Form 3160-5
(June 2019)

UNITED STATES
DEPARTMENT OF THE INTERIOR
BUREAU OF LAND MANAGEMENT

FORM APPROVED
OMB No. 1004-0137
Expires: October 31, 2021

SUNDRY NOTICES AND REPORTS ON WELLS

Do not use this form for proposals to drill or to re-enter an abandoned well. Use Form 3160-3 (APD) for such proposals.

SUBMIT IN TRIPLICATE *- Other instructions on page 2*

5. Lease Serial No.

6. If Indian, Allottee or Tribe Name

7. If Unit of CA/Agreement, Name and/or No.

1. Type of Well
☐ Oil Well ☐ Gas Well ☐ Other

8. Well Name and No.

2. Name of Operator

9. API Well No.

3a. Address

3b. Phone No. *(include area code)*

10. Field and Pool or Exploratory Area

4. Location of Well *(Footage, Sec., T.,R.,M., or Survey Description)*

11. Country or Parish, State

12. CHECK THE APPROPRIATE BOX(ES) TO INDICATE NATURE OF NOTICE, REPORT OR OTHER DATA

TYPE OF SUBMISSION	TYPE OF ACTION			
☐ Notice of Intent	☐ Acidize	☐ Deepen	☐ Production (Start/Resume)	☐ Water Shut-Off
	☐ Alter Casing	☐ Hydraulic Fracturing	☐ Reclamation	☐ Well Integrity
☐ Subsequent Report	☐ Casing Repair	☐ New Construction	☐ Recomplete	☐ Other
	☐ Change Plans	☐ Plug and Abandon	☐ Temporarily Abandon	
☐ Final Abandonment Notice	☐ Convert to Injection	☐ Plug Back	☐ Water Disposal	

13. Describe Proposed or Completed Operation: Clearly state all pertinent details, including estimated starting date of any proposed work and approximate duration thereof. If the proposal is to deepen directionally or recomplete horizontally, give subsurface locations and measured and true vertical depths of all pertinent markers and zones. Attach the Bond under which the work will be perfonned or provide the Bond No. on file with BLM/BIA. Required subsequent reports must be filed within 30 days following completion of the involved operations. If the operation results in a multiple completion or recompletion in a new interval, a Form 3160-4 must be filed once testing has been completed. Final Abandonment Notices must be filed only after all requirements, including reclamation, have been completed and the operator has detennined that the site is ready for final inspection.)

14. I hereby certify that the foregoing is true and correct. Name *(Printed/Typed)*

Title

Signature

Date

THE SPACE FOR FEDERAL OR STATE OFICE USE

Approved by

Title

Date

Conditions of approval, if any, are attached. Approval of this notice does not warrant or certify that the applicant holds legal or equitable title to those rights in the subject lease which would entitle the applicant to conduct operations thereon.

Office

Title 18 U.S.C Section 1001 and Title 43 U.S.C Section 1212, make it a crime for any person knowingly and willfully to make to any department or agency of the United States any false, fictitious or fraudulent statements or representations as to any matter within its jurisdiction.

(Instructions on page 2)

GENERAL INSTRUCTIONS

This form is designed for submitting proposals to perform certain well operations and reports of such operations when completed as indicated on Federal and Indian lands pursuant to applicable Federal law and regulations. Any necessary special instructions concerning the use of this form and the number of copies to be submitted, particularly with regard to local area or regional procedures and practices, are either shown below, will be issued by or may be obtained from the local Federal office.

SPECIFIC INSTRUCTIONS

Item 4 - Locations on Federal or Indian land should be described in accordance with Federal requirements. Consult the local Federal office for specific instructions.

Item 13: Proposals to abandon a well and subsequent reports of abandonment should include such special information as is required by the local Federal office. In addition, such proposals and reports should include reasons for the abandonment; data on any former or present productive zones or other zones with present significant fluid contents not sealed off by cement or otherwise; depths (top and bottom) and method of placement of cement plugs; mud or other material placed below, between and above plugs; amount, size, method of parting of any casing, liner or tubing pulled and the depth to the top of any tubing left in the hole; method of closing top of well and date well site conditioned for final inspection looking for approval of the abandonment. If the proposal will involve **hydraulic fracturing operations**, you must comply with 43 CFR 3162.3-3, including providing information about the protection of usable water. Operators should provide the best available information about all formations containing water and their depths. This information could include data and interpretation of resistivity logs run on nearby wells. Information may also be obtained from state or tribal regulatory agencies and from local BLM offices.

NOTICES

The privacy Act of 1974 and the regulation in 43 CFR 2.48(d) provide that you be furnished the following information in connection with information required by this application.
AUTHORITY: 30 U.S.C. 181 et seq., 351 et seq., 25 U.S.C. 396; 43 CFR 3160.
PRINCIPAL PURPOSE: The information is used to: (1) Evaluate, when appropriate, approve applications, and report completion of subsequent well operations, on a Federal or Indian lease; and (2) document for administrative use, information for the management, disposal and use of National Resource lands and resources, such as: (a) evaluating the equipment and procedures to be used during a proposed subsequent well operation and reviewing the completed well operations for compliance with the approved plan; (b) requesting and granting approval to perform those actions covered by 43 CFR 3162.3-2, 3162.3-3, and 3162.3-4; (c) reporting the beginning or resumption of production, as required by 43 CFR 3162.4-1(c)and (d) analyzing future applications to drill or modify operations in light of data obtained and methods used.
ROUTINE USES: Information from the record and/or the record will be transferred to appropriate Federal, State, local or foreign agencies, when relevant to civil, criminal or regulatory investigations or prosecutions in connection with congressional inquiries or to consumer reporting agencies to facilitate collection of debts owed the Government.
EFFECT OF NOT PROVIDING THE INFORMATION: Filing of this notice and report and disclosure of the information is mandatory for those subsequent well operations specified in 43 CFR 3162.3-2, 3162.3-3, 3162.3-4.

The Paperwork Reduction Act of 1995 requires us to inform you that:
The BLM collects this information to evaluate proposed and/or completed subsequent well operations on Federal or Indian oil and gas leases.
Response to this request is mandatory.
The BLM would like you to know that you do not have to respond to this or any other Federal agency-sponsored information collection unless it displays a currently valid OMB control number.

BURDEN HOURS STATEMENT: Public reporting burden for this form is estimated to average 8 hours per response, including the time for reviewing instructions, gathering and maintaining data, and completing and reviewing the form. Direct comments regarding the burden estimate or any other aspect ofthis form to U.S. Department ofthe Interior, Bureau ofLand Management (1004-0137), Bureau Information Collection Clearance Officer (WO-630), 1849 C St., N.W., Mail Stop 401 LS, Washington, D.C. 20240

Additional Information

Additional Remarks

Change target formation to Brushy Canyon M.

Update casing and cement program to current design.

Update HSU to 799.73 acres.

Update the Pool from 51020 RED HILLS;LOWER BONE SPRING SHALE to (PENDING WILDCAT DELAWARE POOL) as reflected in the C-102.

Location of Well

0. SHL: LOT 2 / 1103 FNL / 1542 FEL / TWSP: 25S / RANGE: 33E / SECTION: 1 / LAT: 32.1637718 / LONG: -103.5224868 (TVD: 0 feet, MD: 0 feet)
PPP: LOT 2 / 100 FNL / 2632 FEL / TWSP: 25S / RANGE: 33E / SECTION: 1 / LAT: 32.1665326 / LONG: -103.5260094 (TVD: 10495 feet, MD: 10705 feet)
BHL: TR O / 100 FSL / 2634 FEL / TWSP: 25S / RANGE: 33E / SECTION: 12 / LAT: 32.1380691 / LONG: -103.5260186 (TVD: 10760 feet, MD: 21162 feet)

C-102 Submit Electronically Via OCD Permitting	State of New Mexico Energy, Minerals & Natural Resources Department OIL CONSERVATION DIVISION	Revised July 9, 2024 Submittal Type: ☐ Initial Submittal ☒ Amended Report ☐ As Drilled

WELL LOCATION AND ACREAGE DEDICATION PLAT

API Number	Pool Code	Pool Name
30-025-53508	98398	WC-025 G-05 S253301L4; DELAWARE ~~(PENDING WILDCAT DELAWARE POOL)~~

Property Code	Property Name	Well Number
330827	LACEY SWISS 1 FED COM	2H

OGRID No.	Operator Name	Ground Level Elevation
7377	EOG RESOURCES, INC.	3459'

Surface Owner: ☐ State ☐ Fee ☐ Tribal ☒ Federal

Mineral Owner: ☐ State ☐ Fee ☐ Tribal ☒ Federal

Surface Location

UL or lot no.	Section	Township	Range	Lot Idn	Feet from the N/S	Feet from the E/W	Latitude	Longitude	County
2	1	25-S	33-E	-	884' N	1540' E	N 32.1643737	W 103.5224815	LEA

Bottom Hole Location

UL or lot no.	Section	Township	Range	Lot Idn	Feet from the N/S	Feet from the E/W	Latitude	Longitude	County
F	13	25-S	33-E	-	2541' N	1950' W	N 32.1308137	W 103.5283072	LEA

Dedicated Acres	Infill or Defining Well	Defining Well API	Overlapping Spacing Unit (Y/N)	Consolidated Code
799.73	INFILL	PENDING	N	C

Order Numbers: PENDING COM #

Well Setbacks are under Common Ownership: ☐ Yes ☐ No

Kick Off Point (KOP)

UL or lot no.	Section	Township	Range	Lot Idn	Feet from the N/S	Feet from the E/W	Latitude	Longitude	County
3	1	25-S	33-E	-	50' N	1950' W	N 32.1666727	W 103.5282772	LEA

First Take Point (FTP)

UL or lot no.	Section	Township	Range	Lot Idn	Feet from the N/S	Feet from the E/W	Latitude	Longitude	County
3	1	25-S	33-E	-	100' N	1950' W	N 32.1665353	W 103.5282773	LEA

Last Take Point (LTP)

UL or lot no.	Section	Township	Range	Lot Idn	Feet from the N/S	Feet from the E/W	Latitude	Longitude	County
F	13	25-S	33-E	-	2541' N	1950' W	N 32.1308137	W 103.5283072	LEA

Unitized Area or Area of Uniform Intrest	Spacing Unity Type	Ground Floor Elevation
UNITIZED AREA	☒ Horizontal ☐ Vertical	3484'

OPERATOR CERTIFICATION

I hereby certify that the information contained herein is true and complete to the best of my knowledge and belief; and, if the well is a vertical or directional well, that this organization either owns a working interest or unleased mineral interest in the land including the proposed bottom hole location or has a right to drill this well at this location pursuant to a contract with an owner of a working interest or unleased mineral interest, or to a voluntary pooling agreement or a compulsory pooling order heretofore entered by the division.

If this well is a horizontal well, I further certify that this organization has received The consent of at least one lessee or owner of a working interest or unleased mineral interest in each tract (in the target pool or formation) in which any part of the well's completed interval will be located or obtained a compulsory pooling order from the division.

Kayla McConnell — Signature — Date: 03/05/2025

KAYLA MCCONNELL — Print Name

KAYLA_MCCONNELL@EOGRESOURCES.COM — E-mail Address

SURVEYORS CERTIFICATION

I hereby certify that the well location shown on this plat was plotted from field notes of actual surveys made by me or under my supervision, and that the same is true and correct to the best of my belief.

RAMON DOMINGUEZ — NEW MEXICO — 24508 — PROFESSIONAL SURVEYOR

2/18/2025 3:11:25 PM

Signature and Seal of Professional Surveyor — Date

Certificate Number

Date of Survey: 02/08/2025

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C-102

Submit Electronically
Via OCD Permitting

State of New Mexico
Energy, Minerals & Natural Resources Department
OIL CONSERVATION DIVISION

Revised July 9, 2024

Submittal Type:
- ☐ Initial Submittal
- ☒ Amended Report
- ☐ As Drilled

Property Name and Well Number

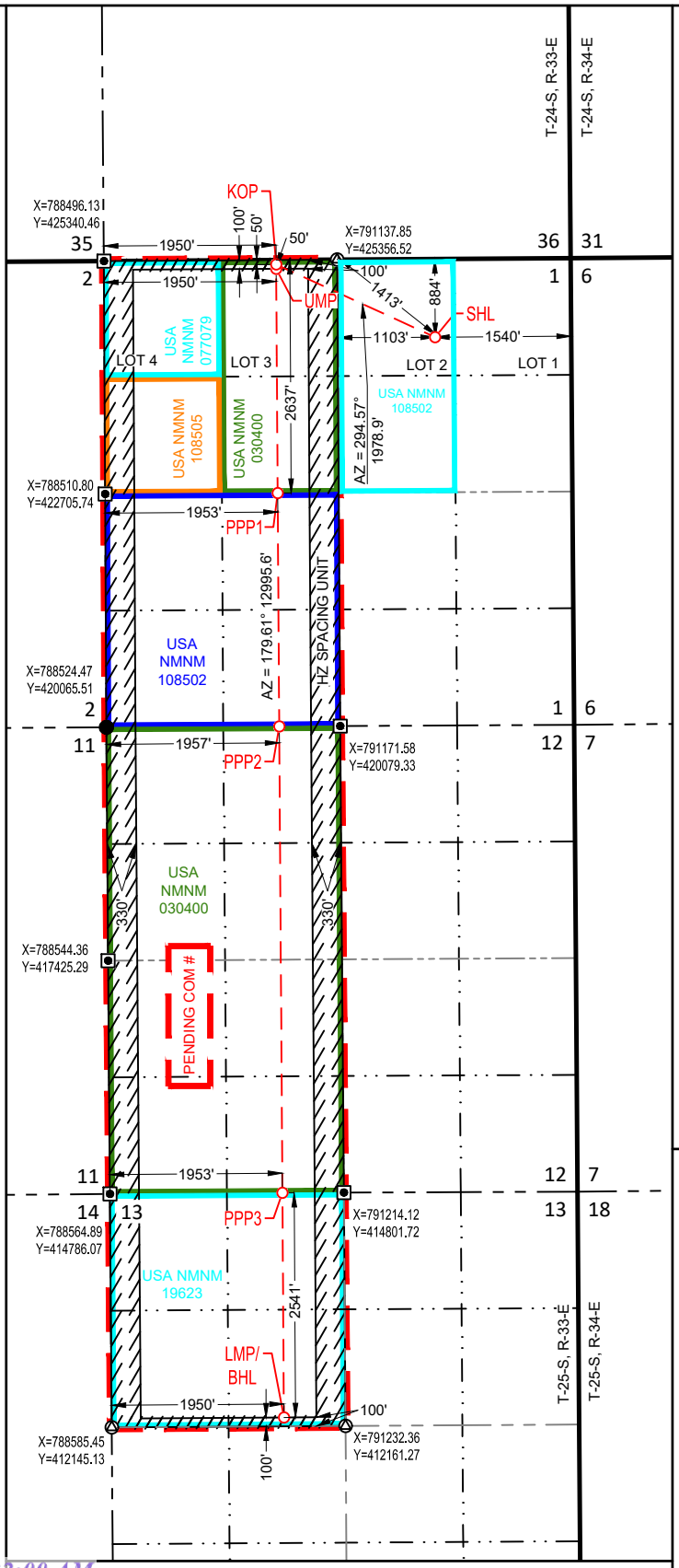
LACEY SWISS 1 FED COM 2H

SURFACE LOCATION (SHL)
NEW MEXICO EAST
NAD 1983
X=792246 Y=424479
LAT.: N 32.1643737
LONG.: W 103.5224815
NAD 1927
X=751061 Y=424421
LAT.: N 32.1642493
LONG.: W 103.5220083
884' FNL 1540' FEL

KICK OFF POINT (KOP)
NEW MEXICO EAST
NAD 1983
X=790446 Y=425302
LAT.: N 32.1666727
LONG.: W 103.5282772
NAD 1927
X=749261 Y=425244
LAT.: N 32.1665484
LONG.: W 103.5278038
50' FNL 1950' FWL

UPPER MOST PERF. (UMP)
NEW MEXICO EAST
NAD 1983
X=790447 Y=425252
LAT.: N 32.1665353
LONG.: W 103.5282773
NAD 1927
X=749261 Y=425194
LAT.: N 32.1664109
LONG.: W 103.5278039
100' FNL 1950' FWL

PROPOSED PERF. POINT (PPP1)
NEW MEXICO EAST
NAD 1983
X=790464 Y=422716
LAT.: N 32.1595625
LONG.: W 103.5282832
NAD 1927
X=749278 Y=422657
LAT.: N 32.1594381
LONG.: W 103.5278102
2637' FNL 1953' FWL



PROPOSED PERF. POINT (PPP2)
NEW MEXICO EAST
NAD 1983
X=790482 Y=420076
LAT.: N 32.1523059
LONG.: W 103.5282893
NAD 1927
X=749296 Y=420018
LAT.: N 32.1521814
LONG.: W 103.5278167
0' FSL 1957' FWL

PROPOSED PERF. POINT (PPP3)
NEW MEXICO EAST
NAD 1983
X=790517 Y=414798
LAT.: N 32.1377973
LONG.: W 103.5283014
NAD 1927
X=749332 Y=414740
LAT.: N 32.1376728
LONG.: W 103.5278298
0' FSL 1953' FWL

LOWER MOST PERF. (LMP)
BOTTOM HOLE LOCATION (BHL)
NEW MEXICO EAST
NAD 1983
X=790535 Y=412257
LAT.: N 32.1308137
LONG.: W 103.5283072
NAD 1927
X=749349 Y=412199
LAT.: N 32.1306892
LONG.: W 103.5278360
2541' FNL 1950' FWL

T-25-S, R-33-E
SECTION 1
LOT 1 - 39.98 ACRES
LOT 2 - 39.93 ACRES
LOT 3 - 39.89 ACRES
LOT 4 - 39.84 ACRES

SURVEYORS CERTIFICATION

I hereby certify that the well location shown on this plat was plotted from field notes of actual surveys made by me or under my supervision, and that the same is true and correct to the best of my belief.

02/08/2025
Date of Survey
Signature and Seal of Professional Surveyor:

RAMON DOMINGUEZ
NEW MEXICO
24508
PROFESSIONAL SURVEYOR

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PECOS DISTRICT
DRILLING CONDITIONS OF APPROVAL

OPERATOR'S NAME:	EOG RESOURCES INCORPORATED
WELL NAME & NO.:	LACEY SWISS 1 FED COM 2H
LOCATION:	Section 2, T.25 S., R.33 E., NMP
COUNTY:	Lea County, New Mexico

COA

H2S	◉ Yes	○ No	
Potash	◉ None	○ Secretary	○ R-111-P
Cave/Karst Potential	◉ Low	○ Medium	○ High
Cave/Karst Potential	○ Critical		
Variance	○ None	◉ Flex Hose	○ Other
Wellhead	○ Conventional	◉ Multibowl	○ Both
Wellhead Variance	○ Diverter		
Other	☐ 4 String	☐ Capitan Reef	☐ WIPP
Other	☑ Fluid Filled	☐ Pilot Hole	☐ Open Annulus
Cementing	☐ Contingency Cement Squeeze	☑ EchoMeter	☑ Primary Cement Squeeze
Special Requirements	☐ Water Disposal	☑ COM	☐ Unit
Special Requirements	☐ Batch Sundry		
Special Requirements Variance	☑ Break Testing	☑ Offline Cementing	☑ Casing Clearance

A. HYDROGEN SULFIDE

A Hydrogen Sulfide (H2S) Drilling Plan shall be activated AT SPUD. As a result, the Hydrogen Sulfide area must meet 43 CFR part 3170 requirements, which includes equipment and personnel/public protection items. If Hydrogen Sulfide is encountered, please provide measured values and formations to the BLM.

B. CASING

Casing Design A:

1. The **13-3/8** inch surface casing shall be set at approximately **1272** feet (a minimum of 25 feet (Lea County) into the Rustler Anhydrite, above the salt, and below usable fresh water) and cemented to the surface.

    a. If cement does not circulate to the surface, the appropriate BLM office shall be notified and a temperature survey utilizing an electronic type temperature

survey with surface log readout will be used or a cement bond log shall be run to verify the top of the cement. Temperature survey will be run a minimum of six hours after pumping cement and ideally between 8-10 hours after completing the cement job.

b. Wait on cement (WOC) time for a primary cement job will be a minimum of **8 hours** or 500 pounds compressive strength, whichever is greater. (This is to include the lead cement)
c. Wait on cement (WOC) time for a remedial job will be a minimum of 4 hours after bringing cement to surface or 500 pounds compressive strength, whichever is greater.
d. If cement falls back, remedial cementing will be done prior to drilling out that string.

2. **CASING TO BE KEPT AT LEAST HALF FULL DURING RUN.** The minimum required fill of cement behind the **9-5/8** inch intermediate casing is:

- Cement to surface. If cement does not circulate see B.1.a, c-d above.

Operator has proposed to pump down 9-5/8" X 13-3/8" annulus. Operator must top out cement after the bradenhead squeeze and verify cement to surface. Operator can also check TOC with Echo-meter. CBL must be run from TD of the 9-5/8" casing to surface if confidence is lacking on the quality of the bradenhead squeeze cement job. Submit results to BLM.

If cement does not tie-back into the previous casing shoe, a third stage remediation BH may be performed. The appropriate BLM office shall be notified.

Bradenhead squeeze in the production interval is only as an edge case remediation measure and is NOT approved in this COA. If production cement job experiences losses and a bradenhead squeeze is needed for tie-back, BLM Engineering should be notified prior to job with volumes and planned wellbore schematic. CBL will be needed when this occurs.

If cement does not reach surface, the next casing string must come to surface. Operator must use a limited flush fluid volume of 1 bbl following backside cementing procedures.

3. The minimum required fill of cement behind the **5-1/2** inch production casing is:

- Cement should tie-back at least **200 feet** into previous casing string. Operator shall provide method of verification.

Casing Design B:

1. The **10-3/4** inch surface casing shall be set at approximately **1272** feet (a minimum of 25 feet (Lea County) into the Rustler Anhydrite, above the salt, and below usable fresh water) and cemented to the surface.

a. If cement does not circulate to the surface, the appropriate BLM office shall be notified and a temperature survey utilizing an electronic type temperature survey with surface log readout will be used or a cement bond log shall be run to verify the top of the cement. Temperature survey will be run a minimum of six hours after pumping cement and ideally between 8-10 hours after completing the cement job.
b. Wait on cement (WOC) time for a primary cement job will be a minimum of **8 hours** or 500 pounds compressive strength, whichever is greater. (This is to include the lead cement)
c. Wait on cement (WOC) time for a remedial job will be a minimum of 4 hours after bringing cement to surface or 500 pounds compressive strength, whichever is greater.
d. If cement falls back, remedial cementing will be done prior to drilling out that string.

