure: 3948

Anticipated Bottom Hole Temperature(F): 185

Anticipated abnormal pressures, temperatures, or potential geologic hazards? NO

Describe:

Contingency Plans geoharzards description:

Contingency Plans geohazards

Hydrogen Sulfide drilling operations plan required? YES

Hydrogen sulfide drilling operations

XTO\_Energy\_H2S\_Plan\_Updated\_20240808094708.pdf

### **Section 8 - Other Information**

# Proposed horizontal/directional/multi-lateral plan submission:

PLU 30 BS 209H DD 20230926142152.pdf

Other proposed operations facets description:

# Other proposed operations facets attachment:

PLU\_30\_BS\_209H\_Cmt\_20240808121312.pdf

PLU\_30\_BS\_209H\_RL\_20240808121312.pdf

PLU\_30\_BS\_H2S\_Plan\_20240808121350.pdf

PLU 30 BS H2S DiaC 20240808121351.pdf

PLU 30 BS H2S DiaA 20240808121351.pdf

PLU 30 BS H2S DiaD 20240808121351.pdf

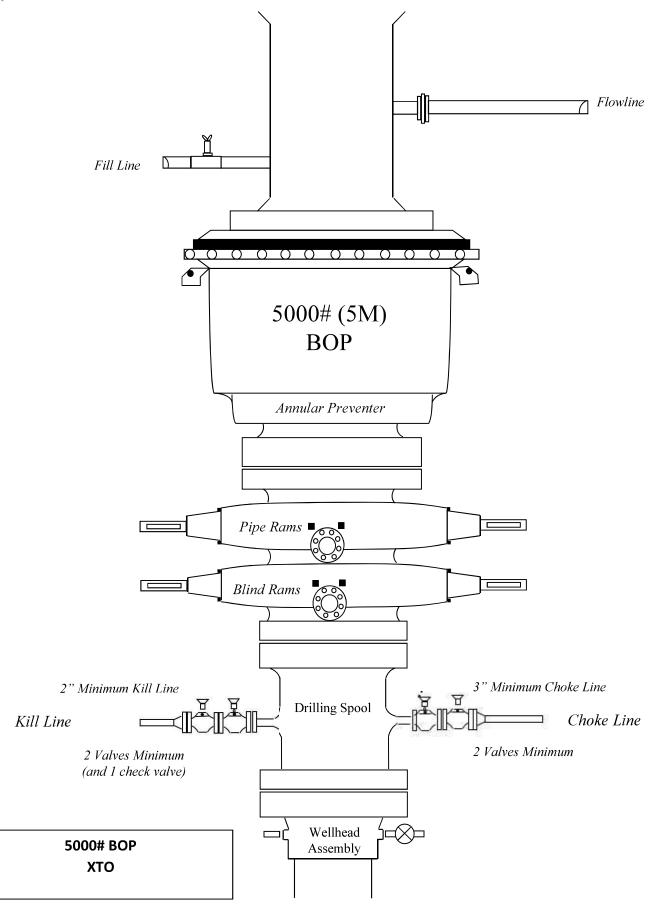
PLU 30 BS H2S DiaB 20240808121351.pdf

PLU 30 BS MBS 20240808121351.pdf

Other Variance attachment:

Well Name: POKER LAKE UNIT 30 BS Well Number: 209H

BOP\_Break\_Test\_Variance\_20240808105749.pdf
Offline\_Cement\_Variance\_Surf\_\_\_Interm\_Csg\_20240808105748.pdf
Spudder\_Rig\_Request\_20240808105750.pdf
Updated\_Flex\_Hose\_20240808105750.pdf



# **Casing Assumptions**

	g Weight Grade Collar New/Used Burst Collapse Tension	40 J-55 BTC New 1.57 5.28 14.65	29.7 RY P-110 Flush Joint New 2.56 2.65 2.12	29.7 HC L-80 Flush Joint New 1.86 2.26 2.82	23 RY P-110 Semi-Premium New 1.21 2.78 2.14	23 RY P-110 Semi-Flush New 1.21 2.56 4.33
	OD Csg	5' 9.625	7.625	50' 7.625	)' 5.5	00' 5.5
	ze Depth	0' - 1075'	0, – 4000,	4000' - 8850'	0, – 8750	8750' - 9500'
Casing Design	Hole Size	12.25	8.75	8.75	6.75	6.75

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# **U. S. Steel Tubular Products**

# 5.500" 23.00lb/ft (0.415" Wall) P110 RY USS-FREEDOM HTQ®



MECHANICAL PROPERTIES	Pipe	USS-FREEDOM HTQ <sup>®</sup>	
Minimum Yield Strength	110,000		psi
Maximum Yield Strength	125,000		psi
Minimum Tensile Strength	125,000		psi
DIMENSIONS	Pipe	USS-FREEDOM HTQ $^{ m  ext{\scriptsize R}}$	
Outside Diameter	5.500	6.300	in.
Wall Thickness	0.415		in.
Inside Diameter	4.670	4.670	in.
Standard Drift	4.545	4.545	in.
Alternate Drift			in.
Nominal Linear Weight, T&C	23.00		lb/ft
Plain End Weight	22.56		lb/ft
SECTION AREA	Pipe	USS-FREEDOM HTQ®	
Critical Area	6.630	6.630	sq. in.
Joint Efficiency		100.0	%
PERFORMANCE	Pipe	USS-FREEDOM HTQ <sup>®</sup>	
Minimum Collapse Pressure	14,540	14,540	psi
Minimum Internal Yield Pressure	14,520	14,520	psi
Minimum Pipe Body Yield Strength	729,000		lb
Joint Strength		729,000	lb
Compression Rating		729,000	lb
Reference Length [4]		21,138	ft
Maximum Uniaxial Bend Rating [2]		91.7	deg/100 ft
MAKE-UP DATA	Pipe	USS-FREEDOM HTQ <sup>®</sup>	
Make-Up Loss		4.13	in.
Minimum Make-Up Torque [3]		15,000	ft-Ib
Maximum Make-Up Torque [3]		21,000	ft-Ib
Maximum Operating Torque[3]		32,500	ft-Ib

# **Notes**

- 1. Other than proprietary collapse and connection values, performance properties have been calculated using standard equations defined by API 5C3 and do not incorporate any additional design or safety factors. Calculations assume nominal pipe OD, nominal wall thickness, and Specified Minimum Yield Strength (SMYS).
- 2. Uniaxial bending rating shown is structural only, and equal to compression efficiency.
- 3. Torques have been calculated assuming a thread compound friction factor of 1.0 and are recommended only. Field make-up torques may require adjustment based on actual field conditions (e.g. make-up speed, temperature, thread compound, etc.).
- 4. Reference length is calculated by joint strength divided by plain end weight with 1.5 safety factor.

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> U. S. Steel Tubular Products 460 Wildwood Forest Drive, Suite 300S Spring, Texas 77380

1-877-893-9461 connections@uss.com www.usstubular.com

1/4/2024 11:09:09 AM

# 5.500" 23.00lb/ft (0.415" Wall) P110 RY USS-TALON HTQ™ RD

Minimum Yield Strength         110,000          psi           Maximum Yield Strength         125,000          psi           Minimum Tensile Strength         125,000          psi           DIMENSIONS         Pipe         USS-TALON HTQ™ RD           Outside Diameter         5.500         5.900         in.           Vall Thickness         0.415          in.           Inside Diameter         4.670         4.670         in.           Standard Drift         4.545         4.545         in.           Alternate Drift           lb/ft           Nominal Linear Weight, T&C         23.00         -         lb/ft           Plain End Weight         22.56         -         lb/ft           SECTION AREA         Pipe         USS-TALON HTQ™ RD           Critical Area         6.630         6.425         sq. in.           Joint Efficiency         -         96.9         %           PERFORMANCE         Pipe         USS-TALON HTQ™ RD         psi           Minimum Internal Yield Pressure         14,540         14,520         psi           Minimum Pipe Body Yield Strength         729,000					
Maximum Yield Strength         125,000          psi           DIMENSIONS         Pipe         USS-TALON HTQ™ RD           Outside Diameter         5.500         5.900         in.           Wall Thickness         0.415         -         in.           Inside Diameter         4.670         4.670         in.           Standard Drift         4.545         4.545         in.           Alternate Drift         -         -         Ib/ft           Nominal Linear Weight, T&C         23.00         -         Ib/ft           Plain End Weight         22.56         -         Ib/ft           SECTION AREA         Pipe         USS-TALON HTQ™ RD         V           Critical Area         6.630         6.425         sq. in.           Joint Efficiency         -         96.9         %           PERFORMACE         Pipe         USS-TALON HTQ™ RD         V           Minimum Collapse Pressure         14,540         14,540         psi           Minimum Pipe Body Yield Strength         720         -         Ib           Joint Strength         -         707,000         Ib           Compression Rating         -         707,000         Ib	MECHANICAL PROPERTIES	Pipe	USS-TALON HTQ™ RD		[6]
DIMENSIONS         Pipe         USS-TALON HTQ™ RD           Outside Diameter         5.500         5.900         in.           Wall Thickness         0.415         -         in.           Inside Diameter         4.670         4.670         in.           Standard Drift         4.545         4.545         in.           Alternate Drift          -         in.           Nominal Linear Weight, T&C         23.00         -         Ib/ft           Plain End Weight         22.56         -         Ib/ft           SECTION AREA         Pipe         USS-TALON HTQ™ RD         V           Critical Area         6.630         6.425         sq. in.           Joint Efficiency          96.9         %           PERFORMANCE         Pipe         USS-TALON HTQ™ RD           Minimum Collapse Pressure         14,540         14,540         psi           Minimum Pipe Body Yield Strength         729,000          Ib           Joint Strength          707,000         Ib           Compression Rating          707,000         Ib           Reference Length          20,490         ft           Make-U	Minimum Yield Strength	110,000		psi	
DIMENSIONS         Pipe         USS-TALON HTQ™ RD           Outside Diameter         5.500         5.900         in.           Wall Thickness         0.415          in.           Inside Diameter         4.670         4.670         in.           Standard Drift         4.545         4.545         in.           Alternate Drift           Ib/ft           Nominal Linear Weight, T&C         23.00          Ib/ft           Plain End Weight         22.56          Ib/ft           SECTION AREA         Pipe         USS-TALON HTQ™ RD         V           Critical Area Joint Efficiency         6.630         6.425         sq. in.           Joint Efficiency          96.9         %           Minimum Collapse Pressure         14,540         14,520         psi           Minimum Internal Yield Pressure         14,520         14,520         psi           Minimum Pipe Body Yield Strength         729,000          Ib           Joint Strength          707,000         Ib           Compression Rating          707,000         Ib           Reference Length          88.9	Maximum Yield Strength	125,000		psi	
Outside Diameter         5.500         5.900         in.           Wall Thickness         0.415          in.           Inside Diameter         4.670         4.670         in.           Standard Drift         4.545         4.545         in.           Alternate Drift           in.           Nominal Linear Weight, T&C         23.00          lb/ft           Plain End Weight         22.56          lb/ft           SECTION AREA         Pipe         USS-TALON HTQ™RD           Critical Area         6.630         6.425         sq. in.           Joint Efficiency          96.9         %           PERFORMANCE         Pipe         USS-TALON HTQ™RD           Minimum Collapse Pressure         14,540         14,520         psi           Minimum Pipe Body Yield Strength         729,000          Ib           Joint Strength          707,000         Ib           Compression Rating          707,000         Ib           Reference Length          88.9         deg/100 ft           MAKE-UP DATA         Pipe         USS-TALON HTQ™RD	Minimum Tensile Strength	125,000		psi	-
Wall Thickness         0.415          in.           Inside Diameter         4.670         4.670         in.           Standard Drift         4.545         4.545         in.           Alternate Drift           in.           Nominal Linear Weight, T&C         23.00          lb/ft           Plain End Weight         22.56          lb/ft           SECTION AREA         Pipe         USS-TALON HTQ™ RD           Critical Area         6.630         6.425         sq. in.           Joint Efficiency          96.9         %           PERFORMANCE         Pipe         USS-TALON HTQ™ RD           Minimum Collapse Pressure         14,540         14,540         psi           Minimum Internal Yield Pressure         14,520         14,520         psi           Minimum Pipe Body Yield Strength         729,000          Ib           Joint Strength          707,000         Ib           Compression Rating          707,000         Ib           Reference Length          88.9         deg/100 ft           MAKE-UP DATA         Pipe         USS-TALON HTQ™ RD      <	DIMENSIONS	Pipe	USS-TALON HTQ™ RD		
Inside Diameter         4.670         4.670         in.           Standard Drift         4.545         4.545         in.           Alternate Drift           in.           Nominal Linear Weight, T&C         23.00          Ib/ft           Plain End Weight         22.56          Ib/ft           SECTION AREA         Pipe         USS-TALON HTQ™ RD         VERTON INTERPRITED INTERPRITE	Outside Diameter	5.500	5.900	in.	
Standard Drift       4.545       4.545       in.         Alternate Drift         in.         Nominal Linear Weight, T&C       23.00        lb/ft         Plain End Weight       22.56        lb/ft         SECTION AREA       Pipe       USS-TALON HTQ™ RD       V         Critical Area       6.630       6.425       sq. in.         Joint Efficiency        96.9       %         PERFORMANCE       Pipe       USS-TALON HTQ™ RD         Minimum Collapse Pressure       14,540       14,540       psi         Minimum Pipe Body Yield Strength       729,000        lb         Joint Strength        707,000       lb         Compression Rating        707,000       lb         Reference Length        88.9       deg/100 ft         MAKE-UP DATA       Pipe       USS-TALON HTQ™ RD         Make-Up Loss        5.58       in.         Minimum Make-Up Torque        20,800       ft-lb         Maximum Make-Up Torque        20,800       ft-lb	Wall Thickness	0.415		in.	-
Alternate Drift         in.         Nominal Linear Weight, T&C       23.00        lb/ft         Plain End Weight       22.56        lb/ft         SECTION AREA       Pipe       USS-TALON HTQ™ RD       Sq. in.         Critical Area       6.630       6.425       sq. in.         Joint Efficiency        96.9       %         PERFORMANCE       Pipe       USS-TALON HTQ™ RD         Minimum Collapse Pressure       14,540       14,540       psi         Minimum Internal Yield Pressure       14,520       14,520       psi         Minimum Pipe Body Yield Strength       729,000        lb         Joint Strength        707,000       lb         Compression Rating        707,000       lb         Reference Length        88.9       deg/100 ft         MAKE-UP DATA       Pipe       USS-TALON HTQ™ RD         Make-Up Loss        5.58       in.         Minimum Make-Up Torque        20,800       ft-lb         Maximum Make-Up Torque        23,800       ft-lb	Inside Diameter	4.670	4.670	in.	-
Nominal Linear Weight, T&C         23.00          Ib/ft           Plain End Weight         22.56          Ib/ft           SECTION AREA         Pipe         USS-TALON HTQ™ RD           Critical Area         6.630         6.425         sq. in.           Joint Efficiency          96.9         %           PERFORMANCE         Pipe         USS-TALON HTQ™ RD           Minimum Collapse Pressure         14,540         14,540         psi           Minimum Internal Yield Pressure         14,520         14,520         psi           Minimum Pipe Body Yield Strength         729,000          Ib           Joint Strength          707,000         Ib           Compression Rating          707,000         Ib           Reference Length          20,490         ft           Maximum Uniaxial Bend Rating          88.9         deg/100 ft           MAKE-UP DATA         Pipe         USS-TALON HTQ™ RD           Make-Up Torque          20,800         ft-Ib           Maximum Make-Up Torque          20,800         ft-Ib	Standard Drift	4.545	4.545	in.	-
Plain End Weight         22.56          Ib/ft           SECTION AREA         Pipe         USS-TALON HTQ™ RD           Critical Area         6.630         6.425         sq. in.           Joint Efficiency          96.9         %           PERFORMANCE         Pipe         USS-TALON HTQ™ RD           Minimum Collapse Pressure         14,540         14,540         psi           Minimum Internal Yield Pressure         14,520         14,520         psi           Minimum Pipe Body Yield Strength         729,000          lb           Joint Strength          707,000         lb           Compression Rating          707,000         lb           Reference Length          20,490         ft           Maximum Uniaxial Bend Rating          88.9         deg/100 ft           MAKE-UP DATA         Pipe         USS-TALON HTQ™ RD           Make-Up Torque          5.58         in.           Minimum Make-Up Torque          20,800         ft-lb           Maximum Make-Up Torque          23,800         ft-lb	Alternate Drift			in.	-
SECTION AREA         Pipe         USS-TALON HTQ™ RD           Critical Area         6.630         6.425         sq. in.           Joint Efficiency          96.9         %           PERFORMANCE         Pipe         USS-TALON HTQ™ RD           Minimum Collapse Pressure         14,540         14,540         psi           Minimum Internal Yield Pressure         14,520         14,520         psi           Minimum Pipe Body Yield Strength         729,000          lb           Joint Strength          707,000         lb           Compression Rating          707,000         lb           Reference Length          20,490         ft           Maximum Uniaxial Bend Rating          88.9         deg/100 ft           MAKE-UP DATA         Pipe         USS-TALON HTQ™ RD           Make-Up Loss          5.58         in.           Minimum Make-Up Torque          20,800         ft-lb           Maximum Make-Up Torque          23,800         ft-lb	Nominal Linear Weight, T&C	23.00		lb/ft	-
Critical Area       6.630       6.425       sq. in.         Joint Efficiency        96.9       %         PERFORMANCE       Pipe       USS-TALON HTQ™ RD         Minimum Collapse Pressure       14,540       14,540       psi         Minimum Internal Yield Pressure       14,520       14,520       psi         Minimum Pipe Body Yield Strength       729,000        Ib         Joint Strength        707,000       Ib         Compression Rating        707,000       Ib         Reference Length        20,490       ft         Maximum Uniaxial Bend Rating        88.9       deg/100 ft         MAKE-UP DATA       Pipe       USS-TALON HTQ™ RD         Make-Up Loss        5.58       in.         Minimum Make-Up Torque        20,800       ft-Ib         Maximum Make-Up Torque        23,800       ft-Ib	Plain End Weight	22.56		lb/ft	-
Joint Efficiency96.9%PERFORMANCEPipeUSS-TALON HTQ™ RDMinimum Collapse Pressure14,54014,540psiMinimum Internal Yield Pressure14,52014,520psiMinimum Pipe Body Yield Strength729,000lbJoint Strength707,000lbCompression Rating707,000lbReference Length20,490ftMaximum Uniaxial Bend Rating88.9deg/100 ftMAKE-UP DATAPipeUSS-TALON HTQ™ RDMake-Up Loss5.58in.Minimum Make-Up Torque20,800ft-lbMaximum Make-Up Torque23,800ft-lb	SECTION AREA	Pipe	USS-TALON HTQ™ RD		
Pipe USS-TALON HTQ™ RD  Minimum Collapse Pressure 14,540 14,540 psi Minimum Internal Yield Pressure 14,520 14,520 psi Minimum Pipe Body Yield Strength 729,000 Ib Joint Strength 707,000 Ib Compression Rating 707,000 Ib Reference Length 20,490 ft Maximum Uniaxial Bend Rating 88.9 deg/100 ft  MAKE-UP DATA Pipe USS-TALON HTQ™ RD  Make-Up Loss 5.58 in. Minimum Make-Up Torque 20,800 ft-Ib Maximum Make-Up Torque 23,800 ft-Ib	Critical Area	6.630	6.425	sq. in.	
Minimum Collapse Pressure 14,540 14,540 psi Minimum Internal Yield Pressure 14,520 14,520 psi Minimum Pipe Body Yield Strength 729,000 Ib  Joint Strength 707,000 Ib  Compression Rating 707,000 Ib  Reference Length 20,490 ft  Maximum Uniaxial Bend Rating 88.9 deg/100 ft  MAKE-UP DATA Pipe USS-TALON HTQ™ RD  Make-Up Loss 5.58 in.  Minimum Make-Up Torque 20,800 ft-Ib  Maximum Make-Up Torque 23,800 ft-Ib	Joint Efficiency		96.9	%	[2
Minimum Internal Yield Pressure       14,520       14,520       psi         Minimum Pipe Body Yield Strength       729,000        Ib         Joint Strength        707,000       Ib         Compression Rating        707,000       Ib         Reference Length        20,490       ft         Maximum Uniaxial Bend Rating        88.9       deg/100 ft         MAKE-UP DATA       Pipe       USS-TALON HTQ™ RD         Make-Up Loss        5.58       in.         Minimum Make-Up Torque        20,800       ft-Ib         Maximum Make-Up Torque        23,800       ft-Ib	PERFORMANCE	Pipe	USS-TALON HTQ™ RD		
Minimum Pipe Body Yield Strength         729,000          Ib           Joint Strength          707,000         Ib           Compression Rating          707,000         Ib           Reference Length          20,490         ft           Maximum Uniaxial Bend Rating          88.9         deg/100 ft           MAKE-UP DATA         Pipe         USS-TALON HTQ™ RD           Make-Up Loss          5.58         in.           Minimum Make-Up Torque          20,800         ft-lb           Maximum Make-Up Torque          23,800         ft-lb	Minimum Collapse Pressure	14,540	14,540	psi	
Joint Strength          707,000         Ib           Compression Rating          707,000         Ib           Reference Length          20,490         ft           Maximum Uniaxial Bend Rating          88.9         deg/100 ft           MAKE-UP DATA         Pipe         USS-TALON HTQ™ RD           Make-Up Loss          5.58         in.           Minimum Make-Up Torque          20,800         ft-lb           Maximum Make-Up Torque          23,800         ft-lb	Minimum Internal Yield Pressure	14,520	14,520	psi	
Compression Rating          707,000         Ib           Reference Length          20,490         ft           Maximum Uniaxial Bend Rating          88.9         deg/100 ft           MAKE-UP DATA         Pipe         USS-TALON HTQ™ RD           Make-Up Loss          5.58         in.           Minimum Make-Up Torque          20,800         ft-lb           Maximum Make-Up Torque          23,800         ft-lb	Minimum Pipe Body Yield Strength	729,000		lb	
Reference Length Maximum Uniaxial Bend Rating        20,490       ft deg/100 ft         MAKE-UP DATA       Pipe       USS-TALON HTQ™ RD         Make-Up Loss Minimum Make-Up Torque        5.58       in.         Maximum Make-Up Torque        20,800       ft-lb         Maximum Make-Up Torque        23,800       ft-lb	Joint Strength		707,000	<b>l</b> b	
Maximum Uniaxial Bend Rating          88.9         deg/100 ft           MAKE-UP DATA         Pipe         USS-TALON HTQ™ RD           Make-Up Loss          5.58         in.           Minimum Make-Up Torque          20,800         ft-lb           Maximum Make-Up Torque          23,800         ft-lb	Compression Rating		707,000	lb	
MAKE-UP DATA         Pipe         USS-TALON HTQ™ RD           Make-Up Loss         -         5.58         in.           Minimum Make-Up Torque         -         20,800         ft-lb           Maximum Make-Up Torque         -         23,800         ft-lb	Reference Length		20,490	ft	[5
Make-Up Loss       -       5.58       in.         Minimum Make-Up Torque       -       20,800       ft-lb         Maximum Make-Up Torque       -       23,800       ft-lb	Maximum Uniaxial Bend Rating		88.9	deg/100 ft	[3
Minimum Make-Up Torque - 20,800 ft-lb  Maximum Make-Up Torque - 23,800 ft-lb	MAKE-UP DATA	Pipe	USS-TALON HTQ™ RD		
Maximum Make-Up Torque – 23,800 ft-lb	Make-Up Loss		5.58	in.	
	Minimum Make-Up Torque		20,800	ft-lb	[4
Maximum Operating Torque – 39,800 ft-lb	Maximum Make-Up Torque		23,800	ft-lb	[4
	Maximum Operating Torque		39,800	ft-lb	[4

