U.S. Department of the Interior BUREAU OF LAND MANAGEMENT

Well Name	Well Number	US Well Number	Lease Number	Case Number	Operator
MORGAN 25-13	625H	3001555638	NMLC062300	NMLC062300	DEVON
MORGAN 25-13	735H	3001555642	NMLC062300	NMLC062300	DEVON

Notice of Intent

Sundry ID: 2833338

Type of Submission: Notice of Intent

Date Sundry Submitted: 01/23/2025

Date proposed operation will begin: 01/23/2025

Type of Action: APD Change

Sundry Print Repor

02/06/2025

Time Sundry Submitted: 08:27

Procedure Description: Devon Energy Production Co., L.P. (Devon) respectfully requests to change the drilling plan with casing changes and slim hole design for the Morgan 25-13 Fed Com 625H and 735H. Devon would also like to request offline cementing and break test variances. Please see attachments. Batch sundry to only include attachments by pad for the drilling plan for the deepest well (TVD).

NOI Attachments

Procedure Description

Offline_Cementing___Variance_Request_20250123082430.pdf

break_test_variance_BOP_1_15_24_20250123082412.pdf

5.5_20lb_P110HP_TALON_RD_20250123082350.pdf

7.625_29.7lb_P110_HP_Talon_SFC_20250123082327.pdf

9.625_40lb_J55_SeAH_20250123082308.pdf

MORGAN_25_13_FED_COM_735H_rev1_20250123082228.pdf

Conditions of Approval

Specialist Review

Morgan_25_13_Fed_Com__Sundry_ID_2833338_20250205152424.pdf

Operator

I certify that the foregoing is true and correct. Title 18 U.S.C. Section 1001 and Title 43 U.S.C. Section 1212, make it a crime for any person knowingly and willfully to make to any department or agency of the United States any false, fictitious or fraudulent statements or representations as to any matter within its jurisdiction. Electronic submission of Sundry Notices through this system satisfies regulations requiring a

Operator Electronic Signature: AMY BROWN Name: DEVON ENERGY PRODUCTION COMPANY LP Title: Regulatory Professional Street Address: 333 WEST SHERIDAN AVENUE City: OKLAHOMA CITY State: OK Phone: (405) 552-6137 Email address: AMY.BROWN@DVN.COM

Field

Representative Name:

Street Address:

City:
State:

Phone:

Email address:

BLM Point of Contact

BLM POC Name: LONG VO BLM POC Phone: 5759885402 Disposition: Approved Signature: Long Vo

BLM POC Title: Petroleum Engineer BLM POC Email Address: LVO@BLM.GOV Disposition Date: 02/05/2025

Received by OCD: 2/6/2025 1:28:34 PM

Form 3160-5 UNITED STAT (June 2019) DEPARTMENT OF THE BUREAU OF LAND MAN			NTERIOR	FORM APPROVED OMB No. 1004-0137 Expires: October 31, 2021 5. Lease Serial No.		
	not use this i		DRTS ON WELLS to drill or to re-enter an .PD) for such proposals.	6. If Indian, Allottee or Tribe N	ame	
	SUBMIT IN	TRIPLICATE - Other instru	uctions on page 2	7. If Unit of CA/Agreement, Na	ame and/or No.	
1. Type of Well	/ell 🗌 Gas V	Vell Other		8. Well Name and No.		
2. Name of Operator				9. API Well No.		
3a. Address			3b. Phone No. (include area code)	10. Field and Pool or Explorate	bry Area	
4. Location of Well (Footage, Sec., T., I	R.,M., or Survey Description))	11. Country or Parish, State		
	12. CHE	CK THE APPROPRIATE B	OX(ES) TO INDICATE NATURE (OF NOTICE, REPORT OR OTH	ER DATA	
TYPE OF SU	BMISSION		TYPI	E OF ACTION		
Notice of Inte	nt	Acidize	Deepen	Production (Start/Resume) Reclamation	Water Shut-Off Well Integrity	
Subsequent R	eport	Casing Repair	New Construction	Recomplete Temporarily Abandon	Other	
Final Abando	nment Notice	Convert to Injection	Plug Back	Water Disposal		
the proposal is to the Bond under v completion of th	b deepen directiona which the work wi e involved operation Abandonment No	ally or recomplete horizontal Il be perfonned or provide th ons. If the operation results in	ly, give subsurface locations and me e Bond No. on file with BLM/BIA. n a multiple completion or recomple	asured and true vertical depths of Required subsequent reports mus tion in a new interval, a Form 31	k and approximate duration thereof. If f all pertinent markers and zones. Attach t be filed within 30 days following 60-4 must be filed once testing has been he operator has detennined that the site	

14. I hereby certify that the foregoing is true and correct. Name (<i>Printed/Typed</i>)			
	Title		
Signature	Date		
THE SPACE FOR FEDE	RAL OR STATE O	FICE USE	
Approved by			
	Title	Ι	Date
Conditions of approval, if any, are attached. Approval of this notice does not warrant certify that the applicant holds legal or equitable title to those rights in the subject lead which would entitle the applicant to conduct operations thereon.			
Title 18 U.S.C Section 1001 and Title 43 U.S.C Section 1212, make it a crime for any any false, fictitious or fraudulent statements or representations as to any matter within		illfully to make to any de	partment or agency of the United States

(Instructions on page 2)

GENERAL INSTRUCTIONS

This form is designed for submitting proposals to perform certain well operations and reports of such operations when completed as indicated on Federal and Indian lands pursuant to applicable Federal law and regulations. Any necessary special instructions concerning the use of this form and the number of copies to be submitted, particularly with regard to local area or regional procedures and practices, are either shown below, will be issued by or may be obtained from the local Federal office.

SPECIFIC INSTRUCTIONS

Item 4 - Locations on Federal or Indian land should be described in accordance with Federal requirements. Consult the local Federal office for specific instructions.

Item 13: Proposals to abandon a well and subsequent reports of abandonment should include such special information as is required by the local Federal office. In addition, such proposals and reports should include reasons for the abandonment; data on any former or present productive zones or other zones with present significant fluid contents not sealed off by cement or otherwise; depths (top and bottom) and method of placement of cement plugs; mud or other material placed below, between and above plugs; amount, size, method of parting of any casing, liner or tubing pulled and the depth to the top of any tubing left in the hole; method of closing top of well and date well site conditioned for final inspection looking for approval of the abandonment. If the proposal will involve **hydraulic fracturing operations**, you must comply with 43 CFR 3162.3-3, including providing information about the protection of usable water. Operators should provide the best available information about all formations containing water and their depths. This information could include data and interpretation of resistivity logs run on nearby wells. Information may also be obtained from state or tribal regulatory agencies and from local BLM offices.

NOTICES

The privacy Act of 1974 and the regulation in 43 CFR 2.48(d) provide that you be furnished the following information in connection with information required by this application.

AUTHORITY: 30 U.S.C. 181 et seq., 351 et seq., 25 U.S.C. 396; 43 CFR 3160.

PRINCIPAL PURPOSE: The information is used to: (1) Evaluate, when appropriate, approve applications, and report completion of subsequent well operations, on a Federal or Indian lease; and (2) document for administrative use, information for the management, disposal and use of National Resource lands and resources, such as: (a) evaluating the equipment and procedures to be used during a proposed subsequent well operation and reviewing the completed well operations for compliance with the approved plan; (b) requesting and granting approval to perform those actions covered by 43 CFR 3162.3-2, 3162.3-3, and 3162.3-4; (c) reporting the beginning or resumption of production, as required by 43 CFR 3162.4-1(c)and (d) analyzing future applications to drill or modify operations in light of data obtained and methods used.

ROUTINE USES: Information from the record and/or the record will be transferred to appropriate Federal, State, local or foreign agencies, when relevant to civil, criminal or regulatory investigations or prosecutions in connection with congressional inquiries or to consumer reporting agencies to facilitate collection of debts owed the Government.

EFFECT OF NOT PROVIDING THE INFORMATION: Filing of this notice and report and disclosure of the information is mandatory for those subsequent well operations specified in 43 CFR 3162.3-2, 3162.3-3, 3162.3-4.

The Paperwork Reduction Act of 1995 requires us to inform you that:

The BLM collects this information to evaluate proposed and/or completed subsequent well operations on Federal or Indian oil and gas leases.

Response to this request is mandatory.

The BLM would like you to know that you do not have to respond to this or any other Federal agency-sponsored information collection unless it displays a currently valid OMB control number.

BURDEN HOURS STATEMENT: Public reporting burden for this form is estimated to average 8 hours per response, including the time for reviewing instructions, gathering and maintaining data, and completing and reviewing the form. Direct comments regarding the burden estimate or any other aspect of this form to U.S. Department of the Interior, Bureau of Land Management (1004-0137), Bureau Information Collection Clearance Officer (WO-630), 1849 C St., N.W., Mail Stop 401 LS, Washington, D.C. 20240

Additional Information

Batch Well Data

MORGAN 25-13 FED COM 735H, US Well Number: 3001555642, Case Number: NMLC062300, Lease Number: NMLC062300, Operator:DEVON ENERGY PRODUCTION COMPANY LP

MORGAN 25-13 FED COM 625H, US Well Number: 3001555638, Case Number: NMLC062300, Lease Number: NMLC062300, Operator:DEVON ENERGY PRODUCTION COMPANY LP

Offline Cementing

Variance Request

Devon Energy requests to offline cement on intermediate strings that are set in formations shallower than the Wolfcamp. Prior to commencing offline cementing operations, the well will be monitored for any abnormal pressures and confirmed to be static. A dual manifold system (equipped with chokes) for the returns will also be utilized as a redundancy. All equipment used for offline cementing will have a minimum 5M rating to match intermediate sections' 5M BOPE requirements.

Section 2 - Blowout Preventer Testing Procedure

Variance Request

Devon Energy requests to only test BOP connection breaks after drilling out of surface casing and while skidding between wells which conforms to API Standard 53 and industry standards. This test will include the Top Pipe Rams, HCR, Kill Line Check Valve, QDC (quick disconnect to wellhead) and Shell of the 10M BOPE to 5M for 10 minutes. If a break to the flex hose that runs to the choke manifold is required due to repositioning from a skid, the HCR will remain open during the shell test to include that additional break. The variance only pertains to intermediate hole-sections and no deeper than the Bone Springs Formation where 5M BOP tests are required. The initial BOP test will follow 43 CFR 3172, and subsequent tests following a skid will only test connections that are broken. The annular preventer will be tested to 100% working pressure. This variance will meet or exceed 43 CFR 3172 per the following: Devon Energy will perform a full BOP test per 43 CFR 3172 before drilling out of the intermediate casing string(s) and starting the production hole, before starting any hole section that requires a 10M test, before the expiration of the allotted 14-days for 5M intermediate batch drilling or when the drilling rig is fully mobilized to a new well pad, whichever is sooner. We will utilize a 200' TVD tolerance between intermediate shoes as the cutoff for a full BOP test. The BLM will be contacted 4hrs prior to a BOPE test. The BLM will be notified if and when a well control event is encountered. Break test will be a 14 day interval and not a 30 day full BOPE test interval. If in the event break testing is not utilized, then a full BOPE test would be conducted.

1. Well Control Response:

1. Primary barrier remains fluid

2. In the event of an influx due to being underbalanced and after a realized gain or flow, the order of closing BOPE is as follows:

- a) Annular first
- b) If annular were to not hold, Upper pipe rams second (which were tested on the skid BOP test)
- c) If the Upper Pipe Rams were to not hold, Lower Pipe Rams would be third



2/21/2024 7:48:59 AM

U. S. Steel Tubular Products P110 HP USS-TALON HTQ™ RD 5.500" 20.00lb/ft (0.361" Wall)

IECHANICAL PROPERTIES	Pipe	USS-TALON HTQ™ RD		[6
Minimum Yield Strength	125,000		psi	
Maximum Yield Strength	140,000		psi	
Minimum Tensile Strength	130,000		psi	
DIMENSIONS	Pipe	USS-TALON HTQ™ RD		-
Outside Diameter	5.500	5.900	in.	
Wall Thickness	0.361		in.	
Inside Diameter	4.778	4.778	in.	
Standard Drift	4.653	4.653	in.	
Alternate Drift			in.	
Nominal Linear Weight, T&C	20.00		lb/ft	
Plain End Weight	19.83		lb/ft	
SECTION AREA	Pipe	USS-TALON HTQ™ RD		-
Critical Area	5.828	5.828	sq. in.	-
Joint Efficiency		100.0	%	[2
PERFORMANCE	Pipe	USS-TALON HTQ™ RD		-
Minimum Collapse Pressure	13,150	13,150	psi	-
Minimum Internal Yield Pressure	14,360	14,360	psi	-
Minimum Pipe Body Yield Strength	729,000		lb	-
Joint Strength		729,000	lb	-
Compression Rating		729,000	lb	-
Reference Length		24,300	ft	[
Maximum Uniaxial Bend Rating		104.2	deg/100 ft	[;
IAKE-UP DATA	Pipe	USS-TALON HTQ™ RD		-
Make-Up Loss		5.58	in.	-
Minimum Make-Up Torque		18,400	ft-lb	[4
Maximum Make-Up Torque		21,400	ft-lb	[/
Maximum Operating Torque		44,400	ft-lb	[4

Notes

- 1. Other than proprietary collapse and connection values, performance properties have been calculated using standard equations defined by API 5C3 and do not incorporate any additional design or safety factors. Calculations assume nominal pipe OD, nominal wall thickness, and Specified Minimum Yield Strength (SMYS).
- 2. Joint efficiencies are calculated by dividing the connection critical area by the pipe body area.

3. Uniaxial bend rating shown is structural only.

- 4. Torques have been calculated assuming a thread compound friction factor of 1.0 and are recommended only. Field make-up torques may require adjustment based on actual field conditions (e.g. make-up speed, temperature, thread compound, etc.).
- 5. Reference length is calculated by Joint Strength divided by Nominal Linear Weight, T&C with a 1.5 Safety factor.
- 6. Coupling must meet minimum mechanical properties of the pipe.