2. **CASING TO BE KEPT AT LEAST HALF FULL DURING RUN.** The minimum required fill of cement behind the **8-5/8** inch intermediate casing is:

- Cement to surface. If cement does not circulate see B.1.a, c-d above.

Operator has proposed to pump down 8-5/8" X 10-3/4" annulus. Operator must top out cement after the bradenhead squeeze and verify cement to surface. Operator can also check TOC with Echo-meter. CBL must be run from TD of the 9-5/8" casing to surface if confidence is lacking on the quality of the bradenhead squeeze cement job. Submit results to BLM.

If cement does not tie-back into the previous casing shoe, a third stage remediation BH may be performed. The appropriate BLM office shall be notified.

Bradenhead squeeze in the production interval is only as an edge case remediation measure and is NOT approved in this COA. If production cement job experiences losses and a bradenhead squeeze is needed for tie-back, BLM Engineering should be notified prior to job with volumes and planned wellbore schematic. CBL will be needed when this occurs.

If cement does not reach surface, the next casing string must come to surface. Operator must use a limited flush fluid volume of 1 bbl following backside cementing procedures.

3. The minimum required fill of cement behind the **5-1/2** inch production casing is:

- Cement should tie-back at least **200 feet** into previous casing string. Operator shall provide method of verification.

Casing Design C:

1. The **13-3/8** inch surface casing shall be set at approximately **1272** feet (a minimum of 25 feet (Lea County) into the Rustler Anhydrite, above the salt, and below usable fresh water) and cemented to the surface.

    a. If cement does not circulate to the surface, the appropriate BLM office shall be notified and a temperature survey utilizing an electronic type temperature survey with surface log readout will be used or a cement bond log shall be run to verify the top of the cement. Temperature survey will be run a minimum of six hours after pumping cement and ideally between 8-10 hours after completing the cement job.
    b. Wait on cement (WOC) time for a primary cement job will be a minimum of **8 hours** or 500 pounds compressive strength, whichever is greater. (This is to include the lead cement)
    c. Wait on cement (WOC) time for a remedial job will be a minimum of 4 hours after bringing cement to surface or 500 pounds compressive strength, whichever is greater.
    d. If cement falls back, remedial cementing will be done prior to drilling out that string.

2. **CASING TO BE KEPT AT LEAST HALF FULL DURING RUN.** The minimum required fill of cement behind the **9-5/8** inch intermediate casing is:

    - Cement to surface. If cement does not circulate see B.1.a, c-d above.

Operator has proposed to pump down 9-5/8" X 13-3/8" annulus. Operator must top out cement after the bradenhead squeeze and verify cement to surface. Operator can also check TOC with Echo-meter. CBL must be run from TD of the 9-5/8" casing to surface if confidence is lacking on the quality of the bradenhead squeeze cement job. Submit results to BLM.

If cement does not tie-back into the previous casing shoe, a third stage remediation BH may be performed. The appropriate BLM office shall be notified.

Bradenhead squeeze in the production interval is only as an edge case remediation measure and is NOT approved in this COA. If production cement job experiences losses and a bradenhead squeeze is needed for tie-back, BLM Engineering should be notified prior to job with volumes and planned wellbore schematic. CBL will be needed when this occurs.

If cement does not reach surface, the next casing string must come to surface. Operator must use a limited flush fluid volume of 1 bbl following backside cementing procedures.

3. The minimum required fill of cement behind the **6** inch production casing is:

- Cement should tie-back at least **200 feet** into previous casing string. Operator shall provide method of verification.

Casing Design D:

1. The **13-3/8** inch surface casing shall be set at approximately **1272** feet (a minimum of 25 feet (Lea County) into the Rustler Anhydrite, above the salt, and below usable fresh water) and cemented to the surface.

    a. If cement does not circulate to the surface, the appropriate BLM office shall be notified and a temperature survey utilizing an electronic type temperature survey with surface log readout will be used or a cement bond log shall be run to verify the top of the cement. Temperature survey will be run a minimum of six hours after pumping cement and ideally between 8-10 hours after completing the cement job.
    b. Wait on cement (WOC) time for a primary cement job will be a minimum of **8 hours** or 500 pounds compressive strength, whichever is greater. (This is to include the lead cement)
    c. Wait on cement (WOC) time for a remedial job will be a minimum of 4 hours after bringing cement to surface or 500 pounds compressive strength, whichever is greater.
    d. If cement falls back, remedial cementing will be done prior to drilling out that string.

2. **CASING TO BE KEPT AT LEAST HALF FULL DURING RUN.** The minimum required fill of cement behind the **9-5/8** inch intermediate casing is:

    - Cement to surface. If cement does not circulate see B.1.a, c-d above.

Operator has proposed to pump down 9-5/8" X 13-3/8" annulus. Operator must top out cement after the bradenhead squeeze and verify cement to surface. Operator can also check TOC with Echo-meter. CBL must be run from TD of the 9-5/8" casing to surface if confidence is lacking on the quality of the bradenhead squeeze cement job. Submit results to BLM.

If cement does not tie-back into the previous casing shoe, a third stage remediation BH may be performed. The appropriate BLM office shall be notified.

Bradenhead squeeze in the production interval is only as an edge case remediation measure and is NOT approved in this COA. If production cement job experiences losses and a bradenhead squeeze is needed for tie-back, BLM Engineering should be notified prior to job with volumes and planned wellbore schematic. CBL will be needed when this occurs.

If cement does not reach surface, the next casing string must come to surface.

Operator must use a limited flush fluid volume of 1 bbl following backside cementing procedures.

3. The minimum required fill of cement behind the **6 X 5-1/2** inch production casing is:

    - Cement should tie-back at least **200 feet** into previous casing string. Operator shall provide method of verification.

NOTE ON PRODUCTION CASING FOR ALTERNATE DESIGN: OPERATOR HAS REQUESTED TO RUN 6" OR 5.5" OR A TAPERED STRING WITH BOTH. ALL THREE OPTIONS REVIEWED AND IS OK.

C. PRESSURE CONTROL

1. Variance approved to use flex line from BOP to choke manifold. Manufacturer's specification to be readily available. No external damage to flex line. Flex line to be installed as straight as possible (no hard bends).'

2. Operator has proposed a multi-bowl wellhead assembly. This assembly will only be tested when installed on the **13-3/8** inch surface casing. Minimum working pressure of the blowout preventer (BOP) and related equipment (BOPE) required for drilling below the surface casing shoe shall be **5000 (5M)** psi. **Variance is approved to use a 5000 (5M) Annular which shall be tested to 3500 (70% Working Pressure) psi.**

    a. Wellhead shall be installed by manufacturer's representatives, submit documentation with subsequent sundry.
    b. If the welding is performed by a third party, the manufacturer's representative shall monitor the temperature to verify that it does not exceed the maximum temperature of the seal.
    c. Manufacturer representative shall install the test plug for the initial BOP test.
    d. If the cement does not circulate and one inch operations would have been possible with a standard wellhead, the well head shall be cut off, cementing operations performed and another wellhead installed.
    e. Whenever any seal subject to test pressure is broken, all the tests in OOGO2.III.A.2.i must be followed.

D. SPECIAL REQUIREMENT (S)

Communitization Agreement

- The operator will submit a Communitization Agreement to the Santa Fe Office, 301 Dinosaur Trail Santa Fe, New Mexico 87508, at least 90 days before the anticipated date of first production from a well subject to a spacing order issued by the New Mexico Oil Conservation Division. The Communitization Agreement will include the signatures of all working interest owners in all Federal and Indian leases subject to the Communitization Agreement (i.e., operating rights owners and lessees of record), or certification that the operator has obtained the written signatures of all such owners and will make those signatures available to the BLM immediately upon request.

- The operator will submit an as-drilled survey well plat of the well completion, but are not limited to, those specified in Onshore Order 1 and 2.
- If the operator does not comply with this condition of approval, the BLM may take enforcement actions that include, but are not limited to, those specified in 43 CFR 3163.1.
- In addition, the well sign shall include the surface and bottom hole lease numbers. When the Communitization Agreement number is known, it shall also be on the sign.

(Note: For a minimum 5M BOPE or less (Utilizing a 10M BOPE system)
BOPE Break Testing Variance

- BOPE Break Testing is ONLY permitted for 5M BOPE or less. **(Annular preventer must be tested to a minimum of 70% of BOPE working pressure and shall be higher than the MASP)**
- BOPE Break Testing is NOT permitted to drilling the production hole section.
- Variance only pertains to the intermediate hole-sections and no deeper than the Bone Springs formation.
- While in transfer between wells, the BOPE shall be secured by the hydraulic carrier or cradle.
- Any well control event while drilling require notification to the BLM Petroleum Engineer **(575-706-2779)** prior to the commencement of any BOPE Break Testing operations.
- A full BOPE test is required prior to drilling the first deep intermediate hole section. If any subsequent hole interval is deeper than the first, a full BOPE test will be required. (200' TVD tolerance between intermediate shoes is allowable).
- The BLM is to be contacted (575-689-5981 Lea County) 4 hours prior to BOPE tests.
- As a minimum, a full BOPE test shall be performed at 21-day intervals.
- In the event any repairs or replacement of the BOPE is required, the BOPE shall test as per Onshore Oil and Gas Order No. 2.
- If in the event break testing is not utilized, then a full BOPE test would be conducted.

Casing Clearance:

i. Overlap clearance OK.
ii. Salt annular variance in place.
iii. 1" surface clearance not met. Operator aware and will perf and squeeze if necessary

Operator shall clean up cycles until wellbore is clear of cuttings and any large debris, ensure cutting sizes are adequate "coffee ground or less" before cementing.

Offline Cementing

Offline cementing approved for all three intervals if the qualifying criteria in the procedure are met. Contact the BLM PETs prior to the commencement of any offline cementing procedure.

GENERAL REQUIREMENTS

The BLM is to be notified in advance for a representative to witness:

a. Spudding well (minimum of 24 hours)
b. Setting and/or Cementing of all casing strings (minimum of 4 hours)
c. BOPE tests (minimum of 4 hours)

☒ Eddy County
EMAIL or call the Carlsbad Field Office, 620 East Greene St., Carlsbad, NM 88220,
BLM_NM_CFO_DrillingNotifications@BLM.GOV
(575) 361-2822

☒ Lea County
Call the Hobbs Field Station, 414 West Taylor, Hobbs NM 88240,
(575) 689-5981

1. Unless the production casing has been run and cemented or the well has been properly plugged, the drilling rig shall not be removed from over the hole without prior approval.
    a. In the event the operator has proposed to drill multiple wells utilizing a skid/walking rig. Operator shall secure the wellbore on the current well, after installing and testing the wellhead, by installing a blind flange of like pressure rating to the wellhead and a pressure gauge that can be monitored while drilling is performed on the other well(s).
    b. When the operator proposes to set surface casing with Spudder Rig
        i. Notify the BLM when moving in and removing the Spudder Rig.
        ii. Notify the BLM when moving in the 2nd Rig. Rig to be moved in within 90 days of notification that Spudder Rig has left the location.
        iii. BOP/BOPE test to be conducted per **43 CFR 3172** as soon as 2nd Rig is rigged up on well.
2. Floor controls are required for 3M or Greater systems. These controls will be on the rig floor, unobstructed, readily accessible to the driller and will be operational at all times during drilling and/or completion activities. Rig floor is defined as the area immediately around the rotary table; the area immediately above the substructure on which the draw works are located, this does not include the dog house or stairway area.
3. For intervals in which cement to surface is required, cement to surface should be verified with a visual check and density or pH check to differentiate cement from

spacer and drilling mud. The results should be documented in the driller's log and daily reports.

A. CASING

1. Changes to the approved APD casing program need prior approval if the items substituted are of lesser grade or different casing size or are Non-API. The Operator can exchange the components of the proposal with that of superior strength (i.e. changing from J-55 to N-80, or from 36# to 40#). Changes to the approved cement program need prior approval if the altered cement plan has less volume or strength or if the changes are substantial (i.e. Multistage tool, ECP, etc.). The initial wellhead installed on the well will remain on the well with spools used as needed.
2. Wait on cement (WOC) for Potash Areas: After cementing but before commencing any tests, the casing string shall stand cemented under pressure until both of the following conditions have been met: 1) cement reaches a minimum compressive strength of 500 psi for all cement blends of both lead and tail cement, 2) until cement has been in place at least 8 hours. WOC time will be recorded in the driller's log. The casing integrity test can be done (prior to the cement setting up) immediately after bumping the plug.
3. Wait on cement (WOC) for Water Basin: After cementing but before commencing any tests, the casing string shall stand cemented under pressure until both of the following conditions have been met: 1) cement reaches a minimum compressive strength of 500 psi at the shoe, 2) until cement has been in place at least 8 hours. WOC time will be recorded in the driller's log. See individual casing strings for details regarding lead cement slurry requirements. The casing integrity test can be done (prior to the cement setting up) immediately after bumping the plug.
4. Provide compressive strengths including hours to reach required 500 pounds compressive strength prior to cementing each casing string. Have well specific cement details onsite prior to pumping the cement for each casing string.
5. No pea gravel permitted for remedial or fall back remedial without prior authorization from the BLM engineer.
6. On that portion of any well approved for a 5M BOPE system or greater, a pressure integrity test of each casing shoe shall be performed. Formation at the shoe shall be tested to a minimum of the mud weight equivalent anticipated to control the formation pressure to the next casing depth or at total depth of the well. This test shall be performed before drilling more than 20 feet of new hole.

7. If hardband drill pipe is rotated inside casing, returns will be monitored for metal. If metal is found in samples, drill pipe will be pulled and rubber protectors which have a larger diameter than the tool joints of the drill pipe will be installed prior to continuing drilling operations.
8. Whenever a casing string is cemented in the R-111-Q potash area, the NMOCD requirements shall be followed.

B. PRESSURE CONTROL

1. All blowout preventer (BOP) and related equipment (BOPE) shall comply with well control requirements as described in **43 CFR 3172**.
2. If a variance is approved for a flexible hose to be installed from the BOP to the choke manifold, the following requirements apply: The flex line must meet the requirements of API 16C. Check condition of flexible line from BOP to choke manifold, replace if exterior is damaged or if line fails test. Line to be as straight as possible with no hard bends and is to be anchored according to Manufacturer's requirements. The flexible hose can be exchanged with a hose of equal size and equal or greater pressure rating. Anchor requirements, specification sheet and hydrostatic pressure test certification matching the hose in service, to be onsite for review. These documents shall be posted in the company man's trailer and on the rig floor.
3. 5M or higher system requires an HCR valve, remote kill line and annular to match. The remote kill line is to be installed prior to testing the system and tested to stack pressure.
4. If the operator has proposed a multi-bowl wellhead assembly in the APD. The following requirements must be met:
    i. Wellhead shall be installed by manufacturer's representatives, submit documentation with subsequent sundry.
    ii. If the welding is performed by a third party, the manufacturer's representative shall monitor the temperature to verify that it does not exceed the maximum temperature of the seal.
    iii. Manufacturer representative shall install the test plug for the initial BOP test.
    iv. Whenever any seal subject to test pressure is broken, all the tests in 43 CFR 3172.6(b)(9) must be followed.
    v. If the cement does not circulate and one inch operations would have been possible with a standard wellhead, the well head shall be cut off, cementing operations performed and another wellhead installed.

5. The appropriate BLM office shall be notified a minimum of 4 hours in advance for a representative to witness the tests.
    i. In a water basin, for all casing strings utilizing slips, these are to be set as soon as the crew and rig are ready and any fallback cement remediation has been done. The casing cut-off and BOP installation can be initiated four hours after installing the slips, which will be approximately six hours after bumping the plug. For those casing strings not using slips, the minimum wait time before cut-off is eight hours after bumping the plug. BOP/BOPE testing can begin after cut-off or once cement reaches 500 psi compressive strength (including lead cement), whichever is greater. However, if the float does not hold, cut-off cannot be initiated until cement reaches 500 psi compressive strength (including lead when specified).
    ii. In potash areas, for all casing strings utilizing slips, these are to be set as soon as the crew and rig are ready and any fallback cement remediation has been done. For all casing strings, casing cut-off and BOP installation can be initiated at twelve hours after bumping the cement plug. The BOPE test can be initiated after bumping the cement plug with the casing valve open. (only applies to single stage cement jobs, prior to the cement setting up.)
    iii. The tests shall be done by an independent service company utilizing a test plug not a cup or J-packer and can be initiated immediately with the casing valve open. The operator also has the option of utilizing an independent tester to test without a plug (i.e. against the casing) pursuant to **43 CFR 3172** with the pressure not to exceed 70% of the burst rating for the casing. Any test against the casing must meet the WOC time for 8 hours or 500 pounds compressive strength, whichever is greater, prior to initiating the test (see casing segment as lead cement may be critical item).
    iv. The test shall be run on a 5000 psi chart for a 2-3M BOP/BOP, on a 10000 psi chart for a 5M BOP/BOPE and on a 15000 psi chart for a 10M BOP/BOPE. If a linear chart is used, it shall be a one hour chart. A circular chart shall have a maximum 2 hour clock. If a twelve hour or twenty-four hour chart is used, tester shall make a notation that it is run with a two hour clock.
    v. The results of the test shall be reported to the appropriate BLM office.
    vi. All tests are required to be recorded on a calibrated test chart. A copy of the BOP/BOPE test chart and a copy of independent

service company test will be submitted to the appropriate BLM office.

vii. The BOP/BOPE test shall include a low pressure test from 250 to 300 psi. The test will be held for a minimum of 10 minutes if test is done with a test plug and 30 minutes without a test plug. This test shall be performed prior to the test at full stack pressure.

viii. BOP/BOPE must be tested by an independent service company within 500 feet of the top of the Wolfcamp formation if the time between the setting of the intermediate casing and reaching this depth exceeds 20 days. This test does not exclude the test prior to drilling out the casing shoe as per **43 CFR 3172**.

C. DRILLING MUD

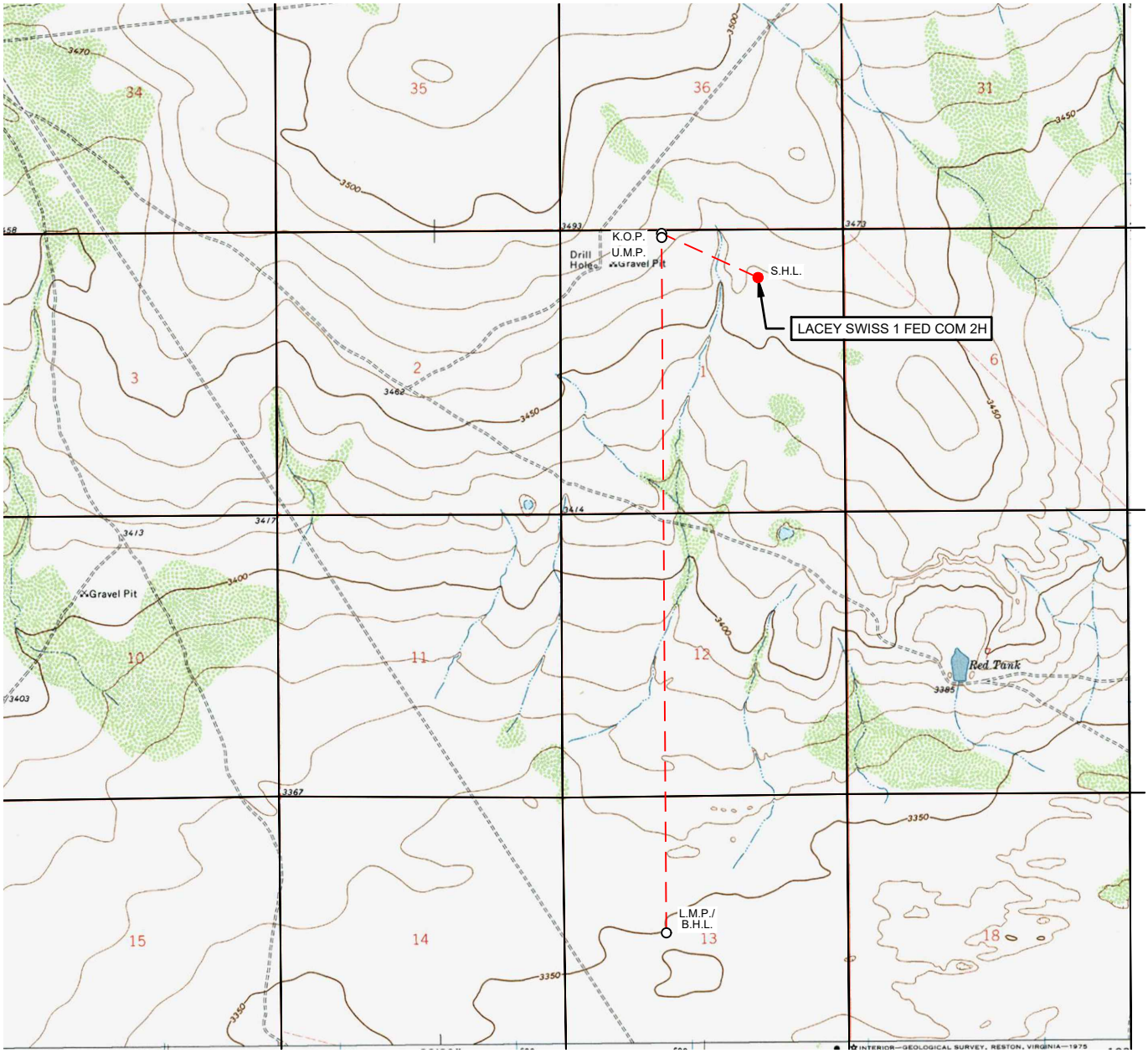
Mud system monitoring equipment, with derrick floor indicators and visual and audio alarms, shall be operating before drilling into the Wolfcamp formation, and shall be used until production casing is run and cemented.

D. WASTE MATERIAL AND FLUIDS

All waste (i.e. drilling fluids, trash, salts, chemicals, sewage, gray water, etc.) created as a result of drilling operations and completion operations shall be safely contained and disposed of properly at a waste disposal facility. No waste material or fluid shall be disposed of on the well location or surrounding area. Porto-johns and trash containers will be on-location during fracturing operations or any other crew-intensive operations.