#### **Notes**

- 1. Other than proprietary collapse and connection values, performance properties have been calculated using standard equations defined by API 5C3 and do not incorporate any additional design or safety factors. Calculations assume nominal pipe OD, nominal wall thickness, and Specified Minimum Yield Strength (SMYS).
- 2. Joint efficiencies are calculated by dividing the connection critical area by the pipe body area.
- 3. Uniaxial bend rating shown is structural only.
- 4. Torques have been calculated assuming a thread compound friction factor of 1.0 and are recommended only. Field make-up torques may require adjustment based on actual field conditions (e.g. make-up speed, temperature, thread compound, etc.).
- 5. Reference length is calculated by Joint Strength divided by Nominal Linear Weight, T&C with a 1.5 Safety factor.
- 6. Coupling must meet minimum mechanical properties of the pipe.

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**<u>Subject:</u>** Request for a Variance Allowing break Testing of the Blowout Preventer Equipment (BOPE)

XTO Energy requests a variance to ONLY test broken pressure seals on the BOPE and function test BOP when skidding a drilling rig between multiple wells on a pad.

# **Background**

Onshore Oil and Gas Order CFR Title 43 Part 3170, Drilling Operations, Sections III.A.2.i.iv.B states that the BOP test must be performed whenever any seal subject to test pressure is broken. The current interpretation of the Bureau of Land Management (BLM) requires a complete BOP test and not just a test of the affected component. CFR Title 43 Part 3170 states, "Some situation may exist either on a well-by-well basis or field-wide basis whereby it is commonly accepted practice to vary a particular minimum standard(s) established in this order. This situation can be resolved by requesting a variance...". XTO Energy feels the break testing the BOPE is such a situation. Therefore, as per CFR Title 43 Part 3170, XTO Energy submits this request for the variance.

# **Supporting Documentation**

CFR Title 43 Part 3170 became effective on December 19, 1988 and has remained the standard for regulating BLM onshore drilling operations for over 30 years. During this time there have been significant changes in drilling technology. BLM continues to use the variance request process to allow for the use of modern technology and acceptable engineering practices that have arisen since CFR Title 43 Part 3170 was originally released. The XTO Energy drilling rig fleet has many modern upgrades that allow the intact BOP stack to be moved between well slots on a multi-well pad, as well as, wellhead designs that incorporate quick connects facilitating release of the BOP from the wellhead without breaking any BOP stack components apart. These technologies have been used extensively offshore, and other regulators, API, and many operators around the world have endorsed break testing as safe and reliable.



Figure 1: Winch System attached to BOP Stack



Figure 2: BOP Winch System

American Petroleum Institute (API) standards, specification and recommended practices are considered the industry standard and are consistently utilized and referenced by the industry. CFR Title 43 Part 3170recognizes API recommended Practices (RP) 53 in its original development. API Standard 53, *Well Control Equipment Systems for Drilling Wells* (Fifth Edition, December 2018, Annex C, Table C.4) recognizes break testing as an acceptable practice. Specifically, API Standard 53, Section 5.3.7.1 states "A pressure test of the pressure containing component shall be performed following the disconnection or repair, limited to the affected component." See Table C.4 below for reference.

2	API STANDARD	53	
Tak	ole C.4—Initial Pressure Te	esting, Surface BOP Stacks	
AND THE RESIDENCE OF THE PARTY OF THE RESIDENCE OF THE RE	Pressure Test—Low	Pressure Test	-High Pressure <mark>ac</mark>
Component to be Pressure Tested	Pressure <sup>ac</sup> psig (MPa)	Change Out of Component, Elastomer, or Ring Gasket	No Change Out of Component, Elastomer, or Ring Gasket
Annular preventer <sup>b</sup>	250 to 350 (1.72 to 2.41)	RWP of annular preventer	MASP or 70% annular RWP, whichever is lower.
Fixed pipe, variable bore, blind, and BSR preventers <sup>bd</sup>	250 to 350 (1.72 to 2.41)	RWP of ram preventer or wellhead system, whichever is lower	ITP
Choke and kill line and BOP side outlet valves below ram preventers (both sides)	250 to 350 (1.72 to 2.41)	RWP of side outlet valve or wellhead system, whichever is lower	ITP
Choke manifold—upstream of chokes <sup>e</sup>	250 to 350 (1.72 to 2.41)	RWP of ram preventers or wellhead system, whichever is lower	ITP
Choke manifold—downstream of chokes <sup>e</sup>	250 to 350 (1.72 to 2.41)	RWP of valve(s), line(s), or N whichever is lower	MASP for the well program,
Kelly, kelly valves, drill pipe safety valves, IBOPs	250 to 350 (1.72 to 2.41)	MASP for the well program	
	during the evaluation period. The p	pressure shall not decrease below the	
<sup>c</sup> For pad drilling operations, moving		n the 21 days, pressure testing is req	
For surface offshore operations, the	ne ram BOPs shall be pressure tes land operations, the ram BOPs sha	ted with the ram locks engaged and all be pressure tested with the ram lo	
e Adjustable chokes are not required	The Control of the Co	testing against a closed choke is no	ot required

The Bureau of Safety and Environmental Enforcement (BSEE), Department of Interior, has also utilized the API standards, specification and best practices in the development of its offshore oil and gas regulations and incorporates them by reference within its regulations.

Break testing has been approved by the BLM in the past with other operators based on the detailed information provided in this document.

XTO Energy feels break testing and our current procedures meet the intent of CFR Title 43 Part 317 Oand often exceed it. There has been no evidence that break testing results in more components failing than seen on full BOP tests. XTO Energy's internal standards requires complete BOPE tests more often than that of CFR Title 43 Part 3170 (Every 21 days). In addition to function testing the annular, pipe rams and blind rams after

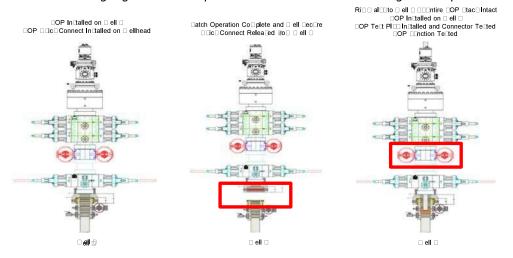
each BOP nipple up, XTO Energy performs a choke drill with the rig crew prior to drilling out every casing shoe. This is additional training for the rig crew that exceeds the requirements of the CFR Title 43 Part 3170.

# **Procedures**

- XTO Energy will use this document for our break testing plan for New Mexico Delaware basin.
   The summary below will be referenced in the APD or Sundry Notice and receive approval prior to implementing this variance.
- 2. XTO Energy will perform BOP break testing on multi-wells pads where multiple intermediate sections can be drilled and cased within the 21-day BOP test window.
  - a. A full BOP test will be conducted on the first well on the pad.
  - b. The first intermediate hole section drilled on the pad will be the deepest. All of the remaining hole sections will be the same depth or shallower.
    - i. Our Lower WC targets set the intermediate casing shoe no deeper than the Wolfcamp B.
    - ii. Our Upper WC targets set the intermediate casing shoe shallower than the Wolfcamp B.
  - c. A Full BOP test will be required if the intermediate hole section being drilled has a MASP over 5M.
  - d. A full BOP test will be required prior to drilling any production hole.
- 3. After performing a complete BOP test on the first well, the intermediate hole section will be drilled and cased, two breaks would be made on the BOP equipment.
  - a. Between the HCV valve and choke line connection
  - b. Between the BOP quick connect and the wellhead
- 4. The BOP is then lifted and removed from the wellhead by a hydraulic system.
- 5. After skidding to the next well, the BOP is moved to the wellhead by the same hydraulic system and installed.
- 6. The connections mentioned in 3a and 3b will then be reconnected.
- 7. Install test plug into the wellhead using test joint or drill pipe.
- 8. A shell test is performed against the upper pipe rams testing the two breaks.
- 9. The shell test will consist of a 250 psi low test and a high test to the value submitted in the APD or Sundry (e.g. 5,000 psi or 10,000psi).
- 10. Function test will be performed on the following components: lower pipe rams, blind rams, and annular.

- 11. For a multi-well pad the same two breaks on the BOP would be made and on the next wells and steps 4 through 10 would be repeated.
- 12. A second break test would only be done if the intermediate hole section being drilled could not be completed within the 21 day BOP test window.