Legal Notice

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> U. S. Steel Tubular Products 460 Wildwood Forest Drive, Suite 300S Spring, Texas 77380

1-877-893-9461 connections@uss.com www.usstubular.com

5/15/2024 6:31:14 PM

U. S. Steel Tubular Products 7.625" 29.70lb/ft (0.375" Wall) P11

t (0.375" Wall)	P110 HP	USS-TALON SFC™

		man person		
MECHANICAL PROPERTIES	Pipe	USS-TALON SFC™		[6
Minimum Yield Strength	125,000		psi	
Maximum Yield Strength	140,000		psi	
Minimum Tensile Strength	130,000		psi	
DIMENSIONS	Pipe	USS-TALON SFC™		
Outside Diameter	7.625	7.900	in.	
Wall Thickness	0.375		in.	
Inside Diameter	6.875	6.815	in.	
Standard Drift	6.750	6.750	in.	
Alternate Drift			in.	
Nominal Linear Weight, T&C	29.70		lb/ft	
Plain End Weight	29.06		lb/ft	
SECTION AREA	Pipe	USS-TALON SFC™		
Critical Area	8.541	7.331	sq. in.	-
Joint Efficiency		85.8	%	[
PERFORMANCE	Pipe	USS-TALON SFC™		-
Minimum Collapse Pressure	7,260	7,260	psi	-
Minimum Internal Yield Pressure	10,750	10,750	psi	-
Minimum Pipe Body Yield Strength	1,068,000		lb	-
Joint Strength		916,000	lb	-
Compression Rating		916,000	lb	-
Reference Length		20,560	ft	[
Maximum Uniaxial Bend Rating		64.4	deg/100 ft	[
MAKE-UP DATA	Pipe	USS-TALON SFC™		-
Make-Up Loss		5.08	in.	-
Minimum Make-Up Torque		30,000	ft-lb	[
Maximum Make-Up Torque		33,000	ft-lb	[
Maximum Operating Torque		80,500	ft-lb	[

Notes

1. Other than proprietary collapse and connection values, performance properties have been calculated using standard equations defined by API 5C3 and do not incorporate any additional design or safety factors. Calculations assume nominal pipe OD, nominal wall thickness, and Specified Minimum Yield Strength (SMYS).

2. Joint efficiencies are calculated by dividing the connection critical area by the pipe body area.

3. Uniaxial bend rating shown is structural only.

4. Torques have been calculated assuming a thread compound friction factor of 1.0 and are recommended only. Field make-up torques may require adjustment based on actual field conditions (e.g. make-up speed, temperature, thread compound, etc.).

- 5. Reference length is calculated by Joint Strength divided by Nominal Linear Weight, T&C with a 1.5 Safety factor.
- 6. Coupling must meet minimum mechanical properties of the pipe.

Legal Notice

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U. S. Steel Tubular Products 460 Wildwood Forest Drive, Suite 300S Spring, Texas 77380 1-877-893-9461 connections@uss.com www.usstubular.com

SěAH 9.625" 40# .395" J-55

Dimensions (Nominal)

Outside Diameter	9.625	in.
Wall	0.395	in.
Inside Diameter	8.835	in.
Drift	8.750	in.
Weight, T&C	40.000	lbs./ft.
Weight, PE	38.970	lbs./ft.

Performance Properties

Collapse, PE	2570	psi
Internal Yield Pressure at Minimum Yield		
PE	3950	psi
LTC	3950	psi
втс	3950	psi
Yield Strength, Pipe Body	630	1000 lbs.
Joint Strength		
STC	452	1000 lbs.
LTC	520	1000 lbs.
втс	714	1000 lbs.

Note: SeAH Steel has produced this specification sheet for general information only. SeAH does not assume liability or responsibility for any loss or injury resulting from the use of information or data contained herein. All applications for the material described are at the customer's own risk and responsibility.

1. Geologic Formations

TVD of target	12103	Pilot hole depth	N/A
MD at TD:	25081	Deepest expected fresh water	

Basin

	Depth	Water/Mineral	
			TT 1 4
Formation	(TVD)	Bearing/Target	Hazards*
	from KB	Zone?	
Rustler	945		
Salt	1355		
Base of Salt	4052		
Delaware	4358		
Cherry Canyon	5321		
Brushy Canyon	6754		
Bone Spring 1st	9341		
Bone Spring 2nd	9976		
Bone Spring 3rd	10421		
Wolfcamp	11645		

*H2S, water flows, loss of circulation, abnormal pressures, etc.

MORGAN 25-13 FED COM 735H

		Wt			Casing	Interval	Casing	Interval
Hole Size	Csg. Size	(PPF)	Grade	Conn	From (MD)	To (MD)	From (TVD)	To (TVD)
13 1/2	9 5/8	40	J-55	BTC	0	970	0	970
8 3/4	7 5/8	29.7	P110HP	TALON SFC	0	11510	0	11510
6 3/4	5 1/2	20	P110HP	TALON RD	0	25081	0	12103

2. Casing Program (Primary Design)

•All casing strings will be tested in accordance with 43 CFR 3172.

3. Cementing Program (Primary Design)

Assuming no returns are established while drilling, Devon requests to pump a two stage cement job on the intermediate casing string with the first stage being pumped conventionally with the calculated top of cement at the Brushy Canyon and the second stage performed as a bradenhead squeeze with planned cement from the Brushy Canyon to surface. The final cement top will be verified by Echo-meter. Devon will include the Echo-meter verified fluid top and the volume of displacement fluid above the cement slurry in the annulus in all post-drill sundries on wells utilizing this cement program. Devon will report to the BLM the volume of fluid (limited to 1 bbls) used to flush intermediate casing valves following backside cementing procedures

Casing	# Sks	тос	Wt. ppg	Yld (ft3/sack)	Slurry Description
Surface	512	Surf	13.2	1.44	Lead: Class C Cement + additives
Int 1	376	Surf	13.0	2.3	2nd State: Bradenhead Squeeze - Lead: Class C Cement + additives
	436	6784	13.2	1.44	Tail: Class H / C + additives
Production	62	9610	9	3.27	Lead: Class H /C + additives
	859	11610	13.2	1.44	Tail: Class H / C + additives

Devon Energy requests to offline cement on intermediate strings that are set in formations shallower than the Wolfcamp. Prior to commencing offline cementing operations, the well will be monitored for any abnormal pressures and confirmed to be static. A dual manifold system (equipped with chokes) for the returns will also be utilized as a redundancy. All equipment used for offline cementing will have a minimum 5M rating to match intermediate sections' 5M BOPE requirements

Casing String	% Excess
Surface	50%
Intermediate 1	30%
Prod	10%

		Wt			Casing	Interval	Casing Interval	
Hole Size	Csg. Size	(PPF)	Grade Conn		From (MD)	To (MD)	From (TVD)	To (TVD)
14 3/4	10 3/4	45 1/2	J-55	BTC	0	970	0	970
9 7/8	8 5/8	32	P110	Sprint FJ	0	11510	0	11510
7 7/8	5 1/2	20	P110	DWC / C-IS+	0	25081	0	12103

2. Casing Program (Secondary Design)

•All casing strings will be tested in accordance with 43 CFR 3172. Must have table for contingency casing.

3. Cementing Program (Secondary Design)

Assuming no returns are established while drilling, Devon requests to pump a two stage cement job on the intermediate casing string with the first stage being pumped conventionally with the calculated top of cement at the Brushy Canyon and the second stage performed as a bradenhead squeeze with planned cement from the Brushy Canyon to surface. The final cement top will be verified by Echo-meter. Devon will include the Echo-meter verified fluid top and the volume of displacement fluid above the cement slurry in the annulus in all post-drill sundries on wells utilizing this cement program. Devon will report to the BLM the volume of fluid (limited to 1 bbls) used to flush intermediate casing valves following backside cementing procedures.

Casing	# Sks	тос	Wt. ppg	Yld (ft3/sack)	Slurry Description
Surface	586	Surf	13.2	1.44	Lead: Class C Cement + additives
Int 1	476	Surf	13.0	2.3	2nd State: Bradenhead Squeeze - Lead: Class C Cement + additives
	548	6784	13.2	1.44	Tail: Class H / C + additives
Droduction	117	9610	9	3.27	Lead: Class H /C + additives
Production	1783	11610	13.2	1.44	Tail: Class H / C + additives

Casing String	% Excess
Surface	50%
Intermediate 1	30%
Prod	10%

.

BOP installed and tested before drilling which hole?	Size?	Min. Required WP	Туре		~	Tested to:	
			Annular		X	50% of rated working pressure	
Int 1	13-5/8"	5M		d Ram	Х		
Int I	15 5/0	5101	Pipe	e Ram		5M	
			Doub	le Ram	X	5101	
			Other*				
	13-5/8"		Annul	Annular (5M)		100% of rated working pressure	
Production		10M	Blind Ram		Х		
Fioduction		10101	Pipe Ram Double Ram			10M	
					Х	10141	
			Other*				
			Annul	ar (5M)			
		Blind Ram					
			Pipe	e Ram			
			Double Ram				
			Other*				
N A variance is requested for	A variance is requested for the use of a diverter on the surface casing. See attached for schematic.						
Y A variance is requested to r	A variance is requested to run a 5 M annular on a 10M system						

4. Pressure Control Equipment (Three String Design)

5. Mud Program (Three String Design)

Section	Туре	Weight (ppg)
Surface	FW Gel	8.5-9
Intermediate	DBE / Cut Brine	10-10.5
Production	OBM	10-10.5

Sufficient mud materials to maintain mud properties and meet minimum lost circulation and weight increase requirements will be kept on location at all times.

What will be used to monitor the loss or gain of fluid?	PVT/Pason/Visual Monitoring

6. Logging and Testing Procedures

Logging,	Logging, Coring and Testing						
	Will run GR/CNL from TD to surface (horizontal well - vertical portion of hole). Stated logs run will be in the						
Х	Completion Rpeort and sbumitted to the BLM.						
	No logs are planned based on well control or offset log information.						
	Drill stem test? If yes, explain.						
	Coring? If yes, explain.						

Additiona	al logs planned	Interval
	Resistivity	Int. shoe to KOP
	Density	Int. shoe to KOP
Х	CBL	Production casing
Х	Mud log	Intermediate shoe to TD
	PEX	

7. Drilling Conditions

Condition	Specfiy what type and where?				
BH pressure at deepest TVD	6608				
Abnormal temperature	No				
$\mathbf{M}' \mathbf{a}' \mathbf{a} \mathbf{a} \mathbf{a}' \mathbf{a} \mathbf{a} \mathbf{a} \mathbf{a} \mathbf{a} \mathbf{a} \mathbf{a} \mathbf{a}$	Mitianting management and things Describe Last simulation material/manage/mud account and				

Mitigation measure for abnormal conditions. Describe. Lost circulation material/sweeps/mud scavengers.

 Hydrogren Sulfide (H2S) monitors will be installed prior to drilling out the surface shoe. If H2S is detected in concentrations greater than 100 ppm, the operator will comply with the provisions of 43 CFR 3176. If Hydrogen Sulfide is encountered measured values and formations will be provided to the BLM.

 N
 H2S is present

Y H2S plan attached.

8. Other facets of operation

Is this a walking operation? Potentially

- 1 If operator elects, drilling rig will batch drill the surface holes and run/cement surface casing; walking the rig to next wells on the pad.
- 2 The drilling rig will then batch drill the intermediate sections and run/cement intermediate casing; the wellbore will be isolated with a blind flange and pressure gauge installed for monitoring the well before walking to the next well.
- 3 The drilling rig will then batch drill the production hole sections on the wells with OBM, run/cement production casing, and install TA caps or tubing heads for completions.

NOTE: During batch operations the drilling rig will be moved from well to well however, it will not be removed from the pad until all wells have production casing run/cemented.

Will be pre-setting casing? Potentially

- 1 Spudder rig will move in and batch drill surface hole.
 - a. Rig will utilize fresh water based mud to drill surface hole to TD. Solids control will be handled entirely on a closed loop basis.,
- 2 After drilling the surface hole section, the spudder rig will run casing and cement following all of the applicable rules and regulations (43 CFR 3172, all COAs and NMOCD regulations).

 3 The wellhead will be installed and tested once the surface casing is cut off and the WOC time has been reached.

- 4 A blind flange with the same pressure rating as the wellhead will be installed to seal the wellbore. Pressure will be monitored with a pressure gauge installed on the wellhead.
- 5 Spudder rig operations is expected to take 4-5 days per well on a multi-well pa.
- 6 The NMOCD will be contacted and notified 24 hours prior to commencing spudder rig operations.
- 7 Drilling operations will be performed with drilling rig. A that time an approved BOP stack will be nippled up and tested on the wellhead before drilling operations commences on each well.
 - a. The NMOCD will be contacted / notified 24 hours before the drilling rig moves back on to the pad with the pre-set surface casing.

Attachments

X Directional Plan Other, describe U.S. Department of the Interior BUREAU OF LAND MANAGEMENT

Well Name	Well Number	US Well Number	Lease Number	Case Number	Operator
MORGAN 25-13	625H	3001555638	NMLC062300	NMLC062300	DEVON
MORGAN 25-13	735H	3001555642	NMLC062300	NMLC062300	DEVON

Notice of Intent

Sundry ID: 2833338

Type of Submission: Notice of Intent

Date Sundry Submitted: 01/23/2025

Date proposed operation will begin: 01/23/2025

Type of Action: APD Change

Time Sundry Submitted: 08:27

Sundry Print Repor

Procedure Description: Devon Energy Production Co., L.P. (Devon) respectfully requests to change the drilling plan with casing changes and slim hole design for the Morgan 25-13 Fed Com 625H and 735H. Devon would also like to request offline cementing and break test variances. Please see attachments. Batch sundry to only include attachments by pad for the drilling plan for the deepest well (TVD).