JS 3/12/2025

LOCATION & ELEVATION VERIFICATION MAP



eog resources, inc.

LEASE NAME & WELL NO.: LACEY SWISS 1 FED COM 2H

SECTION 1 TWP 25-S RGE 33-E SURVEY N.M.P.M.
COUNTY LEA STATE NM ELEVATION 3459'
DESCRIPTION 884' FNL & 1540' FEL

LATITUDE N 32.1643737 LONGITUDE W 103.5224815

N

SCALE: 1" = 3000'
0' 1500' 3000'

THIS EASEMENT/SERVITUDE LOCATION SHOWN HEREON HAS BEEN SURVEYED ON THE GROUND UNDER MY SUPERVISION AND PREPARED ACCORDING TO THE EVIDENCE FOUND AT THE TIME OF SURVEY, AND DATA PROVIDED BY EOG RESOURCES, INC. THIS CERTIFICATION IS MADE AND LIMITED TO THOSE PERSONS OR ENTITIES SHOWN ON THE FACE OF THIS PLAT AND IS NON-TRANSFERABLE. THIS SURVEY IS CERTIFIED FOR THIS TRANSACTION ONLY.

ALL BEARINGS, DISTANCES, AND COORDINATE VALUES CONTAINED HEREON ARE GRID BASED UPON THE NEW MEXICO COORDINATE SYSTEM OF 1983, EAST ZONE, U.S. SURVEY FEET.

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2903 NORTH BIG SPRING • MIDLAND, TEXAS 79705
TELEPHONE: (432) 682-1653 OR (800) 767-1653 • FAX (432) 682-1743
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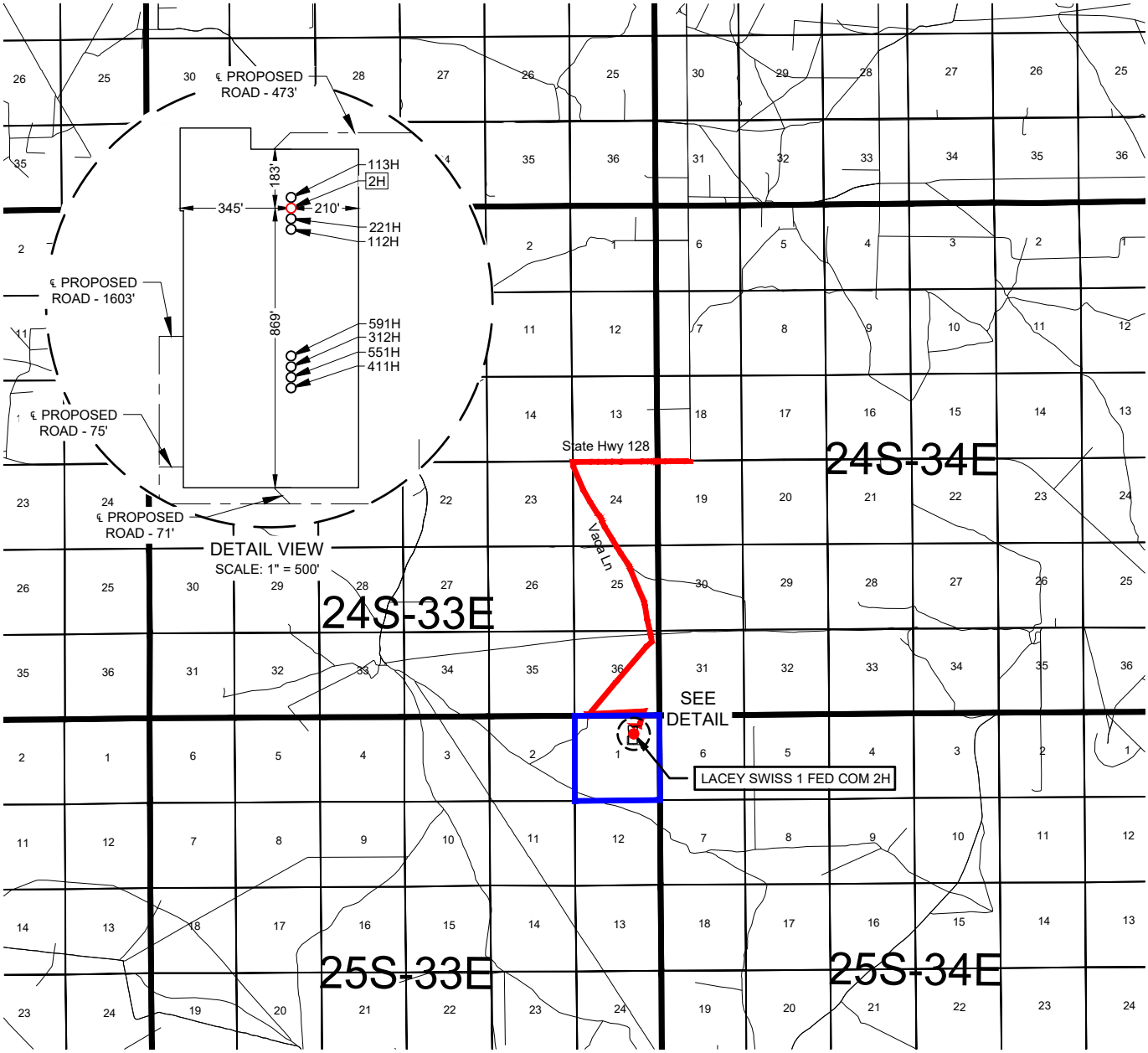
EXHIBIT 2

VICINITY MAP



eog resources, inc.

LEASE NAME & WELL NO.: LACEY SWISS 1 FED COM 2H

SECTION 1 TWP 25-S RGE 33-E SURVEY N.M.P.M.
COUNTY LEA STATE NM
DESCRIPTION 884' FNL & 1540' FEL

DISTANCE & DIRECTION

FROM INT. OF NM-128, & DELAWARE BASIN RD., GO WEST ON NM-128 ±1.4 MILES, THENCE SOUTH (LEFT) ON VACA LN. ±3.5 MILES, THENCE EAST (LEFT) ON A LEASE RD. ±0.6 MILES, THENCE CONTINUE SOUTH ON A PROPOSED RD. ±1234 FEET, THENCE WEST (RIGHT) ON A PROPOSED RD. ±473 FEET TO A POINT ±190 FEET NORTHWEST OF THE LOCATION.

THIS EASEMENT/SERVITUDE LOCATION SHOWN HEREON HAS BEEN SURVEYED ON THE GROUND UNDER MY SUPERVISION AND PREPARED ACCORDING TO THE EVIDENCE FOUND AT THE TIME OF SURVEY, AND DATA PROVIDED BY EOG RESOURCES, INC. THIS CERTIFICATION IS MADE AND LIMITED TO THOSE PERSONS OR ENTITIES SHOWN ON THE FACE OF THIS PLAT AND IS NON-TRANSFERABLE. THIS SURVEY IS CERTIFIED FOR THIS TRANSACTION ONLY.

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–N–

SCALE: 1" = 10000'

0' 5000' 10000'

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EXHIBIT 2A

SECTION 1, TOWNSHIP 25-S, RANGE 33-E, N.M.P.M.
LEA COUNTY, NEW MEXICO

SURFACE LOCATION (SHL)
NEW MEXICO EAST
NAD 1983
X=792246 Y=424479
LAT.: N 32.1643737
LONG.: W 103.5224815
884' FNL 1540' FEL

KICK OFF POINT (KOP)
NEW MEXICO EAST
NAD 1983
X=790446 Y=425302
LAT.: N 32.1666727
LONG.: W 103.5282772
50' FNL 1950' FWL

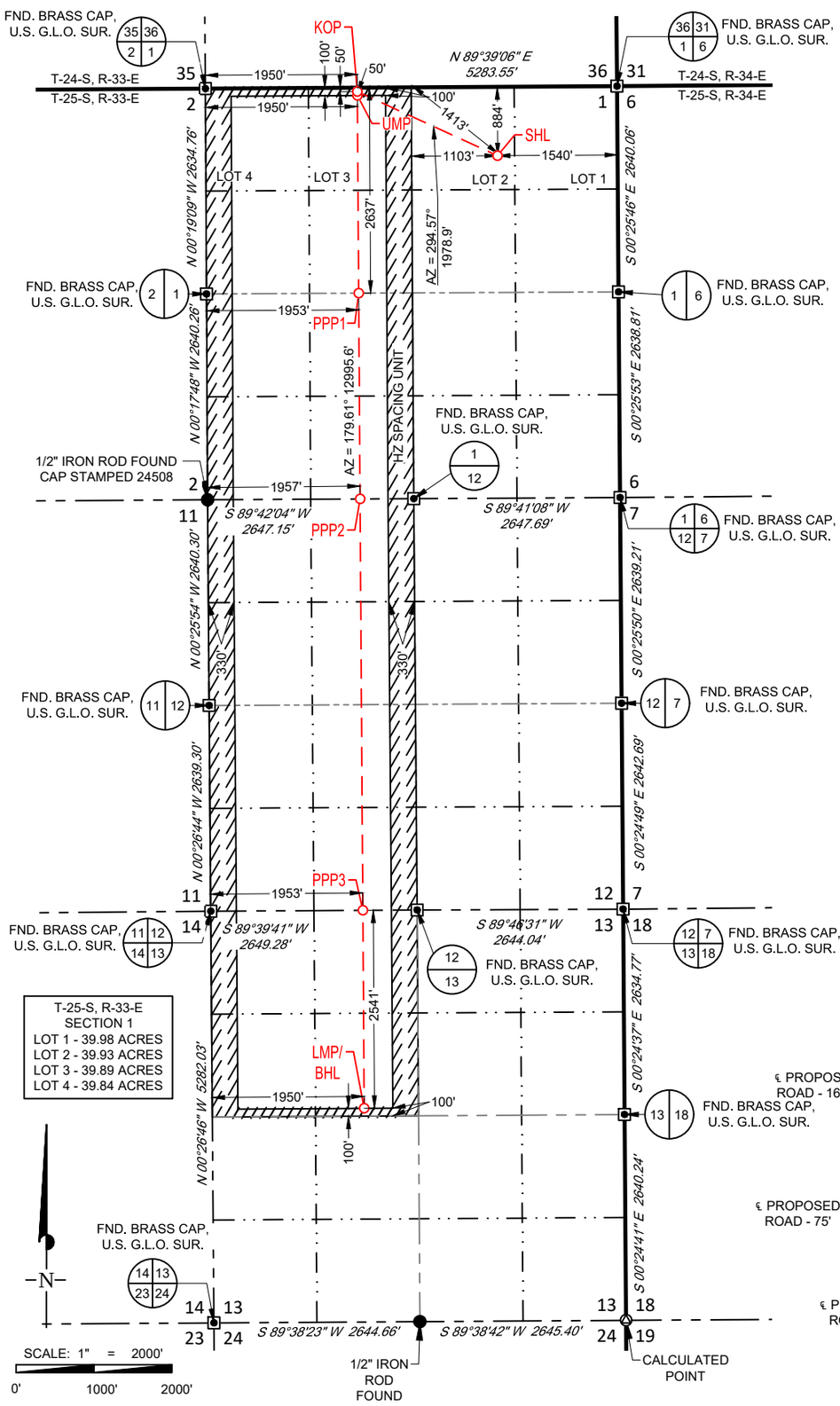
UPPER MOST PERF. (UMP)
NEW MEXICO EAST
NAD 1983
X=790447 Y=425252
LAT.: N 32.1665353
LONG.: W 103.5282773
100' FNL 1950' FWL

PROPOSED PERF. POINT (PPP1)
NEW MEXICO EAST
NAD 1983
X=790464 Y=422716
LAT.: N 32.1595625
LONG.: W 103.5282832
2637' FNL 1953' FWL

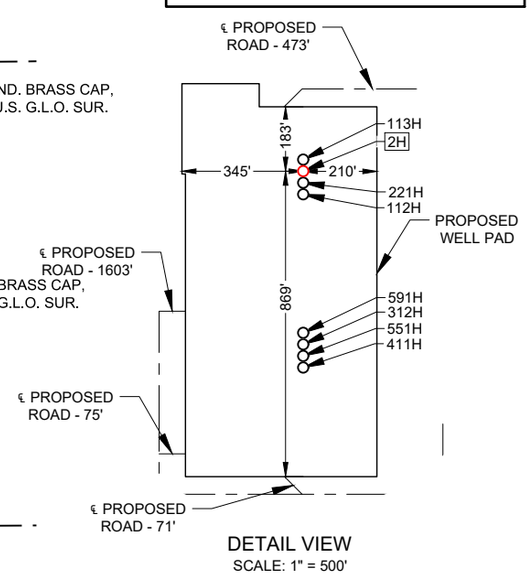
PROPOSED PERF. POINT (PPP2)
NEW MEXICO EAST
NAD 1983
X=790482 Y=420076
LAT.: N 32.1523059
LONG.: W 103.5282893
0' FSL 1957' FWL

PROPOSED PERF. POINT (PPP3)
NEW MEXICO EAST
NAD 1983
X=790517 Y=414798
LAT.: N 32.1377973
LONG.: W 103.5283014
0' FSL 1953' FWL

LOWER MOST PERF. (LMP)
BOTTOM HOLE LOCATION (BHL)
NEW MEXICO EAST
NAD 1983
X=790535 Y=412257
LAT.: N 32.1308137
LONG.: W 103.5283072
2541' FNL 1950' FWL



T-25-S, R-33-E
SECTION 1
LOT 1 - 39.98 ACRES
LOT 2 - 39.93 ACRES
LOT 3 - 39.89 ACRES
LOT 4 - 39.84 ACRES



DETAIL VIEW
SCALE: 1" = 500'

LEASE NAME & WELL NO.: LACEY SWISS 1 FED COM 2H

SECTION 1 TWP 25-S RGE 33-E SURVEY N.M.P.M.
COUNTY LEA STATE NM
DESCRIPTION 884' FNL & 1540' FEL

DISTANCE & DIRECTION
FROM INT. OF NM-128, & DELAWARE BASIN RD., GO WEST ON NM-128 ±1.4 MILES, THENCE SOUTH (LEFT) ON VACA LN. ±3.5 MILES, THENCE EAST (LEFT) ON A LEASE RD. ±0.6 MILES, THENCE CONTINUE SOUTH ON A PROPOSED RD. ±1234 FEET, THENCE WEST (RIGHT) ON A PROPOSED RD. ±473 FEET TO A POINT ±190 FEET NORTHWEST OF THE LOCATION.

ALL BEARINGS, DISTANCES, AND COORDINATE VALUES CONTAINED HEREON ARE GRID BASED UPON THE NEW MEXICO COORDINATE SYSTEM OF 1983, EAST ZONE, U.S. SURVEY FEET.

THIS EASEMENT/SERVITUDE LOCATION SHOWN HEREON HAS BEEN SURVEYED ON THE GROUND UNDER MY SUPERVISION AND PREPARED ACCORDING TO THE EVIDENCE FOUND AT THE TIME OF SURVEY, AND DATA PROVIDED BY EOG RESOURCES, INC. THIS CERTIFICATION IS MADE AND LIMITED TO THOSE PERSONS OR ENTITIES SHOWN ON THE FACE OF THIS PLAT AND IS NON-TRANSFERABLE. THIS SURVEY IS CERTIFIED FOR THIS TRANSACTION ONLY.

RAMON DOMINGUEZ NEW MEXICO 24508 PROFESSIONAL SURVEYOR

2/18/2025 3:11:42 PM

Ramon A. Dominguez, P.S. No. 24508

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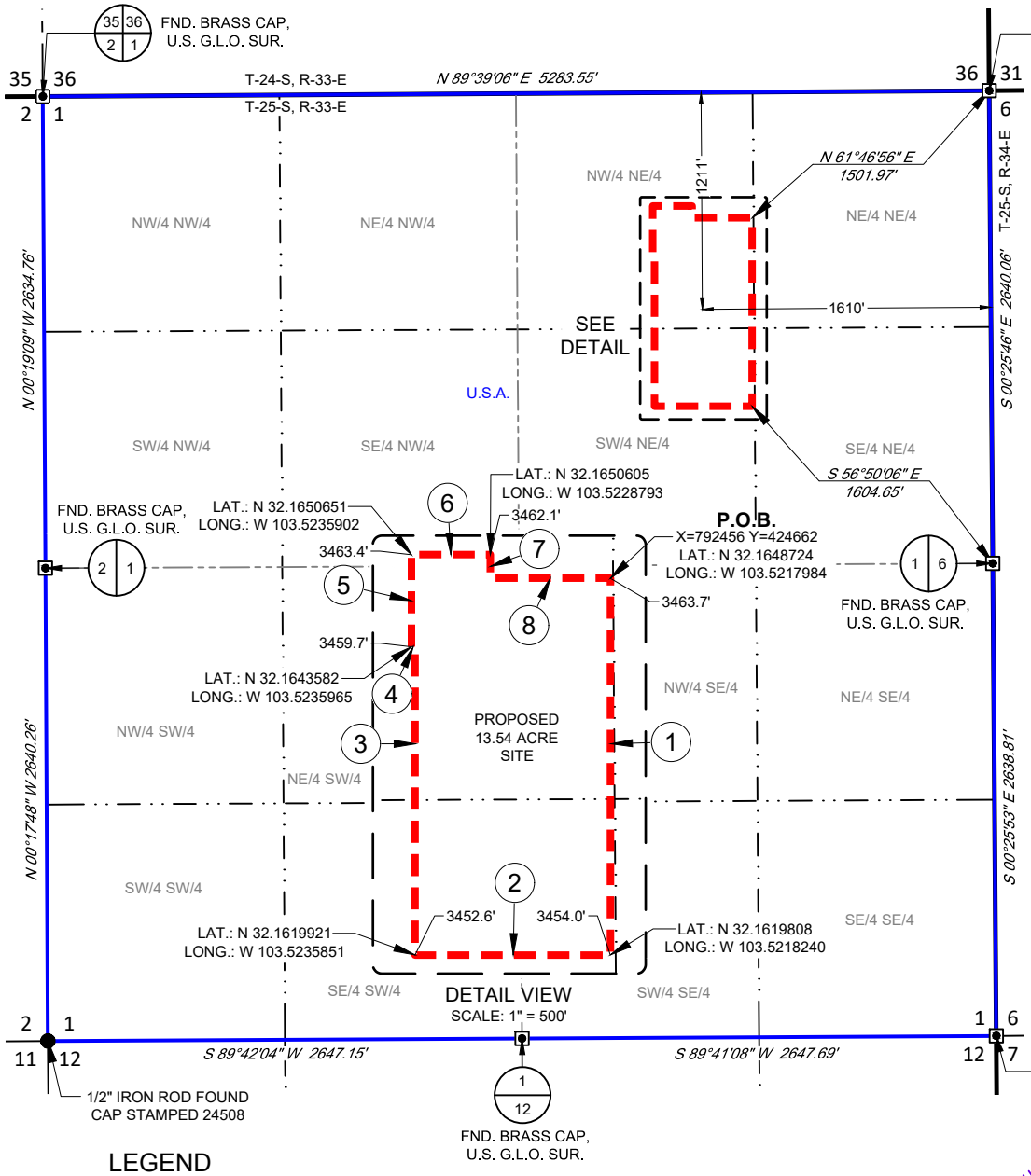
SCALE: 1" = 1000'
0' 500' 1000'

SECTION 1, TOWNSHIP 25-S, RANGE 33-E, N.M.P.M.
LEA COUNTY, NEW MEXICO



PAD D
LACEY SWISS 1 FED COM 2H

Metes and Bounds Description of a proposed 13.54 acre pad site located within Section 1, Township 25 South, Range 33 East, N.M.P.M., in Lea County, New Mexico.

BEGINNING at a point for the Northeast corner of this site, from whence a brass cap found for the Northeast corner of said Section 1, bears: N 61°46'56" E, a distance of 1501.97 feet;

Thence S 00°00'01" W, a distance of 1052.00 feet to a point for the Southeast corner of this site;

Thence S 90°00'00" W, a distance of 545.00 feet to a point for the Southwest corner of this site;

Thence N 00°00'00" W, a distance of 860.74 feet to a point for an interior ell corner of this site;

Thence N 90°00'00" W, a distance of 10.00 feet to a point for an exterior ell corner of this site;

Thence N 00°00'00" W, a distance of 257.19 feet to a point for the Northwest corner of this site;

Thence N 90°00'00" E, a distance of 220.00 feet to a point for an exterior ell corner of this site;

Thence S 00°00'00" E, a distance of 65.93 feet to a point for an interior ell corner of this site;

Thence S 89°59'59" E, a distance of 335.00 feet to the Point of Beginning.

LINE TABLE

LINE	BEARING	DISTANCE
1	S 00°00'01" W	1052.00'
2	S 90°00'00" W	545.00'
3	N 00°00'00" W	860.74'
4	N 90°00'00" W	10.00'
5	N 00°00'00" W	257.19'
6	N 90°00'00" E	220.00'
7	S 00°00'00" E	65.93'
8	S 89°59'59" E	335.00'

LEGEND

- TOWNSHIP/RANGE LINE
- SECTION LINE
- QUARTER SECTION LINE
- SIXTEENTH SECTION LINE
- TRACT BORDER
- PROPOSED SITE
- MONUMENT
- IRON ROD FOUND

RAMON DOMINGUEZ NEW MEXICO 24508 PROFESSIONAL SURVEYOR

2/18/2025 3:11:46 PM

Ramon A. Dominguez, P.S. No. 24508

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PAD D LACEY SWISS 1 FED COM 2H	REVISION: INT	DATE
DATE: 02/12/2025		
FILE: LO_LACEY_SWISS_1_FED_COM_2H		
DRAWN BY: GJU		

NOTES:
1. ORIGINAL DOCUMENT SIZE: 8.5" X 11"
2. ALL BEARINGS, DISTANCES, AND COORDINATE VALUES CONTAINED HEREIN ARE GRID BASED UPON THE NEW MEXICO COORDINATE SYSTEM OF 1983, EAST ZONE, U.S. SURVEY FEET.
3. CERTIFICATION IS MADE ONLY TO THE LOCATION OF THIS EASEMENT, IN RELATION TO THE EVIDENCE FOUND DURING A FIELD SURVEY, MADE ON THE GROUND, UNDER MY SUPERVISION, AND USING DOCUMENTATION PROVIDED BY EOG RESOURCES, INC. ONLY UTILITIES/EASEMENTS THAT WERE VISIBLE ON THE DATE OF THIS SURVEY, WITHIN/ADJOINING THIS EASEMENT, HAVE BEEN LOCATED AS SHOWN HEREON OF WHICH I HAVE KNOWLEDGE. THIS CERTIFICATION IS LIMITED TO THOSE PERSONS OR ENTITIES SHOWN ON THE FACE OF THIS PLAT AND IS NON-TRANSFERABLE, AND MADE FOR THIS TRANSACTION ONLY.
4. P.O.B. = POINT OF BEGINNING
5. ADJOINER INFORMATION SHOWN FOR INFORMATIONAL PURPOSES ONLY.