Note: Picture below highlights BOP components that will be tested during batch operations



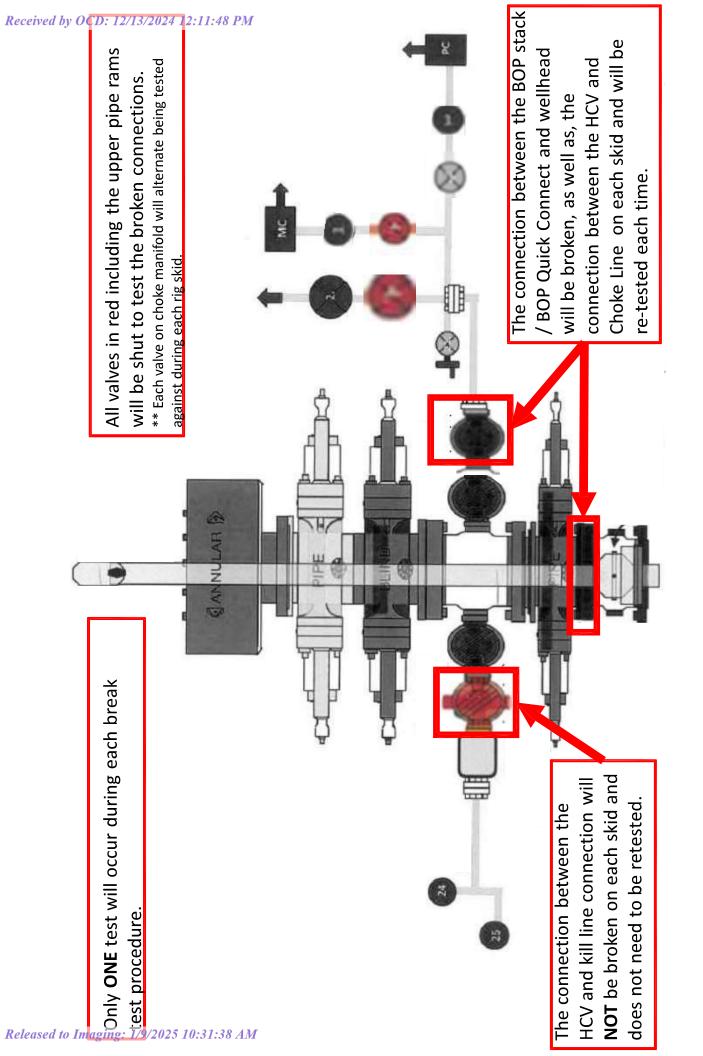
## **Summary**

A variance is requested to **ONLY** test broken pressure seals on the BOP equipment when moving from wellhead to wellhead which is in compliance with API Standard 53. API Standard 53 states, that for pad drilling operation, moving from one wellhead to another within 21 days, pressure testing is required for pressure-containing and pressure-controlling connections when the integrity of a pressure seal is broken.

The BOP will be secured by a hydraulic carrier or cradle. The BLM will be contacted if a Well Control event occurs prior to the commencement of a BOPE Break Testing operation.

Based on discussions with the BLM on February 27th 2020 and the supporting documentation submitted to the BLM, we will request permission to ONLY retest broken pressure seals if the following conditions are met:

- 1. After a full BOP test is conducted on the first well on the pad.
- 2. The first intermediate hole section drilled on the pad will be the deepest. All of the remaining hole sections will be the same depth or shallower.
- 3. Full BOP test will be required if the intermediate hole section being drilled has a MASP over 5M.
- 4. Full BOP test will be required prior to drilling the production hole.



#### **XTO Permian Operating, LLC Offline Cementing Variance Request**

XTO requests the option to cement the surface and intermediate casing strings offline as a prudent batch drilling efficiency of acreage development.

# 1. Cement Program

No changes to the cement program will take place for offline cementing.

# 2. Offline Cementing Procedure

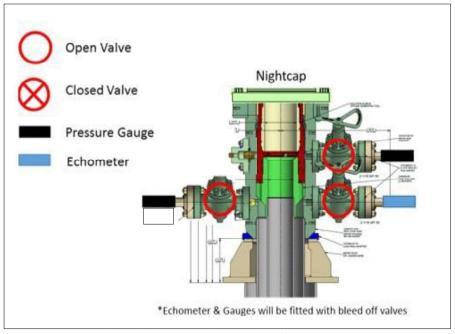
The operational sequence will be as follows. If a well control event occurs, the BLM will be contacted for approval prior to conducting offline cementing operations.

- 1. Run casing as per normal operations. While running casing, conduct negative pressure test and confirm integrity of the float equipment (float collar and shoe)
- 2. Land casing with mandrel
- 3. Fill pipe with kill weight fluid, do not circulate through floats and confirm well is static
- 4. Set annular packoff shown below and pressure test to confirm integrity of the seal. Pressure ratings of wellhead components and valves is 5,000 psi.
- 5. After confirmation of both annular barriers and internal barriers, nipple down BOP and install cap flange.
  - a. If any barrier fails to test, the BOP stack will not be nippled down until after the cement job is completed with cement 500ft above the highest formation capable of flow with kill weight mud above or after it has achieved 50-psi compressive strength if kill weight fluid cannot be verified.



Annular packoff with both external and internal seals

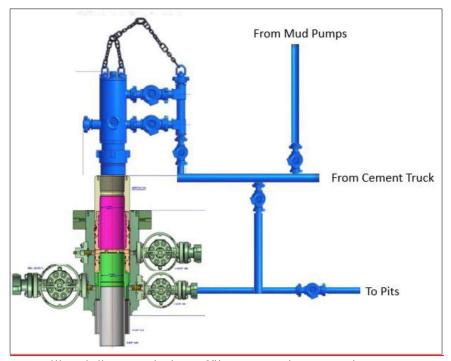
#### **XTO Permian Operating, LLC Offline Cementing Variance Request**



Wellhead diagram during skidding operations

- 6. Skid rig to next well on pad.
- 7. Confirm well is static before removing cap flange, flange will not be removed and offline cementing operations will not commence until well is under control. If well is not static, casing outlet valves will provide access to both the casing ID and annulus. Rig or third party pump truck will kill well prior to cementing or nippling up for further remediation.
  - a. Well Control Plan
    - i. The Drillers Method will be the primary well control method to regain control of the wellbore prior to cementing, if wellbore conditions do not permit the drillers method other methods of well control may be used
    - ii. Rig pumps or a 3<sup>rd</sup> party pump will be tied into the upper casing valve to pump down the casing ID
    - iii. A high pressure return line will be rigged up to lower casing valve and run to choke manifold to control annular pressure
    - iv. Once influx is circulated out of the hole, kill weight mud will be circulated
    - v. Well will be confirmed static
    - vi. Once confirmed static, cap flange will be removed to allow for offline cementing operations to commence
- 8. Install offline cement tool
- 9. Rig up cement equipment

# XTO Permian Operating, LLC Offline Cementing Variance Request



Wellhead diagram during offline cementing operations

- 10. Circulate bottoms up with cement truck
  - a. If gas is present on bottoms up, well will be shut in and returns rerouted through gas buster to handle entrained gas
  - b. Max anticipated time before circulating with cement truck is 6 hrs
- 11. Perform cement job taking returns from the annulus wellhead valve
- 12. Confirm well is static and floats are holding after cement job
- 13. Remove cement equipment, offline cement tools and install night cap with pressure gauge for monitoring.

XTO respectfully requests approval to utilize a spudder rig to pre-set surface casing.

#### Description of Operations:

- Spudder rig will move in to drill the surface hole and pre-set surface casing on the well.
  - a. After drilling the surface hole section, the spudder rig will run casing and cement following all of the applicable rules and regulations (OnShore Order 2, all COAs and NMOCD regulations).
  - The spudder rig will utilize fresh water-based mud to drill the surface hole to TD.
     Solids control will be handled entirely on a closed loop basis. No earth pits will be used.
- 2. The wellhead will be installed and tested as soon as the surface casing is cut off and WOC time has been reached.
- 3. A blind flange at the same pressure rating as the wellhead will be installed to seal the wellbore. Pressure will be monitored with needle valves installed on two wing valves.
  - a. A means for intervention will be maintained while the drilling rig is not over the well.
- 4. Spudder rig operations are expected to take 2-3 days per well on the pad.
- 5. The BLM will be contacted and notified 24 hours prior to commencing spudder rig operations.
- 6. Drilling Operations will begin with a larger rig and a BOP stack equal to or greater than the pressure rating that was permitted will be nippled up and tested on the wellhead before drilling operations resume on each well.
  - a. The larger rig will move back onto the location within 90 days from the point at which the wells are secured and the spudder rig is moved off location.
  - b. The BLM will be notified 24 hours before the larger rig moves back on the pre-set locations
- 7. XTO will have supervision on the rig to ensure compliance with all BLM and NMOCD regulations and to oversee operations.
- 8. Once the rig is removed, XTO will secure the wellhead area by placing a guard rail around the cellar area.



**GATES ENGINEERING & SERVICES NORTH AMERICA** 

7603 Prairie Oak Dr.

Houston, TX. 77086

PHONE: +1 (281) 602-4100

FAX: +1 (281) 602-4147

EMAIL: gesna.quality@gates.com

WEB: www.gates.com/oilandgas

NEW CHOKE HOSE

INSTRUED 02-10-2024

## CERTIFICATE OF CONFORMANCE

This is to verify that the items detailed below meet the requirements of the Customer's Purchase Order referenced herein, and are in Conformance with applicable specifications, and that Records of Required Tests are on file and subject to examination. The following items were inspected and hydrostatically tested at **Gates Engineering & Services North America** facilities in Houston, TX, USA.

CUSTOMER:

NABORS DRILLING TECHNOLOGIES USA DBA NABORS DRILLING USA

CUSTOMER P.O.#:

15582803 (TAG NABORS PO #15582803 SN 74621 ASSET 66-1531)

CUSTOMER P/N:

IMR RETEST SN 74621 ASSET #66-1531

PART DESCRIPTION:

RETEST OF CUSTOMER 3" X 45 FT 16C CHOKE & KILL HOSE ASSEMBLY C/W 4 1/16" 10K

FLANGES

SALES ORDER #:

529480

QUANTITY:

1

SERIAL #:

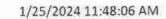
74621 H3-012524-1

SIGNATURE: F. CUSTUS S

TITLE: QUALITY ASSURANCE

DATE: 1/25/2024

#### H3-15/16





### **TEST REPORT**

CUSTOMER

Company:

Nabors Industries Inc.

TEST OBJECT

Serial number: H3-012524-1

Lot number:

Production description:

74621/66-1531

Description:

74621/66-1531

Sales order #: Customer reference: 529480 FG1213

Hose ID:

3" 16C CK

Part number:

**TEST INFORMATION** 

Test procedure:

GTS-04-053

15000.00 psi

Fitting 1: Part number: 3.0 x 4-1/16 10K

Test pressure: Test pressure hold:

3600.00

sec

Description:

Work pressure:

10000.00

psi

Fitting 2:

3.0 x 4-1/16 10K

Work pressure hold: Length difference: Length difference: 900.00 0.00 0.00 sec % inch

Part number: Description:

Visual check:

Pressure test result:

PASS

Length measurement result:

Length:

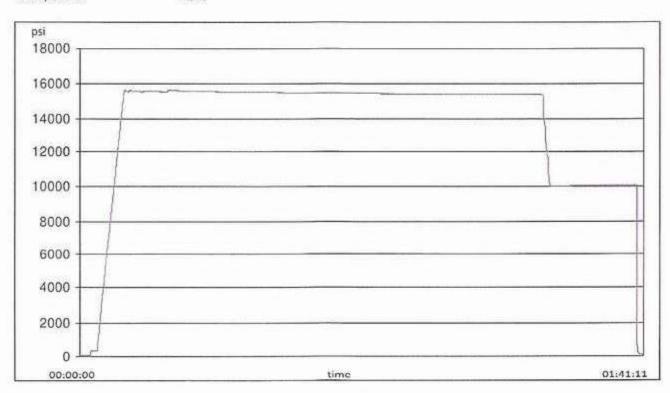
45

feet

m . . . . 14

Test operator:

Travis





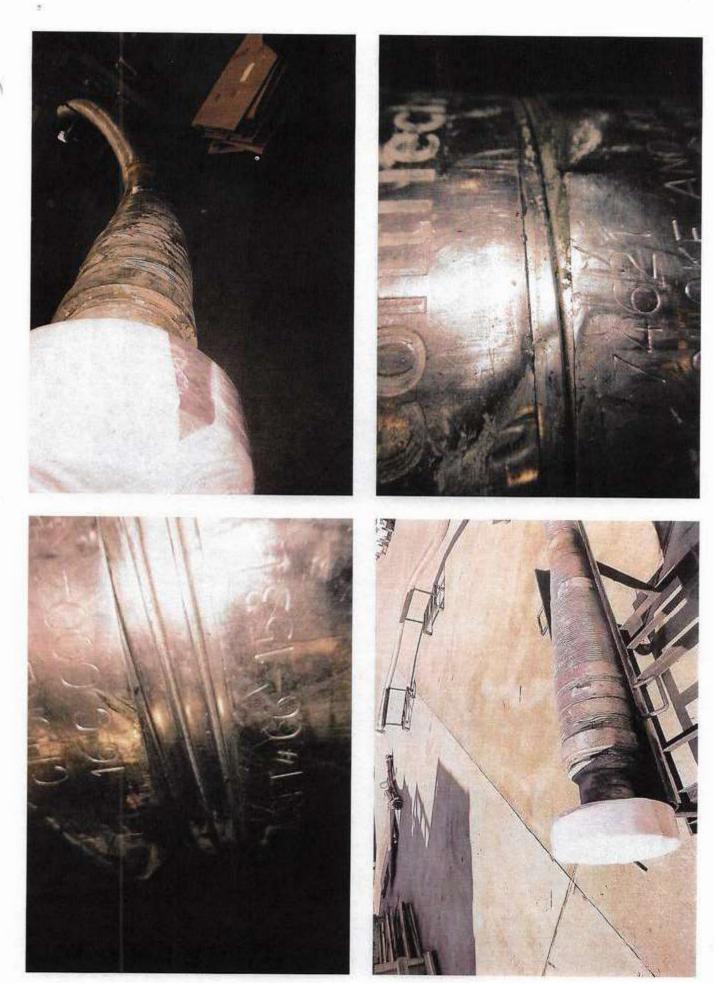
H3-15/16

1/25/2024 11:48:06 AM

## **TEST REPORT**

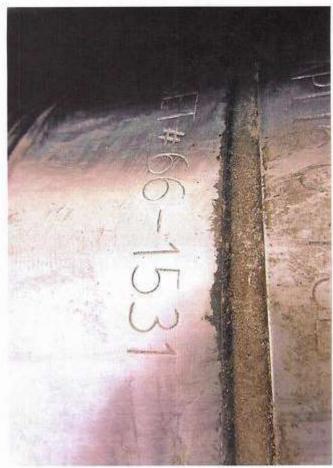
#### **GAUGE TRACEABILITY**

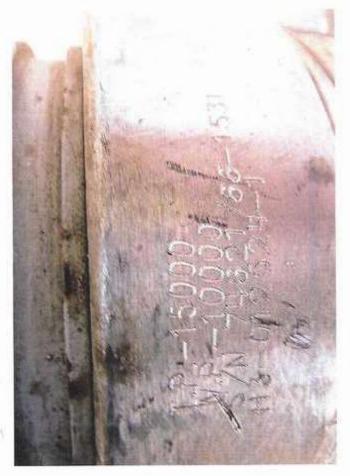
Description	Serial number	Calibration date	Calibration due date
S-25-A-W	110D3PHO	2023-06-06	2024-06-06
S-25-A-W	110IQWDG	2023-05-16	2024-05-16
Comment			
Comment			