NOI Attachments

Procedure Description

Offline_Cementing___Variance_Request_20250123082430.pdf

break_test_variance_BOP_1_15_24_20250123082412.pdf

5.5_20lb_P110HP_TALON_RD_20250123082350.pdf

7.625_29.7lb_P110_HP_Talon_SFC_20250123082327.pdf

9.625_40lb_J55_SeAH_20250123082308.pdf

MORGAN_25_13_FED_COM_735H_rev1_20250123082228.pdf

Signed on: JAN 23, 2025 08:24 AM

Operator

I certify that the foregoing is true and correct. Title 18 U.S.C. Section 1001 and Title 43 U.S.C. Section 1212, make it a crime for any person knowingly and willfully to make to any department or agency of the United States any false, fictitious or fraudulent statements or representations as to any matter within its jurisdiction. Electronic submission of Sundry Notices through this system satisfies regulations requiring a

Operator Electronic Signature: AMY BROWN Name: DEVON ENERGY PRODUCTION COMPANY LP Title: Regulatory Professional Street Address: 333 WEST SHERIDAN AVENUE City: OKLAHOMA CITY State: OK Phone: (405) 552-6137 Email address: AMY.BROWN@DVN.COM **Field**

State:

Representative Name:

Street Address:

City:

Phone:

Email address:

Zip:

PECOS DISTRICT DRILLING CONDITIONS OF APPROVAL

OPERATOR'S NAME:	Devon Energy Production Company LP -
LOCATION:	Section 25, T.25 S., R.31 E., NMPM
COUNTY:	Eddy County, New Mexico
-	
WELL NAME & NO.:	Morgan 25-13 Fed Com 625H
ATS/API ID:	3001555638
APD ID:	10400097838
Sundry ID:	2833338
WELL NAME & NO.:	Morgan 25-13 Fed Com 735H
ATS/API ID:	3001555642
APD ID:	10400097830
Sundry ID:	2833338

COA

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Primary Desig	<u>, , , , , , , , , , , , , , , , , , , </u>		
H2S	No		
Potash	None 🔻	None	
Cave/Karst Potential	Medium 💌		
Cave/Karst Potential	Critical		
Variance	C None	🖸 Flex Hose	C Other
Wellhead	Conventional and Multibov	vl 🔽	
Other	□ 4 String □ 5 String	Capitan Reef	□ WIPP
		None 🔻	
Other	Pilot Hole None	Open Annulus	
Cementing	Contingency Squeeze	Echo-Meter	Primary Cement Squeeze None
Special Requirements	□ Water Disposal/Injection	COM	Unit Unit
Special	Batch Sundry	Waste Prevention	
Requirements		None 🔽	
Special	BOPE Break Testing	✓ Offline	Casing
Requirements Variance	□ Offline BOPE Testing	Cementing	Clearance

Primary Design:

•

Alternate Design:

Potash	None	None	
Cave/Karst Potential	Medium 💌		
Cave/Karst Potential	Critical		
Other	□ 4 String □ 5 String	Capitan Reef None	WIPP
Other	Pilot Hole None	Open Annulus	
Cementing	Contingency Squeeze	Echo-Meter	Primary Cement Squeeze None

A. HYDROGEN SULFIDE

Hydrogen Sulfide (H2S) monitors shall be installed prior to drilling out the surface shoe. If H2S is detected in concentrations greater than 100 ppm, the Hydrogen Sulfide area shall meet **43 CFR part 3170 Subpart 3176**, which includes equipment and personnel/public protection items. If Hydrogen Sulfide is encountered, provide measured values and formations to the BLM.

Primary Design

B. CASING

- 1. The 9-5/8 inch surface casing shall be set at approximately 1030 feet (a minimum of 70 feet (Eddy County) into the Rustler Anhydrite and above the salt when present, and below usable fresh water) and cemented to the surface. The surface hole shall be 13 1/2 inch in diameter.
 - a. If cement does not circulate to the surface, the appropriate BLM office shall be notified and a temperature survey utilizing an electronic type temperature survey with surface log readout will be used or a cement bond log shall be run to verify the top of the cement. Temperature survey will be run a minimum of six hours after pumping cement and ideally between 8-10 hours after completing the cement job.
 - b. Wait on cement (WOC) time for a primary cement job will be a minimum of <u>8</u> <u>hours</u> or 500 pounds compressive strength, whichever is greater. (This is to include the lead cement)
 - c. Wait on cement (WOC) time for a remedial job will be a minimum of 4 hours after bringing cement to surface or 500 pounds compressive strength, whichever is greater.
 - d. If cement falls back, remedial cementing will be done prior to drilling out that string.
- 2. The minimum required fill of cement behind the **7-5/8** inch intermediate casing is:

Option 1 (Single Stage):

• Cement to surface. If cement does not circulate see B.1.a, c-d above. Wait on cement (WOC) time for a primary cement job is to include the lead cement slurry due to cave/karst or potash.

Option 2:

Operator has proposed to cement in two stages by conventionally cementing the first stage and performing a bradenhead squeeze on the second stage, contingent upon no returns to surface.

- a. First stage: Operator will cement with intent to reach the top of the **Brushy** Canyon at 6754'.
- b. Second stage:
 - Operator will perform bradenhead squeeze and top-out. Cement to surface. If cement does not reach surface, the appropriate BLM office shall be notified. (Squeeze 376 sxs Class C)
 Wait on cement (WOC) time for a primary cement job is to include the lead cement slurry due to cave/karst or potash.

Operator has proposed to pump down **9-5/8**" X **7-5/8**" annulus after primary cementing stage. <u>Operator must run Echo-meter to verify Cement Slurry/Fluid top in the annulus Or operator shall run a CBL from TD of the **7-5/8**" casing to surface after the second stage <u>BH to verify TOC.</u></u>

Submit results to the BLM. No displacement fluid/wash out shall be utilized at the top of the cement slurry between second stage BH and top out. Operator must run one CBL per Well Pad. Operator may conduct a negative and positive pressure test during completion to remediate sustained casing pressure.

If cement does not reach surface, the next casing string must come to surface.

Operator must use a limited flush fluid volume of 1 bbl following backside cementing procedures.

- In <u>Medium Cave/Karst Areas</u> if cement does not circulate to surface on the first two casing strings, the cement on the 3rd casing string must come to surface.
- 3. The minimum required fill of cement behind the 5-1/2 inch production casing is:
 - Cement should tie-back at least 200 feet into previous casing string. Operator shall provide method of verification.
 Wait on cement (WOC) time for a primary cement job is to include the lead cement slurry due to cave/karst or potash.

Alternate Design

C. CASING

- 4. The 10-3/4 inch surface casing shall be set at approximately 1030 feet (a minimum of 70 feet (Eddy County) into the Rustler Anhydrite and above the salt when present, and below usable fresh water) and cemented to the surface. The surface hole shall be 14 3/4 inch in diameter.
 - e. If cement does not circulate to the surface, the appropriate BLM office shall be notified and a temperature survey utilizing an electronic type temperature

survey with surface log readout will be used or a cement bond log shall be run to verify the top of the cement. Temperature survey will be run a minimum of six hours after pumping cement and ideally between 8-10 hours after completing the cement job.

- f. Wait on cement (WOC) time for a primary cement job will be a minimum of $\underline{\mathbf{8}}$ <u>hours</u> or 500 pounds compressive strength, whichever is greater. (This is to include the lead cement)
- g. Wait on cement (WOC) time for a remedial job will be a minimum of 4 hours after bringing cement to surface or 500 pounds compressive strength, whichever is greater.
- h. If cement falls back, remedial cementing will be done prior to drilling out that string.

Intermediate casing must be kept fluid filled to meet BLM minimum collapse requirement.

5. The minimum required fill of cement behind the 8-5/8 inch intermediate casing is:

Option 1 (Single Stage):

• Cement to surface. If cement does not circulate see B.1.a, c-d above. Wait on cement (WOC) time for a primary cement job is to include the lead cement slurry due to cave/karst or potash.

Option 2:

Operator has proposed to cement in two stages by conventionally cementing the first stage and performing a bradenhead squeeze on the second stage, contingent upon no returns to surface.

- c. First stage: Operator will cement with intent to reach the top of the **Brushy** Canyon at 6754'.
- d. Second stage:
 - Operator will perform bradenhead squeeze and top-out. Cement to surface. If cement does not reach surface, the appropriate BLM office shall be notified. (Squeeze 476 sxs Class C)
 Wait on cement (WOC) time for a primary cement job is to include the lead cement slurry due to cave/karst or potash.

Operator has proposed to pump down **10-3/4**" X **8-5/8**" annulus after primary cementing stage. <u>Operator must run Echo-meter to verify Cement Slurry/Fluid top in the annulus Or operator shall run a CBL from TD of the **8-5/8**" casing to surface after the second stage <u>BH to verify TOC.</u></u>

Submit results to the BLM. No displacement fluid/wash out shall be utilized at the top of the cement slurry between second stage BH and top out. Operator must run one CBL per Well Pad. Operator may conduct a negative and positive pressure test during completion to remediate sustained casing pressure.

If cement does not reach surface, the next casing string must come to surface.

Operator must use a limited flush fluid volume of 1 bbl following backside cementing procedures.

- In <u>Medium Cave/Karst Areas</u> if cement does not circulate to surface on the first two casing strings, the cement on the 3rd casing string must come to surface.
- 6. The minimum required fill of cement behind the 5-1/2 inch production casing is:
 - Cement should tie-back at least 200 feet into previous casing string. Operator shall provide method of verification.
 Wait on cement (WOC) time for a primary cement job is to include the lead cement slurry due to cave/karst or potash. Cement excess is less than 25%, more cement is required if washout occurs. Adjust cement volume and excess based on a fluid caliper or similar method that reflects the as-drilled size of the wellbore.

D. PRESSURE CONTROL

- 1. Variance approved to use flex line from BOP to choke manifold. Manufacturer's specification to be readily available. No external damage to flex line. Flex line to be installed as straight as possible (no hard bends).'
- 2.

Option 1:

- a. Minimum working pressure of the blowout preventer (BOP) and related equipment (BOPE) required for drilling below the surface casing shoe shall be **5000 (5M)** psi. Annular which shall be tested to **5000 (5M)** psi.
- b. Minimum working pressure of the blowout preventer (BOP) and related equipment (BOPE) required for drilling below the 8-5/8 inch or the 7-5/8 inch intermediate casing shoe shall be 10,000 (10M) psi. Variance is approved to use a 5000 (5M) Annular which shall be tested to 5000 (5M) psi.

Option 2:

Operator has proposed a multi-bowl wellhead assembly. This assembly will only be tested when installed on the **9-5/8** inch surface casing. Minimum working pressure of the blowout preventer (BOP) and related equipment (BOPE) required for drilling below the surface casing shoe shall be **10,000 (10M)** psi. Variance is approved to use a 5000 (5M) Annular which shall be tested to 5000 (5M) psi.

- a. Wellhead shall be installed by manufacturer's representatives, submit documentation with subsequent sundry.
- b. If the welding is performed by a third party, the manufacturer's representative shall monitor the temperature to verify that it does not exceed the maximum temperature of the seal.
- c. Manufacturer representative shall install the test plug for the initial BOP test.
- d. If the cement does not circulate and one inch operations would have been possible with a standard wellhead, the well head shall be cut off, cementing operations performed and another wellhead installed.
- e. Whenever any seal subject to test pressure is broken, all the tests in 43 CFR 3172.6(b)(9) must be followed.

Option 3:

Operator has proposed a multi-bowl wellhead assembly. This assembly will only be tested when installed on the **10-3/4** inch surface casing. Minimum working pressure of the blowout preventer (BOP) and related equipment (BOPE) required for drilling below the surface casing shoe shall be **10,000** (**10M**) psi. Variance is approved to use a **5000** (**5M**) Annular which shall be tested to **5000** (**5M**) psi.

- a. Wellhead shall be installed by manufacturer's representatives, submit documentation with subsequent sundry.
 - b. If the welding is performed by a third party, the manufacturer's representative shall monitor the temperature to verify that it does not exceed the maximum temperature of the seal.
 - c. Manufacturer representative shall install the test plug for the initial BOP test.
 - d. If the cement does not circulate and one inch operations would have been possible with a standard wellhead, the well head shall be cut off, cementing operations performed and another wellhead installed.
 - e. Whenever any seal subject to test pressure is broken, all the tests in 43 CFR 3172.6(b)(9) must be followed.

E. SPECIAL REQUIREMENT (S)

Communitization Agreement

- The operator will submit a Communitization Agreement to the Santa Fe Office, 301 Dinosaur Trail Santa Fe, New Mexico 87508, at least 90 days before the anticipated date of first production from a well subject to a spacing order issued by the New Mexico Oil Conservation Division. The Communitization Agreement will include the signatures of all working interest owners in all Federal and Indian leases subject to the Communitization Agreement (i.e., operating rights owners and lessees of record), or certification that the operator has obtained the written signatures of all such owners and will make those signatures available to the BLM immediately upon request.
- The operator will submit an as-drilled survey well plat of the well completion, but are not limited to, those specified in 43 CFR part 3170 Subpart 3171
- If the operator does not comply with this condition of approval, the BLM may take enforcement actions that include, but are not limited to, those specified in 43 CFR 3163.1.
- In addition, the well sign shall include the surface and bottom hole lease numbers. <u>When the Communitization Agreement number is known, it shall also be on the sign.</u>

BOPE Break Testing Variance (Approved)

- BOPE Break Testing is ONLY permitted for 5M BOPE or less. (Annular preventer must be tested to a minimum of 70% of BOPE working pressure and shall be higher than the MASP)
- BOPE Break Testing is NOT permitted to drilling the production hole section.
- Variance only pertains to the intermediate hole-sections and no deeper than the Bone Springs formation.
- While in transfer between wells, the BOPE shall be secured by the hydraulic carrier or cradle.
- Any well control event while drilling require notification to the BLM Petroleum Engineer (575-706-2779) prior to the commencement of any BOPE Break Testing operations.
- A full BOPE test is required prior to drilling the first deep intermediate hole section. If any subsequent hole interval is deeper than the first, a full BOPE test will be required. (200' TVD tolerance between intermediate shoes is allowable).
- The BLM is to be contacted (575-361-2822 Eddy County) 4 hours prior to BOPE tests.
- As a minimum, a full BOPE test shall be performed at **21**-day intervals.
- In the event any repairs or replacement of the BOPE is required, the BOPE shall test as per **43 CFR part 3170 Subpart 3172**.
- If in the event break testing is not utilized, then a full BOPE test would be conducted.