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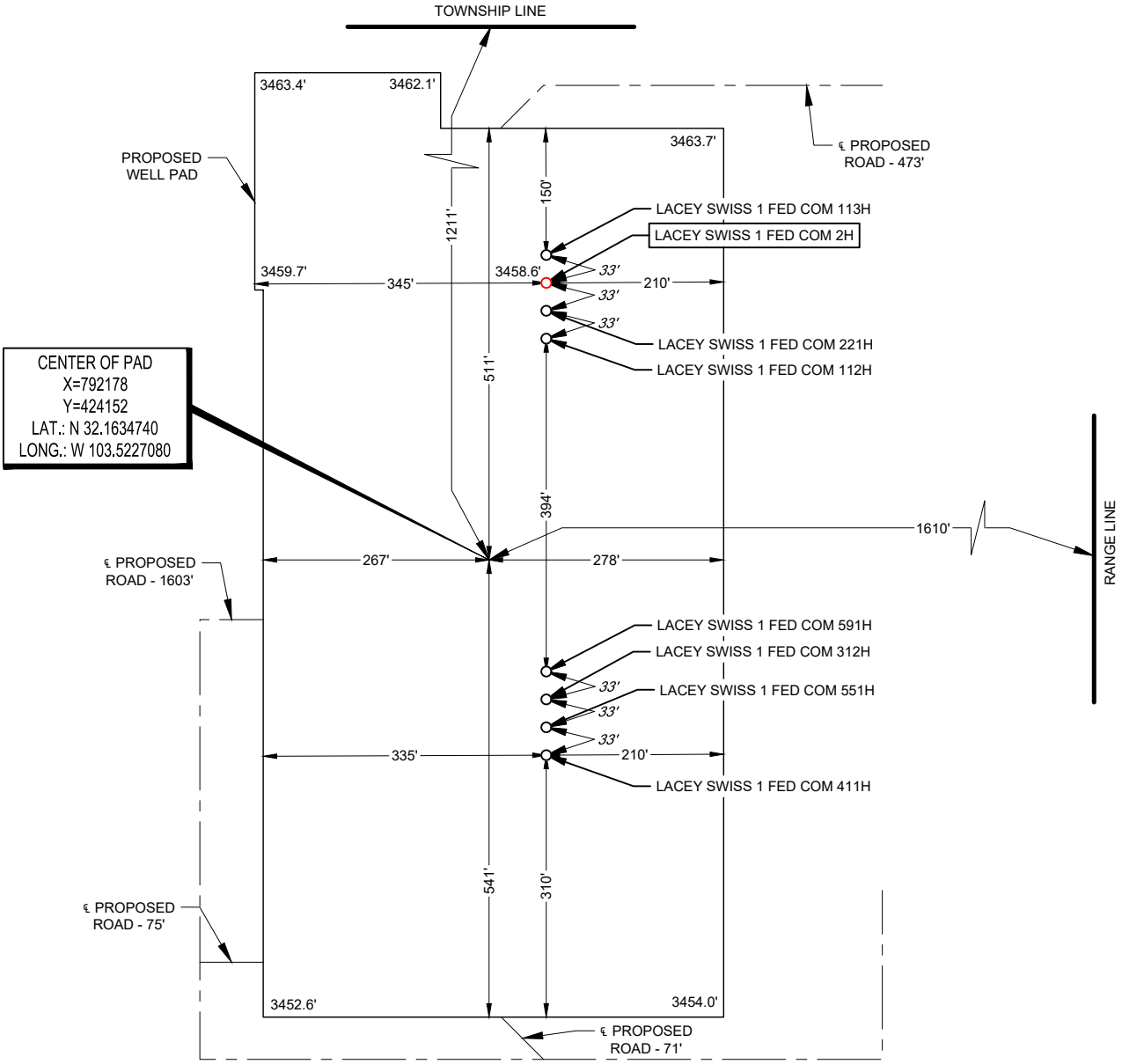
EXHIBIT 2B

eog resources, inc.

LEGEND

TOWNSHIP/RANGE LINE
PROPOSED ROAD

SECTION 1, TOWNSHIP 25-S, RANGE 33-E, N.M.P.M.
LEA COUNTY, NEW MEXICO



LEASE NAME & WELL NO.: LACEY SWISS 1 FED COM 2H

2H LATITUDE N 32.1643737 2H LONGITUDE W 103.5224815

CENTER OF PAD IS 1211' FNL & 1610' FEL

RAMON DOMINGUEZ NEW MEXICO 24508 PROFESSIONAL SURVEYOR

2/18/2025 3:11:49 PM

Ramon A. Dominguez, P.S. No. 24508

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ORIGINAL DOCUMENT SIZE: 8.5" X 11"

–N–

SCALE: 1" = 200'

0' 100' 200'

TOPOGRAPHIC
LOYALTY INNOVATION LEGACY
481 WINSCOTT ROAD, Ste. 200 • BENBROOK, TEXAS 76126
TELEPHONE: (817) 744-7512 • FAX (817) 744-7554
2903 NORTH BIG SPRING • MIDLAND, TEXAS 79705
TELEPHONE: (432) 682-1653 OR (800) 767-1653 • FAX (432) 682-1743
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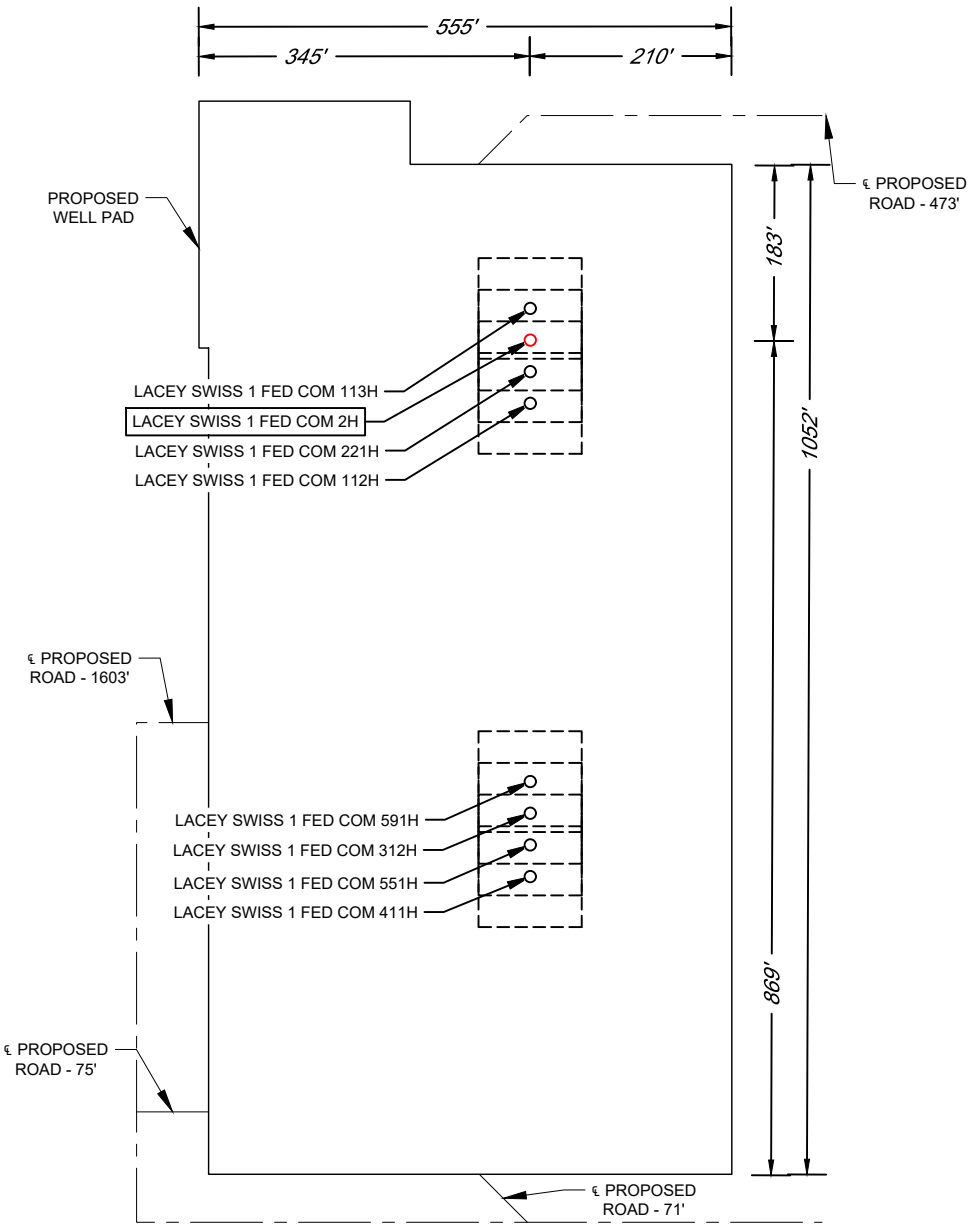
EXHIBIT 2C

RECLAMATION AND FACILITY DIAGRAM - PRODUCTION FACILITIES DIAGRAM

SECTION 1, TOWNSHIP 25-S, RANGE 33-E, N.M.P.M.
LEA COUNTY, NEW MEXICO

DETAIL VIEW
SCALE: 1" = 200'



LEASE NAME & WELL NO.: LACEY SWISS 1 FED COM 2H

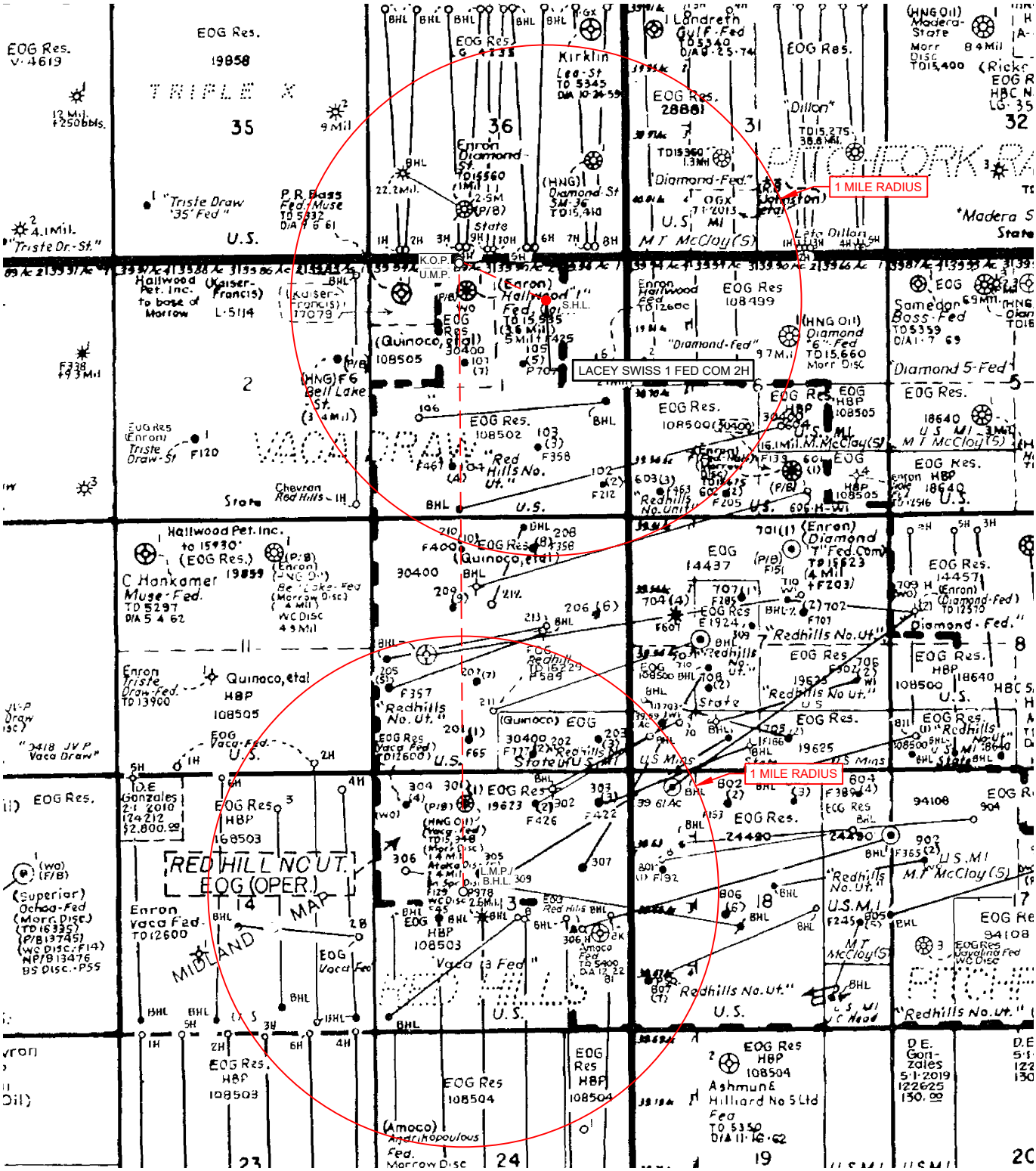
2H LATITUDE N 32.1643737 2H LONGITUDE W 103.5224815

S:\SURVEY\EOG_MIDLAND\LACEY_SWISS_1_FED_COM\FINAL_PRODUCTS\LO_LACEY_SWISS_1_FED_COM_2H.DWG 2/18/2025 3:11:52 PM russell.waterman

EXHIBIT 3

eog resources, inc.

SECTION 1, TOWNSHIP 25-S, RANGE 33-E, N.M.P.M.
LEA COUNTY, NEW MEXICO



LEASE NAME & WELL NO.: LACEY SWISS 1 FED COM 2H

2H LATITUDE N 32.1643737 2H LONGITUDE W 103.5224815

SCALE: NTS

ALL BEARINGS, DISTANCES, AND COORDINATE VALUES CONTAINED HEREON ARE GRID BASED UPON THE NEW MEXICO COORDINATE SYSTEM OF 1983, EAST ZONE, U.S. SURVEY FEET.

THIS EASEMENT/SERVITUDE LOCATION SHOWN HEREON HAS BEEN SURVEYED ON THE GROUND UNDER MY SUPERVISION AND PREPARED ACCORDING TO THE EVIDENCE FOUND AT THE TIME OF SURVEY, AND DATA PROVIDED BY EOG RESOURCES, INC. THIS CERTIFICATION IS MADE AND LIMITED TO THOSE PERSONS OR ENTITIES SHOWN ON THE FACE OF THIS PLAT AND IS NON-TRANSFERABLE. THIS SURVEY IS CERTIFIED FOR THIS TRANSACTION ONLY.

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eog resources

Lacey Swiss 1 Fed Com #2H (FKA 403H) API #: 30-025-53508 Variances

EOG respectfully requests the below variances to be applied to the above well:

- Variance is requested to waive the centralizer requirements for the intermediate casing in the intermediate hole. An expansion additive will be utilized, in the cement slurry, for the entire length of the intermediate interval to maximize cement bond and zonal isolation.
- Variance is also requested to waive the centralizer requirements for the production casing in the production hole. An expansion additive will be utilized, in the cement slurry, for the entire length of the production interval to maximize cement bond and zonal isolation.
- Bradenhead will be the primary option for production cementing. EOG also requests to have the conventional option in place to accommodate for logistical or wellbore conditions. The tie back requirements will be met if the cement is pumped conventionally, and cement volumes will be adjusted accordingly. TOC will be verified by CBL.

- Variance is requested to use a co-flex line between the BOP and choke manifold (instead of using a 4" OD steel line).- Variance is requested to use a 5,000 psi annular BOP with the 10,000 psi BOP stack.
- EOG Resources requests the option to contract a Surface Rig to drill, set surface casing, and Cement on the subject well. After WOC 8 hours or 500 psi compressive strength (whichever is greater), the Surface Rig will move off so the wellhead can be installed. A welder will cut the casing to the proper height and weld on the wellhead (both "A" and "B" sections). The weld will be tested to 1,500 psi. All valves will be closed and a wellhead cap will be installed (diagram attached). If the timing between rigs is such that EOG Resources would not be able to preset the surface, the Primary Rig will MIRU and drill the well in its entirety per the APD.

EOG requests the additional variance(s) in the attached document(s):

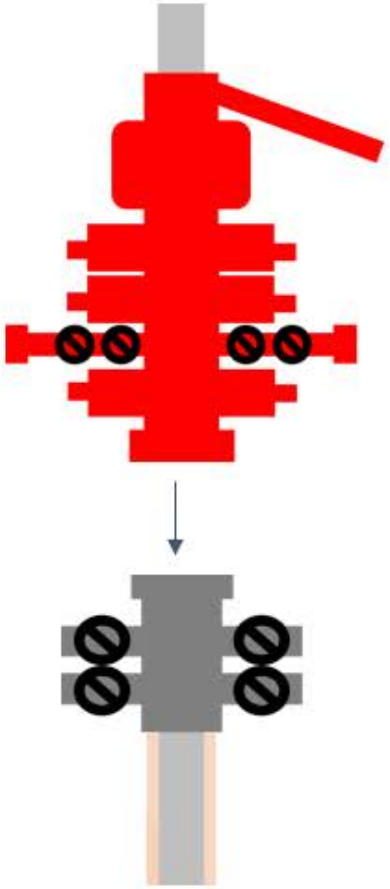
- EOG BLM Variance 3a_b - BOP Break-test and Offline Intermediate Cement
- EOG BLM Variance 3d - Production Offline Cement
- EOG BLM Variance 4a - Salt Section Annular Clearance
- EOG BLM Variance 5a - Alternate Shallow Casing Designs

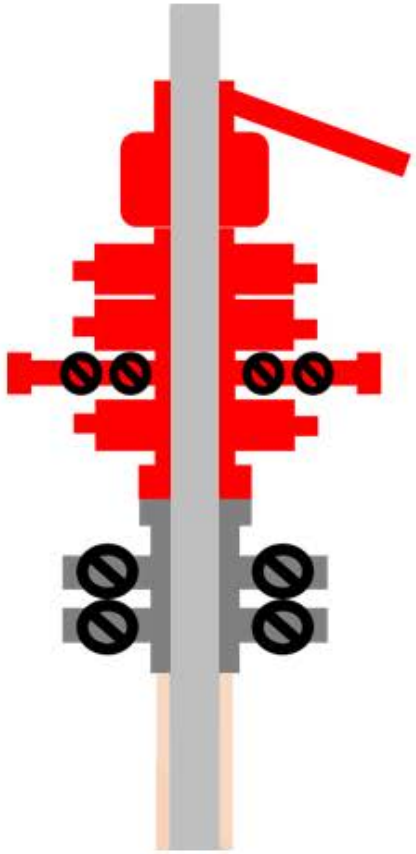
Break-test BOP & Offline Cementing:

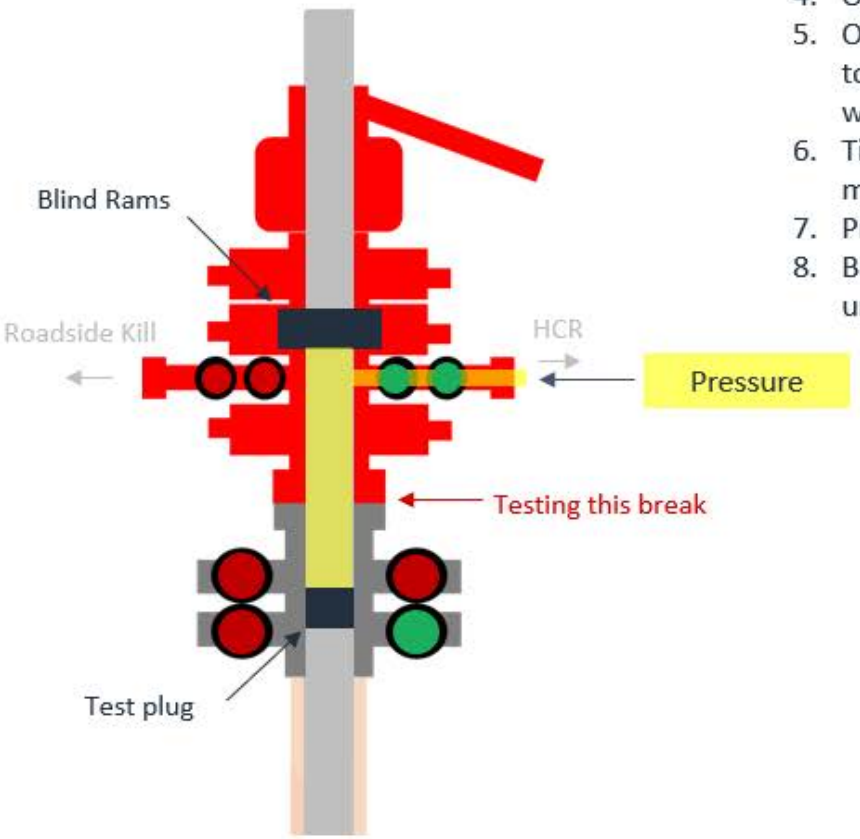
EOG Resources Inc. (EOG) respectfully requests a variance from the minimum standards for well control equipment testing of ECFR Title 43 Part 3172.6(b)(9)(iv) to allow a testing schedule of the blow out preventer (BOP) and blow out prevention equipment (BOPE) along with Batch Drilling & Offline cement operations to include the following:

- Full BOPE test at first installation on the pad.
- Full BOPE test every 21 days.
- This test will be conducted for 5M rated hole intervals only.
- Each rig requesting the break-test variance is capable of picking up the BOP without damaging components using winches, following API Standard 53, Well Control Equipment Systems for Drilling Wells (Fifth edition, December 2018, Annex C. Table C.4) which recognizes break testing as an acceptable practice.
- Function tests will be performed on the following BOP elements:
    - Annular à during each full BOPE test
    - Upper Pipe Rams à On trip ins where FIT required
    - Blind Rams à Every trip
    - Lower Pipe Rams à during each full BOPE test
- Break testing BOP and BOPE coupled with batch drilling operations and option to offline cement and/or remediate (if needed) any surface or intermediate sections, according to attached offline cementing support documentation.
- After the well section is secured, the BOP will be disconnected from the wellhead and walked with the rig to another well on the pad.
- TA cap will also be installed per Wellhead vendor procedure and pressure inside the casing will be monitored via the valve on the TA cap as per standard batch drilling ops.