Released to Imaging: 1/9/2025 10:31:38 AM

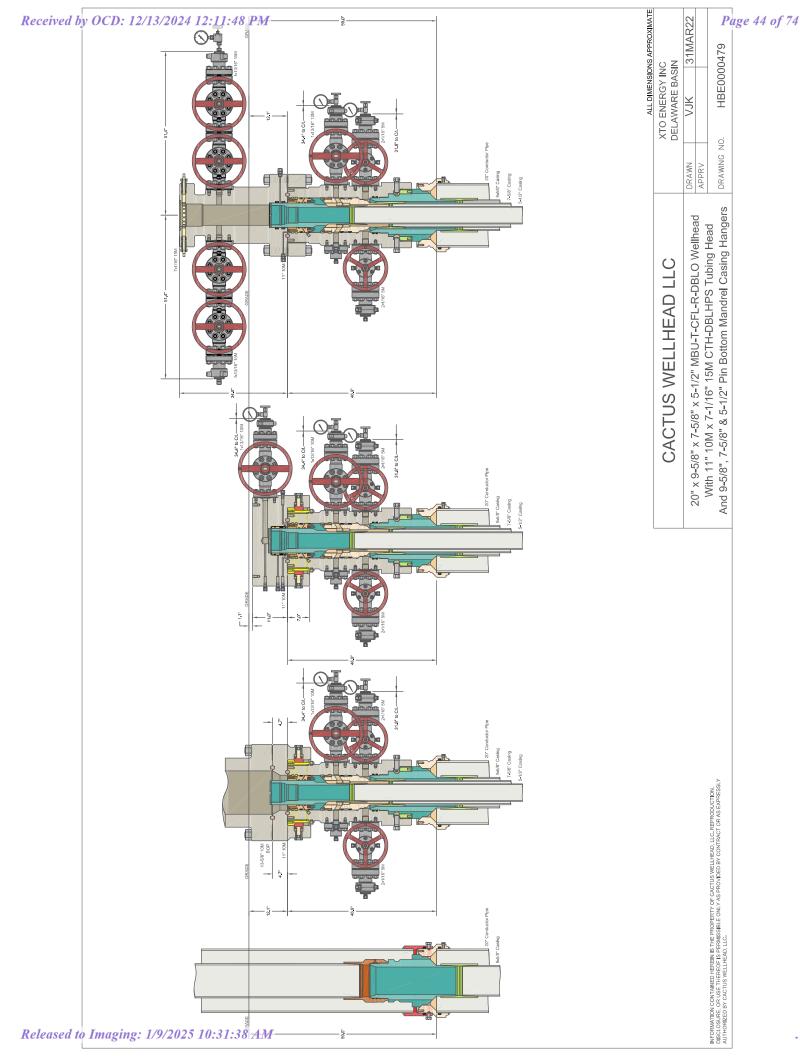








Released to Imaging: 1/9/2025 10:31:38 AM





## **XTO Energy**

EDDY COUNTY, NM (NAD-27) POKER LAKE UNIT 30 BS 209H

Wellbore #1

**Plan: PERMIT** 

## **Standard Planning Report**

23 June, 2023



Project: EDDY COUNTY, NM (NAD-27) Site: POKER LAKE UNIT 30 BS Well: 209H Wellbore: Wellbore #1 Design: PERMIT

PROJECT DETAILS: EDDY COUNTY, NM (NAD-27)

Geodetic System: US State Plane 1927 (Exact solution)
Datum: NAD 1927 (NADCON CONUS)
Ellipsoid: Clarke 1866
Zone: New Mexico East 3001
System Datum: Mean Sea Level

West(-)/East(+) (2500 usft/in)

1250

209H FTP

-1250

--1250

-2500

-2500

-1250

209H SHL

#### WELL DETAILS: 209H

			Rig Name: RKB = 30' @ 3409.	TBD 00usft (TBD)	
+N/-S 0.00	+E/-W 0.00	Northing 401106.38	Ground Level: Easting 659249.96	3379.00 Latittude 32.1017134	Longitude -103.8190495

#### SECTION DETAILS

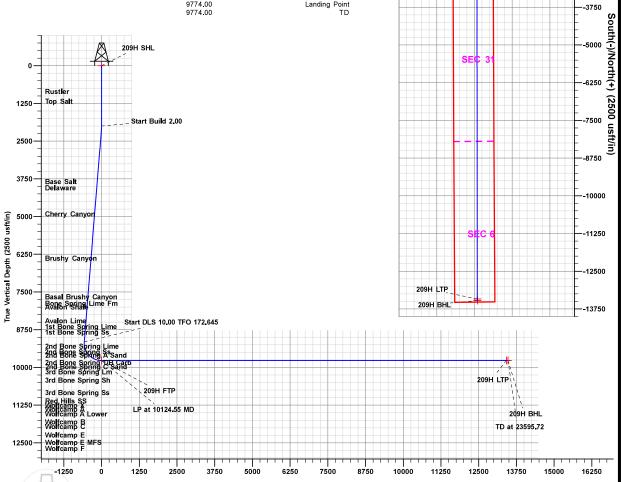
Sec	MD	Inc	Azi	TVD	+N/-S	+E/-W	Dleg	TFace	VSect	Target
1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.000	0.00	-
2	2000.00	0.00	0.00	2000.00	0.00	0.00	0.00	0.000	0.00	
3	2234.07	4.68	7.26	2233.80	9.48	1.21	2.00	7.256	-9.48	
4	9178.12	4.68	7.26	9154.70	571.67	72.79	0.00	0.000	-571.58	
5	10124.55	90.00	179.93	9774.00	0.60	80.00	10.00	172.645	-0.50	209H FTP
6	23545.72	90.00	179.93	9774.00	-13420.56	97.46	0.00	0.000	13420.67	209H LTP
7	23595.72	90.00	179.93	9774.00	-13470.56	97.53	0.00	0.000	13470.67	209H BHL

#### DESIGN TARGET DETAILS

Name 209H SHL	TVD 0.00	+N/-S 0.00	+E/-W 0.00	Northing 401106.38	Easting 659249.96	Latitude 32.1017134	Longitude -103.8190495
209H BHL	9774.00	13470.56	97.53	387635.82	659347.49	32.0646823	-103.8189420
209H FTP	9774.00	0.60	80.00	401106.98	659329.96	32.1017140	-103.8187911
209H LTP	9774.00	13420.56	97.23	387685.82	659347.19	32.0648197	-103.8189422

#### FORMATION TOP DETAILS

TVDPath	Formation
975.00	Rustler
1302.00	Top Salt
3963.00	Base Salt
4173.00	Delaware
5034.00	Cherry Canyon
6505.00	Brushy Canyon
7782.00	Basal Brushy Canyon
7999.00	Bone Spring Lime Fm
8121.00	Avalon Shale
8577.00	Avalon Lime
8765.00	1st Bone Spring Lime
8951.00	1st Bone Spring Ss
9420.00	2nd Bone Spring Lime
9674.00	2nd Bone Spring Ss
9774.00	Landing Point
9774.00	TD



District I
1625 N. French Dr., Hobbs, NM 88240
Phone: (575) 393-6161 Fax: (575) 393-0720
District II
811 S. First St., Artesia, NM 88210
Phone: (575) 748-1283 Fax: (575) 748-9720
District III

| 1000 Rio Brazos Road, Aztec, NM 87410 | Phone: (505) 334-6178 Fax: (505) 334-6170 | <u>District IV</u> | 1220 S. St. Francis Dr., Santa Fe, NM 87505

1220 S. St. Francis Dr., Santa Fe, NM 87505 Phone: (505) 476-3460 Fax: (505) 476-3462

## State of New Mexico Energy, Minerals & Natural Resources Department OIL CONSERVATION DIVISION 1220 South St. Francis Dr. Santa Fe, NM 87505

Form C-102
Revised August 1, 2011
Submit one copy to appropriate
District Office

☐ AMENDED REPORT

#### WELL LOCATION AND ACREAGE DEDICATION PLAT

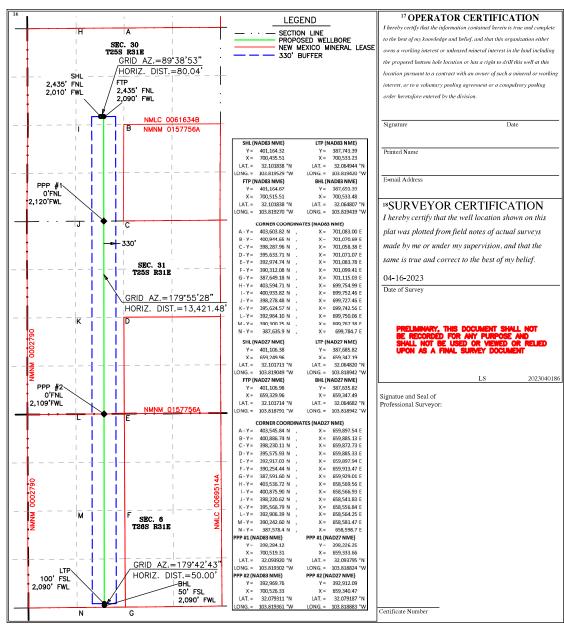
<sup>1</sup> API Numbe	er	<sup>2</sup> Pool Code	<sup>3</sup> Pool Name	
4 Property Code		<sup>5</sup> Pr	operty Name	<sup>6</sup> Well Number
		POKER L	AKE UNIT 30 BD	209H
7 OGRID No.		8 OI	perator Name	9 Elevation
373075		XTO PERMIA	AN OPERATING, LLC	3,379'

#### <sup>10</sup> Surface Location

UL or lot no.	Section	Township	Range	Lot Idn	Feet from the	North/South line	Feet from the	East/West line	County
F	30	25S	31E		2,435	NORTH	2,010	WEST	EDDY
			11 Bot	ttom Hol	e Location If	Different Fron	n Surface		

UL or lot no.	Section	Township	Range	Lot Idn	Feet from the	North/South line	Feet from the	East/West line	County
N	6	26S	31E		50	SOUTH	2,090	WEST	EDDY
12 Dedicated Acre	s 13 Joint o	· Infill 14 C	onsolidation	Code 15 Or	der No.				

No allowable will be assigned to this completion until all interests have been consolidated or a non-standard unit has been approved by the division.





Database: EDM 5000.1.13 Single User Db

Company: XTO Energy

Project: EDDY COUNTY, NM (NAD-27)
Site: POKER LAKE UNIT 30 BS

Well: 209H
Wellbore: Wellbore #1
Design: PERMIT

Local Co-ordinate Reference:

TVD Reference: MD Reference: North Reference:

Survey Calculation Method:

Well 209H

RKB = 30' @ 3409.00usft (TBD) RKB = 30' @ 3409.00usft (TBD)

Grid

Minimum Curvature

Project EDDY COUNTY, NM (NAD-27)

Map System: US State Plane 1927 (Exact solution)

Geo Datum: NAD 1927 (NADCON CONUS)

Map Zone: New Mexico East 3001

System Datum: Mean Sea Level

Site POKER LAKE UNIT 30 BS

401,221.20 usft Site Position: Northing: 32.1020486 Latitude: From: Мар Easting: 657,754.30 usft Longitude: -103.8238776 **Position Uncertainty:** 0.00 usft Slot Radius: 13-3/16 " **Grid Convergence:** 0.271

Well 209H

 Well Position
 +N/-S
 -114.82 usft
 Northing:
 401,106.38 usft
 Latitude:
 32.1017134

+E/-W 1,495.66 usft Easting: 659,249.96 usft Longitude: -103.8190495

Position Uncertainty0.00 usftWellhead Elevation:0.00 usftGround Level:3,379.00 usft

Wellbore Wellbore #1

 Magnetics
 Model Name
 Sample Date
 Declination (°)
 Dip Angle (°)
 Field Strength (nT)

 IGRF2020
 06/23/23
 6.413
 59.685
 47,186

Design PERMIT

**Audit Notes:** 

Version: Phase: PLAN Tie On Depth: 0.00

 Vertical Section:
 Depth From (TVD) (usft)
 +N/-S (usft)
 +E/-W (usft)
 Direction (°)

 0.00
 0.00
 0.00
 179.93

Plan Section	s									
Measured Depth (usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)	TFO (°)	Target
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.000	
2,000.00	0.00	0.00	2,000.00	0.00	0.00	0.00	0.00	0.00	0.000	
2,234.07	4.68	7.26	2,233.80	9.48	1.21	2.00	2.00	0.00	7.256	
9,178.12	4.68	7.26	9,154.70	571.67	72.79	0.00	0.00	0.00	0.000	
10,124.55	90.00	179.93	9,774.00	0.60	80.00	10.00	9.01	18.24	172.645	209H FTP
23,545.72	90.00	179.93	9,774.00	-13,420.56	97.46	0.00	0.00	0.00	0.000	209H LTP
23,595.72	90.00	179.93	9,774.00	-13,470.56	97.53	0.00	0.00	0.00	0.000	209H BHL



EDM 5000.1.13 Single User Db Database: Company:

XTO Energy

EDDY COUNTY, NM (NAD-27) Project: POKER LAKE UNIT 30 BS Site:

Well: 209H Wellbore: Wellbore #1 PERMIT Design:

Local Co-ordinate Reference:

TVD Reference: MD Reference: North Reference:

**Survey Calculation Method:** 

Well 209H

RKB = 30' @ 3409.00usft (TBD)

RKB = 30' @ 3409.00usft (TBD)

Desig	J. 1.	PERMIT								
Plani	ned Survey									
	Measured Depth (usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Vertical Section (usft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)
	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	209H SHL 100.00 200.00 300.00 400.00	0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00	100.00 200.00 300.00 400.00	0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00
	500.00 600.00 700.00 800.00 900.00	0.00 0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00 0.00	500.00 600.00 700.00 800.00 900.00	0.00 0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00 0.00
	975.00	0.00	0.00	975.00	0.00	0.00	0.00	0.00	0.00	0.00
	1,000.00 1,100.00 1,200.00 1,300.00	0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00	1,000.00 1,100.00 1,200.00 1,300.00	0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00
	1,302.00	0.00	0.00	1,302.00	0.00	0.00	0.00	0.00	0.00	0.00
	Top Salt 1,400.00 1,500.00 1,600.00 1,700.00	0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00	1,400.00 1,500.00 1,600.00 1,700.00	0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00
	1,800.00 1,900.00 2,000.00 2,100.00 2,200.00	0.00 0.00 0.00 2.00 4.00	0.00 0.00 0.00 7.26 7.26	1,800.00 1,900.00 2,000.00 2,099.98 2,199.84	0.00 0.00 0.00 1.73 6.92	0.00 0.00 0.00 0.22 0.88	0.00 0.00 0.00 -1.73 -6.92	0.00 0.00 0.00 2.00 2.00	0.00 0.00 0.00 2.00 2.00	0.00 0.00 0.00 0.00 0.00
	2,234.07 2,300.00 2,400.00 2,500.00 2,600.00	4.68 4.68 4.68 4.68 4.68	7.26 7.26 7.26 7.26 7.26	2,233.80 2,299.52 2,399.19 2,498.85 2,598.52	9.48 14.82 22.91 31.01 39.11	1.21 1.89 2.92 3.95 4.98	-9.48 -14.82 -22.91 -31.01 -39.10	2.00 0.00 0.00 0.00 0.00	2.00 0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00 0.00
	2,700.00 2,800.00 2,900.00 3,000.00 3,100.00	4.68 4.68 4.68 4.68 4.68	7.26 7.26 7.26 7.26 7.26	2,698.19 2,797.85 2,897.52 2,997.18 3,096.85	47.20 55.30 63.39 71.49 79.59	6.01 7.04 8.07 9.10 10.13	-47.19 -55.29 -63.38 -71.48 -79.57	0.00 0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00 0.00
	3,200.00 3,300.00 3,400.00 3,500.00 3,600.00	4.68 4.68 4.68 4.68 4.68	7.26 7.26 7.26 7.26 7.26	3,196.52 3,296.18 3,395.85 3,495.52 3,595.18	87.68 95.78 103.87 111.97 120.07	11.16 12.19 13.23 14.26 15.29	-87.67 -95.76 -103.86 -111.95 -120.05	0.00 0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00 0.00
	3,700.00 3,800.00 3,900.00 3,969.05 <b>Base Salt</b>	4.68 4.68 4.68 4.68	7.26 7.26 7.26 7.26	3,694.85 3,794.52 3,894.18 3,963.00	128.16 136.26 144.35 149.94	16.32 17.35 18.38 19.09	-128.14 -136.24 -144.33 -149.92	0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00
	4,000.00	4.68	7.26	3,993.85	152.45	19.41	-152.43	0.00	0.00	0.00
	4,100.00 4,179.75	4.68 4.68	7.26 7.26	4,093.52 4,173.00	160.55 167.00	20.44 21.26	-160.52 -166.98	0.00 0.00	0.00 0.00	0.00 0.00
	<b>Delaware</b> 4,200.00 4,300.00	4.68 4.68	7.26 7.26	4,193.18 4,292.85	168.64 176.74	21.47 22.50	-168.62 -176.71	0.00 0.00	0.00 0.00	0.00 0.00



EDM 5000.1.13 Single User Db Database: Company:

XTO Energy

EDDY COUNTY, NM (NAD-27) Project: POKER LAKE UNIT 30 BS Site:

Well: 209H Wellbore: Wellbore #1 PERMIT Design:

Local Co-ordinate Reference:

TVD Reference: MD Reference: North Reference:

**Survey Calculation Method:** 

Well 209H

RKB = 30' @ 3409.00usft (TBD) RKB = 30' @ 3409.00usft (TBD)