Offline Cementing

Operator has been (**Approved**) to pump the proposed cement program offline in the **Intermediate(s) interval**.

Offline cementing should commence within 24 hours of landing the casing for the interval.

Notify the BLM 4hrs prior to cementing offline at Eddy County: 575-361-2822.

Batch Sundry:

- Approval shall be for wells with surface, intermediate, and production section within 200' TVD tolerance between shoes above the deepest well shoe(s) set depth.
- Approval shall be for wells with same drill plan design. (Casing depth may vary and cement volumes may vary per Condition of Approval.)
- Approval shall be for wells within the same drill pad.
- Cement excess shall be a minimum of 25%, adjust cement volume and excess based on a fluid caliper or similar method that reflects the as-drilled size of the wellbore.

GENERAL REQUIREMENTS

The BLM is to be notified in advance for a representative to witness:

- a. Spudding well (minimum of 24 hours)
- b. Setting and/or Cementing of all casing strings (minimum of 4 hours)
- c. BOPE tests (minimum of 4 hours)

Eddy County EMAIL or call the Carlsbad Field Office, 620 East Greene St., Carlsbad, NM 88220,

BLM_NM_CFO_DrillingNotifications@BLM.GOV (575) 361-2822

- 1. Unless the production casing has been run and cemented or the well has been properly plugged, the drilling rig shall not be removed from over the hole without prior approval.
 - a. In the event the operator has proposed to drill multiple wells utilizing a skid/walking rig. Operator shall secure the wellbore on the current well, after installing and testing the wellhead, by installing a blind flange of like pressure rating to the wellhead and a pressure gauge that can be monitored while drilling is performed on the other well(s).
 - b. When the operator proposes to set surface casing with Spudder Rig
 - Notify the BLM when moving in and removing the Spudder Rig.
 - Notify the BLM when moving in the 2nd Rig. Rig to be moved in within 90 days of notification that Spudder Rig has left the location.
 - BOP/BOPE test to be conducted per **43** CFR part **3170** Subpart **3172** as soon as 2nd Rig is rigged up on well.
- 2. Floor controls are required for 3M or Greater systems. These controls will be on the rig floor, unobstructed, readily accessible to the driller and will be operational at all times during drilling and/or completion activities. Rig floor is defined as the area immediately around the rotary table; the area immediately above the substructure on which the draw works are located, this does not include the dog house or stairway area.

A. CASING

1. Changes to the approved APD casing program need prior approval if the items substituted are of lesser grade or different casing size or are Non-API. The Operator can exchange the components of the proposal with that of superior strength (i.e. changing from J-55 to N-80, or from 36# to 40#). Changes to the approved cement program need prior approval if the altered cement plan has less volume or strength or

if the changes are substantial (i.e. Multistage tool, ECP, etc.). The initial wellhead installed on the well will remain on the well with spools used as needed.

- <u>Wait on cement (WOC) for Potash Areas:</u> After cementing but before commencing any tests, the casing string shall stand cemented under pressure until both of the following conditions have been met: 1) cement reaches a minimum compressive strength of 500 psi for all cement blends of both lead and tail cement, 2) until cement has been in place at least <u>8 hours</u>. WOC time will be recorded in the driller's log. The casing integrity test can be done (prior to the cement setting up) immediately after bumping the plug.
- 3. <u>Wait on cement (WOC) for Water Basin:</u> After cementing but before commencing any tests, the casing string shall stand cemented under pressure until both of the following conditions have been met: 1) cement reaches a minimum compressive strength of 500 psi at the shoe, 2) until cement has been in place at least <u>8 hours</u>. WOC time will be recorded in the driller's log. See individual casing strings for details regarding lead cement slurry requirements. The casing integrity test can be done (prior to the cement setting up) immediately after bumping the plug.
- 4. Provide compressive strengths including hours to reach required 500 pounds compressive strength prior to cementing each casing string. Have well specific cement details onsite prior to pumping the cement for each casing string.
- 5. No pea gravel permitted for remedial or fall back remedial without prior authorization from the BLM engineer.
- 6. On that portion of any well approved for a 5M BOPE system or greater, a pressure integrity test of each casing shoe shall be performed. Formation at the shoe shall be tested to a minimum of the mud weight equivalent anticipated to control the formation pressure to the next casing depth or at total depth of the well. This test shall be performed before drilling more than 20 feet of new hole.
- 7. If hardband drill pipe is rotated inside casing, returns will be monitored for metal. If metal is found in samples, drill pipe will be pulled and rubber protectors which have a larger diameter than the tool joints of the drill pipe will be installed prior to continuing drilling operations.
- 8. Whenever a casing string is cemented in the R-111-P potash area, the NMOCD requirements shall be followed.
- B. PRESSURE CONTROL
- All blowout preventer (BOP) and related equipment (BOPE) shall comply with well control requirements as described in 43 CFR part 3170 Subpart 3172 and API STD 53 Sec. 5.3.

- 2. If a variance is approved for a flexible hose to be installed from the BOP to the choke manifold, the following requirements apply: The flex line must meet the requirements of API 16C. Check condition of flexible line from BOP to choke manifold, replace if exterior is damaged or if line fails test. Line to be as straight as possible with no hard bends and is to be anchored according to Manufacturer's requirements. The flexible hose can be exchanged with a hose of equal size and equal or greater pressure rating. Anchor requirements, specification sheet and hydrostatic pressure test certification matching the hose in service, to be onsite for review. These documents shall be posted in the company man's trailer and on the rig floor.
- 3. 5M or higher system requires an HCR valve, remote kill line and annular to match. The remote kill line is to be installed prior to testing the system and tested to stack pressure.
- 4. If the operator has proposed a multi-bowl wellhead assembly in the APD. The following requirements must be met:
 - a. Wellhead shall be installed by manufacturer's representatives, submit documentation with subsequent sundry.
 - b. If the welding is performed by a third party, the manufacturer's representative shall monitor the temperature to verify that it does not exceed the maximum temperature of the seal.
 - c. Manufacturer representative shall install the test plug for the initial BOP test.
 - d. Whenever any seal subject to test pressure is broken, all the tests in 43 CFR 3172.6(b)(9) must be followed.
 - e. If the cement does not circulate and one inch operations would have been possible with a standard wellhead, the well head shall be cut off, cementing operations performed and another wellhead installed.
- 5. The appropriate BLM office shall be notified a minimum of 4 hours in advance for a representative to witness the tests.
 - a. In a water basin, for all casing strings utilizing slips, these are to be set as soon as the crew and rig are ready and any fallback cement remediation has been done. The casing cut-off and BOP installation can be initiated four hours after installing the slips, which will be approximately six hours after bumping the plug. For those casing strings not using slips, the minimum wait time before cut-off is eight hours after bumping the plug. BOP/BOPE testing can begin after cut-off or once cement reaches 500 psi compressive strength (including lead cement), whichever is greater. However, if the float does not hold, cut-off cannot be initiated until cement reaches 500 psi compressive strength (including lead when specified).
 - b. In potash areas, for all casing strings utilizing slips, these are to be set as soon as the crew and rig are ready and any fallback cement remediation has been

done. For all casing strings, casing cut-off and BOP installation can be initiated at twelve hours after bumping the cement plug. The BOPE test can be initiated after bumping the cement plug with the casing valve open. (only applies to single stage cement jobs, prior to the cement setting up.)

- c. The tests shall be done by an independent service company utilizing a test plug not a cup or J-packer and can be initiated immediately with the casing valve open. The operator also has the option of utilizing an independent tester to test without a plug (i.e. against the casing) pursuant to 43 CFR part 3170 Subpart 3172 with the pressure not to exceed 70% of the burst rating for the casing. Any test against the casing must meet the WOC time for 8 hours or 500 pounds compressive strength, whichever is greater, prior to initiating the test (see casing segment as lead cement may be critical item).
- d. The test shall be run on a 5000 psi chart for a 2-3M BOP/BOP, on a 10000 psi chart for a 5M BOP/BOPE and on a 15000 psi chart for a 10M BOP/BOPE. If a linear chart is used, it shall be a one hour chart. A circular chart shall have a maximum 2 hour clock. If a twelve hour or twenty-four hour chart is used, tester shall make a notation that it is run with a two hour clock.
- e. The results of the test shall be reported to the appropriate BLM office.
- f. All tests are required to be recorded on a calibrated test chart. A copy of the BOP/BOPE test chart and a copy of independent service company test will be submitted to the appropriate BLM office.
- g. The BOP/BOPE test shall include a low pressure test from 250 to 300 psi. The test will be held for a minimum of 10 minutes if test is done with a test plug and 30 minutes without a test plug. This test shall be performed prior to the test at full stack pressure.
- h. BOP/BOPE must be tested by an independent service company within 500 feet of the top of the Wolfcamp formation if the time between the setting of the intermediate casing and reaching this depth exceeds 20 days. This test does not exclude the test prior to drilling out the casing shoe as per 43 CFR part 3170 Subpart 3172.

C. DRILLING MUD

Mud system monitoring equipment, with derrick floor indicators and visual and audio alarms, shall be operating before drilling into the Wolfcamp formation, and shall be used until production casing is run and cemented.

D. WASTE MATERIAL AND FLUIDS

All waste (i.e. drilling fluids, trash, salts, chemicals, sewage, gray water, etc.) created as a result of drilling operations and completion operations shall be safely contained and disposed of properly at a waste disposal facility. No waste material or fluid shall be disposed of on the well location or surrounding area.

Porto-johns and trash containers will be on-location during fracturing operations or any other crew-intensive operations.

Long Vo (LVO) 1/30/2025

Received by OCD: 2/6/2025 1:28:34 PM

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Form 3160-5 (June 2019)		UNITED STATES DEPARTMENT OF THE INTERIOR UREAU OF LAND MANAGEMENT		FORM APPROVED OMB No. 1004-0137 Expires: October 31, 2021 5. Lease Serial No.	
Do not	UNDRY N use this f	IOTICES AND REPO		6. If Indian, Allottee or Tribe N	ame
	SUBMIT IN T	TRIPLICATE - Other instru	uctions on page 2	7. If Unit of CA/Agreement, Na	ame and/or No.
1. Type of Well Oil Well	Gas W	Vell Other		8. Well Name and No.	
2. Name of Operator				9. API Well No.	
3a. Address			3b. Phone No. (include area code)	10. Field and Pool or Explorate	bry Area
4. Location of Well (Foot	age, Sec., T.,K	R.,M., or Survey Description))	11. Country or Parish, State	
	12. CHE	CK THE APPROPRIATE B	OX(ES) TO INDICATE NATURE (J OF NOTICE, REPORT OR OTH	ER DATA
TYPE OF SUBMIS	SSION		TYPE	E OF ACTION	
Notice of Intent		Acidize	Deepen [Hydraulic Fracturing	Production (Start/Resume) Reclamation	Water Shut-Off Well Integrity
Subsequent Report	;	Casing Repair Change Plans	New Construction [Recomplete	Other
Final Abandonmen	t Notice	Convert to Injection	Plug Back	Water Disposal	
the proposal is to deep the Bond under which completion of the invo	pen directiona a the work wil olved operation ndonment No	lly or recomplete horizontal l be perfonned or provide thons. If the operation results in	ly, give subsurface locations and me e Bond No. on file with BLM/BIA. 1 n a multiple completion or recomple	easured and true vertical depths of Required subsequent reports mus etion in a new interval, a Form 31	k and approximate duration thereof. If f all pertinent markers and zones. Attach t be filed within 30 days following 60-4 must be filed once testing has been he operator has detennined that the site

14. I hereby certify that the foregoing is true and correct. Name (<i>Printed/Typed</i>)			
	Title		
Signature	Date		
THE SPACE FOR FEDE	RAL OR STATE O	OFICE USE	
Approved by			
	Title	Date	
Conditions of approval, if any, are attached. Approval of this notice does not warrant of certify that the applicant holds legal or equitable title to those rights in the subject lease which would entitle the applicant to conduct operations thereon.			
Title 18 U.S.C Section 1001 and Title 43 U.S.C Section 1212, make it a crime for any any false, fictitious or fraudulent statements or representations as to any matter within		villfully to make to any department or agency of the United S	States

(Instructions on page 2)

This form is designed for submitting proposals to perform certain well operations and reports of such operations when completed as indicated on Federal and Indian lands pursuant to applicable Federal law and regulations. Any necessary special instructions concerning the use of this form and the number of copies to be submitted, particularly with regard to local area or regional procedures and practices, are either shown below, will be issued by or may be obtained from the local Federal office.

SPECIFIC INSTRUCTIONS

Item 4 - Locations on Federal or Indian land should be described in accordance with Federal requirements. Consult the local Federal office for specific instructions.