Break Test Diagram (HCR valve)



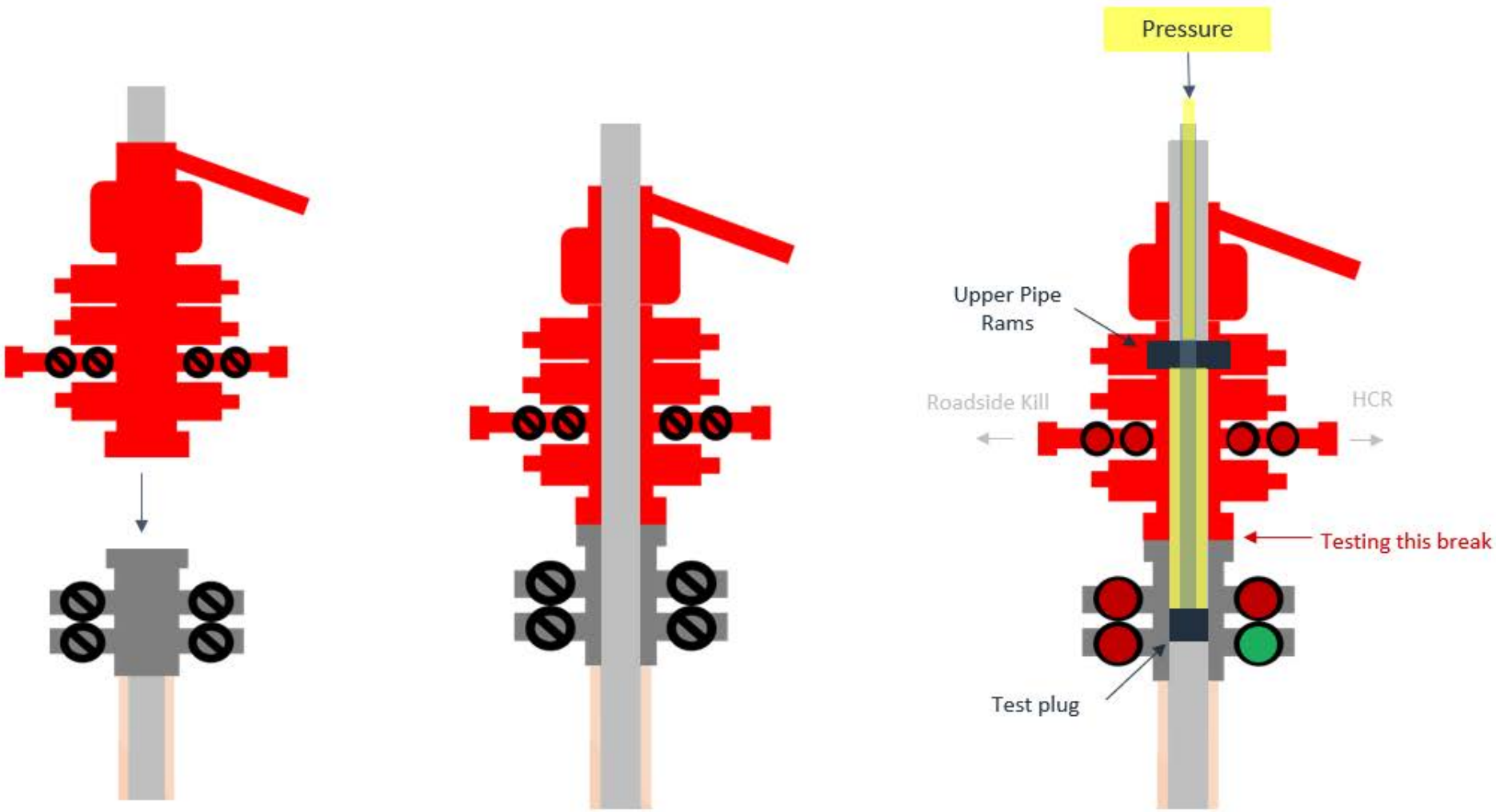




Steps

1. Set plug in wellhead (lower barrier)
2. Close Blind Rams (upper barrier)
3. Close roadside kill
4. Open HCR (pressure application)
5. Open wellhead valves below test plug to ensure if leak past test plug, pressure won't be applied to wellbore
6. Tie BOP testers high pressure line to main choke manifold crown valve
7. Pressure up to test break
8. Bleed test pressure from BOP testing unit

Break Test Diagram (Test Joint)



Steps

1. Set plug in with test joint wellhead (lower barrier)
2. Close Upper Pipe Rams (upper barrier)
3. Close roadside kill
4. Close HCR
5. Open wellhead valves below test plug to ensure if leak past test plug, pressure won't be applied to wellbore
6. Tie BOP testers high pressure line to top of test joint
7. Pressure up to test break
8. Bleed test pressure from BOP testing unit

Cement Program

1. No changes to the cement program will take place for offline cementing.

Summarized Operational Procedure for Intermediate Casing

1. Run casing as per normal operations. While running casing, conduct negative pressure test and confirm integrity of the float equipment back pressure valves.
    a. Float equipment is equipped with two back pressure valves rated to a minimum of 5,000 psi.
2. Land production casing on mandrel hanger through BOP.
    a. If casing is unable to be landed with a mandrel hanger, then the **casing will be cemented online**.
3. Break circulation and confirm no restrictions.
    a. Ensure no blockage of float equipment and appropriate annular returns.
    b. Perform flow check to confirm well is static.
4. Set pack-off
    a. If utilizing a fluted/ported mandrel hanger, ensure well is static on the annulus and inside the casing by filling the pipe with kill weight fluid, remove landing joint, and set annular packoff through BOP. Pressure test to 5,000 psi for 10 min.
    b. If utilizing a solid mandrel hanger, ensure well is static on the annulus and inside the casing by filling the pipe with kill weight fluid. Pressure test seals to 5,000 psi for 10 min. Remove landing joint through BOP.
5. After confirmation of both annular barriers and the two casing barriers, install TA plug and pressure test to 5,000 psi for 10 min. Notify the BLM with intent to proceed with nipple down and offline cementing.
    a. Minimum 4 hrs notice.
6. With the well secured and BLM notified, nipple down BOP and secure on hydraulic carrier or cradle.
    a. Note, if any of the barriers fail to test, the BOP stack will not be nippled down until after the cement job has concluded and both lead and tail slurry have reached 500 psi.
7. Skid/Walk rig off current well.
8. Confirm well is static before removing TA Plug.
    a. Cementing operations will not proceed until well is under control. (If well is not static, notify BLM and proceed to kill)
    b. Casing outlet valves will provide access to both the casing ID and annulus. Rig or third party pump truck will kill well prior to cementing.
    c. Well control plan can be seen in Section B, Well Control Procedures.
    d. If need be, rig can be moved back over well and BOP nippled back up for any further remediation.

   e. Diagram for rig positioning relative to offline cementing can be seen in Figure 4.
9. Rig up return lines to take returns from wellhead to pits and rig choke.
   a. Test all connections and lines from wellhead to choke manifold to 5,000 psi high for 10 min.
   b. If either test fails, perform corrections and retest before proceeding.
   c. Return line schematics can be seen in Figure 3.
10. Remove TA Plug from the casing.
11. Install offline cement tool.
   a. Current offline cement tool schematics can be seen in Figure 1 (Cameron) and Figure 2 (Cactus).
12. Rig up cement head and cementing lines.
   a. Pressure test cement lines against cement head to 80% of casing burst for 10 min.
13. Break circulation on well to confirm no restrictions.
   a. If gas is present on circulation, well will be shut in and returns rerouted through gas buster.
   b. Max anticipated time before circulating with cement truck is 6 hrs.
14. Pump cement job as per plan.
   a. At plug bump, test casing to 0.22 psi/ft or 1500 psi, whichever is greater.
   b. If plug does not bump on calculated, shut down and wait 8 hrs or 500 psi compressive strength, whichever is greater before testing casing.
15. Confirm well is static and floats are holding after cement job.
   a. With floats holding and backside static:
      i. Remove cement head.
   b. If floats are leaking:
      i. Shut-in well and WOC (Wait on Cement) until tail slurry reaches 500 psi compressive strength and the casing is static prior to removing cement head.
   c. If there is flow on the backside:
      i. Shut in well and WOC until tail slurry reaches 500 psi compressive strength. Ensure that the casing is static prior to removing cement head.
16. Remove offline cement tool.
17. Install night cap with pressure gauge for monitoring.
18. Test night cap to 5,000 psi for 10 min.

Example Well Control Plan Content

A. Well Control Component Table

The table below, which covers the cementing of the **5M MASP (Maximum Allowable Surface Pressure) portion of the well**, outlines the well control component rating in use. This table, combined with the mud program, documents that two barriers to flow can be maintained at all times, independent of the BOP nippled up to the wellhead.

Intermediate hole section, 5M requirement

Component	RWP
Pack-off	10M
Casing Wellhead Valves	10M
Annular Wellhead Valves	5M
TA Plug	10M
Float Valves	5M
2” 1502 Lo-Torque Valves	15M

B. Well Control Procedures

Well control procedures are specific to the rig equipment and the operation at the time the kick occurs. Below are the minimal high-level tasks prescribed to assure a proper shut-in while circulating and cementing through the Offline Cement Adapter.

General Procedure While Circulating

1. Sound alarm (alert crew).
2. Shut down pumps.
3. Shut-in Well (close valves to rig pits and open valve to rig choke line. Rig choke will already be in the closed position).
4. Confirm shut-in.
5. Notify tool pusher/company representative.

6. Read and record the following:
    a. SICP (Shut in Casing Pressure) and AP (Annular Pressure)
    b. Pit gain
    c. Time
    d. Regroup and identify forward plan to continue circulating out kick via rig choke and mud/gas separator. Circulate and adjust mud density as needed to control well.

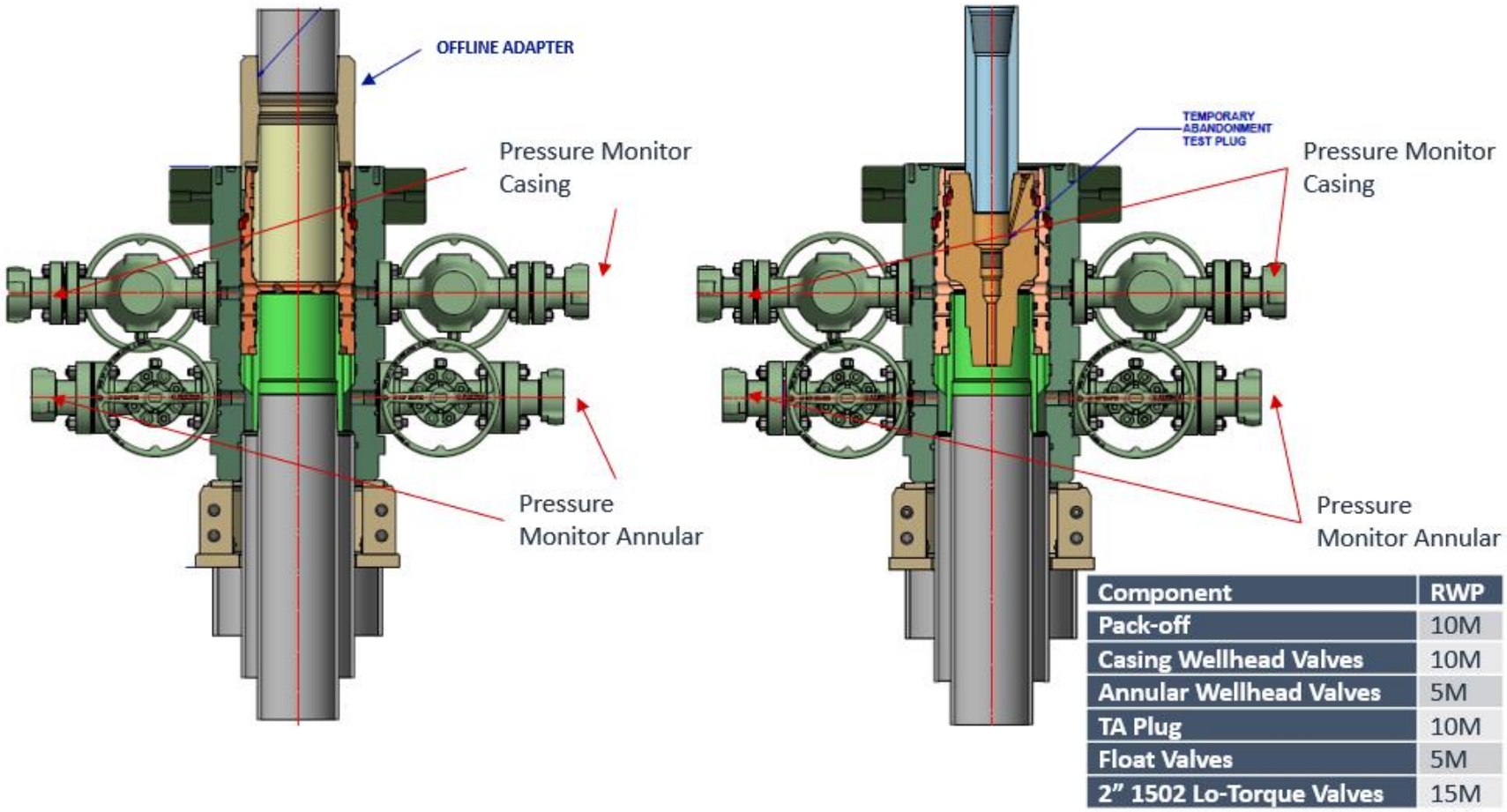
General Procedure While Cementing

1. Sound alarm (alert crew).
2. Shut down pumps.
3. Shut-in Well (close valves to rig pits and open valve to rig choke line. Rig choke will already be in the closed position).
4. Confirm shut-in.
5. Notify tool pusher/company representative.
6. Open rig choke and begin pumping again taking returns through choke manifold and mud/gas separator.
7. Continue to place cement until plug bumps.
8. At plug bump close rig choke and cement head.
9. Read and record the following
    a. SICP and AP
    b. Pit gain
    c. Time
    d. Shut-in annulus valves on wellhead

General Procedure After Cementing

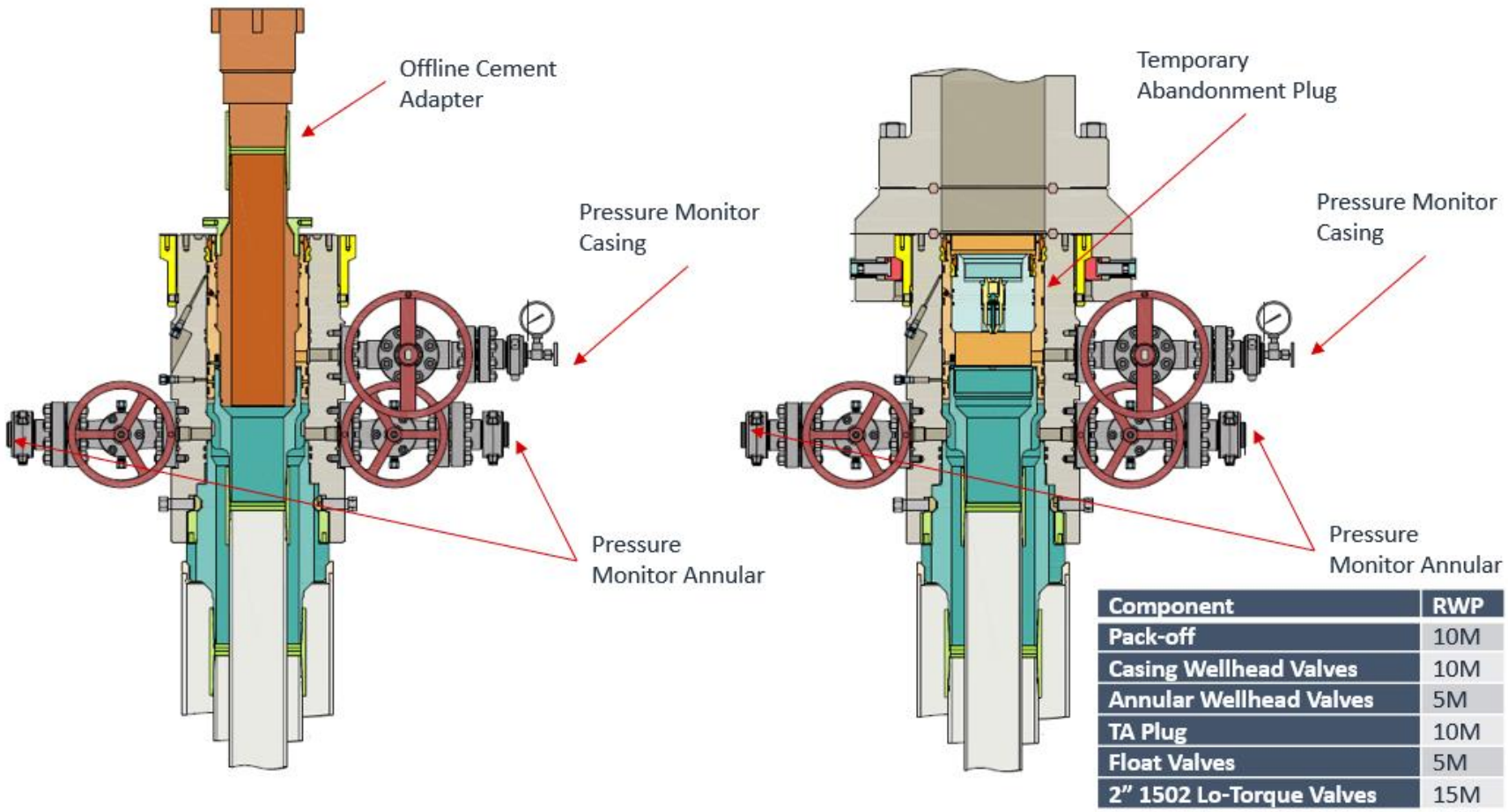
1. Sound alarm (alert crew).
2. Shut-in Well (close valves to rig pits and open valve to rig choke line. Rig choke will already be in the closed position).
3. Confirm shut-in.
4. Notify tool pusher/company representative.
5. Read and record the following:
    a. SICP and AP
    b. Pit gain
    c. Time
    d. Shut-in annulus valves on wellhead

Figure 1: Cameron TA Plug and Offline Adapter Schematic



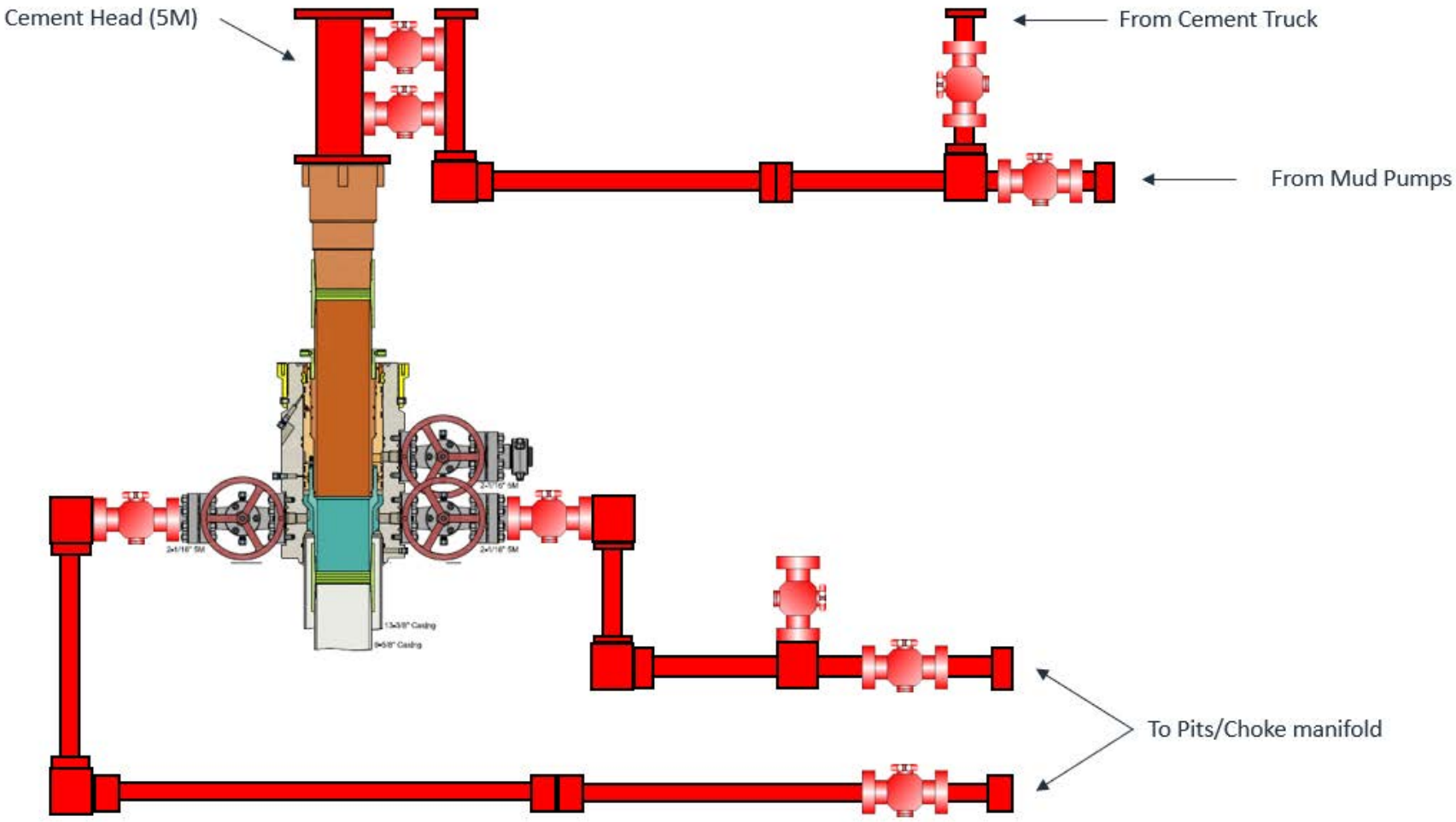
Component	RWP
Pack-off	10M
Casing Wellhead Valves	10M
Annular Wellhead Valves	5M
TA Plug	10M
Float Valves	5M
2" 1502 Lo-Torque Valves	15M