Design.		FLIXIVIII								
Planned	l Survey									
N	leasured Depth (usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Vertical Section (usft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)
	4,400.00	4.68	7.26	4,392.51	184.83	23.53	-184.80	0.00	0.00	0.00
	4,500.00	4.68	7.26	4,492.18	192.93	24.56	-192.90	0.00	0.00	0.00
	4,600.00	4.68	7.26	4,591.85	201.03	25.60	-200.99	0.00	0.00	0.00
	4,700.00	4.68	7.26	4,691.51	209.12	26.63	-209.09	0.00	0.00	0.00
	4,800.00	4.68	7.26	4,791.18	217.22	27.66	-217.18	0.00	0.00	0.00
	4,900.00	4.68	7.26	4,890.85	225.31	28.69	-225.28	0.00	0.00	0.00
	5,000.00	4.68	7.26	4,990.51	233.41	29.72	-233.37	0.00	0.00	0.00
	5,043.63	4.68	7.26	5,034.00	236.94	30.17	-236.90	0.00	0.00	0.00
	Cherry Car			•						
	5,100.00	4.68	7.26	5,090.18	241.51	30.75	-241.47	0.00	0.00	0.00
	5,200.00	4.68	7.26	5,189.85	249.60	31.78	-249.56	0.00	0.00	0.00
	5,300.00	4.68	7.26	5,289.51	257.70	32.81	-257.66	0.00	0.00	0.00
	5,400.00	4.68	7.26	5,389.18	265.79	33.84	-265.75	0.00	0.00	0.00
	5,500.00	4.68	7.26	5,488.84	273.89	34.87	-273.85	0.00	0.00	0.00
	5,600.00	4.68	7.26	5,588.51	281.99	35.90	-281.94	0.00	0.00	0.00
	5,700.00	4.68	7.26	5,688.18	290.08	36.93	-290.04	0.00	0.00	0.00
	5,800.00	4.68	7.26	5,787.84	298.18	37.96	-298.13	0.00	0.00	0.00
	5,900.00	4.68	7.26	5,887.51	306.27	39.00	-306.23	0.00	0.00	0.00
	6,000.00	4.68	7.26	5,987.18	314.37	40.03	-314.32	0.00	0.00	0.00
	6,100.00	4.68	7.26	6,086.84	322.46	41.06	-322.41	0.00	0.00	0.00
	6,200.00	4.68	7.26	6,186.51	330.56	42.09	-330.51	0.00	0.00	0.00
	6,300.00	4.68	7.26	6,286.18	338.66	43.12	-338.60	0.00	0.00	0.00
	6,400.00	4.68	7.26	6,385.84	346.75	44.15	-346.70	0.00	0.00	0.00
	6,500.00	4.68	7.26	6,485.51	354.85	45.18	-354.79	0.00	0.00	0.00
	6,519.56	4.68	7.26	6,505.00	356.43	45.38	-356.38	0.00	0.00	0.00
	<b>Brushy Car</b>									
	6,600.00	4.68	7.26	6,585.18	362.94	46.21	-362.89	0.00	0.00	0.00
	6,700.00	4.68	7.26	6,684.84	371.04	47.24	-370.98	0.00	0.00	0.00
	6,800.00	4.68	7.26	6,784.51	379.14	48.27	-379.08	0.00	0.00	0.00
	6,900.00	4.68	7.26	6,884.17	387.23	49.30	-387.17	0.00	0.00	0.00
	7,000.00	4.68	7.26	6,983.84	395.33	50.33	-395.27	0.00	0.00	0.00
	7,100.00	4.68	7.26	7,083.51	403.42	51.37	-403.36	0.00	0.00	0.00
	7,200.00	4.68	7.26	7,183.17	411.52	52.40	-411.46	0.00	0.00	0.00
	7,300.00	4.68	7.26	7,282.84	419.62	53.43	-419.55	0.00	0.00	0.00
	7,400.00	4.68	7.26	7,382.51	427.71	54.46	-427.65	0.00	0.00	0.00
	7,500.00	4.68	7.26	7,482.17	435.81	55.49	-435.74	0.00	0.00	0.00
	7,600.00	4.68	7.26	7,581.84	443.90	56.52	-443.84	0.00	0.00	0.00
	7,700.00	4.68	7.26	7,681.51	452.00	57.55	-451.93	0.00	0.00	0.00
	7,800.00	4.68	7.26	7,781.17	460.10	58.58	-460.02	0.00	0.00	0.00
	7,800.83	4.68	7.26	7,782.00	460.16	58.59	-460.09	0.00	0.00	0.00
		hy Canyon		7.000.07	400.40		400.45	2.25	2.25	0.00
	7,900.00	4.68	7.26	7,880.84	468.19	59.61	-468.12	0.00	0.00	0.00
	8,000.00	4.68	7.26	7,980.51	476.29	60.64	-476.21	0.00	0.00	0.00
	8,018.56	4.68	7.26	7,999.00	477.79	60.83	-477.72	0.00	0.00	0.00
	Bone Sprin	ng Lime Fm								
	8,100.00	4.68	7.26	8,080.17	484.38	61.67	-484.31	0.00	0.00	0.00
	8,140.97	4.68	7.26	8,121.00	487.70	62.10	-487.62	0.00	0.00	0.00
	Avalon Sha 8,200.00 8,300.00 8,400.00	4.68 4.68 4.68	7.26 7.26 7.26	8,179.84 8,279.50 8,379.17	492.48 500.58 508.67	62.70 63.73 64.77	-492.40 -500.50 -508.59	0.00 0.00 0.00	0.00 0.00 0.00	0.00 0.00 0.00
	8,500.00	4.68	7.26	8,478.84	516.77	65.80	-516.69	0.00	0.00	0.00
	8,598.49	4.68	7.26	8,577.00	524.74	66.81	-524.66	0.00	0.00	0.00



EDM 5000.1.13 Single User Db Database:

XTO Energy

Company: EDDY COUNTY, NM (NAD-27) Project: POKER LAKE UNIT 30 BS Site:

Well: 209H Wellbore: Wellbore #1 PERMIT Design:

Local Co-ordinate Reference:

TVD Reference: MD Reference: North Reference:

**Survey Calculation Method:** 

Well 209H

RKB = 30' @ 3409.00usft (TBD)

RKB = 30' @ 3409.00usft (TBD)

Design.	FERIVITI								
Planned Survey									
Measured Depth I (usft)	nclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Vertical Section (usft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)
Avalon Lime									
8,600.00	4.68	7.26	8,578.50	524.86	66.83	-524.78	0.00	0.00	0.00
8,700.00	4.68	7.26	8,678.17	532.96	67.86	-532.88	0.00	0.00	0.00
8,787.12	4.68	7.26	8,765.00	540.01	68.76	-539.93	0.00	0.00	0.00
1st Bone Spr	ing Lime								
8,800.00	4.68	7.26	8,777.84	541.06	68.89	-540.97	0.00	0.00	0.00
8,900.00	4.68	7.26	8,877.50	549.15	69.92	-549.07	0.00	0.00	0.00
8,973.74	4.68	7.26	8,951.00	555.12	70.68	-555.04	0.00	0.00	0.00
1st Bone Spi 9,000.00	ang Ss 4.68	7.26	8,977.17	557.25	70.95	557 16	0.00	0.00	0.00
9,100.00	4.68 4.68	7.26 7.26	9,076.84	565.34	70.95 71.98	-557.16 -565.26	0.00	0.00	0.00
9,178.12	4.68	7.26	9,154.70	571.67	72.79	-571.58	0.00	0.00	0.00
9,200.00	2.53	13.62	9,176.53	573.02	73.01	-572.93	10.00	-9.85	29.09
9,250.00	2.61	166.70	9,226.51	572.98	73.53	-572.89	10.00	0.17	306.16
9,300.00	7.57	175.42	9,276.30	568.59	74.06	-568.50	10.00	9.91	17.44
9,350.00	12.56	177.24	9,325.51	559.87	74.59	-559.78	10.00	9.98	3.64
9,400.00	17.55	178.03	9,373.78	546.90	75.11	-546.81	10.00	9.99	1.59
9,449.20	22.47	178.48	9,420.00	530.07	75.61	-529.98	10.00	10.00	0.91
2nd Bone Sp		170.40	3,420.00	330.07	70.01	323.30	10.00	10.00	0.51
9,450.00	22.55	178.48	9,420.74	529.77	75.62	-529.67	10.00	10.00	0.71
9,500.00	27.55	178.78	9,466.02	508.61	76.12	-508.51	10.00	10.00	0.59
9,550.00	32.55	178.99	9,509.28	483.58	76.61	-483.49	10.00	10.00	0.42
9,600.00	37.55	179.15	9,550.20	454.88	77.07	-454.79	10.00	10.00	0.32
9,650.00	42.55	179.27	9,588.47	422.72	77.51	-422.63	10.00	10.00	0.25
9,700.00	47.55	179.38	9,623.78	387.35	77.93	-387.26	10.00	10.00	0.21
9,750.00	52.55	179.47	9,655.88	349.04	78.31	-348.94	10.00	10.00	0.18
9,780.90	55.64	179.52	9,674.00	324.01	78.53	-323.92	10.00	10.00	0.16
2nd Bone Sp	ring Ss								
9,800.00	57.55	179.54	9,684.52	308.07	78.66	-307.97	10.00	10.00	0.15
9,850.00	62.55	179.61	9,709.47	264.76	78.98	-264.67	10.00	10.00	0.14
9,900.00	67.55	179.68	9,730.56	219.45	79.26	-219.35	10.00	10.00	0.13
9,950.00	72.55	179.74	9,747.62	172.46	79.50	-172.37	10.00	10.00	0.12
10,000.00	77.55	179.79	9,760.52	124.17	79.70	-124.08	10.00	10.00	0.11
10,050.00	82.55	179.85	9,769.16	74.94	79.85	-74.84	10.00	10.00	0.11
10,100.00	87.54	179.90	9,773.47	25.14	79.96	-25.05	10.00	10.00	0.11
10,124.55	90.00	179.93	9,774.00	0.60	80.00	-0.50	10.00	10.00	0.10
TD - Landing	Point - 209l								
10,200.00	90.00	179.93	9,774.00	-74.85	80.10	74.95	0.00	0.00	0.00
10,300.00	90.00	179.93	9,774.00	-174.85	80.23	174.95	0.00	0.00	0.00
10,400.00	90.00	179.93	9,774.00	-274.85	80.36	274.95	0.00	0.00	0.00
10,500.00	90.00	179.93	9,774.00	-374.85	80.49	374.95	0.00	0.00	0.00
10,600.00	90.00	179.93	9,774.00	-474.85	80.62	474.95	0.00	0.00	0.00
10,700.00	90.00	179.93	9,774.00	-574.85	80.75	574.95	0.00	0.00	0.00
10,800.00	90.00	179.93	9,774.00	-674.85	80.88	674.95	0.00	0.00	0.00
10,900.00	90.00	179.93	9,774.00	-774.85	81.01	774.95	0.00	0.00	0.00
11,000.00	90.00	179.93	9,774.00	-874.85	81.14	874.95	0.00	0.00	0.00
11,100.00	90.00	179.93	9,774.00	-974.85	81.27	974.95	0.00	0.00	0.00
11,200.00	90.00	179.93	9,774.00	-1,074.85	81.40	1,074.95	0.00	0.00	0.00
11,300.00	90.00	179.93	9,774.00	-1,174.85	81.53	1,174.95	0.00	0.00	0.00
11,400.00	90.00	179.93	9,774.00	-1,274.85	81.66	1,274.95	0.00	0.00	0.00
11,500.00	90.00	179.93	9,774.00	-1,374.85	81.79	1,374.95	0.00	0.00	0.00
11,600.00	90.00	179.93	9,774.00	-1,474.85	81.92	1,474.95	0.00	0.00	0.00
11,700.00	90.00	179.93	9,774.00	-1,574.85	82.05	1,574.95	0.00	0.00	0.00



EDM 5000.1.13 Single User Db Database: Company:

XTO Energy

EDDY COUNTY, NM (NAD-27) Project: POKER LAKE UNIT 30 BS Site:

Well: 209H Wellbore: Wellbore #1 PERMIT Design:

Local Co-ordinate Reference:

TVD Reference: MD Reference: North Reference:

**Survey Calculation Method:** 

Well 209H

RKB = 30' @ 3409.00usft (TBD)

RKB = 30' @ 3409.00usft (TBD)

Design.	FLIXIVIII								
Planned Survey									
Measured Depth (usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Vertical Section (usft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)
11,800.00	90.00	179.93	9,774.00	-1,674.85	82.18	1,674.95	0.00	0.00	0.00
11,900.00	90.00	179.93	9,774.00	-1,774.85	82.31	1,774.95	0.00	0.00	0.00
12,000.00	90.00	179.93	9,774.00	-1,874.85	82.44	1,874.95	0.00	0.00	0.00
12,100.00	90.00	179.93	9,774.00	-1,974.85	82.57	1,974.95	0.00	0.00	0.00
12,200.00	90.00	179.93	9,774.00	-2,074.85	82.70	2,074.95	0.00	0.00	0.00
12,300.00	90.00	179.93	9,774.00	-2,174.85	82.83	2,174.95	0.00	0.00	0.00
12,400.00	90.00	179.93	9,774.00	-2,274.85	82.96	2,274.95	0.00	0.00	0.00
12,500.00	90.00	179.93	9,774.00	-2,374.85	83.09	2,374.95	0.00	0.00	0.00
12,600.00	90.00	179.93	9,774.00	-2,474.85	83.22	2,474.95	0.00	0.00	0.00
12,700.00	90.00	179.93	9,774.00	-2,574.85	83.35	2,574.95	0.00	0.00	0.00
12,800.00	90.00	179.93	9,774.00	-2,674.85	83.48	2,674.95	0.00	0.00	0.00
12,900.00	90.00	179.93	9,774.00	-2,774.85	83.61	2,774.95	0.00	0.00	0.00
13,000.00	90.00	179.93	9,774.00	-2,874.85	83.74	2,874.95	0.00	0.00	0.00
13,100.00	90.00	179.93	9,774.00	-2,974.85	83.87	2,974.95	0.00	0.00	0.00
13,200.00	90.00	179.93	9,774.00	-3,074.85	84.00	3,074.95	0.00	0.00	0.00
13,300.00	90.00	179.93	9,774.00	-3,174.85	84.13	3,174.95	0.00	0.00	0.00
13,400.00	90.00	179.93	9,774.00	-3,274.85	84.26	3,274.95	0.00	0.00	0.00
13,500.00	90.00	179.93	9,774.00	-3,374.85	84.39	3,374.95	0.00	0.00	0.00
13,600.00	90.00	179.93	9,774.00	-3,474.85	84.52	3,474.95	0.00	0.00	0.00
13,700.00	90.00	179.93	9,774.00	-3,574.84	84.65	3,574.95	0.00	0.00	0.00
13,800.00	90.00	179.93	9,774.00	-3,674.84	84.78	3,674.95	0.00	0.00	0.00
13,900.00	90.00	179.93	9,774.00	-3,774.84	84.91	3,774.95	0.00	0.00	0.00
14,000.00	90.00	179.93	9,774.00	-3,874.84	85.04	3,874.95	0.00	0.00	0.00
14,100.00	90.00	179.93	9,774.00	-3,974.84	85.17	3,974.95	0.00	0.00	0.00
14,200.00	90.00	179.93	9,774.00	-4,074.84	85.30	4,074.95	0.00	0.00	0.00
14,300.00	90.00	179.93	9,774.00	-4,174.84	85.43	4,174.95	0.00	0.00	0.00
14,400.00	90.00	179.93	9,774.00	-4,274.84	85.56	4,274.95	0.00	0.00	0.00
14,500.00	90.00	179.93	9,774.00	-4,374.84	85.69	4,374.95	0.00	0.00	0.00
14,600.00	90.00	179.93	9,774.00	-4,474.84	85.82	4,474.95	0.00	0.00	0.00
14,700.00	90.00	179.93	9,774.00	-4,574.84	85.95	4,574.95	0.00	0.00	0.00
14,800.00	90.00	179.93	9,774.00	-4,674.84	86.08	4,674.95	0.00	0.00	0.00
14,900.00	90.00	179.93	9,774.00	-4,774.84	86.21	4,774.95	0.00	0.00	0.00
15,000.00	90.00	179.93	9,774.00	-4,874.84	86.34	4,874.95	0.00	0.00	0.00
15,100.00	90.00	179.93	9,774.00	-4,974.84	86.47	4,974.95	0.00	0.00	0.00
15,200.00	90.00	179.93	9,774.00	-5,074.84	86.60	5,074.95	0.00	0.00	0.00
15,300.00	90.00	179.93	9,774.00	-5,174.84	86.73	5,174.95	0.00	0.00	0.00
15,400.00	90.00	179.93	9,774.00	-5,274.84	86.86	5,274.95	0.00	0.00	0.00
15,500.00	90.00	179.93	9,774.00	-5,374.84	87.00	5,374.95	0.00	0.00	0.00
15,600.00	90.00	179.93	9,774.00	-5,474.84	87.13	5,474.95	0.00	0.00	0.00
15,700.00	90.00	179.93	9,774.00	-5,574.84	87.26	5,574.95	0.00	0.00	0.00
15,800.00	90.00	179.93	9,774.00	-5,674.84	87.39	5,674.95	0.00	0.00	0.00
15,900.00	90.00	179.93	9,774.00	-5,774.84	87.52	5,774.95	0.00	0.00	0.00
16,000.00	90.00	179.93	9,774.00	-5,874.84	87.65	5,874.95	0.00	0.00	0.00
16,100.00	90.00	179.93	9,774.00	-5,974.84	87.78	5,974.95	0.00	0.00	0.00
16,200.00	90.00	179.93	9,774.00	-6,074.84	87.91	6,074.95	0.00	0.00	0.00
16,300.00	90.00	179.93	9,774.00	-6,174.84	88.04	6,174.95	0.00	0.00	0.00
16,400.00	90.00	179.93	9,774.00	-6,274.84	88.17	6,274.95	0.00	0.00	0.00
16,500.00	90.00	179.93	9,774.00	-6,374.84	88.30	6,374.95	0.00	0.00	0.00
16,600.00	90.00	179.93	9,774.00	-6,474.84	88.43	6,474.95	0.00	0.00	0.00
16,700.00	90.00	179.93	9,774.00	-6,574.84	88.56	6,574.95	0.00	0.00	0.00
16,800.00	90.00	179.93	9,774.00	-6,674.84	88.69	6,674.95	0.00	0.00	0.00
16,900.00	90.00	179.93	9,774.00	-6,774.84	88.82	6,774.95	0.00	0.00	0.00
17,000.00	90.00	179.93	9,774.00	-6,874.84	88.95	6,874.95	0.00	0.00	0.00
17,100.00	90.00	179.93	9,774.00	-6,974.84	89.08	6,974.95	0.00	0.00	0.00