Item 13: Proposals to abandon a well and subsequent reports of abandonment should include such special information as is required by the local Federal office. In addition, such proposals and reports should include reasons for the abandonment; data on any former or present productive zones or other zones with present significant fluid contents not sealed off by cement or otherwise; depths (top and bottom) and method of placement of cement plugs; mud or other material placed below, between and above plugs; amount, size, method of parting of any casing, liner or tubing pulled and the depth to the top of any tubing left in the hole; method of closing top of well and date well site conditioned for final inspection looking for approval of the abandonment. If the proposal will involve **hydraulic fracturing operations**, you must comply with 43 CFR 3162.3-3, including providing information about the protection of usable water. Operators should provide the best available information about all formations containing water and their depths. This information could include data and interpretation of resistivity logs run on nearby wells. Information may also be obtained from state or tribal regulatory agencies and from local BLM offices.

NOTICES

The privacy Act of 1974 and the regulation in 43 CFR 2.48(d) provide that you be furnished the following information in connection with information required by this application.

AUTHORITY: 30 U.S.C. 181 et seq., 351 et seq., 25 U.S.C. 396; 43 CFR 3160.

PRINCIPAL PURPOSE: The information is used to: (1) Evaluate, when appropriate, approve applications, and report completion of subsequent well operations, on a Federal or Indian lease; and (2) document for administrative use, information for the management, disposal and use of National Resource lands and resources, such as: (a) evaluating the equipment and procedures to be used during a proposed subsequent well operation and reviewing the completed well operations for compliance with the approved plan; (b) requesting and granting approval to perform those actions covered by 43 CFR 3162.3-2, 3162.3-3, and 3162.3-4; (c) reporting the beginning or resumption of production, as required by 43 CFR 3162.4-1(c)and (d) analyzing future applications to drill or modify operations in light of data obtained and methods used.

ROUTINE USES: Information from the record and/or the record will be transferred to appropriate Federal, State, local or foreign agencies, when relevant to civil, criminal or regulatory investigations or prosecutions in connection with congressional inquiries or to consumer reporting agencies to facilitate collection of debts owed the Government.

EFFECT OF NOT PROVIDING THE INFORMATION: Filing of this notice and report and disclosure of the information is mandatory for those subsequent well operations specified in 43 CFR 3162.3-2, 3162.3-3, 3162.3-4.

The Paperwork Reduction Act of 1995 requires us to inform you that:

The BLM collects this information to evaluate proposed and/or completed subsequent well operations on Federal or Indian oil and gas leases.

Response to this request is mandatory.

The BLM would like you to know that you do not have to respond to this or any other Federal agency-sponsored information collection unless it displays a currently valid OMB control number.

BURDEN HOURS STATEMENT: Public reporting burden for this form is estimated to average 8 hours per response, including the time for reviewing instructions, gathering and maintaining data, and completing and reviewing the form. Direct comments regarding the burden estimate or any other aspect of this form to U.S. Department of the Interior, Bureau of Land Management (1004-0137), Bureau Information Collection Clearance Officer (WO-630), 1849 C St., N.W., Mail Stop 401 LS, Washington, D.C. 20240

Additional Information

Batch Well Data

MORGAN 25-13 FED COM 735H, US Well Number: 3001555642, Case Number: NMLC062300, Lease Number: NMLC062300, Operator: DEVON ENERGY PRODUCTION COMPANY LP

MORGAN 25-13 FED COM 625H, US Well Number: 3001555638, Case Number: NMLC062300, Lease Number: NMLC062300, Operator:DEVON ENERGY PRODUCTION COMPANY LP

Offline Cementing

Variance Request

Devon Energy requests to offline cement on intermediate strings that are set in formations shallower than the Wolfcamp. Prior to commencing offline cementing operations, the well will be monitored for any abnormal pressures and confirmed to be static. A dual manifold system (equipped with chokes) for the returns will also be utilized as a redundancy. All equipment used for offline cementing will have a minimum 5M rating to match intermediate sections' 5M BOPE requirements.

Section 2 - Blowout Preventer Testing Procedure

Variance Request

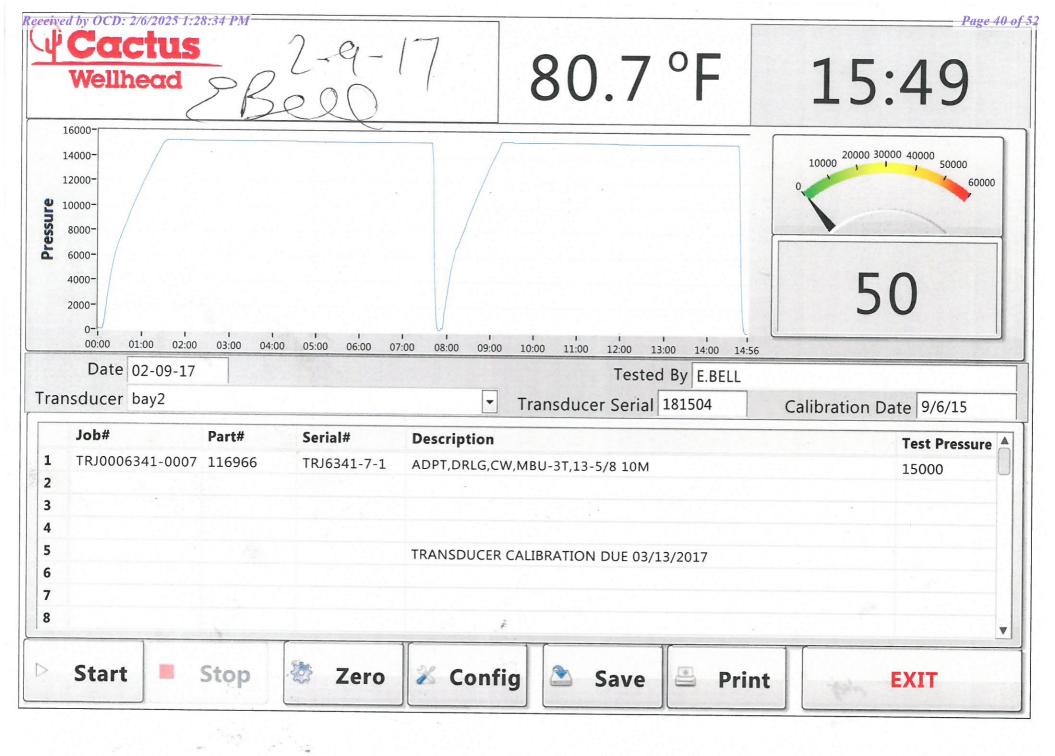
Devon Energy requests to only test BOP connection breaks after drilling out of surface casing and while skidding between wells which conforms to API Standard 53 and industry standards. This test will include the Top Pipe Rams, HCR, Kill Line Check Valve, QDC (quick disconnect to wellhead) and Shell of the 10M BOPE to 5M for 10 minutes. If a break to the flex hose that runs to the choke manifold is required due to repositioning from a skid, the HCR will remain open during the shell test to include that additional break. The variance only pertains to intermediate hole-sections and no deeper than the Bone Springs Formation where 5M BOP tests are required. The initial BOP test will follow 43 CFR 3172, and subsequent tests following a skid will only test connections that are broken. The annular preventer will be tested to 100% working pressure. This variance will meet or exceed 43 CFR 3172 per the following: Devon Energy will perform a full BOP test per 43 CFR 3172 before drilling out of the intermediate casing string(s) and starting the production hole, before starting any hole section that requires a 10M test, before the expiration of the allotted 14-days for 5M intermediate batch drilling or when the drilling rig is fully mobilized to a new well pad, whichever is sooner. We will utilize a 200' TVD tolerance between intermediate shoes as the cutoff for a full BOP test. The BLM will be contacted 4hrs prior to a BOPE test. The BLM will be notified if and when a well control event is encountered. Break test will be a 14 day interval and not a 30 day full BOPE test interval. If in the event break testing is not utilized, then a full BOPE test would be conducted.

1. Well Control Response:

1. Primary barrier remains fluid

2. In the event of an influx due to being underbalanced and after a realized gain or flow, the order of closing BOPE is as follows:

- a) Annular first
- b) If annular were to not hold, Upper pipe rams second (which were tested on the skid BOP test)
- c) If the Upper Pipe Rams were to not hold, Lower Pipe Rams would be third



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RD

U. S. Steel Tubular Products 5.500" 20.00lb/ft (0.361" Wall) P110 H

)/ft (0	.361" Wall)	P110 HP	USS-TALON HTQ™

IECHANICAL PROPERTIES	Pipe	USS-TALON HTQ™ RD		[
Minimum Yield Strength	125,000		psi	
Maximum Yield Strength	140,000		psi	
Minimum Tensile Strength	130,000		psi	
DIMENSIONS	Pipe	USS-TALON HTQ™ RD		
Outside Diameter	5.500	5.900	in.	
Wall Thickness	0.361		in.	
Inside Diameter	4.778	4.778	in.	
Standard Drift	4.653	4.653	in.	
Alternate Drift			in.	
Nominal Linear Weight, T&C	20.00		lb/ft	
Plain End Weight	19.83		lb/ft	
SECTION AREA	Pipe	USS-TALON HTQ™ RD		
Critical Area	5.828	5.828	sq. in.	
Joint Efficiency		100.0	%	
PERFORMANCE	Pipe	USS-TALON HTQ™ RD		
Minimum Collapse Pressure	13,150	13,150	psi	
Minimum Internal Yield Pressure	14,360	14,360	psi	
Minimum Pipe Body Yield Strength	729,000		lb	
Joint Strength		729,000	lb	
Compression Rating		729,000	lb	
Reference Length		24,300	ft	
Maximum Uniaxial Bend Rating		104.2	deg/100 ft	
IAKE-UP DATA	Pipe	USS-TALON HTQ™ RD		
Make-Up Loss		5.58	in.	
Minimum Make-Up Torque		18,400	ft-lb	
Maximum Make-Up Torque		21,400	ft-lb	

Notes

- 1. Other than proprietary collapse and connection values, performance properties have been calculated using standard equations defined by API 5C3 and do not incorporate any additional design or safety factors. Calculations assume nominal pipe OD, nominal wall thickness, and Specified Minimum Yield Strength (SMYS).
- 2. Joint efficiencies are calculated by dividing the connection critical area by the pipe body area.

3. Uniaxial bend rating shown is structural only.

4. Torques have been calculated assuming a thread compound friction factor of 1.0 and are recommended only. Field make-up torques may require adjustment based on actual field conditions (e.g. make-up speed, temperature, thread compound, etc.).

- 5. Reference length is calculated by Joint Strength divided by Nominal Linear Weight, T&C with a 1.5 Safety factor.
- 6. Coupling must meet minimum mechanical properties of the pipe.

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5/15/2024 6:31:14 PM

U. S. Steel Tubular Products 7.625" 29.70lb/ft (0.375" Wall) P110 HP USS-TALON SFC™

MECHANICAL PROPERTIES	Pipe	USS-TALON SFC™		[6
Minimum Yield Strength	125,000		psi	
Maximum Yield Strength	140,000		psi	
Minimum Tensile Strength	130,000		psi	
DIMENSIONS	Pipe	USS-TALON SFC™		
Outside Diameter	7.625	7.900	in.	
Wall Thickness	0.375		in.	
Inside Diameter	6.875	6.815	in.	
Standard Drift	6.750	6.750	in.	
Alternate Drift			in.	
Nominal Linear Weight, T&C	29.70		lb/ft	
Plain End Weight	29.06		lb/ft	
SECTION AREA	Pipe	USS-TALON SFC™		
Critical Area	8.541	7.331	sq. in.	
Joint Efficiency		85.8	%	
PERFORMANCE	Pipe	USS-TALON SFC™		
Minimum Collapse Pressure	7,260	7,260	psi	
Minimum Internal Yield Pressure	10,750	10,750	psi	
Minimum Pipe Body Yield Strength	1,068,000		lb	
Joint Strength		916,000	lb	
Compression Rating		916,000	lb	
Reference Length		20,560	ft	
Maximum Uniaxial Bend Rating		64.4	deg/100 ft	
MAKE-UP DATA	Pipe	USS-TALON SFC™		
Make-Up Loss		5.08	in.	
Minimum Make-Up Torque		30,000	ft-lb	
Maximum Make-Up Torque		33,000	ft-lb	
Maximum Operating Torque		80,500	ft-lb	

1. Other than proprietary collapse and connection values, performance properties have been calculated using standard equations defined by API 5C3 and do not incorporate any additional design or safety factors. Calculations assume nominal pipe OD, nominal wall thickness, and Specified Minimum Yield Strength (SMYS).

2. Joint efficiencies are calculated by dividing the connection critical area by the pipe body area.

3. Uniaxial bend rating shown is structural only.

4. Torques have been calculated assuming a thread compound friction factor of 1.0 and are recommended only. Field make-up torques may require adjustment based on actual field conditions (e.g. make-up speed, temperature, thread compound, etc.).

- 5. Reference length is calculated by Joint Strength divided by Nominal Linear Weight, T&C with a 1.5 Safety factor.
- 6. Coupling must meet minimum mechanical properties of the pipe.

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SěAH 9.625" 40# .395" J-55

Dimensions (Nominal)

Outside Diameter	9.625	in.
Wall	0.395	in.
Inside Diameter	8.835	in.
Drift	8.750	in.
Weight, T&C	40.000	lbs./ft.
Weight, PE	38.970	lbs./ft.

Performance Properties

Collapse, PE	2570	psi
Internal Yield Pressure at Minimum Yield		
PE	3950	psi
LTC	3950	psi
BTC	3950	psi
Yield Strength, Pipe Body	630	1000 lbs.
Joint Strength		
STC	452	1000 lbs.
LTC	520	1000 lbs.
втс	714	1000 lbs.

Note: SeAH Steel has produced this specification sheet for general information only. SeAH does not assume liability or responsibility for any loss or injury resulting from the use of information or data contained herein. All applications for the material described are at the customer's own risk and responsibility.