Figure 2: Cactus TA Plug and Offline Adapter Schematic



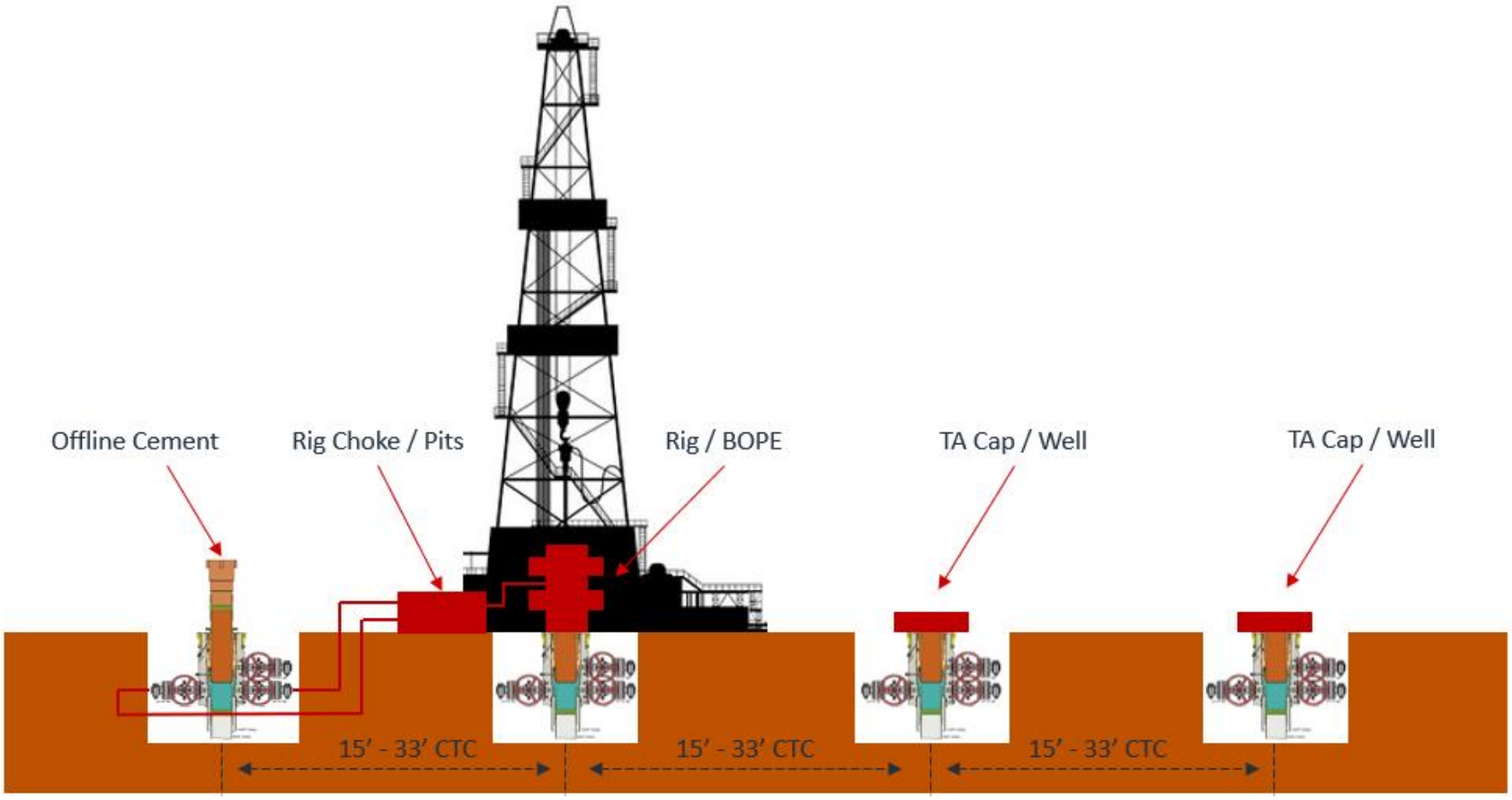
Component	RWP
Pack-off	10M
Casing Wellhead Valves	10M
Annular Wellhead Valves	5M
TA Plug	10M
Float Valves	5M
2" 1502 Lo-Torque Valves	15M

Figure 3: Back Yard Rig Up



*** All Lines 10M rated working pressure

Figure 4: Rig Placement Diagram



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Salt Section Annular Clearance Variance Request

Daniel Moose

Current Design (Salt Strings)

0.422” Annular clearance requirement

- Casing collars shall have a minimum clearance of 0.422 inches on all sides in the hole/casing annulus, with recognition that variances can be granted for justified exceptions.

- 12.25” Hole x 9.625”40# J55/HCK55 LTC Casing
  - 1.3125” Clearance to casing OD
  - 0.8125” Clearance to coupling OD
- 9.875” Hole x 8.75” 38.5# P110 Sprint-SF Casing
  - 0.5625” Clearance to casing OD
  - 0.433” Clearance to coupling OD

Annular Clearance Variance Request

EOG request permission to allow deviation from the 0.422” annulus clearance requirement for the intermediate (salt) section from Onshore Order #2 under the following conditions:

- The variance is not applicable within the Potash Boundaries or Capitan Reef areas.
- Operator takes responsibility to get casing to set point in the event that the clearance causes stuck pipe issues

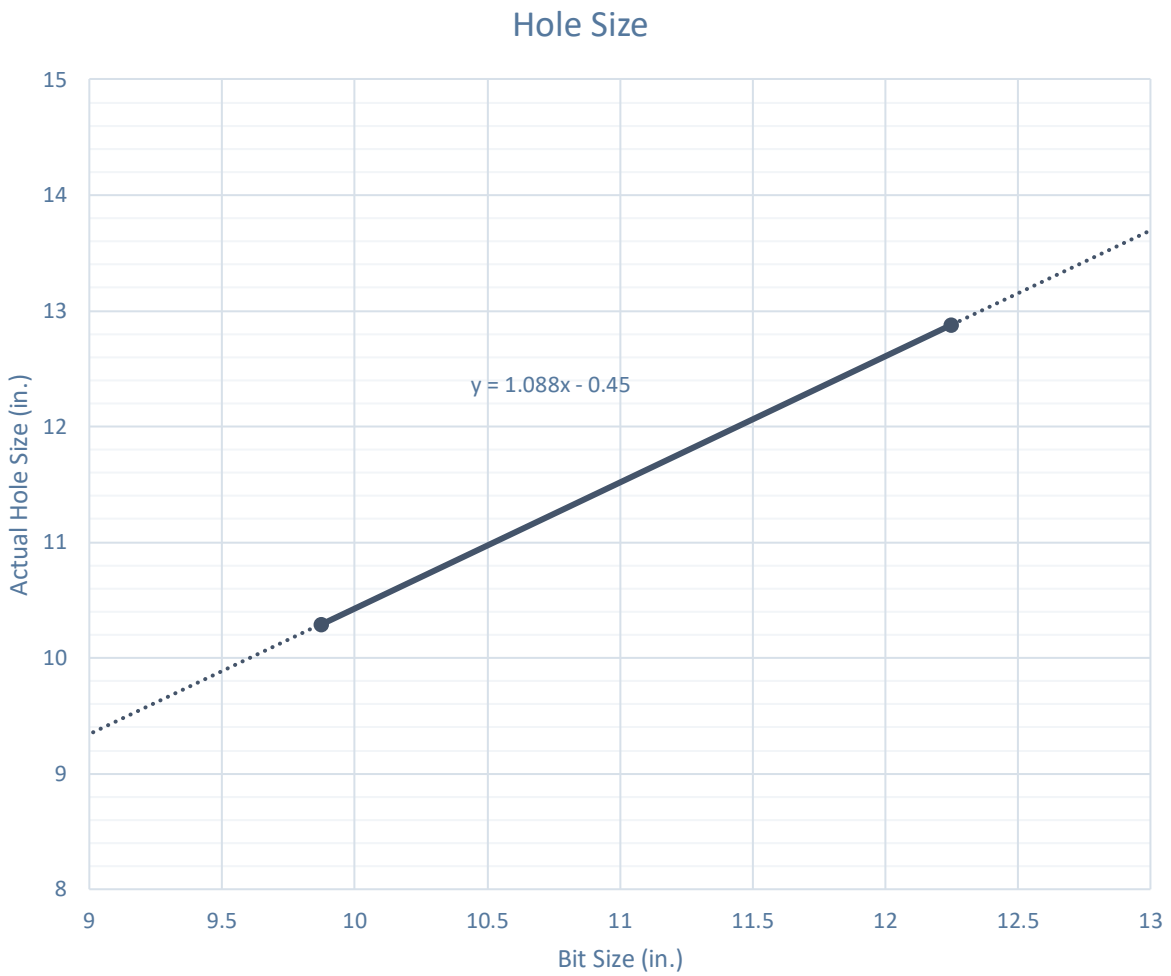
Volumetric Hole Size Calculation

Hole Size Calculations Off Cement Volumes

- Known volume of cement pumped
- Known volume of cement returned to surface
- Must not have had any losses
- Must have bumped plug

Average Hole Size

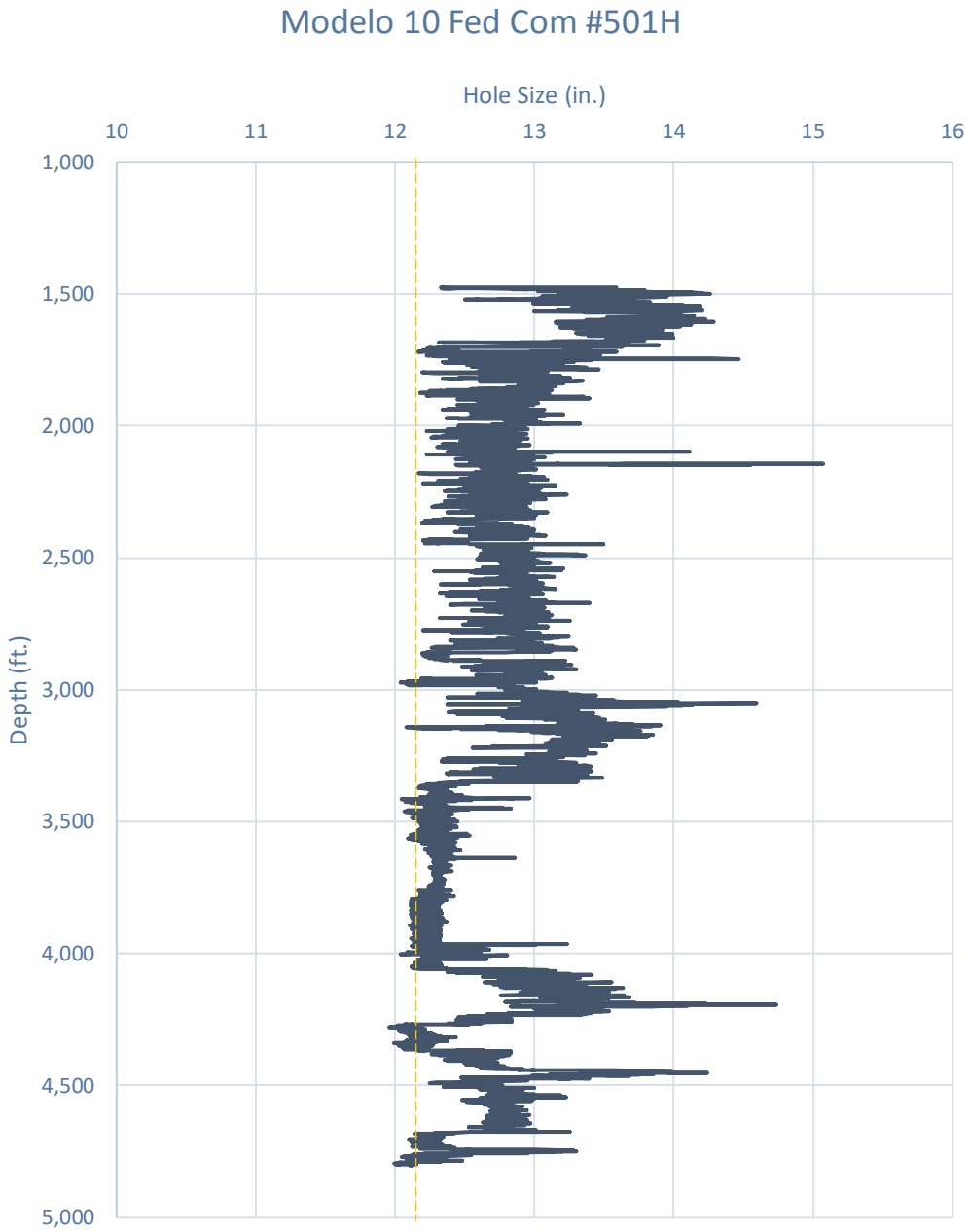
- 12.25” Hole
  - 12.88” Hole
    - 5.13% diameter increase
    - 10.52% area increase
  - 0.63” Average enlargement
  - 0.58” Median enlargement
  - 179 Well Count
- 9.875” Hole
  - 10.30” Hole
    - 4.24% diameter increase
    - 9.64% area increase
  - 0.42” Average enlargement
  - 0.46” Median enlargement
  - 11 Well Count



Caliper Hole Size (12.25”)

Average Hole Size

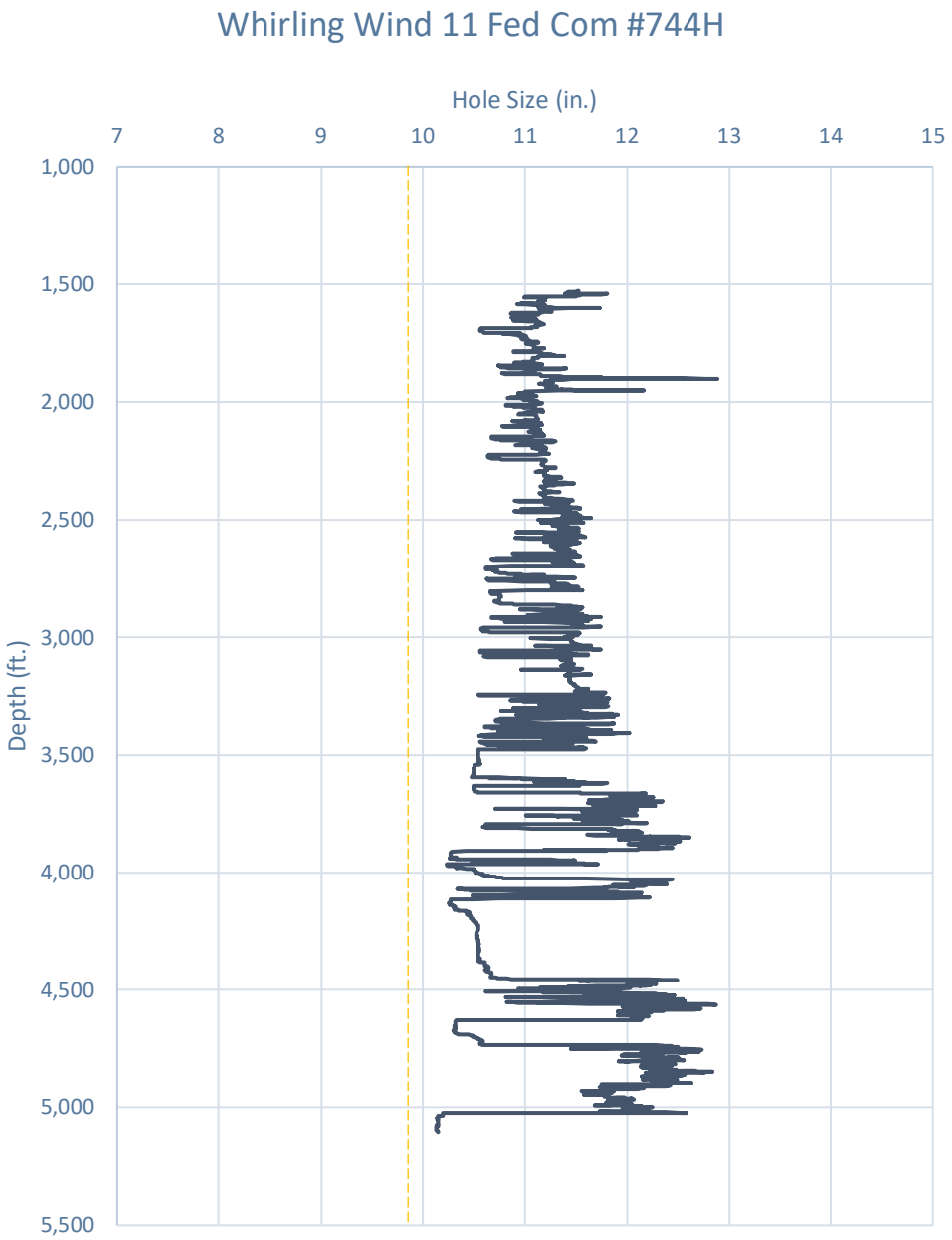
- 12.25” Bit
  - 12.76” Hole
    - 4.14% diameter increase
    - 8.44% area increase
  - 0.51” Average enlargement
  - 0.52” Median enlargement
  - Brine



Caliper Hole Size (9.875”)

Average Hole Size

- 9.875” Hole
  - 11.21” Hole
    - 13.54% diameter increase
    - 28.92% area increase
  - 1.33” Average enlargement
  - 1.30” Median enlargement
  - EnerLite



Design A

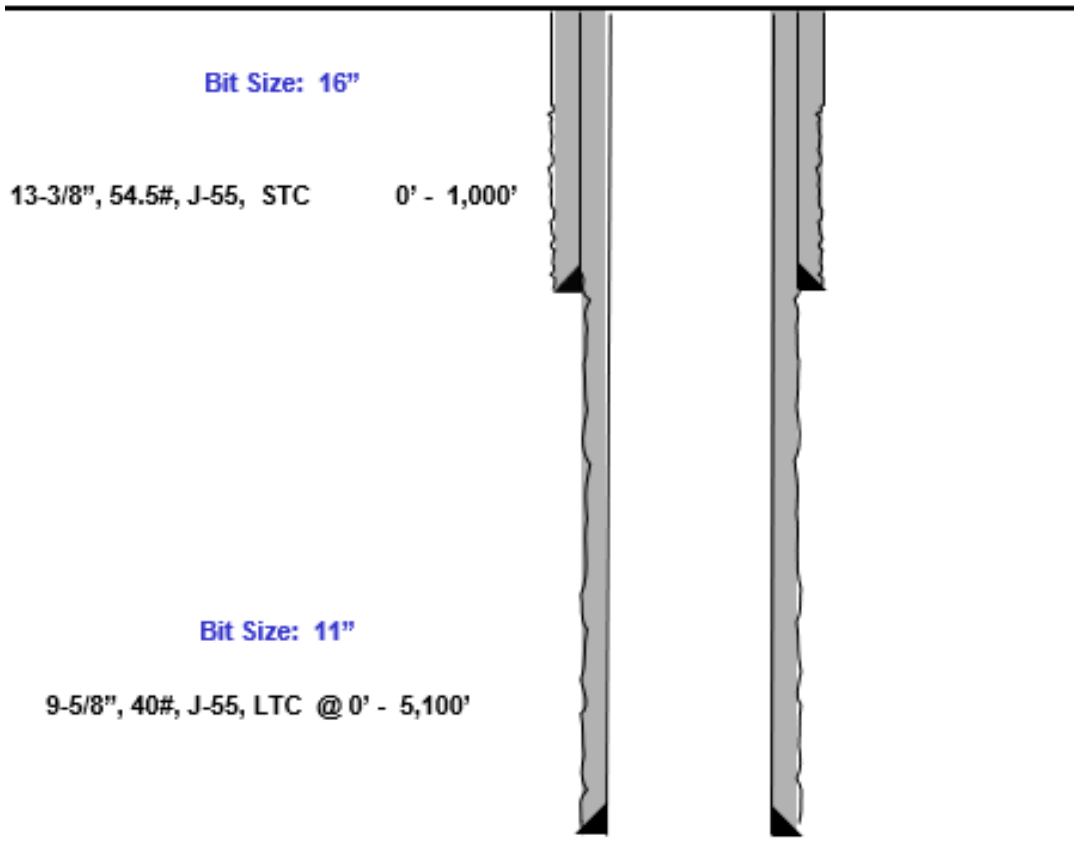
Proposed 11” Hole with 9.625” 40# J55/HCK55 LTC Casing