EDM 5000.1.13 Single User Db Database: Company:

XTO Energy

EDDY COUNTY, NM (NAD-27) Project: POKER LAKE UNIT 30 BS Site:

Well: 209H Wellbore: Wellbore #1 PERMIT Design:

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**Survey Calculation Method:** 

Well 209H

RKB = 30' @ 3409.00usft (TBD)

RKB = 30' @ 3409.00usft (TBD)

Design.	FLIXIVIII								
Planned Survey									
<b>M</b> easured Depth (usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Vertical Section (usft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)
17,200.00	90.00	179.93	9,774.00	-7,074.84	89.21	7,074 <b>.</b> 95	0.00	0.00	0.00
17,300.00	90.00	179.93	9,774.00	-7,174.84	89.34	7,174 <b>.</b> 95	0.00	0.00	0.00
17,400.00	90.00	179.93	9,774.00	-7,274.84	89.47	7,274.95	0.00	0.00	0.00
17,500.00	90.00	179.93	9,774.00	-7,374.84	89.60	7,374.95	0.00	0.00	0.00
17,600.00	90.00	179.93	9,774.00	-7,474.84	89.73	7,474.95	0.00	0.00	0.00
17,700.00	90.00	179.93	9,774.00	-7,574.84	89.86	7,574.95	0.00	0.00	0.00
17,800.00	90.00	179.93	9,774.00	-7,674.84	89.99	7,674.95	0.00	0.00	0.00
17,900.00	90.00	179.93	9,774.00	-7,774.84	90.12	7,774.95	0.00	0.00	0.00
18,000.00	90.00	179.93	9,774.00	-7,874.84	90.25	7,874.95	0.00	0.00	0.00
18,100.00	90.00	179.93	9,774.00	-7,974.84	90.38	7,974.95	0.00	0.00	0.00
18,200.00	90.00	179.93	9,774.00	-8,074.84	90.51	8,074.95	0.00	0.00	0.00
18,300.00	90.00	179.93	9,774.00	-8,174.84	90.64	8,174.95	0.00	0.00	0.00
18,400.00	90.00	179.93	9,774.00	-8,274.84	90.77	8,274.95	0.00	0.00	0.00
18,500.00	90.00	179.93	9,774.00	-8,374.84	90.90	8,374.95	0.00	0.00	0.00
18,600.00	90.00	179.93	9,774.00	-8,474.84	91.03	8,474.95	0.00	0.00	0.00
18,700.00	90.00	179.93	9,774.00	-8,574.84	91.16	8,574.95	0.00	0.00	0.00
18,800.00	90.00	179.93	9,774.00	-8,674.84	91.29	8,674.95	0.00	0.00	0.00
18,900.00	90.00	179.93	9,774.00	-8,774.84	91.42	8,774.95	0.00	0.00	0.00
19,000.00	90.00	179.93	9,774.00	-8,874.84	91.55	8,874.95	0.00	0.00	0.00
19,100.00	90.00	179.93	9,774.00	-8,974.84	91.68	8,974.95	0.00	0.00	0.00
19,200.00	90.00	179.93	9,774.00	-9,074.84	91.81	9,074.95	0.00	0.00	0.00
19,300.00	90.00	179.93	9,774.00	-9,174.84	91.94	9,174.95	0.00	0.00	0.00
19,400.00	90.00	179.93	9,774.00	-9,274.84	92.07	9,274.95	0.00	0.00	0.00
19,500.00	90.00	179.93	9,774.00	-9,374.84	92.20	9,374.95	0.00	0.00	0.00
19,600.00	90.00	179.93	9,774.00	-9,474.84	92.33	9,474.95	0.00	0.00	0.00
19,700.00	90.00	179.93	9,774.00	-9,574.84	92.46	9,574.95	0.00	0.00	0.00
19,800.00	90.00	179.93	9,774.00	-9,674.84	92.59	9,674.95	0.00	0.00	0.00
19,900.00	90.00	179.93	9,774.00	-9,774.84	92.72	9,774.95	0.00	0.00	0.00
20,000.00	90.00	179.93	9,774.00	-9,874.84	92.85	9,874.95	0.00	0.00	0.00
20,100.00	90.00	179.93	9,774.00	-9,974.84	92.98	9,974.95	0.00	0.00	0.00
20,200.00	90.00	179.93	9,774.00	-10,074.84	93.11	10,074.95	0.00	0.00	0.00
20,300.00	90.00	179.93	9,774.00	-10,174.84	93.24	10,174.95	0.00	0.00	0.00
20,400.00	90.00	179.93	9,774.00	-10,474.84	93.37	10,274.95	0.00	0.00	0.00
20,500.00	90.00	179.93	9,774.00		93.50	10,374.95	0.00	0.00	0.00
20,600.00	90.00	179.93	9,774.00		93.63	10,474.95	0.00	0.00	0.00
20,700.00	90.00	179.93	9,774.00		93.76	10,574.95	0.00	0.00	0.00
20,800.00	90.00	179.93	9,774.00		93.89	10,674.95	0.00	0.00	0.00
20,900.00 21,000.00 21,100.00 21,200.00 21,300.00	90.00 90.00 90.00 90.00 90.00	179.93 179.93 179.93 179.93 179.93		-10,774.84 -10,874.84 -10,974.84 -11,074.84 -11,174.84		10,774.95 10,874.95 10,974.95 11,074.95 11,174.95	0.00 0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00 0.00
21,400.00	90.00	179.93	9,774.00	-11,274.84	94.67	11,274.95	0.00	0.00	0.00
21,500.00	90.00	179.93	9,774.00	-11,374.84	94.80	11,374.95	0.00	0.00	0.00
21,600.00	90.00	179.93	9,774.00	-11,474.84	94.93	11,474.95	0.00	0.00	0.00
21,700.00	90.00	179.93	9,774.00	-11,574.84	95.06	11,574.95	0.00	0.00	0.00
21,800.00	90.00	179.93	9,774.00	-11,674.84	95.19	11,674.95	0.00	0.00	0.00
21,900.00	90.00	179.93	9,774.00	-11,774.84	95.32	11,774.95	0.00	0.00	0.00
22,000.00	90.00	179.93	9,774.00	-11,874.84	95.45	11,874.95	0.00	0.00	0.00
22,100.00	90.00	179.93	9,774.00	-11,974.84	95.58	11,974.95	0.00	0.00	0.00
22,200.00	90.00	179.93	9,774.00	-12,074.84	95.71	12,074.95	0.00	0.00	0.00
22,300.00	90.00	179.93	9,774.00	-12,174.84	95.84	12,174.95	0.00	0.00	0.00
22,400.00	90.00	179.93	9,774.00	-12,274.84	95.97	12,274.95	0.00	0.00	0.00
22,500.00	90.00	179.93	9,774.00	-12,374.84	96.10	12,374.95	0.00	0.00	0.00



Database: EDM 5000.1.13 Single User Db

Company: XTO Energy

Project: EDDY COUNTY, NM (NAD-27)
Site: POKER LAKE UNIT 30 BS

Well: 209H
Wellbore: Wellbore #1
Design: PERMIT

Local Co-ordinate Reference:

TVD Reference: MD Reference: North Reference:

Survey Calculation Method:

Well 209H

RKB = 30' @ 3409.00usft (TBD) RKB = 30' @ 3409.00usft (TBD)

Grid

Planned Survey									
Measured Depth (usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Vertical Section (usft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)
22,600.00 22,700.00 22,800.00	90.00 90.00 90.00	179.93 179.93 179.93	9,774.00 9,774.00 9,774.00	-12,474.84 -12,574.84 -12,674.84	96.23 96.36 96.49	12,474.95 12,574.95 12,674.95	0.00 0.00 0.00	0.00 0.00 0.00	0.00 0.00 0.00
22,900.00 23,000.00 23,100.00	90.00 90.00 90.00	179.93 179.93 179.93	9,774.00 9,774.00 9,774.00	-12,774.84 -12,874.84 -12,974.84	96.62 96.75 96.88	12,774.95 12,874.95 12,974.95	0.00 0.00 0.00	0.00 0.00 0.00	0.00 0.00 0.00
23,200.00 23,300.00 23,400.00	90.00 90.00 90.00	179.93 179.93 179.93	9,774.00 9,774.00 9,774.00	-13,074.84 -13,174.84 -13,274.84	97.02 97.15 97.28	13,074.95 13,174.95 13,274.95	0.00 0.00 0.00	0.00 0.00 0.00	0.00 0.00 0.00
23,500.00 23,545.72	90.00 90.00 90.00	179.93 179.93 179.93	9,774.00 9,774.00 9,774.00	-13,374.84 -13,420.56	97.41 97.46	13,274.95 13,374.95 13,420.67	0.00 0.00	0.00 0.00	0.00 0.00
<b>209H LTP</b> 23,595.72 <b>209H BHL</b>	90.00	179.93	9,774.00	-13,470.56	97.53	13,470.67	0.00	0.00	0.00

Design Targets									
Target Name - hit/miss target - Shape	Dip Angle (°)	Dip Dir. (°)	TVD (usft)	+N/-S (usft)	+E/-W (usft)	Northing (usft)	Easting (usft)	Latitude	Longitude
209H SHL - plan hits target c - Point	0.00 enter	0.00	0.00	0.00	0.00	401,106.38	659,249.96	32.1017134	-103.8190495
209H LTP - plan misses targe - Point	0.00 et center by		,	-13,420.56 Isft MD (9774	97.23 00 TVD, -13	387,685.82 3420.56 <b>N</b> , 97.46	659,347.19 E)	32.0648198	-103.8189421
209H BHL - plan hits target c - Point	0.00 enter	0.00	9,774.00	-13,470.56	97.53	387,635.82	659,347.49	32.0646823	-103.8189419
209H FTP - plan hits target c - Point	0.00 enter	0.00	9,774.00	0.60	80.00	401,106.98	659,329.96	32.1017140	-103.8187911



Database: EDM 5000.1.13 Single User Db

Company: XTO Energy

Project: EDDY COUNTY, NM (NAD-27)
Site: POKER LAKE UNIT 30 BS

Well: 209H
Wellbore: Wellbore #1
Design: PERMIT

Local Co-ordinate Reference:

TVD Reference: MD Reference: North Reference:

Survey Calculation Method:

Well 209H

RKB = 30' @ 3409.00usft (TBD)

RKB = 30' @ 3409.00usft (TBD)

Grid

Jesigii.	I LIXIVIII					
Formations						
	Measured Depth (usft)	Vertical Depth (usft)	Name	Lithology	Dip (°)	Dip Direction (°)
	975.00	975.00	Rustler			
	1,302.00	1,302.00	Top Salt			
	3,969.05	3,963.00	Base Salt			
	4,179.75	4,173.00	Delaware			
	5,043.63	5,034.00	Cherry Canyon			
	6,519.56	6,505.00	Brushy Canyon			
	7,800.83	7,782.00	Basal Brushy Canyon			
	8,018.56	7,999.00	Bone Spring Lime Fm			
	8,140.97	8,121.00	Avalon Shale			
	8,598.49	8,577.00	Avalon Lime			
	8,787.12	8,765.00	1st Bone Spring Lime			
	8,973.74	8,951.00	1st Bone Spring Ss			
	9,449.20	9,420.00	2nd Bone Spring Lime			
	9,780.90	9,674.00	2nd Bone Spring Ss			
	10,124.55	9,774.00	TD			
	10,124.55	9,774.00	Landing Point			

#### PECOS DISTRICT DRILLING CONDITIONS OF APPROVAL

**OPERATOR'S NAME:** XTO LEASE NO.: NMLC061634B LOCATION: Sec. 30, T.25 S, R 31 E **COUNTY:** Eddy County, New Mexico WELL NAME & NO.: Poker Lake Unit 30 BS 209H **SURFACE HOLE FOOTAGE:** 2435'/N & 2010'/W

**BOTTOM HOLE FOOTAGE:** 50'/S & 2090'/W

COA

H <sub>2</sub> S	•	No	0	Yes
Potash /	None	Secretary	© R-111-Q	Open Annulus
WIPP	Choos	e an option (including bla	nk option.)	■ WIPP
Cave / Karst	C Low	Medium	High	Critical
Wellhead	Conventional	Multibowl	Both	Diverter
Cementing	Primary Squeeze	Cont. Squeeze	EchoMeter	DV Tool
Special Req	Capitan Reef	Water Disposal	COM	Unit
Waste Prev.	Self-Certification	C Waste Min. Plan	APD Submitted p	prior to 06/10/2024
Additional	Flex Hose	Casing Clearance	Pilot Hole	Break Testing
Language	Four-String	Offline Cementing	Fluid-Filled	

#### A. HYDROGEN SULFIDE

Hydrogen Sulfide (H2S) monitors shall be installed prior to drilling out the surface shoe. If H2S is detected in concentrations greater than 100 ppm, the Hydrogen Sulfide area shall meet 43 CFR 3176 requirements, which includes equipment and personnel/public protection items. If Hydrogen Sulfide is encountered, provide measured values and formations to the BLM.

#### **B.** CASING

- 1. The 9-5/8 inch surface casing shall be set at approximately 1084 feet (a minimum of 70 feet (Eddy County) into the Rustler Anhydrite, above the salt, and below usable fresh water) and cemented to the surface.
  - a. If cement does not circulate to the surface, the appropriate BLM office shall be notified and a temperature survey utilizing an electronic type temperature survey with surface log readout will be used or a cement bond log shall be run to verify the top of the cement. Temperature survey will be run a minimum of six hours after pumping cement and ideally between 8-10 hours after completing the cement job.
  - b. Wait on cement (WOC) time for a primary cement job will be a minimum of **8 hours** or 500 pounds compressive strength, whichever is greater. (This is to include the

lead cement)

- c. Wait on cement (WOC) time for a remedial job will be a minimum of 4 hours after bringing cement to surface or 500 pounds compressive strength, whichever is greater.
- d. If cement falls back, remedial cementing will be done prior to drilling out that string.
- 2. The minimum required fill of cement behind the 7-5/8 inch intermediate casing is: Operator has proposed to cement in two stages by conventionally cementing the first stage and performing a bradenhead squeeze on the second stage, contingent upon no returns to surface.
  - a. First stage: Operator will cement with intent to reach the top of the Brushy Canyon at 6505'.
  - b. **Second stage:** Operator will perform bradenhead squeeze and top-out. Cement to surface. If cement does not reach surface, the appropriate BLM office shall be notified

Wait on cement (WOC) time for a primary cement job is to include the lead cement slurry due to cave/karst.