1. Geologic Formations

TVD of target	12103	Pilot hole depth	N/A
MD at TD:	25081	Deepest expected fresh water	

Basin

	Depth	Water/Mineral	
Formation	(TVD)	Bearing/Target	Hazards*
	from KB	Zone?	
Rustler	945		
Salt	1355		
Base of Salt	4052		
Delaware	4358		
Cherry Canyon	5321		
Brushy Canyon	6754		
Bone Spring 1st	9341		
Bone Spring 2nd	9976		
Bone Spring 3rd	10421		
Wolfcamp	11645		

*H2S, water flows, loss of circulation, abnormal pressures, etc.

MORGAN 25-13 FED COM 735H

		Wt	Grade Conn		Casing	Interval	Casing	Interval
Hole Size	Csg. Size	(PPF)			From (MD)	To (MD)	From (TVD)	To (TVD)
13 1/2	9 5/8	40	J-55	BTC	0	970	0	970
8 3/4	7 5/8	29.7	P110HP	TALON SFC	0	11510	0	11510
6 3/4	5 1/2	20	P110HP	TALON RD	0	25081	0	12103

2. Casing Program (Primary Design)

•All casing strings will be tested in accordance with 43 CFR 3172.

3. Cementing Program (Primary Design)

Assuming no returns are established while drilling, Devon requests to pump a two stage cement job on the intermediate casing string with the first stage being pumped conventionally with the calculated top of cement at the Brushy Canyon and the second stage performed as a bradenhead squeeze with planned cement from the Brushy Canyon to surface. The final cement top will be verified by Echo-meter. Devon will include the Echo-meter verified fluid top and the volume of displacement fluid above the cement slurry in the annulus in all post-drill sundries on wells utilizing this cement program. Devon will report to the BLM the volume of fluid (limited to 1 bbls) used to flush intermediate casing valves following backside cementing procedures

Casing	# Sks	тос	Wt. ppg	Yld (ft3/sack)	Slurry Description
Surface	512	Surf	13.2	1.44	Lead: Class C Cement + additives
Int 1	376	Surf	13.0	2.3	2nd State: Bradenhead Squeeze - Lead: Class C Cement + additives
1111 1	436	6784	13.2	1.44	Tail: Class H / C + additives
Draduation	62	9610	9	3.27	Lead: Class H /C + additives
Production	859	11610	13.2	1.44	Tail: Class H / C + additives

Devon Energy requests to offline cement on intermediate strings that are set in formations shallower than the Wolfcamp. Prior to commencing offline cementing operations, the well will be monitored for any abnormal pressures and confirmed to be static. A dual manifold system (equipped with chokes) for the returns will also be utilized as a redundancy. All equipment used for offline cementing will have a minimum 5M rating to match intermediate sections' 5M BOPE requirements

Casing String	% Excess
Surface	50%
Intermediate 1	30%
Prod	10%

		Wt			Casing	Interval	Casing	Interval
Hole Size	Csg. Size	(PPF)	Grade	Conn	From (MD)	To (MD)	From (TVD)	To (TVD)
14 3/4	10 3/4	45 1/2	J-55	BTC	0	970	0	970
9 7/8	8 5/8	32	P110	Sprint FJ	0	11510	0	11510
7 7/8	5 1/2	20	P110	DWC / C-IS+	0	25081	0	12103

2. Casing Program (Secondary Design)

•All casing strings will be tested in accordance with 43 CFR 3172. Must have table for contingency casing.

3. Cementing Program (Secondary Design)

Assuming no returns are established while drilling, Devon requests to pump a two stage cement job on the intermediate casing string with the first stage being pumped conventionally with the calculated top of cement at the Brushy Canyon and the second stage performed as a bradenhead squeeze with planned cement from the Brushy Canyon to surface. The final cement top will be verified by Echo-meter. Devon will include the Echo-meter verified fluid top and the volume of displacement fluid above the cement slurry in the annulus in all post-drill sundries on wells utilizing this cement program. Devon will report to the BLM the volume of fluid (limited to 1 bbls) used to flush intermediate casing valves following backside cementing procedures.

Casing	# Sks	тос	Wt. ppg	Yld (ft3/sack)	Slurry Description
Surface	586	Surf	13.2	1.44	Lead: Class C Cement + additives
Int 1	476	Surf	13.0	2.3	2nd State: Bradenhead Squeeze - Lead: Class C Cement + additives
Int I	548	6784	13.2	1.44	Tail: Class H / C + additives
Production	117	9610	9	3.27	Lead: Class H /C + additives
Froduction	1783	11610	13.2	1.44	Tail: Class H / C + additives

Casing String	% Excess
Surface	50%
Intermediate 1	30%
Prod	10%

.

BOP installed and tested before drilling which hole?	Size?	Min. Required WP	Туре		~	Tested to:																			
			Anı	nular	X	50% of rated working pressure																			
Int 1	13-5/8"	5M		d Ram	Х																				
Int I	15 5/0	5101	Pipe	e Ram		5M																			
			Doub	le Ram	X	5101																			
			Other*																						
			Annul	Annular (5M)		100% of rated working pressure																			
Production	13-5/8"	10M	Blind Ram		Х																				
Fioduction	13-3/8	10101	10111	10101	1011	10111	10111	10111	10111	10101	10111	10111	10101	10111	10101	10101	10111	10111	1011	10101	10101	Pipe	e Ram		10M
			Doub	le Ram	Х	10141																			
			Other*																						
			Annul	ar (5M)																					
			Blind Ram																						
			Pipe	Pipe Ram																					
			Doub	le Ram																					
			Other*																						
N A variance is requested for	the use of a	a diverter or	n the surface	casing. See	attached for	schematic.																			
Y A variance is requested to r	un a 5 M a	nnular on a	10M system																						

4. Pressure Control Equipment (Three String Design)

5. Mud Program (Three String Design)

Section	Туре	Weight (ppg)
Surface	FW Gel	8.5-9
Intermediate	DBE / Cut Brine	10-10.5
Production	OBM	10-10.5

Sufficient mud materials to maintain mud properties and meet minimum lost circulation and weight increase requirements will be kept on location at all times.

What will be used to monitor the loss or gain of fluid?	PVT/Pason/Visual Monitoring

6. Logging and Testing Procedures

Logging,	Logging, Coring and Testing								
	Will run GR/CNL from TD to surface (horizontal well - vertical portion of hole). Stated logs run will be in the								
Х	Completion Rpeort and sbumitted to the BLM.								
	No logs are planned based on well control or offset log information.								
	Drill stem test? If yes, explain.								
	Coring? If yes, explain.								

Additiona	al logs planned	Interval
	Resistivity	Int. shoe to KOP
	Density	Int. shoe to KOP
Х	CBL	Production casing
Х	Mud log	Intermediate shoe to TD
	PEX	

7. Drilling Conditions

Specfiy what type and where?
6608
No

Mitigation measure for abnormal conditions. Describe. Lost circulation material/sweeps/mud scavengers.

Hydrogren Sulfide (H2S) monitors will be installed prior to drilling out the surface shoe. If H2S is detected in concentrationsgreater than 100 ppm, the operator will comply with the provisions of 43 CFR 3176. If Hydrogen Sulfide is encounteredmeasured values and formations will be provided to the BLM.NH2S is present

Y H2S plan attached.

8. Other facets of operation

Is this a walking operation? Potentially

- 1 If operator elects, drilling rig will batch drill the surface holes and run/cement surface casing; walking the rig to next wells on the pad.
- 2 The drilling rig will then batch drill the intermediate sections and run/cement intermediate casing; the wellbore will be isolated with a blind flange and pressure gauge installed for monitoring the well before walking to the next well.
- 3 The drilling rig will then batch drill the production hole sections on the wells with OBM, run/cement production casing, and install TA caps or tubing heads for completions.

NOTE: During batch operations the drilling rig will be moved from well to well however, it will not be removed from the pad until all wells have production casing run/cemented.

Will be pre-setting casing? Potentially

- 1 Spudder rig will move in and batch drill surface hole.
 - a. Rig will utilize fresh water based mud to drill surface hole to TD. Solids control will be handled entirely on a closed loop basis.,
- 2 After drilling the surface hole section, the spudder rig will run casing and cement following all of the applicable rules and regulations (43 CFR 3172, all COAs and NMOCD regulations).

 3 The wellhead will be installed and tested once the surface casing is cut off and the WOC time has been reached.

- 4 A blind flange with the same pressure rating as the wellhead will be installed to seal the wellbore. Pressure will be monitored with a pressure gauge installed on the wellhead.
- 5 Spudder rig operations is expected to take 4-5 days per well on a multi-well pa.
- 6 The NMOCD will be contacted and notified 24 hours prior to commencing spudder rig operations.
- 7 Drilling operations will be performed with drilling rig. A that time an approved BOP stack will be nippled up and tested on the wellhead before drilling operations commences on each well.
 - a. The NMOCD will be contacted / notified 24 hours before the drilling rig moves back on to the pad with the pre-set surface casing.