- 11” Bit + 0.52” Average hole enlargement = 11.52” Hole Size
  - 0.9475” Clearance to casing OD

    $$= \frac{11.52 - 9.625}{2}$$
  - 0.4475” Clearance to coupling OD

    $$= \frac{11.52 - 10.625}{2}$$
- Previous Shoe – 13.375” 54.5# J55 STC
  - 0.995” Clearance to coupling OD (~1,200’ overlap)

    $$= \frac{12.615 - 10.625}{2}$$



Design B

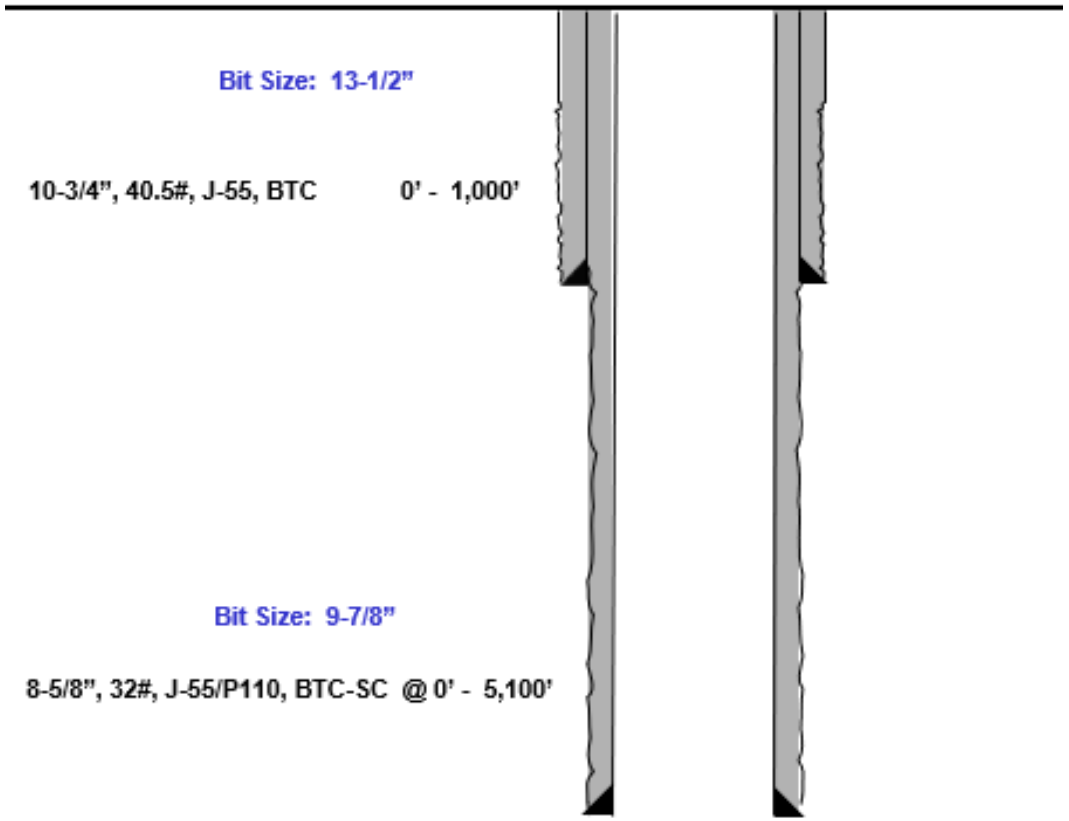
Proposed 9.875” Hole with 8.625” 32# J55/P110 BTC-SC Casing

- 9.875” Bit + 0.42” Average hole enlargement = 10.295” Hole Size
  - 0.835” Clearance to casing OD

    $$= \frac{10.295 - 8.625}{2}$$
  - 0.585” Clearance to coupling OD

    $$= \frac{10.295 - 9.125}{2}$$
- Previous Shoe – 10.75” 40.5# J55 STC
  - 0.4625” Clearance to coupling OD (~1,200’ overlap)

    $$= \frac{10.05 - 9.125}{2}$$



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Index

Casing Spec Sheets

PERFORMANCE DATA

API LTC 9.625 in 40.00 lbs/ft K55 HC

Technical Data Sheet

Tubular Parameters

Size	9.625	in	Minimum Yield	55	ksi
Nominal Weight	40.00	lbs/ft	Minimum Tensile	95	ksi
Grade	K55 HC		Yield Load	629	kips
PE Weight	38.94	lbs/ft	Tensile Load	1088	kips
Wall Thickness	0.395	in	Min. Internal Yield Pressure	3,950	psi
Nominal ID	8.835	in	Collapse Pressure	3600	psi
Drift Diameter	8.750	in			
Nom. Pipe Body Area	11.454	in²			

Connection Parameters

Connection OD	10.625	in
Coupling Length	10.500	in
Threads Per Inch	8	tpi
Standoff Thread Turns	3.50	turns
Make-Up Loss	4.750	in
Min. Internal Yield Pressure	3,950	psi

Pipe Body and API Connections Performance Data

13.375 54.50/0.380 J55 PDF

New Search »

« Back to Previous List

USC Metric

6/8/2015 10:04:37 AM

Mechanical Properties	Pipe	BTC	LTC	STC	
Minimum Yield Strength	55,000	--	--	--	psi
Maximum Yield Strength	80,000	--	--	--	psi
Minimum Tensile Strength	75,000	--	--	--	psi
Dimensions	**Pipe**	**BTC**	**LTC**	**STC**	
Outside Diameter	13.375	14.375	--	14.375	in.
Wall Thickness	0.380	--	--	--	in.
Inside Diameter	12.615	12.615	--	12.615	in.
Standard Drift	12.459	12.459	--	12.459	in.
Alternate Drift	--	--	--	--	in.
Nominal Linear Weight, T&C	54.50	--	--	--	lbs/ft
Plain End Weight	52.79	--	--	--	lbs/ft
Performance	**Pipe**	**BTC**	**LTC**	**STC**	
Minimum Collapse Pressure	1,130	1,130	--	1,130	psi
Minimum Internal Yield Pressure	2,740	2,740	--	2,740	psi
Minimum Pipe Body Yield Strength	853.00	--	--	--	1000 lbs
Joint Strength	--	909	--	514	1000 lbs
Reference Length	--	11,125	--	6,290	ft
Make-Up Data	**Pipe**	**BTC**	**LTC**	**STC**	
Make-Up Loss	--	4.81	--	3.50	in.
Minimum Make-Up Torque	--	--	--	3,860	ft-lbs
Maximum Make-Up Torque	--	--	--	6,430	ft-lbs

Casing Spec Sheets

Pipe Body and API Connections Performance Data

10.750 40.50/0.350 J55

PDF

New Search »

« Back to Previous List

USC Metric

6/8/2015 10:14:05 AM

Mechanical Properties	Pipe	BTC	LTC	STC	
Minimum Yield Strength	55,000	--	--	--	psi
Maximum Yield Strength	80,000	--	--	--	psi
Minimum Tensile Strength	75,000	--	--	--	psi
Dimensions	**Pipe**	**BTC**	**LTC**	**STC**	
Outside Diameter	10.750	11.750	--	11.750	in.
Wall Thickness	0.350	--	--	--	in.
Inside Diameter	10.050	10.050	--	10.050	in.
Standard Drift	9.894	9.894	--	9.894	in.
Alternate Drift	--	--	--	--	in.
Nominal Linear Weight, T&C	40.50	--	--	--	lbs/ft
Plain End Weight	38.91	--	--	--	lbs/ft
Performance	**Pipe**	**BTC**	**LTC**	**STC**	
Minimum Collapse Pressure	1,580	1,580	--	1,580	psi
Minimum Internal Yield Pressure	3,130	3,130	--	3,130	psi
Minimum Pipe Body Yield Strength	629.00	--	--	--	1000 lbs
Joint Strength	--	700	--	420	1000 lbs
Reference Length	--	11,522	--	6,915	ft
Make-Up Data	**Pipe**	**BTC**	**LTC**	**STC**	
Make-Up Loss	--	4.81	--	3.50	in.
Minimum Make-Up Torque	--	--	--	3,150	ft-lbs
Maximum Make-Up Torque	--	--	--	5,250	ft-lbs

VALLOUREC STAR 8.625 32# J55 S S2L2 DA 7.875 W/O# SLN # PO# MADE IN USA FT LB

vallourec

API 5CT, 10th Ed. Connection Data Sheet

O.D. (in)	WEIGHT (lb/ft)	WALL (in)	GRADE	*API DRIFT (in)	RBW %
8.625	Nominal: 32.00 Plain End: 31.13	0.352	J55	7.796	87.5

Material Properties (PE)	
Pipe	
Minimum Yield Strength:	55 ksi
Maximum Yield Strength:	80 ksi
Minimum Tensile Strength:	75 ksi
Coupling	
Minimum Yield Strength:	55 ksi
Maximum Yield Strength:	80 ksi
Minimum Tensile Strength:	75 ksi

Pipe Body Data (PE)	
Geometry	
Nominal ID:	7.92 inch
Nominal Area:	9.149 in^2
*Special/Alt. Drift:	7.875 inch
Performance	
Pipe Body Yield Strength:	503 kips
Collapse Resistance:	2,530 psi
Internal Yield Pressure: (API Historical)	3,930 psi

API Connection Data Coupling OD: 9.625"	
STC Performance	
STC Internal Pressure:	3,930 psi
STC Joint Strength:	372 kips
LTC Performance	
LTC Internal Pressure:	3,930 psi
LTC Joint Strength:	417 kips
SC-BTC Performance - Cplg OD = 9.125"	
BTC Internal Pressure:	3,930 psi
BTC Joint Strength:	503 kips

API Connection Torque					
STC Torque (ft-lbs)					
Min:	2,793	Opti:	3,724	Max:	4,655
LTC Torque (ft-lbs)					
Min:	3,130	Opti:	4,174	Max:	5,217
BTC Torque (ft-lbs)					
follow API guidelines regarding positional make up					

*Alt. Drift will be used unless API Drift is specified on order.

**If above API connections do not suit your needs, VAM® premium connections are available up to 100% of pipe body ratings.

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Rev 3, 7/30/2021

10/21/2022 15:24

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EOG BLANKET CASING DESIGN VARIANCE

EOG respectfully requests the drill plans in the attached document 'EOG Alternate Casing Designs – BLM APPROVED' be added to the COA's for this well. These designs have been approved by the BLM down to the TVDs listed below and will allow EOG to run alternate casing designs for this well if necessary.

The designs and associated details listed are the "worst case scenario" boundaries for design safety factors. Location and lithology have NOT been accounted for in these designs. The specific well details will be based on the APD/Sundry package and the information listed in the COA.

The mud program will not change from the original design for this well. Summary of the mud programs for both shallow and deep targets are listed at the end of this document. If the target is changing, a sundry will be filed to update the casing design and mud/cement programs.

Cement volumes listed in this document are for reference only. The cement volumes for the specific well will be adjusted to ensure cement tops meet BLM requirements as listed in the COA and to allow bradenhead cementing when applicable.

This blanket document only applies to wells with three string designs outside of Potash and Capitan Reef boundaries.

Shallow Design Boundary Conditions				
	Deepest MD (ft)	Deepest TVD (ft)	Max Inc (deg)	Max DLS (°/100usft)
Surface	2030	2030	0	0
Intermediate	7793	5650	40	8
Production	28578	12000	90	25

eog resources

Shallow Design A

4. CASING PROGRAM

Hole Size	Interval MD From (ft)	Interval MD To (ft)	Interval TVD From (ft)	Interval TVD To (ft)	Csg OD	Weight	Grade	Conn
16"	0	2,161	0	2,030	13-3/8"	54.5#	J-55	STC
11"	0	7,951	0	5,650	9-5/8"	40#	J-55	LTC
6-3/4"	0	29,353	0	12,000	5-1/2"	20#	P110-EC	DWC/C IS MS

Hole will be full during casing run for well control and tensile SF factor. Casing will be kept at least half full during run for this design to meet BLM collapse SF requirement. External pressure will be reviewed prior to conducting casing pressure tests to ensure that 70% of the yield is not exceeded.

Variance is requested to waive the centralizer requirements for the 9-5/8" casing in the 11" hole size. An expansion additive will be utilized, in the cement slurry, for the entire length of the 11" hole interval to maximize cement bond and zonal isolation.

Variance is also requested to waive any centralizer requirements for the 5-1/2" casing in the 6-3/4" hole size. An expansion additive will be utilized, in the cement slurry, for the entire length of the 6-3/4" hole interval to maximize cement bond and zonal isolation.

EOG requests permission to allow deviation from the 0.422'' annulus clearance requirement for the intermediate (salt) section from Title 43 CFR Part 3170 under the following conditions:

- The variance is not applicable within the Potash Boundaries or Capitan Reef areas.
- Operator takes responsibility to get casing to set point in the event that the clearance causes stuck pipe issues.

5. CEMENTING PROGRAM:

Depth	No. Sacks	Wt. ppg	Yld Ft3/sk	Slurry Description
2,030' 13-3/8"	570	13.5	1.73	Lead: Class C/H + 4.0% Bentonite Gel + 0.5% CaCl2 + 0.25 lb/sk Cello-Flake (TOC @ Surface)
	160	14.8	1.34	Tail: Class C/H + 0.6% FL-62 + 0.25 lb/sk Cello-Flake + 0.2% Sodium Metasilicate (TOC @ 1830')
8,050' 9-5/8"	760	12.7	2.22	Lead: Class C/H + 10% NaCl + 6% Bentonite Gel + 3% MagOx (TOC @ Surface)
	250	14.8	1.32	Tail: Class C/H + 10% NaCL + 3% MagOx (TOC @ 6360')
29,353' 5-1/2"	1000	14.8	1.32	Bradenhead squeeze: Class C/H + 3% Salt + 1% PreMag-M + 6% Bentonite Gel (TOC @ surface)
	1480	13.2	1.52	Tail: Class C/H + 5% NEX-020 + 0.2% NAC-102 + 0.15% NAS-725 + 0.5% NFL-549 + 0.2% NFP-703 + 1% NBE-737 + 0.3% NRT-241 (TOC @ Top of Brushy)

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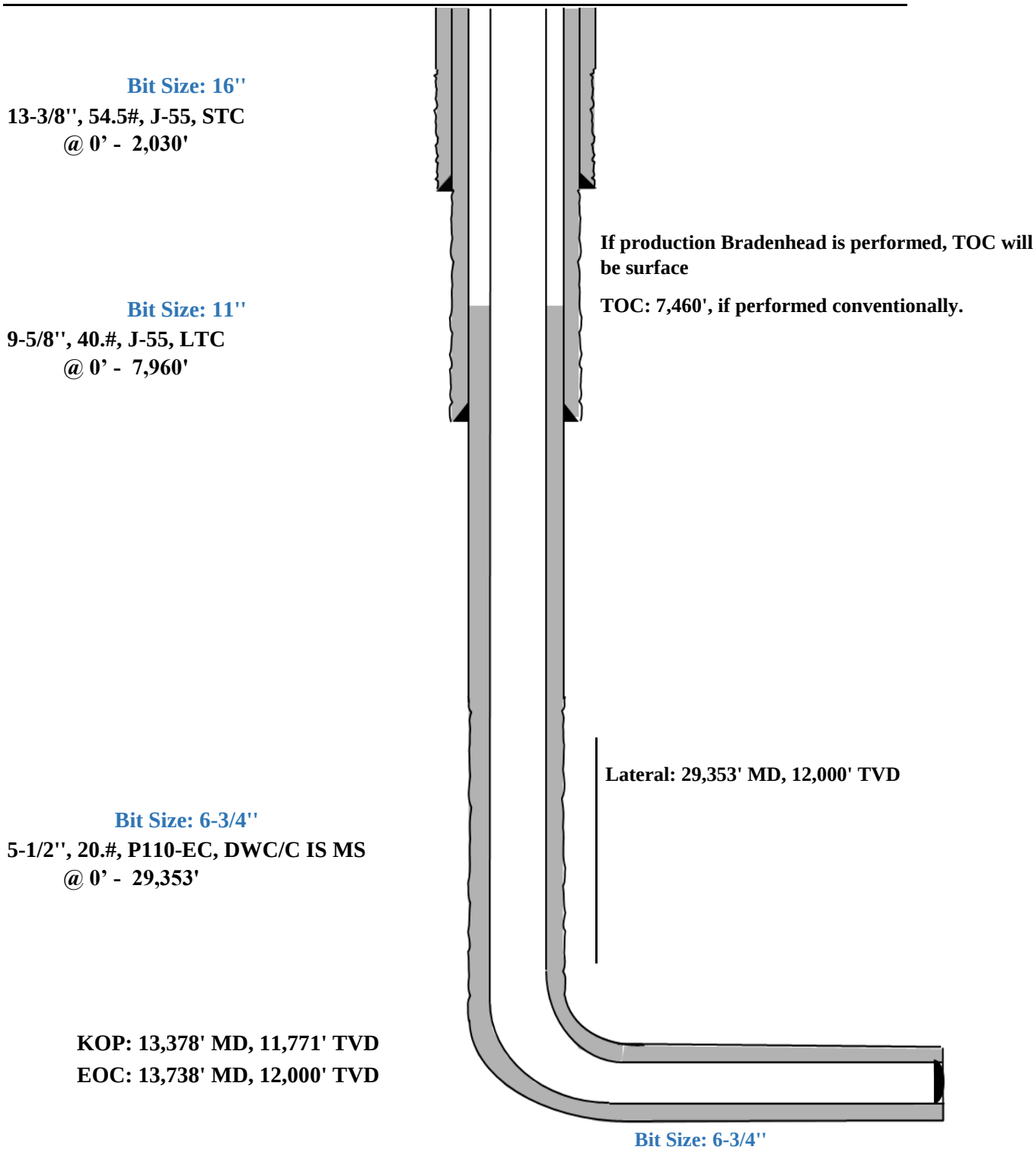
Shallow Design A

Proposed Wellbore

KB: 3558'
GL: 3533'



Stresscheck - [Triaxial Results - Shallow 3.0 Mile - Big Hole]

File Edit Wellbore Tubular View Composer Tools Window Help

9 5/8" Intermediate Casing

Pressure Test

Triaxial Results

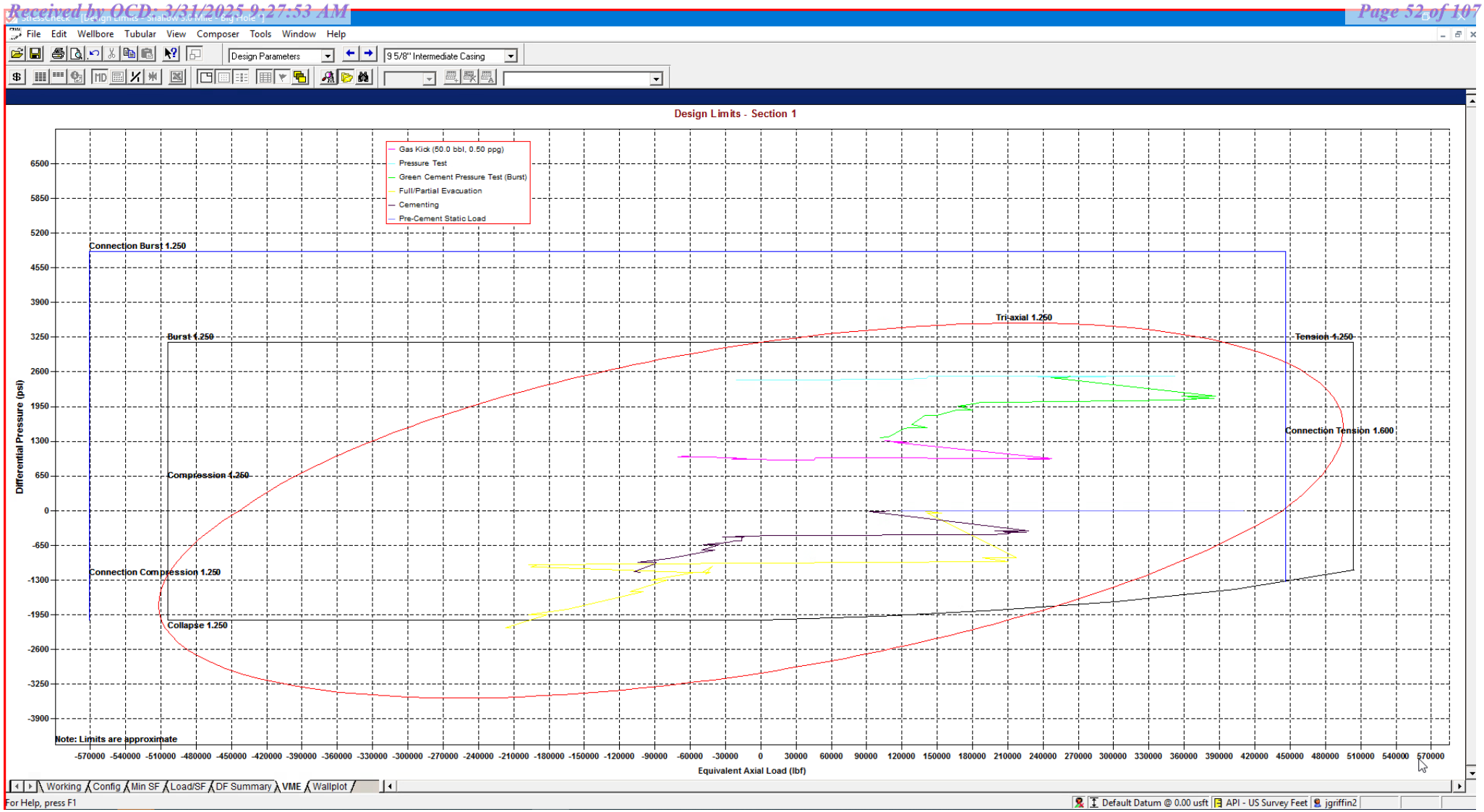
	Depth (MD) (usft)	Axial Force (lbf) Apparent (w/Bending)	Axial Force (lbf) Actual (w/o Bending)	Equivalent Axial Load (lbf)	Bending Stress at OD (psi)	Absolute Safety Factor Triaxial	Absolute Safety Factor Burst	Absolute Safety Factor Collapse (V)	Absolute Safety Factor Axial	Temperature (°F)	Pressure (psi) Internal	Pressure (psi) External	Addt'l Pickup To Prevent Buck. (lbf)	Buckled Length (usft)
1	0	252987	228954	253140	2098.2	1.69	1.58	N/A	2.82 F	70.00	2500.00	0.00	N/A	N/A
2	100	247735	223702	248466	2098.2	1.69	1.58	N/A	2.88 F	71.10	2543.63	43.63		
3	100	234996	223701	235716	986.2	1.71	1.58	N/A	3.04 F	71.10	2543.64	43.64		
4	1700	341565	139667	352253	17627.2	1.53	1.57	N/A	2.09 F	88.70	3241.64	741.64		
5	1700	312979	139666	323488	15131.5	1.58	1.57	N/A	2.28 F	88.70	3241.65	741.65		
6	1850	336881	132027	348440	17885.2	1.51	1.57	N/A	2.12 F	90.29	3305.05	805.05		
7	1850	318549	132027	329984	16284.8	1.54	1.57	N/A	2.24 F	90.29	3305.06	805.06		
8	1950	320468	127243	332475	16869.9	1.52	1.57	N/A	2.23 F	91.30	3344.87	844.87		
9	1950	312802	127243	324756	16200.7	1.53	1.57	N/A	2.28 F	91.30	3344.87	844.87		
10	2050	307858	122773	320295	16159.3	1.52	1.57	N/A	2.32 F	92.23	3381.89	881.89		
11	2050	303560	122772	315965	15784.1	1.53	1.57	N/A	2.35 F	92.23	3381.89	881.89		
12	2300	151294	112633	163658	3375.4	1.71	1.57	N/A	4.72 F	94.35	3466.13	966.13		
13	2300	132741	112633	144956	1755.6	1.72	1.57	N/A	5.38 F	94.35	3466.14	966.14		
14	2370	129966	109858	142452	1755.6	1.72	1.57	N/A	5.49 F	94.94	3489.28	989.28		
15	2370	127909	107800	140922	1755.6	1.75	1.60	N/A	5.58 F	94.94	3489.29	1036.40		
16	2700	105515	94232	119785	985.1	1.75	1.60	N/A	6.77 F	97.73	3599.97	1152.35		
17	2700	111680	94231	126006	1523.4	1.75	1.60	N/A	6.39 F	97.73	3599.97	1152.35		
18	3100	110766	77783	126839	2879.6	1.71	1.60	N/A	6.44 F	101.11	3734.23	1293.00		
19	3100	97392	77783	113331	1712.1	1.73	1.60	N/A	7.33 F	101.11	3734.23	1293.01		
20	3700	71565	53303	89806	1594.4	1.70	1.61	N/A	9.97 F	106.15	3934.24	1502.54		
21	3700	60887	53302	79004	662.3	1.71	1.61	N/A	11.72 F	106.16	3934.25	1502.55		
22	4650	34671	14219	56495	1785.6	1.64	1.61	N/A	20.59 F	114.20	4253.37	1836.86		
23	4900	44595	4828	67626	3472.0	1.59	1.61	N/A	16.01 F	116.32	4337.37	1924.87		
24	4900	28975	4828	51775	2108.2	1.62	1.61	N/A	24.64 F	116.32	4337.38	1924.87		
25	5029	22103	34	45340	1926.8	1.61	1.61	N/A	32.30 F	117.40	4380.40	1969.94		
26	5029	22102	33	45339	1926.8	1.61	1.61	N/A	32.30 F	117.40	4380.41	1969.95		
27	5600	-45329	-21341	-20805	2094.3	1.57	1.62	N/A	(13.67)	122.23	4572.11	2170.78		
28	5650	-40465	-23210	-15657	1506.5	1.58	1.62	N/A	(15.31)	122.66	4588.87	2188.34		
29														
30	F	Conn Fracture												
31	( )	Compression												
32	(V)	Vector Collapse Safety Factor												
33														