❖ In Medium Cave/Karst Areas if cement does not circulate to surface on the first two casing strings, the cement on the 3rd casing string must come to surface.

Operator has proposed to pump down Surface X Intermediate 1 annulus after primary cementing stage. Operator must run Echo-meter to verify Cement Slurry/Fluid top in the annulus OR operator shall run a CBL from TD of the Surface casing to tieback requirements listed above after the second stage BH to verify TOC. Submit results to the BLM. No displacement fluid/wash out shall be utilized at the top of the cement slurry between second stage BH and top out. Operator must use a limited flush fluid volume of 1 bbl following backside cementing procedures.

If cement does not reach surface, the next casing string must come to surface.

- 3. The minimum required fill of cement behind the 5-1/2 inch production casing is:
  - Cement should tie-back at least **200 feet** into previous casing string. Operator shall provide method of verification.

#### C. PRESSURE CONTROL

- 1. Variance approved to use flex line from BOP to choke manifold. Manufacturer's specification to be readily available. No external damage to flex line. Flex line to be installed as straight as possible (no hard bends).
  - 2. Operator has proposed a multi-bowl wellhead assembly. Minimum working pressure of the blowout preventer (BOP) and related equipment (BOPE) required for drilling below the surface casing shoe shall be **5000 (5M)** psi.

- a. Wellhead shall be installed by manufacturer's representatives, submit documentation with subsequent sundry.
- b. If the welding is performed by a third party, the manufacturer's representative shall monitor the temperature to verify that it does not exceed the maximum temperature of the seal.
- c. Manufacturer representative shall install the test plug for the initial BOP test.
- d. If the cement does not circulate and one-inch operations would have been possible with a standard wellhead, the well head shall be cut off, cementing operations performed and another wellhead installed.
- e. Whenever any seal subject to test pressure is broken, all the tests in 43 CFR 3172 must be followed.

#### D. SPECIAL REQUIREMENT (S)

#### **Unit Wells**

The well sign for a unit well shall include the unit number in addition to the surface and bottom hole lease numbers. This also applies to participating area numbers. If a participating area has not been established, the operator can use the general unit designation, but will replace the unit number with the participating area number when the sign is replaced.

#### **Commercial Well Determination**

A commercial well determination shall be submitted after production has been established for at least six months. (This is not necessary for secondary recovery unit wells)

#### **BOPE Break Testing Variance**

- BOPE Break Testing is ONLY permitted for intervals utilizing a 5M BOPE or less. (Annular preventer must be tested to a minimum of 70% of BOPE working pressure and shall be higher than the MASP.)
- BOPE Break Testing is NOT permitted to drilling the production hole section.
- Variance only pertains to the intermediate hole-sections and no deeper than the Bone Springs formation.
- While in transfer between wells, the BOPE shall be secured by the hydraulic carrier or cradle
- Any well control event while drilling require notification to the BLM Petroleum Engineer (575-706-2779) prior to the commencement of any BOPE Break Testing operations.
- A full BOPE test is required prior to drilling the first deep intermediate hole section. If any subsequent hole interval is deeper than the first, a full BOPE test will be required. (200' TVD tolerance between intermediate shoes is allowable).
- The BLM is to be contacted (575-361-2822 Eddy County) 4 hours prior to BOPE tests.
- As a minimum, a full BOPE test shall be performed at 21-day intervals.
- In the event any repairs or replacement of the BOPE is required, the BOPE shall test as per 43 CFR 3172.
- If in the event break testing is not utilized, then a full BOPE test would be conducted.

#### **Offline Cementing**

Contact the BLM prior to the commencement of any offline cementing procedure.

Engineer may elect to vary this language. Speak with Chris about implementing changes and whether that change seems reasonable.

#### **Casing Clearance**

String does not meet 0.422" clearance requirement per 43 CFR 3172. Cement tieback requirement increased 100' for 1st Intermediate casing tieback. Operator may contact approving engineer to discuss changing casing set depth or grade to meet clearance requirement.

#### **GENERAL REQUIREMENTS**

The BLM is to be notified in advance for a representative to witness:

- a. Spudding well (minimum of 24 hours)
- b. Setting and/or Cementing of all casing strings (minimum of 4 hours)
- c. BOPE tests (minimum of 4 hours)

#### **Contact Eddy County Petroleum Engineering Inspection Staff:**

Email or call the Carlsbad Field Office, 620 East Greene St., Carlsbad, NM 88220; **BLM NM CFO DrillingNotifications@BLM.GOV**; (575) 361-2822

- 1. Unless the production casing has been run and cemented or the well has been properly plugged, the drilling rig shall not be removed from over the hole without prior approval.
  - a. In the event the operator has proposed to drill multiple wells utilizing a skid/walking rig. Operator shall secure the wellbore on the current well, after installing and testing the wellhead, by installing a blind flange of like pressure rating to the wellhead and a pressure gauge that can be monitored while drilling is performed on the other well(s).
  - b. When the operator proposes to set surface casing with Spudder Rig
    - i. Notify the BLM when moving in and removing the Spudder Rig.
    - ii. Notify the BLM when moving in the 2<sup>nd</sup> Rig. Rig to be moved in within 90 days of notification that Spudder Rig has left the location.
    - iii. BOP/BOPE test to be conducted per **43 CFR 3172** as soon as 2<sup>nd</sup> Rig is rigged up on well.
- 2. Floor controls are required for 3M or Greater systems. These controls will be on the rig floor, unobstructed, readily accessible to the driller and will be operational at all times during drilling and/or completion activities. Rig floor is defined as the area immediately around the rotary table; the area immediately above the substructure on which the draw works are located, this does not include the dog house or stairway area.
- 3. For intervals in which cement to surface is required, cement to surface should be verified with a visual check and density or pH check to differentiate cement from spacer and drilling mud. The results should be documented in the driller's log and daily reports.

#### A. CASING

1. Changes to the approved APD casing program need prior approval if the items substituted are of lesser grade or different casing size or are Non-API. The Operator can exchange the components of the proposal with that of superior strength (i.e. changing from J-55 to N-80, or from 36# to 40#). Changes to the approved cement program need prior approval if the altered cement plan has less volume or strength or if the changes are substantial (i.e. Multistage tool, ECP, etc.). The initial wellhead installed on the well will remain on the well with spools used as needed.

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- 2. Wait on cement (WOC) for Potash Areas: After cementing but before commencing any tests, the casing string shall stand cemented under pressure until both of the following conditions have been met: 1) cement reaches a minimum compressive strength of 500 psi for all cement blends of both lead and tail cement, 2) until cement has been in place at least 8 hours. WOC time will be recorded in the driller's log. The casing integrity test can be done (prior to the cement setting up) immediately after bumping the plug.
- 3. Wait on cement (WOC) for Water Basin: After cementing but before commencing any tests, the casing string shall stand cemented under pressure until both of the following conditions have been met: 1) cement reaches a minimum compressive strength of 500 psi at the shoe, 2) until cement has been in place at least 8 hours. WOC time will be recorded in the driller's log. See individual casing strings for details regarding lead cement slurry requirements. The casing integrity test can be done (prior to the cement setting up) immediately after bumping the plug.
- 4. Provide compressive strengths including hours to reach required 500 pounds compressive strength prior to cementing each casing string. Have well specific cement details onsite prior to pumping the cement for each casing string.
- 5. No pea gravel permitted for remedial or fall back remedial without prior authorization from the BLM engineer.
- 6. On that portion of any well approved for a 5M BOPE system or greater, a pressure integrity test of each casing shoe shall be performed. Formation at the shoe shall be tested to a minimum of the mud weight equivalent anticipated to control the formation pressure to the next casing depth or at total depth of the well. This test shall be performed before drilling more than 20 feet of new hole.
- 7. If hardband drill pipe is rotated inside casing, returns will be monitored for metal. If metal is found in samples, drill pipe will be pulled and rubber protectors which have a larger diameter than the tool joints of the drill pipe will be installed prior to continuing drilling operations.
- 8. Whenever a casing string is cemented in the R-111-Q potash area, the NMOCD requirements shall be followed.

#### **B.** PRESSURE CONTROL

- 1. All blowout preventer (BOP) and related equipment (BOPE) shall comply with well control requirements as described in 43 CFR 3172.
- 2. If a variance is approved for a flexible hose to be installed from the BOP to the choke manifold, the following requirements apply: The flex line must meet the requirements of API 16C. Check condition of flexible line from BOP to choke manifold, replace if exterior is damaged or if line fails test. Line to be as straight as possible with no hard bends and is to be anchored according to Manufacturer's

- requirements. The flexible hose can be exchanged with a hose of equal size and equal or greater pressure rating. Anchor requirements, specification sheet and hydrostatic pressure test certification matching the hose in service, to be onsite for review. These documents shall be posted in the company man's trailer and on the rig floor.
- 3. 5M or higher system requires an HCR valve, remote kill line and annular to match. The remote kill line is to be installed prior to testing the system and tested to stack pressure.
- 4. If the operator has proposed a multi-bowl wellhead assembly in the APD. The following requirements must be met:
  - i. Wellhead shall be installed by manufacturer's representatives, submit documentation with subsequent sundry.
  - ii. If the welding is performed by a third party, the manufacturer's representative shall monitor the temperature to verify that it does not exceed the maximum temperature of the seal.
  - iii. Manufacturer representative shall install the test plug for the initial BOP test.
  - iv. Whenever any seal subject to test pressure is broken, all the tests in 43 CFR 3172.6(b)(9) must be followed.
  - v. If the cement does not circulate and one inch operations would have been possible with a standard wellhead, the well head shall be cut off, cementing operations performed and another wellhead installed.
- 5. The appropriate BLM office shall be notified a minimum of 4 hours in advance for a representative to witness the tests.
  - i. In a water basin, for all casing strings utilizing slips, these are to be set as soon as the crew and rig are ready and any fallback cement remediation has been done. The casing cut-off and BOP installation can be initiated four hours after installing the slips, which will be approximately six hours after bumping the plug. For those casing strings not using slips, the minimum wait time before cut-off is eight hours after bumping the plug. BOP/BOPE testing can begin after cut-off or once cement reaches 500 psi compressive strength (including lead cement), whichever is greater. However, if the float does not hold, cut-off cannot be initiated until cement reaches 500 psi compressive strength (including lead when specified).
  - ii. In potash areas, for all casing strings utilizing slips, these are to be set as soon as the crew and rig are ready and any fallback cement remediation has been done. For all casing strings, casing cut-off and BOP installation can be initiated at twelve hours after bumping the cement plug. The BOPE test can be initiated after bumping the cement plug with the casing valve

- open. (only applies to single stage cement jobs, prior to the cement setting up.)
- iii. The tests shall be done by an independent service company utilizing a test plug not a cup or J-packer and can be initiated immediately with the casing valve open. The operator also has the option of utilizing an independent tester to test without a plug (i.e. against the casing) pursuant to 43 CFR 3172 with the pressure not to exceed 70% of the burst rating for the casing. Any test against the casing must meet the WOC time for 8 hours or 500 pounds compressive strength, whichever is greater, prior to initiating the test (see casing segment as lead cement may be critical item).
- iv. The test shall be run on a 5000 psi chart for a 2-3M BOP/BOP, on a 10000 psi chart for a 5M BOP/BOPE and on a 15000 psi chart for a 10M BOP/BOPE. If a linear chart is used, it shall be a one hour chart. A circular chart shall have a maximum 2 hour clock. If a twelve hour or twenty-four hour chart is used, tester shall make a notation that it is run with a two hour clock.
- v. The results of the test shall be reported to the appropriate BLM office.
- vi. All tests are required to be recorded on a calibrated test chart. A copy of the BOP/BOPE test chart and a copy of independent service company test will be submitted to the appropriate BLM office.
- vii. The BOP/BOPE test shall include a low pressure test from 250 to 300 psi. The test will be held for a minimum of 10 minutes if test is done with a test plug and 30 minutes without a test plug. This test shall be performed prior to the test at full stack pressure.
- viii. BOP/BOPE must be tested by an independent service company within 500 feet of the top of the Wolfcamp formation if the time between the setting of the intermediate casing and reaching this depth exceeds 20 days. This test does not exclude the test prior to drilling out the casing shoe as per 43 CFR 3172.

#### C. DRILLING MUD

Mud system monitoring equipment, with derrick floor indicators and visual and audio alarms, shall be operating before drilling into the Wolfcamp formation, and shall be used until production casing is run and cemented.

#### D. WASTE MATERIAL AND FLUIDS

All waste (i.e. drilling fluids, trash, salts, chemicals, sewage, gray water, etc.) created as a result of drilling operations and completion operations shall be safely contained and disposed of properly at a waste disposal facility. No waste material or fluid shall be

disposed of on the well location or surrounding area. Porto-johns and trash containers will be on-location during fracturing operations or any other crew-intensive operations.

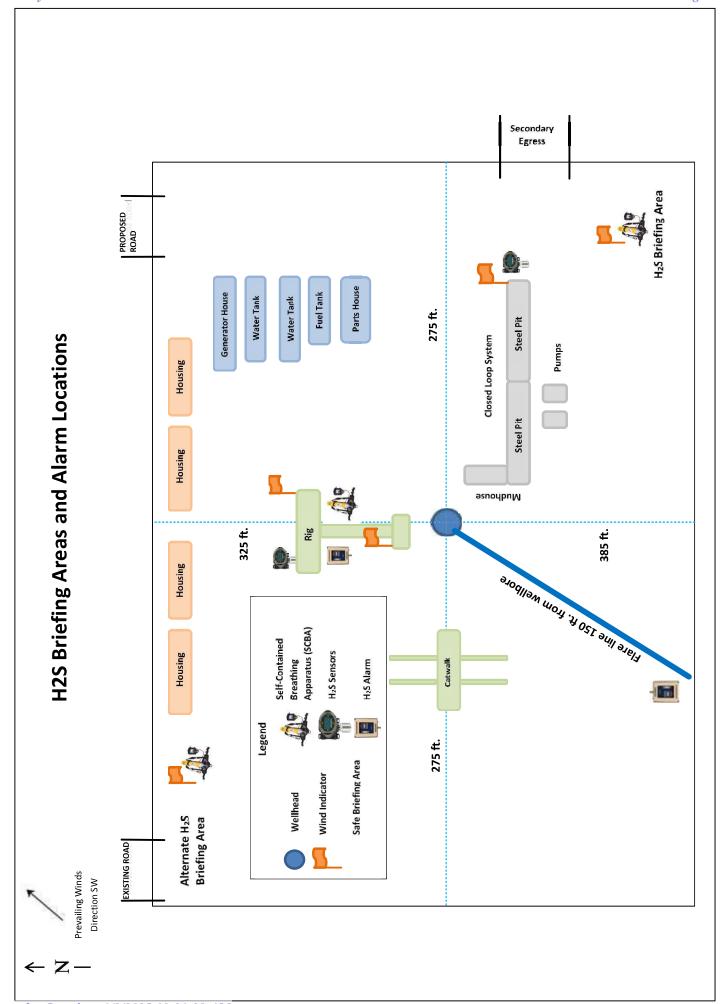
**Approved by Zota Stevens on 10/2/2024** 575-234-5998 / zstevens@blm.gov