Attachments

X Directional Plan Other, describe

Morgan 25-13 Fed Com 625H

A	S	urface csg in a	14 3/4	inch hole.		Design	Factors			Surface		
Segment	#/ft	Grade		Coupling	Body	Collapse	Burst	Length	B@s	a-B	a-C	Weight
"A"	45.50		j 55	btc	15.26	4.34	0.57	1,030	8	0.96	8.20	•
"B"			,	btc				0	U	0.00		0
_	w/8	.4#/g mud, 30min Sfc Csg Test p	nsig: 1 500	Tail Cmt	does not	circ to sfc.	Totals:	1,030				46,865
comparison o		Minimum Required Ceme						.,				,
Hole	Annular	1 Stage	1 Stage	Min	1 Stage	Drilling	Calc	Rea'd				Min Dis
Size	Volume	Cmt Sx	CuFt Cmt	Cu Ft	% Excess	Mud Wt	MASP	BOPE				Hole-Cpl
14 3/4	0.5563	586	844	573	47	9.00	3746	5M				1.50
unt Francisco d	:											
	lent(s) for seg	ment(s) A, B = , b All > 0.7	o, ok.		Site plat (pip							
8 5/8	ca	sing inside the	10 3/4			Design	Factors			Int 1		
Segment	#/ft	Grade		Coupling	Joint	Collapse	Burst	Length	B@s	a-B	a-C	Weigh
"A"	32.00		p 110	vam sprint fj	2.02	0.64	1.08	11,510	1	1.82	1.07	-
"B"								0				0
	w/8	.4#/g mud, 30min Sfc Csg Test p	osig: -18				Totals:	11,510				368,32
			-	ded to achieve a top of	0	ft from su	rface or a	1030				overlap.
Hole	Annular	1 Stage	1 Stage	Min	1 Stage	Drilling	Calc	Req'd				Min Dis
Size	Volume	Cmt Sx	CuFt Cmt	Cu Ft	% Excess	Mud Wt	MASP	BOPE				Hole-Cpl
9 7/8	0.1261	548	789	1460	-46	10.50	3939	5M				0.61
D V Tool(s):			6754				sum of sx	<u>Σ CuFt</u>				Σ%exces
oy stage % :		32	27				1024	1884				29
Tail cmt 5 1/2		sing inside the	8 5/8			Design Fa				Prod 1		
5 1/2 Segment	#/ft	sing inside the Grade		Coupling	Joint	Collapse	Burst	Length	B@s	a-B	a-C	-
5 1/2 Segment "A"		0	8 5/8 p 110	Coupling dwc/c is+	Joint 3.01	-		25,081	B@s 2		a-C 3.07	501,62
5 1/2 Segment "A" "B"	#/ft	0				Collapse	Burst	25,081 0		a-B	-	501,62 0
5 1/2 Segment "A" "B" "C"	#/ft	0				Collapse	Burst	25,081 0 0		a-B	-	501,62 0 0
5 1/2 Segment "A" "B"	#/ft 20.00	Grade	p 110			Collapse	Burst 2.18	25,081 0 0		a-B	-	501,620 0 0
5 1/2 Segment "A" "B" "C"	#/ft 20.00	Grade	p 110	dwc/c is+	3.01	Collapse 1.83	Burst 2.18 Totals:	25,081 0 0 25,081		a-B	-	501,62 0 0 501,62
5 1/2 Segment "A" "B" "C" "D"	#/ft 20.00 w/8	Grade 4#/g mud, 30min Sfc Csg Test p The cement vo	p 110 osig: 2,663 olume(s) are inten	dwc/c is+	3.01	Collapse 1.83 ft from su	Burst 2.18 Totals: rface or a	25,081 0 0 25,081 200		a-B	-	501,62 0 0 501,62 overlap.
5 1/2 Segment "A" "B" "C" "D" Hole	#/ft 20.00 w/8 Annular	Grade .4#/g mud, 30min Sfc Csg Test p The cement vo 1 Stage	p 110 p	dwc/c is+ ded to achieve a top of Min	3.01 11310 1 Stage	Collapse 1.83 ft from su Drilling	Burst 2.18 Totals: rface or a Calc	25,081 0 0 25,081 200 Req'd		a-B	-	501,62 0 0 501,62 overlap. Min Dis
5 1/2 Segment "A" "B" "C" "D" Hole Size	#/ft 20.00 w/8 Annular Volume	Grade 4#/g mud, 30min Sfc Csg Test r The cement vo 1 Stage Cmt Sx	p 110 p 110 psig: 2,663 plume(s) are inten 1 Stage CuFt Cmt	dwc/c is+ ded to achieve a top of Min Cu Ft	3.01 11310 1 Stage % Excess	Collapse 1.83 ft from su Drilling Mud Wt	Burst 2.18 Totals: rface or a	25,081 0 0 25,081 200		a-B	-	501,620 0 0 501,620 overlap. Min Dis Hole-Cpl
5 1/2 Segment "A" "C" "D" Hole Size 7 7/8	#/ft 20.00 w/8 Annular Volume 0.1733	Grade .4#/g mud, 30min Sfc Csg Test p The cement vo 1 Stage	p 110 p	dwc/c is+ ded to achieve a top of Min	3.01 11310 1 Stage	Collapse 1.83 ft from su Drilling	Burst 2.18 Totals: rface or a Calc	25,081 0 0 25,081 200 Req'd		a-B	-	501,620 0 0 501,620 overlap. Min Dist
5 1/2 Segment "A" "B" "C" "D" Hole Size 7 7/8	#/ft 20.00 w/8 Annular Volume 0.1733	Grade 4#/g mud, 30min Sfc Csg Test r The cement vo 1 Stage Cmt Sx	p 110 p 110 psig: 2,663 plume(s) are inten 1 Stage CuFt Cmt	dwc/c is+ ded to achieve a top of Min Cu Ft	3.01 11310 1 Stage % Excess	Collapse 1.83 ft from su Drilling Mud Wt	Burst 2.18 Totals: rface or a Calc	25,081 0 0 25,081 200 Req'd		a-B	-	0 0 501,620 overlap. Min Dist
5 1/2 Segment "A" "B" "C" "D" Hole Size 7 7/8 Class 'C' tail cm	#/ft 20.00 w/8 Annular Volume 0.1733	Grade 4#/g mud, 30min Sfc Csg Test r The cement vo 1 Stage Cmt Sx	p 110 p 110 psig: 2,663 plume(s) are inten 1 Stage CuFt Cmt	dwc/c is+ ded to achieve a top of Min Cu Ft	3.01 11310 1 Stage % Excess	Collapse 1.83 ft from su Drilling Mud Wt	Burst 2.18 Totals: rface or a Calc	25,081 0 0 25,081 200 Req'd		a-B	-	501,620 0 0 501,620 overlap. Min Dist Hole-Cpl
5 1/2 Segment "A" "B" "C" "D" Hole Size 7 7/8 Class 'C' tail cm	#/ft 20.00 w/8 Annular Volume 0.1733	Grade 4#/g mud, 30min Sfc Csg Test r The cement vo 1 Stage Cmt Sx	p 110 osig: 2,663 olume(s) are inten 1 Stage CuFt Cmt 2950	dwc/c is+ ded to achieve a top of Min Cu Ft	3.01 11310 1 Stage % Excess	Collapse 1.83 ft from su Drilling Mud Wt 10.50	Burst 2.18 Totals: rface or a Calc MASP	25,081 0 0 25,081 200 Req'd	2	a-B 3.65	3.07	501,620 0 0 501,620 overlap. Min Dist Hole-Cpl
5 1/2 Segment "A" "B" "C" "D" Hole Size 7 7/8 Siass 'C' tail cm #N/A 0	#/ft 20.00 w/8 Annular Volume 0.1733 t yld > 1.35	Grade 4#/g mud, 30min Sfc Csg Test p The cement vo 1 Stage Cmt Sx 1900	p 110 p 110 psig: 2,663 plume(s) are inten 1 Stage CuFt Cmt	dwc/c is+ ded to achieve a top of Min Cu Ft 2387	3.01 11310 1 Stage % Excess 24	Collapse 1.83 ft from su Drilling Mud Wt 10.50 Design	Burst 2.18 Totals: rface or a Calc MASP Factors	25,081 0 0 25,081 200 Req'd BOPE	2	a-B 3.65	3.07	501,620 0 0 501,620 overlap. Min Diss Hole-Cpl 0.79
5 1/2 Segment "A" "B" "C" "D" Hole Size 7 7/8 class 'C' tail cm #N/A 0 Segment	#/ft 20.00 w/8 Annular Volume 0.1733	Grade 4#/g mud, 30min Sfc Csg Test r The cement vo 1 Stage Cmt Sx	p 110 osig: 2,663 olume(s) are inten 1 Stage CuFt Cmt 2950	dwc/c is+ ded to achieve a top of Min Cu Ft 2387 Coupling	3.01 11310 1 Stage % Excess	Collapse 1.83 ft from su Drilling Mud Wt 10.50	Burst 2.18 Totals: rface or a Calc MASP	25,081 0 0 25,081 200 Req'd BOPE	2	a-B 3.65	3.07	501,620 0 0 501,620 overlap. Min Dis Hole-Cpl 0.79
5 1/2 Segment "A" "B" "C" "D" Hole Size 7 7/8 Class 'C' tail cm #N/A 0 Segment "A"	#/ft 20.00 w/8 Annular Volume 0.1733 t yld > 1.35	Grade 4#/g mud, 30min Sfc Csg Test p The cement vo 1 Stage Cmt Sx 1900	p 110 osig: 2,663 olume(s) are inten 1 Stage CuFt Cmt 2950	dwc/c is+ ded to achieve a top of Min Cu Ft 2387 Coupling 0.00	3.01 11310 1 Stage % Excess 24	Collapse 1.83 ft from su Drilling Mud Wt 10.50 Design	Burst 2.18 Totals: rface or a Calc MASP Factors	25,081 0 0 25,081 200 Req'd BOPE	2	a-B 3.65	3.07	501,62 0 0 501,62 overlap. Min Dis Hole-Cpl 0.79 Weigh 0
5 1/2 Segment "A" "B" "C" "D" Hole Size 7 7/8 Hass 'C' tail cm #N/A 0 Segment	#/ft 20.00 w/8 Annular Volume 0.1733 tyld > 1.35 #/ft	Grade 4#/g mud, 30min Sfc Csg Test r The cement vo 1 Stage Cmt Sx 1900 Grade	p 110 p 110 psig: 2,663 plume(s) are inten 1 Stage CuFt Cmt 2950 5 1/2	dwc/c is+ ded to achieve a top of Min Cu Ft 2387 Coupling	3.01 11310 1 Stage % Excess 24	Collapse 1.83 ft from su Drilling Mud Wt 10.50 Design	Burst 2.18 Totals: rface or a Calc MASP	25,081 0 0 25,081 200 Req'd BOPE	2	a-B 3.65	3.07	501,62 0 0 501,62 overlap. Min Dis Hole-Cp 0.79 Weigh 0
5 1/2 Segment "A" "B" "C" "D" Hole Size 7 7/8 Class 'C' tail cm #N/A 0 Segment "A"	#/ft 20.00 w/8 Annular Volume 0.1733 tyld > 1.35 #/ft	Grade 4#/g mud, 30min Sfc Csg Test p The cement vo 1 Stage Cmt Sx 1900 Grade 4#/g mud, 30min Sfc Csg Test p	p 110 p 110 psig: 2,663 plume(s) are inten 1 Stage CuFt Cmt 2950 5 1/2 psig:	dwc/c is+ ded to achieve a top of Min Cu Ft 2387 Coupling 0.00 0.00	3.01 11310 1 Stage % Excess 24 #N/A	Collapse 1.83 ft from su Drilling Mud Wt 10.50 <u>Design</u> Collapse	Burst 2.18 Totals: rface or a Calc MASP	25,081 0 0 25,081 200 Req'd BOPE	2	a-B 3.65	3.07 ing> a-C	501,62 0 0 501,62 overlap. Min Dis Hole-Cp 0.79 Weigh 0 0
5 1/2 Segment "A" "B" "C" "D" Hole Size 7 7/8 Jass 'C' tail cm #N/A 0 Segment "A" "B"	#/ft 20.00 w/8 Annular Volume 0.1733 t yld > 1.35 #/ft w/8	Grade 4#/g mud, 30min Sfc Csg Test p The cement vo 1 Stage Cmt Sx 1900 Grade 4#/g mud, 30min Sfc Csg Test p Cmt vol cal	p 110 p	dwc/c is+	3.01 11310 1 Stage % Excess 24 #N/A #N/A	Collapse 1.83 ft from su Drilling Mud Wt 10.50 <u>Design I</u> Collapse ft from su	Burst 2.18 Totals: rface or a Calc MASP Factors Burst	25,081 0 0 25,081 200 Req'd BOPE	2	a-B 3.65	3.07 ing> a-C	501,62 0 0 501,62 overlap. Min Dis Hole-Cp 0.79 Weigh 0 0 0 0 0 0 0 0
5 1/2 Segment "A" "B" "C" "D" Hole Size 7 7/8 ilass 'C' tail cm #N/A 0 Segment "A" "B" Hole	#/ft 20.00 w/8 Annular Volume 0.1733 t yld > 1.35 #/ft w/8 Annular	Grade 4#/g mud, 30min Sfc Csg Test r The cement vo 1 Stage Cmt Sx 1900 Grade 4#/g mud, 30min Sfc Csg Test r Cmt vol cal 1 Stage	p 110 p 110 p 110 psig: 2,663 plume(s) are inten 1 Stage CuFt Cmt 2950 5 1/2 psig: c below includes 1 1 Stage	dwc/c is+	3.01 11310 1 Stage % Excess 24 #N/A 1 Stage	Collapse 1.83 ft from su Drilling Mud Wt 10.50 <u>Design I</u> Collapse ft from su Drilling	Burst 2.18 Totals: rface or a Calc MASP Factors Burst	25,081 0 0 25,081 200 Req'd BOPE Length 0 0 0 #N/A Req'd	2	a-B 3.65	3.07 ing> a-C	501,62 0 0 501,62 overlap. Min Dis Hole-Cp 0.79 Weigh 0 0 0 overlap. Min Dis
5 1/2 Segment "A" "B" "C" "D" Hole Size 7 7/8 Class 'C' tail cm #N/A 0 Segment "A" "B" Hole Size	#/ft 20.00 w/8 Annular Volume 0.1733 t yld > 1.35 #/ft w/8	Grade 4#/g mud, 30min Sfc Csg Test r The cement vo 1 Stage Cmt Sx 1900 Grade 4#/g mud, 30min Sfc Csg Test r Cmt vol cal 1 Stage Cmt Sx	p 110 sig: 2,663 sig: 2,663 sig: CuFt Cmt 2950 5 1/2 sig: c below includes f 1 Stage CuFt Cmt	dwc/c is+	3.01 11310 1 Stage % Excess 24 #N/A 1 Stage % Excess	Collapse 1.83 ft from su Drilling Mud Wt 10.50 <u>Design I</u> Collapse ft from su	Burst 2.18 Totals: rface or a Calc MASP Factors Burst	25,081 0 0 25,081 200 Req'd BOPE	2	a-B 3.65	3.07 ing> a-C	501,620 0 0 501,620 overlap. Min Dist Hole-Cpl 0.79 Weight 0 0
5 1/2 Segment "A" "B" "C" "D" Hole Size 7 7/8 ilass 'C' tail cm #N/A 0 Segment "A" "B" Hole	#/ft 20.00 w/8 Annular Volume 0.1733 t yld > 1.35 #/ft w/8 Annular	Grade 4#/g mud, 30min Sfc Csg Test r The cement vo 1 Stage Cmt Sx 1900 Grade 4#/g mud, 30min Sfc Csg Test r Cmt vol cal 1 Stage	p 110 p 110 p 110 psig: 2,663 plume(s) are inten 1 Stage CuFt Cmt 2950 5 1/2 psig: c below includes 1 1 Stage	dwc/c is+	3.01 11310 1 Stage % Excess 24 #N/A 1 Stage	Collapse 1.83 ft from su Drilling Mud Wt 10.50 <u>Design I</u> Collapse ft from su Drilling	Burst 2.18 Totals: rface or a Calc MASP Factors Burst	25,081 0 0 25,081 200 Req'd BOPE Length 0 0 0 #N/A Req'd	2	a-B 3.65	3.07 ing> a-C	501,62 0 0 501,62 overlap. Min Dis Hole-Cp 0.79 Weigh 0 0 0 overlap. Min Dis

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Morgan 25-13 Fed Com 625H

Segment	S	urface csg in a	13 1/2	inch hole.		Design	Factors			Surface		
Segment	#/ft	Grade		Coupling	Body	Collapse	Burst	Length	B@s	a-B	a-C	Weight
"A"	40.00		j 55	btc	15.29	5.34	0.63	1,030	9	1.05	10.08	41,200
"B"				btc				0				0
	w/8.	4#/g mud, 30min Sfc Csg Test	psig: 1,500	Tail Cmt	does not	circ to sfc.	Totals:	1,030				41,200
omparison o		Minimum Required Ceme										
Hole	Annular	1 Stage	1 Stage	Min	1 Stage	Drilling	Calc	Req'd				Min Dis
Size	Volume	Cmt Sx	CuFt Cmt	Cu Ft	% Excess	Mud Wt	MASP	BOPE				Hole-Cpl
13 1/2	0.4887	512	737	503	46	9.00	3746	5M				1.44
urst Frac Grad	ient(s) for Segr	nent(s) A, B = , b All > 0.7	70, OK.									
7 5/8		sing inside the	9 5/8	Counting	laint	Design		ا میں میڈ	Dec	Int 1	- 0	Malak
Segment	#/ft	Grade	- 110	Coupling	Joint	Collapse	Burst	Length	B@s	a-B	a-C	Weight
"A" "B"	29.70		p 110	talon sfc	2.68	1.16	1.63	11,510 0	2	2.73	1.94	341,847 0
D		4#/a mud 20min 5f- 0 T	ncia: 2 5 2 2				Totals:	U 11,510			1	U 341,847
	w/8.	4#/g mud, 30min Sfc Csg Test The coment y		ded to achieve a top of	0	ft from su		1030				overlap.
Hole	Annular	1 Stage	1 Stage	Min	1 Stage	Drilling	Calc	Reg'd				Min Dist
Size	Volume	Cmt Sx	CuFt Cmt	Cu Ft	% Excess	Mud Wt	MASP	BOPE				Hole-Cpl
8 3/4	0.1005	436	628	1165	-46	10.50	3939	5M				0.43
D V Tool(s):	011000		6754				sum of sx	Σ CuFt				Σ%exces
by stage % :		31	26				812	1493				28
Tail cmt												
5 1/2		sing inside the	7 5/8			<u>Design Fa</u>	<u>ctors</u>			Prod 1		
Segment	#/ft	sing inside the Grade		 Coupling	Joint	Collapse	Burst	Length	B@s	a-B	a-C	
Segment "A"		0	7 5/8 p 110	Coupling talon rd	Joint 3.01	-		25,081	B@s 2		a-C 3.34	501,620
Segment "A" "B"	#/ft	0				Collapse	Burst	25,081 0		a-B		501,620 0
Segment "A" "B" "C"	#/ft	0				Collapse	Burst	25,081 0 0		a-B		501,620 0 0
Segment "A" "B"	#/ft 20.00	Grade	p 110			Collapse	Burst 2.18	25,081 0 0		a-B		501,620 0 0
Segment "A" "B" "C"	#/ft 20.00	Grade 4#/g mud, 30min Sfc Csg Test	p 110 psig: 2,663	talon rd	3.01	Collapse 1.99	Burst 2.18 Totals:	25,081 0 0 25,081		a-B	3.34	501,620 0 0 501,620
Segment "A" "B" "C" "D"	#/ft 20.00 w/8.	Grade 4#/g mud, 30min Sfc Csg Test The cement v	p 110 psig: 2,663 olume(s) are inten	talon rd	3.01	Collapse 1.99 ft from su	Burst 2.18 Totals: Irface or a	25,081 0 0 25,081 200		a-B	3.34	501,620 0 0 501,620 overlap.
Segment "A" "B" "C" "D" Hole	#/ft 20.00 w/8. Annular	Grade 4#/g mud, 30min Sfc Csg Test The cement v 1 Stage	p 110 psig: 2,663 olume(s) are inten 1 Stage	talon rd ded to achieve a top of Min	3.01 11310 1 Stage	Collapse 1.99 ft from su Drilling	Burst 2.18 Totals: Irface or a Calc	25,081 0 0 25,081 200 Req'd		a-B	3.34	501,620 0 0 501,620 overlap. Min Dist
Segment "A" "B" "C" "D" Hole Size	#/ft 20.00 w/8. Annular Volume	Grade 4#/g mud, 30min Sfc Csg Test The cement v 1 Stage Cmt Sx	p 110 psig: 2,663 olume(s) are inten 1 Stage CuFt Cmt	taion rd ded to achieve a top of Min Cu Ft	3.01 11310 1 Stage % Excess	Collapse 1.99 ft from su Drilling Mud Wt	Burst 2.18 Totals: Irface or a	25,081 0 0 25,081 200		a-B	3.34	501,620 0 0 501,620 overlap. Min Dist Hole-Cpl
Segment "A" "C" "D" Hole Size 6 3/4	#/ft 20.00 w/8. Annular Volume 0.0835	Grade 4#/g mud, 30min Sfc Csg Test The cement v 1 Stage	p 110 psig: 2,663 olume(s) are inten 1 Stage	talon rd ded to achieve a top of Min	3.01 11310 1 Stage	Collapse 1.99 ft from su Drilling	Burst 2.18 Totals: Irface or a Calc	25,081 0 0 25,081 200 Req'd		a-B	3.34	501,620 0 0 501,620 overlap. Min Dist
Segment "A" "B" "C" "D" Hole Size 6 3/4 Class 'C' tail cm	#/ft 20.00 w/8. Annular Volume 0.0835	Grade 4#/g mud, 30min Sfc Csg Test The cement v 1 Stage Cmt Sx	p 110 psig: 2,663 rolume(s) are inten 1 Stage CuFt Cmt 1440	taion rd ded to achieve a top of Min Cu Ft	3.01 11310 1 Stage % Excess	Collapse 1.99 ft from su Drilling Mud Wt 10.50	Burst 2.18 Totals: urface or a Calc MASP	25,081 0 0 25,081 200 Req'd	2	a-B 3.65	3.34	501,620 0 0 501,620 overlap. Min Dist Hole-Cpl
Segment "A" "B" "C" "D" Hole Size 6 3/4 Class 'C' tail cm #N/A 0	#/ft 20.00 w/8. Annular Volume 0.0835 t yld > 1.35	Grade 4#/g mud, 30min Sfc Csg Test The cement v 1 Stage Cmt Sx 921	p 110 psig: 2,663 olume(s) are inten 1 Stage CuFt Cmt	talon rd ded to achieve a top of Min Cu Ft 1151	3.01 11310 1 Stage % Excess 25	Collapse 1.99 ft from su Drilling Mud Wt 10.50 Design	Burst 2.18 Totals: Inface or a Calc MASP Factors	25,081 0 0 25,081 200 Req'd BOPE	2	a-B 3.65	3.34 ing>	501,620 0 0 501,620 overlap. Min Dist Hole-Cpl 0.43
Segment "A" "B" "C" "D" Hole Size 6 3/4 Class 'C' tail cm #N/A 0 Segment	#/ft 20.00 w/8. Annular Volume 0.0835	Grade 4#/g mud, 30min Sfc Csg Test The cement v 1 Stage Cmt Sx	p 110 psig: 2,663 rolume(s) are inten 1 Stage CuFt Cmt 1440	talon rd ded to achieve a top of Min Cu Ft 1151 Coupling	3.01 11310 1 Stage % Excess	Collapse 1.99 ft from su Drilling Mud Wt 10.50	Burst 2.18 Totals: urface or a Calc MASP	25,081 0 0 25,081 200 Req'd BOPE	2	a-B 3.65	3.34	501,620 0 0 501,620 overlap. Min Dist Hole-Cpl 0.43 Weight
Segment "A" "B" "C" "D" Hole Size 6 3/4 Class 'C' tail cm #N/A 0 Segment "A"	#/ft 20.00 w/8. Annular Volume 0.0835 t yld > 1.35	Grade 4#/g mud, 30min Sfc Csg Test The cement v 1 Stage Cmt Sx 921	p 110 psig: 2,663 rolume(s) are inten 1 Stage CuFt Cmt 1440	talon rd ded to achieve a top of Min Cu Ft 1151 Coupling 0.00	3.01 11310 1 Stage % Excess 25	Collapse 1.99 ft from su Drilling Mud Wt 10.50 Design	Burst 2.18 Totals: Inface or a Calc MASP Factors	25,081 0 0 25,081 200 Req'd BOPE	2	a-B 3.65	3.34 ing>	501,620 0 0 501,620 overlap. Min Dist Hole-Cpl 0.43 Weight 0
Segment "A" "B" "C" "D" Hole Size 6 3/4 Class 'C' tail cm #N/A 0 Segment	#/ft 20.00 w/8. Annular Volume 0.0835 tyld > 1.35 #/ft	Grade 4#/g mud, 30min Sfc Csg Test The cement v 1 Stage Cmt Sx 921 Grade	p 110 psig: 2,663 olume(s) are inten 1 Stage CuFt Cmt 1440 5 1/2	talon rd ded to achieve a top of Min Cu Ft 1151 Coupling	3.01 11310 1 Stage % Excess 25	Collapse 1.99 ft from su Drilling Mud Wt 10.50 Design	Burst 2.18 Totals: Inface or a Calc MASP Factors Burst	25,081 0 0 25,081 200 Req'd BOPE	2	a-B 3.65	3.34 ing>	501,620 0 0 501,620 Min Dist Hole-Cpl 0.43 Weight 0 0
Segment "A" "B" "C" "D" Hole Size 6 3/4 Class 'C' tail cm #N/A 0 Segment "A"	#/ft 20.00 w/8. Annular Volume 0.0835 tyld > 1.35 #/ft	4#/g mud, 30min Sfc Csg Test The cement v 1 Stage Cmt Sx 921 Grade 4#/g mud, 30min Sfc Csg Test	p 110 psig: 2,663 olume(s) are inten 1 Stage CuFt Cmt 1440 5 1/2	taion rd ded to achieve a top of Min Cu Ft 1151 Coupling 0.00 0.00	3.01 11310 1 Stage % Excess 25 #N/A	Collapse 1.99 ft from su Drilling Mud Wt 10.50 <u>Design</u> Collapse	Burst 2.18 Totals: urface or a Calc MASP Factors Burst Totals:	25,081 0 0 25,081 200 Req'd BOPE	2	a-B 3.65	3.34 ing> a-C	501,620 0 0 501,620 overlap. Min Dist Hole-Cpl 0.43 Weight 0 0 0
Segment "A" "B" "C" "D" Hole Size 6 3/4 Class 'C' tail cm (C) Segment "A" "B"	#/ft 20.00 w/8. Annular Volume 0.0835 t yld > 1.35 #/ft w/8.	Grade 4#/g mud, 30min Sfc Csg Test The cement v 1 Stage Cmt Sx 921 Grade 4#/g mud, 30min Sfc Csg Test Cmt vol ca	p 110 psig: 2,663 rolume(s) are inten 1 Stage CuFt Cmt 1440 5 1/2 psig: Ic below includes f	taion rd ded to achieve a top of Min Cu Ft 1151 Coupling 0.00 0.00 this csg, TOC intended	3.01 11310 1 Stage % Excess 25 #N/A #N/A	Collapse 1.99 ft from su Drilling Mud Wt 10.50 <u>Design</u> Collapse	Burst 2.18 Totals: urface or a Calc MASP Factors Burst Totals: urface or a	25,081 0 0 25,081 200 Req'd BOPE	2	a-B 3.65	3.34 ing> a-C	501,620 0 0 501,620 overlap. Min Dis Hole-Cpl 0.43 Weigh 0 0 0 0 0 0 0 0
Segment "A" "B" "C" "D" Hole Size 6 3/4 Class 'C' tail cm #N/A 0 Segment "A" "B" Hole	#/ft 20.00 w/8. Annular Volume 0.0835 t yld > 1.35 #/ft w/8. Annular	Grade 4#/g mud, 30min Sfc Csg Test The cement v 1 Stage Cmt Sx 921 Grade 4#/g mud, 30min Sfc Csg Test Cmt vol ca 1 Stage	p 110 psig: 2,663 olume(s) are inten 1 Stage CuFt Cmt 1440 5 1/2 psig: Ic below includes i 1 Stage	talon rd ded to achieve a top of Min Cu Ft 1151 Coupling 0.00 0.00 0.00 this csg, TOC intended Min	3.01 11310 1 Stage % Excess 25 #N/A 1 Stage	Collapse 1.99 ft from su Drilling Mud Wt 10.50 <u>Design</u> Collapse ft from su Drilling	Burst 2.18 Totals: urface or a Calc MASP Factors Burst Totals: urface or a Calc	25,081 0 0 25,081 200 Req'd BOPE Length 0 0 0 #N/A Req'd	2	a-B 3.65	3.34 ing> a-C	501,620 0 0 501,620 overlap. Min Dist Hole-Cpl 0.43 Weight 0 0 0 overlap. Min Dist
Segment "A" "B" "C" "D" Hole Size 6 3/4 Class 'C' tail cm #N/A 0 Segment "A" "B" Hole Size	#/ft 20.00 w/8. Annular Volume 0.0835 t yld > 1.35 #/ft w/8.	Grade 4#/g mud, 30min Sfc Csg Test The cement v 1 Stage Cmt Sx 921 Grade 4#/g mud, 30min Sfc Csg Test Cmt vol ca 1 Stage Cmt Sx	p 110 psig: 2,663 olume(s) are inten 1 Stage CuFt Cmt 1440 5 1/2 psig: Ic below includes f 1 Stage CuFt Cmt	taion rd ded to achieve a top of Min Cu Ft 1151 Coupling 0.00 0.00 this csg, TOC intended Min Cu Ft	3.01 11310 1 Stage % Excess 25 #N/A 1 Stage % Excess	Collapse 1.99 ft from su Drilling Mud Wt 10.50 <u>Design</u> Collapse	Burst 2.18 Totals: urface or a Calc MASP Factors Burst Totals: urface or a	25,081 0 0 25,081 200 Req'd BOPE	2	a-B 3.65	3.34 ing> a-C	0 0 501,620 overlap. Min Dist Hole-Cply 0.43 Weight 0 0 0
Segment "A" "B" "C" "D" Hole Size 6 3/4 C Liass 'C' tail cm #N/A 0 Segment "A" "B" Hole	#/ft 20.00 w/8. Annular Volume 0.0835 t yld > 1.35 #/ft w/8. Annular	Grade 4#/g mud, 30min Sfc Csg Test The cement v 1 Stage Cmt Sx 921 Grade 4#/g mud, 30min Sfc Csg Test Cmt vol ca 1 Stage	p 110 psig: 2,663 olume(s) are inten 1 Stage CuFt Cmt 1440 5 1/2 psig: Ic below includes i 1 Stage	taion rd ded to achieve a top of Min Cu Ft 1151 Coupling 0.00 0.00 0.00 this csg, TOC intended Min Cu Ft 0	3.01 11310 1 Stage % Excess 25 #N/A 1 Stage	Collapse 1.99 ft from su Drilling Mud Wt 10.50 <u>Design</u> Collapse ft from su Drilling	Burst 2.18 Totals: urface or a Calc MASP Factors Burst Totals: urface or a Calc	25,081 0 0 25,081 200 Req'd BOPE Length 0 0 0 #N/A Req'd	2	a-B 3.65	3.34 ing> a-C	501,620 0 0 501,620 overlap. Min Dist Hole-Cpl 0.43 Weight 0 0 0 overlap. Min Dist

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Sante Fe Main Office Phone: (505) 476-3441

General Information Phone: (505) 629-6116

Online Phone Directory https://www.emnrd.nm.gov/ocd/contact-us

State of New Mexico Energy, Minerals and Natural Resources Oil Conservation Division 1220 S. St Francis Dr. Santa Fe, NM 87505

CONDITIONS

OGRID:
6137
Action Number:
429254
Action Type:
[C-103] NOI Change of Plans (C-103A)

C	ONDITIONS		
	Created By	Condition	Condition Date
	ward.rikala	Any previous COA's not addressed within the updated COA's still apply.	4/1/2025

Released to Imaging: 4/1/2025 2:49:06 PM

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Action 429254