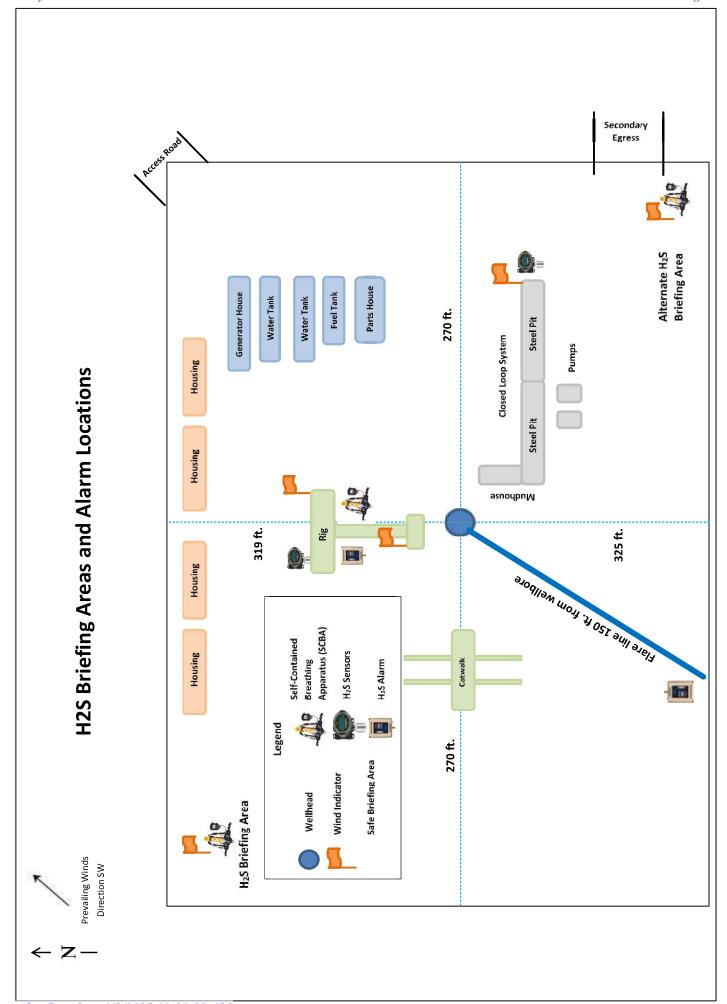


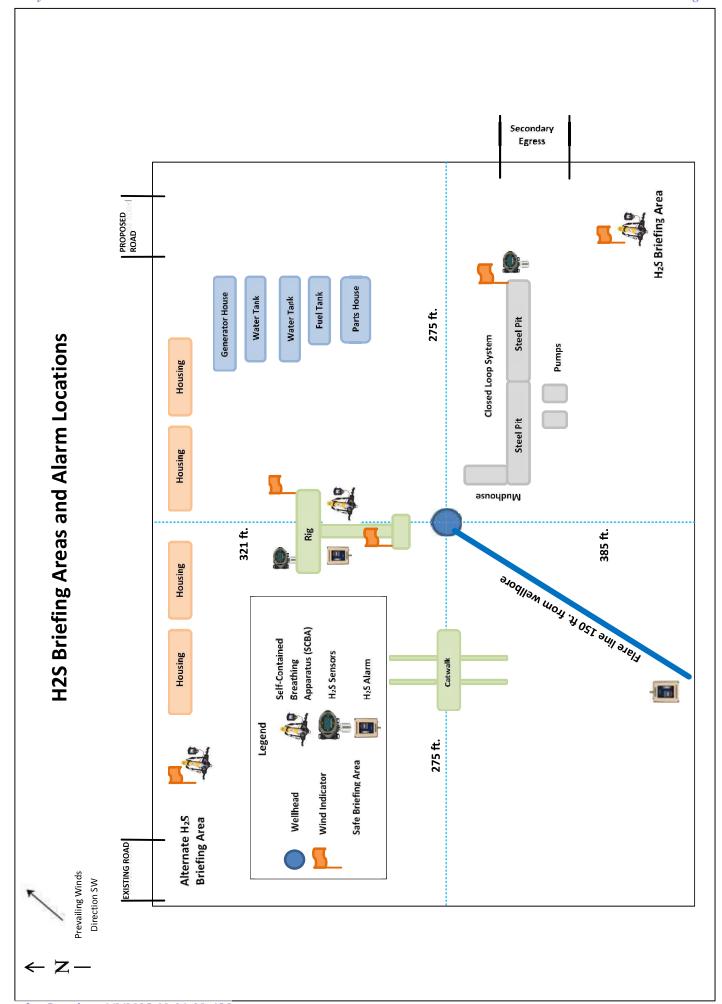
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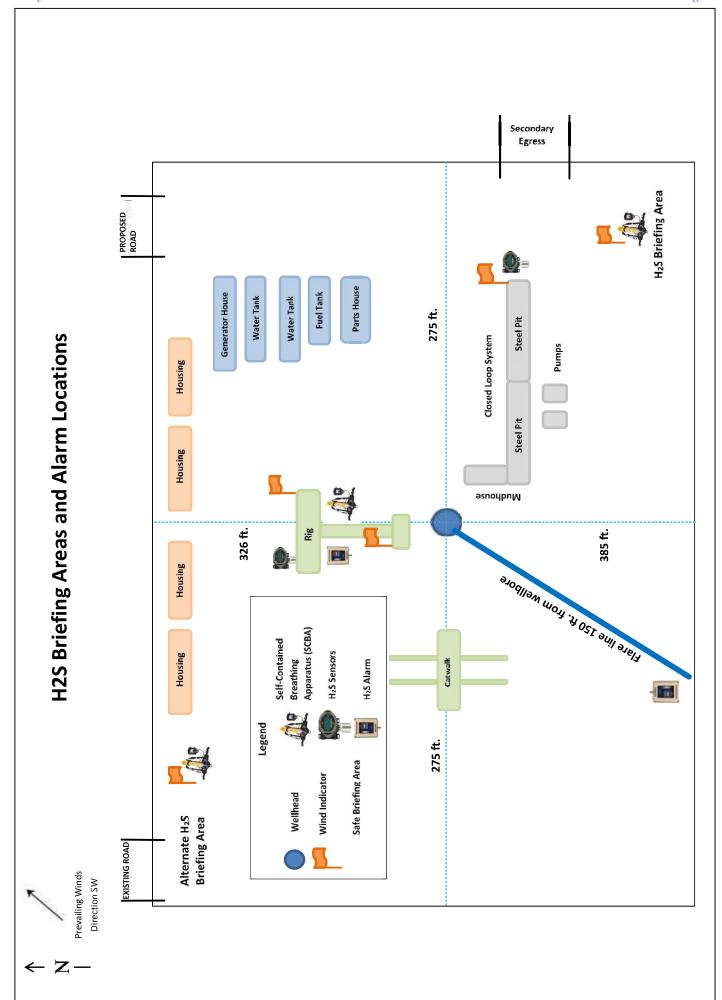
#### **CARLSBAD OFFICE – EDDY & LEA COUNTIES**

3104 E. Greene St., Carlsbad, NM 88220 Carlsbad, NM	575-887-7329
XTO PERSONNEL: Christopher Cha, Drilling Manager Matt Water, Drilling Superintendent Robert Bartels, Construction Foreman Andy Owens, EH & S Manager Mike Allen, Production Foreman	432-701-1730 432-967-8203 406-478-3617 903-245-2602 918-421-9056
SHERIFF DEPARTMENTS:	
Eddy County	575-887-7551
Lea County	575-396-3611
NEW MEXICO STATE POLICE:	575-392-5588
FIRE DEPARTMENTS: Carlsbad Eunice Hobbs Jal Lovington	911 575-885-2111 575-394-2111 575-397-9308 575-395-2221 575-396-2359
HOSPITALS:	911
Carlsbad Medical Emergency	575-885-2111
Eunice Medical Emergency	575-394-2112
Hobbs Medical Emergency	575-397-9308
Jal Medical Emergency	575-395-2221
Lovington Medical Emergency	575-396-2359
AGENT NOTIFICATIONS: For Lea County: Bureau of Land Management – Hobbs New Mexico Oil Conservation Division – Hobbs	575-393-3612 505-629-6116
For Eddy County	
For Eddy County: Bureau of Land Management - Carlsbad	575-234-5972
New Mexico Oil Conservation Division - Artesia	505-629-6116









**Operator Name: XTO PERMIAN OPERATING LLC** 

Well Name: POKER LAKE UNIT 30 BS Well Number: 209H

Safe containment attachment:

Waste disposal type: HAUL TO COMMERCIAL Disposal location ownership: COMMERCIAL

**FACILITY** 

Disposal type description:

Disposal location description: A licensed 3rd party contractor will be used to haul and dispose of garbage.

#### **Reserve Pit**

Reserve Pit being used? NO

Temporary disposal of produced water into reserve pit? NO

Reserve pit length (ft.) Reserve pit width (ft.)

Reserve pit depth (ft.) Reserve pit volume (cu. yd.)

Is at least 50% of the reserve pit in cut?

Reserve pit liner

Reserve pit liner specifications and installation description

#### **Cuttings Area**

Cuttings Area being used? NO

Are you storing cuttings on location? Y

**Description of cuttings location** Cuttings. The well will be drilled utilizing a closed-loop mud system. Drill cuttings will be held in roll-off style mud boxes and taken to a New Mexico Oil Conservation Division (NMOCD) approved disposal site. Drilling Fluids. These will be contained in steel mud pits and then taken to a NMOCD approved commercial disposal facility. Produced Fluids. Water produced from the well during completion will be held temporarily in steel tanks and then taken to a NMOCD approved commercial disposal facility. Oil produced during operations will be stored in tanks until sold.

Cuttings area length (ft.) Cuttings area width (ft.)

Cuttings area depth (ft.) Cuttings area volume (cu. yd.)

Is at least 50% of the cuttings area in cut?

WCuttings area liner

Cuttings area liner specifications and installation description

#### **Section 8 - Ancillary**

Are you requesting any Ancillary Facilities?: N

**Ancillary Facilities** 

Comments:

Operator Name: XTO PERMIAN OPERATING LLC

Well Name: POKER LAKE UNIT 30 BS Well Number: 209H

#### Section 9 - Well Site

#### Well Site Layout Diagram:

PLU\_30\_BS\_209H\_Well\_20230926142537.pdf

Comments: Multi-well pad.

#### Section 10 - Plans for Surface Reclamation

Type of disturbance: New Surface Disturbance Multiple Well Pad Name: PLU 30 BS

Multiple Well Pad Number: B

#### Recontouring

PLU 30 BS IR2 20240607044539.pdf PLU 30 BS IR4 20240607044541.pdf PLU 30 BS IR3 20240607044541.pdf PLU 30 BS IR1 20240607132829.pdf

Drainage/Erosion control construction: Initial seedbed preparation will consist of recontouring to the appropriate interim or final reclamation standard. All compacted areas to be seeded will be ripped to a minimum depth of 18 inches with a minimum furrow spacing of 2 feet, followed by recontouring the surface and then evenly spreading the stockpiled topsoil. Prior to seeding, the seedbed will be scarified to a depth of no less than 4-6 inches.

Drainage/Erosion control reclamation: Erosion features are equal to or less than surrounding area and erosion control is sufficient so that water naturally infiltrates into the soil and gullying, headcutting, slumping, and deep or excessive rills (greater than 3 inches) are not observed.

Well pad proposed disturbance

(acres): 11.37

Road proposed disturbance (acres):

3.85

Powerline proposed disturbance

(acres): 0

Pipeline proposed disturbance

(acres): 0

Well pad interim reclamation (acres):

Road interim reclamation (acres): 0

Powerline interim reclamation (acres): Powerline long term disturbance

Pipeline interim reclamation (acres): 0 Pipeline long term disturbance

Other proposed disturbance (acres): 0 Other interim reclamation (acres): 0

Well pad long term disturbance

(acres): 9.75

Road long term disturbance (acres):

3.85

(acres): 0

(acres): 0

Other long term disturbance (acres): 0

Total proposed disturbance: 15.21999999999999

**Disturbance Comments:** 

Total interim reclamation: 1.62 Total long term disturbance: 13.6

Reconstruction method: The original stock piled topsoil will be spread over the areas being reclaimed and the original landform will be restored for all disturbed areas including well pads, production facilities, roads, pipelines, and utility corridors as close as possible to the original topography. The location will then be ripped and seeded.

Topsoil redistribution: The original stock piled topsoil will be spread over the areas being reclaimed and the original landform will be restored for all disturbed areas including well pads, production facilities, roads, pipelines, and utility corridors as close as possible to the original topography. The location will then be ripped and seeded.

Soil treatment: A self-sustaining, vigorous, diverse, native (or otherwise approved) plan community will be established on the site with a density sufficient to control erosion and invasion by non-native plants and to re-establish wildlife habitat or forage production. At a minimum, the established plant community will consist of species included in the seed mix and/or desirable species occurring in the surrounding natural vegetation.

**Operator Name: XTO PERMIAN OPERATING LLC** 

Well Name: POKER LAKE UNIT 30 BS Well Number: 209H

**Existing Vegetation at the well pad:** Soils are classified as Simona Gravelly Fine Sandy Loam and Simona-Bippus Complex. Simona soils are found on alluvial fans and plans and form in mixed alluvium and/or Aeolian sands. Bippus soils are found on alluvial fans and floodplains and form in mixed alluvium. The Simona-Bippus soils are dominant to the east and the Simona Gravelly Fine Sandy Loams are dominant to the West. Dominant vegetation species include: mesquite, sumac snakeweed, and various forbs and grasses. Ground cover is minimal, offering 90 percent visibility

Existing Vegetation at the well pad

**Existing Vegetation Community at the road:** Soils are classified as Simona Gravelly Fine Sandy Loam and Simona-Bippus Complex. Simona soils are found on alluvial fans and plans and form in mixed alluvium and/or Aeolian sands. Bippus soils are found on alluvial fans and floodplains and form in mixed alluvium. The Simona-Bippus soils are dominant to the east and the Simona Gravelly Fine Sandy Loams are dominant to the West. Dominant vegetation species include: mesquite, sumac snakeweed, and various forbs and grasses. Ground cover is minimal, offering 90 percent visibility

#### **Existing Vegetation Community at the road**

**Existing Vegetation Community at the pipeline:** Soils are classified as Simona Gravelly Fine Sandy Loam and Simona-Bippus Complex. Simona soils are found on alluvial fans and plans and form in mixed alluvium and/or Aeolian sands. Bippus soils are found on alluvial fans and floodplains and form in mixed alluvium. The Simona-Bippus soils are dominant to the east and the Simona Gravelly Fine Sandy Loams are dominant to the West. Dominant vegetation species include: mesquite, sumac snakeweed, and various forbs and grasses. Ground cover is minimal, offering 90 percent visibility

#### **Existing Vegetation Community at the pipeline**

**Existing Vegetation Community at other disturbances:** Soils are classified as Simona Gravelly Fine Sandy Loam and Simona-Bippus Complex. Simona soils are found on alluvial fans and plans and form in mixed alluvium and/or Aeolian sands. Bippus soils are found on alluvial fans and floodplains and form in mixed alluvium. The Simona-Bippus soils are dominant to the east and the Simona Gravelly Fine Sandy Loams are dominant to the West. Dominant vegetation species include: mesquite, sumac snakeweed, and various forbs and grasses. Ground cover is minimal, offering 90 percent visibility

#### **Existing Vegetation Community at other disturbances**

Non native seed used? N

Non native seed description:

Seedling transplant description:

Will seedlings be transplanted for this project? N

Seedling transplant description

Will seed be harvested for use in site reclamation? N

Seed harvest description:

Seed harvest description attachment:

Sante Fe Main Office Phone: (505) 476-3441

General Information Phone: (505) 629-6116

Online Phone Directory https://www.emnrd.nm.gov/ocd/contact-us

# State of New Mexico Energy, Minerals and Natural Resources Oil Conservation Division 1220 S. St Francis Dr. Santa Fe, NM 87505

CONDITIONS

Action 411771

#### **CONDITIONS**

Operator:	OGRID:
XTO PERMIAN OPERATING LLC.	373075
6401 HOLIDAY HILL ROAD	Action Number:
MIDLAND, TX 79707	411771
	Action Type:
	[C-101] BLM - Federal/Indian Land Lease (Form 3160-3)

#### CONDITIONS

Created By	Condition	Condition Date
sweis	Cement is required to circulate on both surface and intermediate1 strings of casing.	12/13/2024
sweis	If cement does not circulate on any string, a Cement Bond Log (CBL) is required for that string of casing.	12/13/2024
ward.rikala	Notify the OCD 24 hours prior to casing & cement.	1/9/2025
ward.rikala	File As Drilled C-102 and a directional Survey with C-104 completion packet.	1/9/2025
ward.rikala	Once the well is spud, to prevent ground water contamination through whole or partial conduits from the surface, the operator shall drill without interruption through the fresh water zone or zones and shall immediately set in cement the water protection string.	1/9/2025
ward.rikala	Oil base muds are not to be used until fresh water zones are cased and cemented providing isolation from the oil or diesel. This includes synthetic oils. Oil based mud, drilling fluids and solids must be contained in a steel closed loop system.	1/9/2025