Working / Config / Min SF / Load/SF / DF Summary / VME / Wallplot

For Help, press F1

Default Datum @ 0.00 usft | API - US Survey Feet | jqriffin2

9-5/8" Intermediate Casing Pressure Test:
Internal Profile based off Surface Pressure + Hydrostatic: 4589 psi
External Profile based off Pore Pressure: 2188 psi

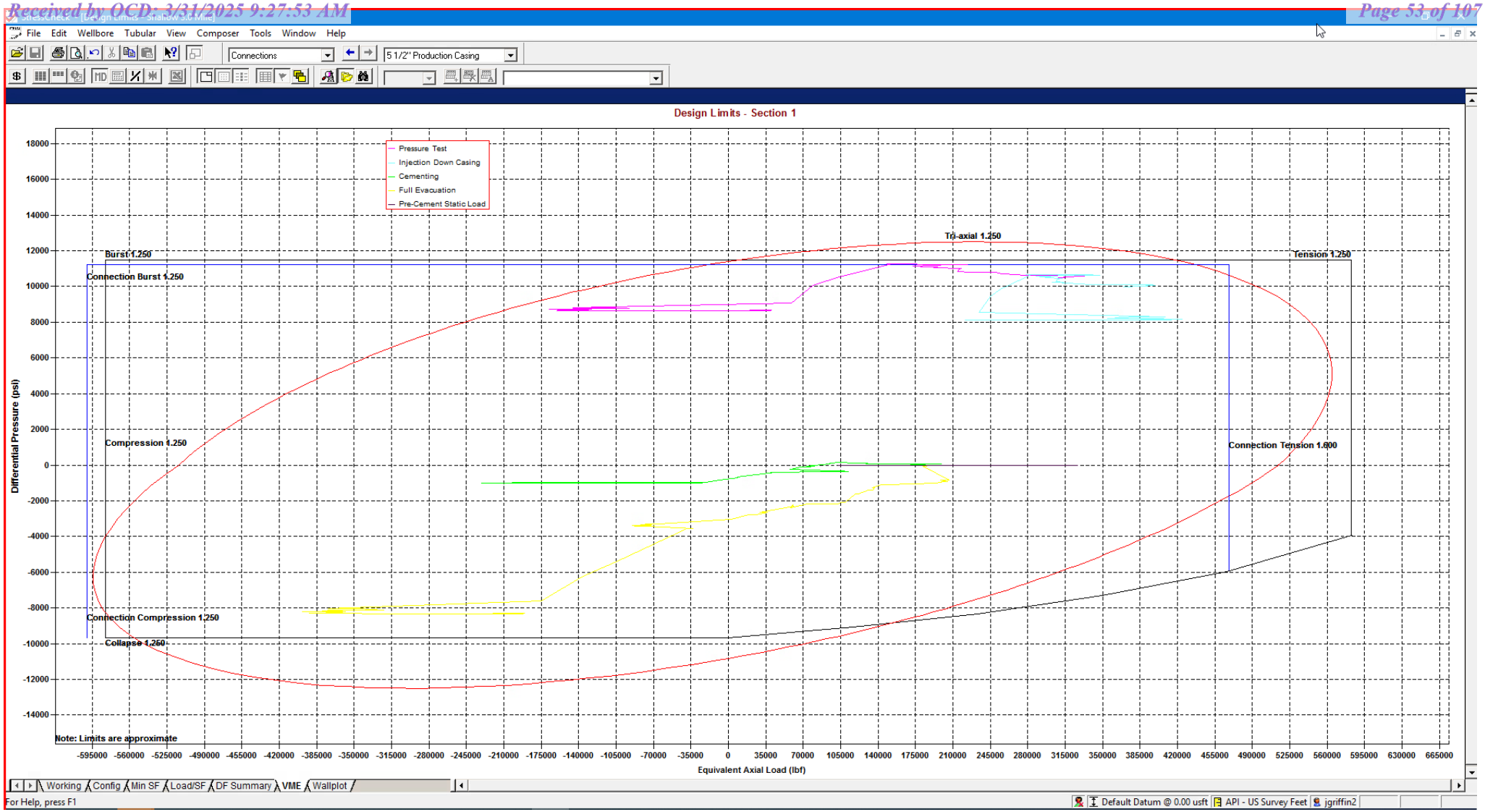


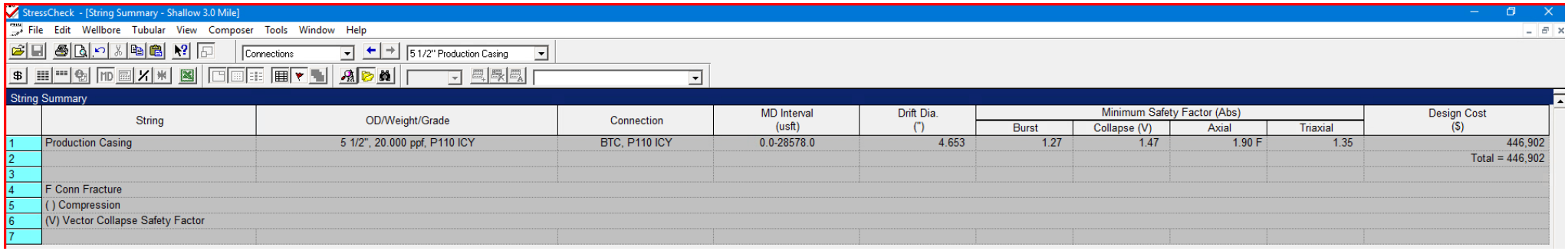
StressCheck - [String Summary - Shallow 3.0 Mile - Big Hole *]

String Summary

	String	OD/Weight/Grade	Connection	MD Interval (usft)	Drift Dia. (")	Minimum Safety Factor (Abs)				Design Cost ($)
						Burst	Collapse (V)	Axial	Triaxial	
1	Intermediate Casing	9 5/8", 40.000 ppf, J-55	BTC, J-55	0.0-5650.0	8.750 A	1.57	1.59	1.80 F	1.35	98,141
2										Total = 98,141
3										
4	F Conn Fracture									
5	A Alternate Drift									
6	(V) Vector Collapse Safety Factor									
7										

*Modelling done with 9-5/8" 40# Intermediate Casing. Passes all Burst, Collapse and Tensile design criteria.





	String	OD/Weight/Grade	Connection	MD Interval (usft)	Drift Dia. (")	Minimum Safety Factor (Abs)				Design Cost ($)
						Burst	Collapse (V)	Axial	Triaxial	
1	Production Casing	5 1/2", 20.000 ppf, P110 ICY	BTC, P110 ICY	0.0-28578.0	4.653	1.27	1.47	1.90 F	1.35	446,902
2										Total = 446,902
3										
4	F Conn Fracture									
5	( ) Compression									
6	(V) Vector Collapse Safety Factor									
7										

*Modelling done with 5-1/2" 20# Production Casing with a 125ksi Control Yield. Passes all Burst, Collapse and Tensile design criteria.

eog resources

Shallow Design B

4. CASING PROGRAM

Hole Size	Interval MD From (ft)	Interval MD To (ft)	Interval TVD From (ft)	Interval TVD To (ft)	Csg OD	Weight	Grade	Conn
13-1/2"	0	2,161	0	2,030	10-3/4"	40.5#	J-55	STC
9-7/8"	0	7,951	0	5,650	8-5/8"	32#	J-55	BTC-SC
6-3/4"	0	29,353	0	12,000	5-1/2"	20#	P110-EC	DWC/C IS MS

Hole will be full during casing run for well control and tensile SF factor. Casing will be kept at least half full during run for this design to meet BLM collapse SF requirement. External pressure will be reviewed prior to conducting casing pressure tests to ensure that 70% of the yield is not exceeded.

Variance is requested to waive the centralizer requirements for the 8-5/8" casing in the 9-7/8" hole size. An expansion additive will be utilized, in the cement slurry, for the entire length of the 9-7/8" hole interval to maximize cement bond and zonal isolation.

Variance is also requested to waive any centralizer requirements for the 5-1/2" casing in the 6-3/4" hole size. An expansion additive will be utilized, in the cement slurry, for the entire length of the 6-3/4" hole interval to maximize cement bond and zonal isolation.

EOG requests permission to allow deviation from the 0.422'' annulus clearance requirement for the intermediate (salt) section from Title 43 CFR Part 3170 under the following conditions:

- The variance is not applicable within the Potash Boundaries or Capitan Reef areas.
- Operator takes responsibility to get casing to set point in the event that the clearance causes stuck pipe issues.

5. CEMENTING PROGRAM:

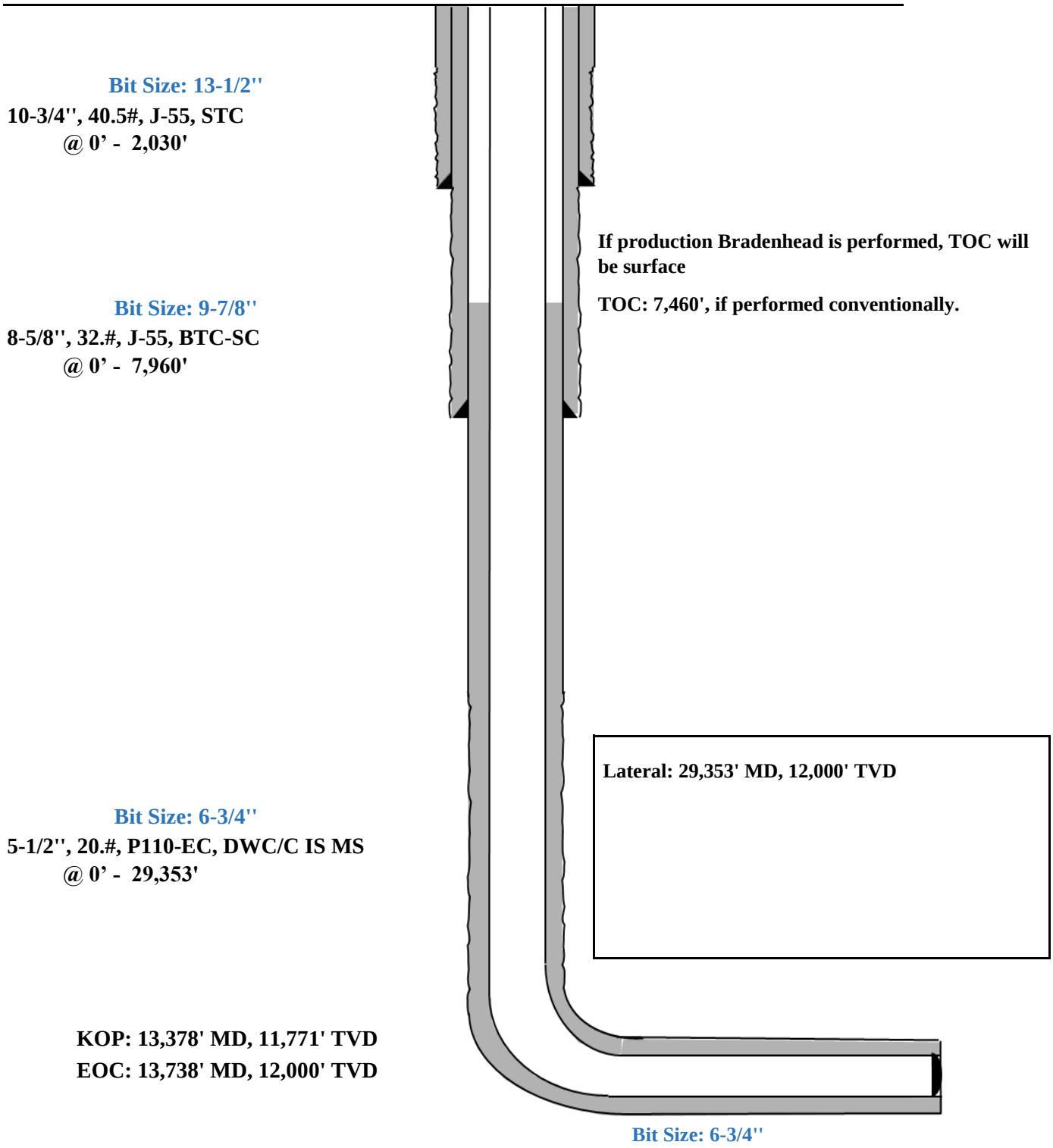
Depth	No. Sacks	Wt. ppg	Yld Ft3/sk	Slurry Description
2,030' 10-3/4"	530	13.5	1.73	Lead: Class C/H + 4.0% Bentonite Gel + 0.5% CaCl2 + 0.25 lb/sk Cello-Flake (TOC @ Surface)
	140	14.8	1.34	Tail: Class C/H + 0.6% FL-62 + 0.25 lb/sk Cello-Flake + 0.2% Sodium Metasilicate (TOC @ 1830')
8,050' 8-5/8"	470	12.7	2.22	Lead: Class C/H + 10% NaCl + 6% Bentonite Gel + 3% MagOx (TOC @ Surface)
	210	14.8	1.32	Tail: Class C/H + 10% NaCL + 3% MagOx (TOC @ 6360')
29,353' 5-1/2"	1000	14.8	1.32	Bradenhead squeeze: Class C/H + 3% Salt + 1% PreMag-M + 6% Bentonite Gel (TOC @ surface)
	1480	13.2	1.52	Tail: Class C/H + 5% NEX-020 + 0.2% NAC-102 + 0.15% NAS-725 + 0.5% NFL-549 + 0.2% NFP-703 + 1% NBE-737 + 0.3% NRT-241 (TOC @ Top of Brushy)

eog resources

Shallow Casing Design B

Proposed Wellbore

KB: 3558'
GL: 3533'



StressCheck - [Triaxial Results - Shallow 3.0 Mile *]

File Edit Wellbore Tubular View Composer Tools Window Help

Burst Design | 8 5/8" Intermediate Casing | Pressure Test

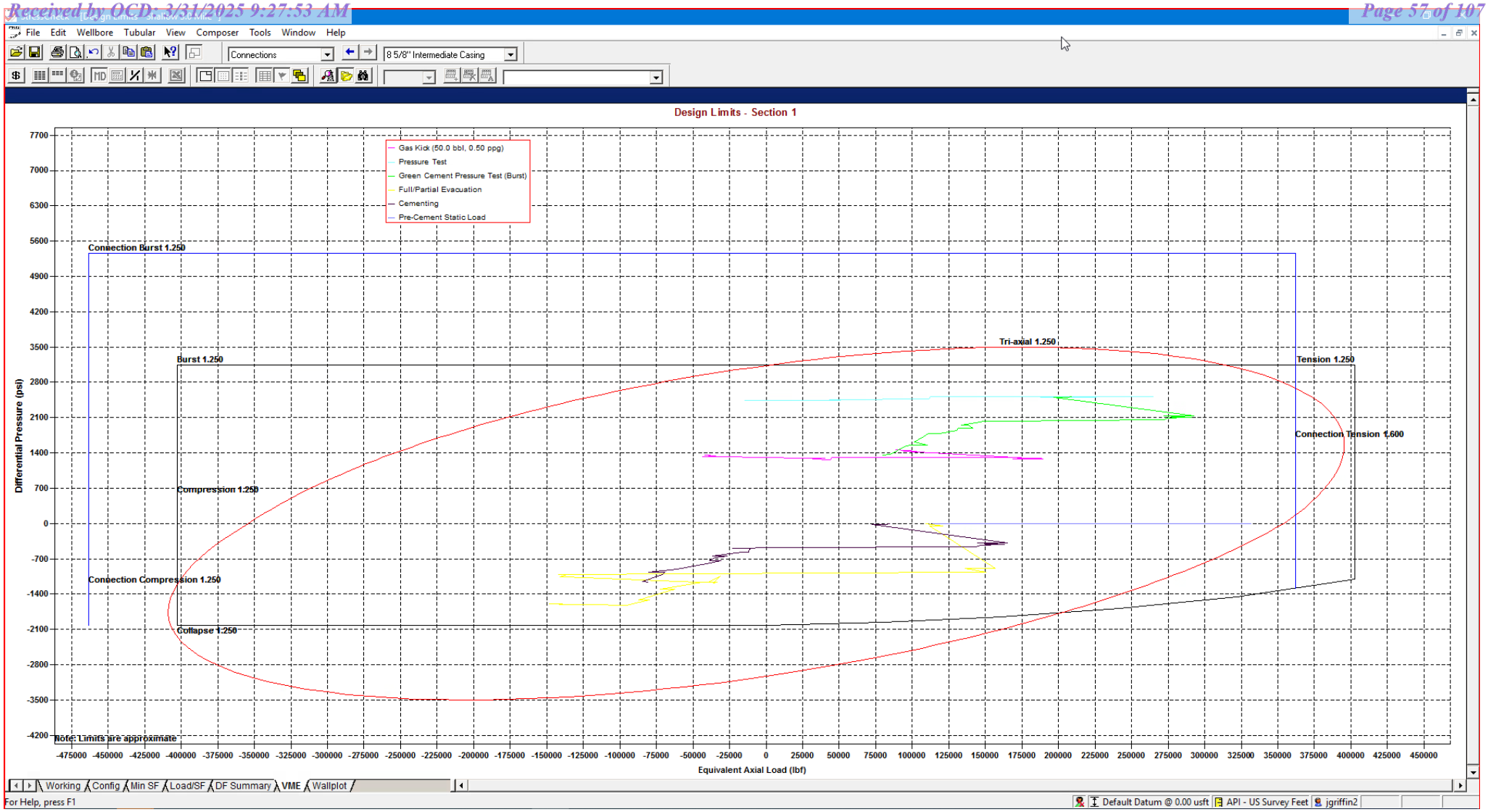
Triaxial Results

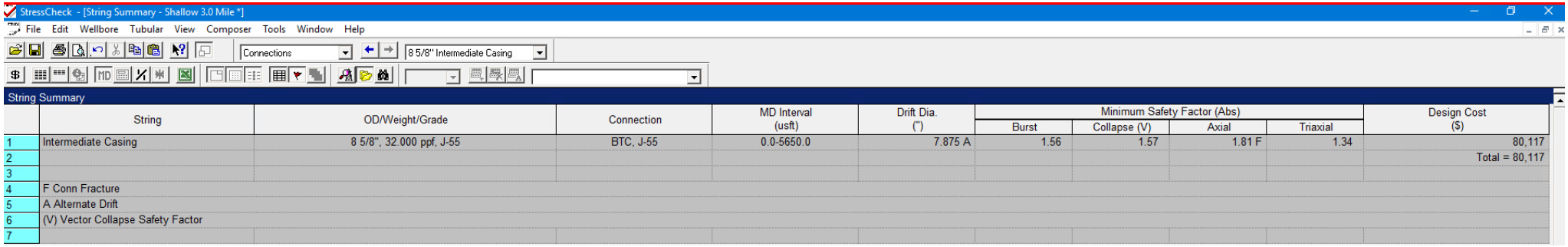
	Depth (MD) (usft)	Axial Force (lbf) Apparent (w/Bending)	Axial Force (lbf) Actual (w/o Bending)	Equivalent Axial Load (lbf)	Bending Stress at OD (psi)	Absolute Safety Factor Triaxial	Absolute Safety Factor Burst	Absolute Safety Factor Collapse (V)	Absolute Safety Factor Axial	Temperature (°F)	Pressure (psi) Internal	Pressure (psi) External	Addt'l Pickup To Prevent Buck. (lbf)	Buckled Length (usft)
1	0	200426	183224	200546	1880.2	1.68	1.57	N/A	2.89 F	70.00	2500.00	0.00	N/A	N/A
2	100	196229	179028	196812	1880.2	1.69	1.57	N/A	2.95 F	71.10	2543.63	43.63		
3	100	187111	179027	187686	883.7	1.70	1.57	N/A	3.10 F	71.10	2543.64	43.64		
4	1700	256401	111891	264835	15795.8	1.56	1.56	N/A	2.26 F	88.70	3241.64	741.64		
5	1700	235940	111891	244247	13559.4	1.60	1.56	N/A	2.45 F	88.70	3241.65	741.65		
6	1850	252413	105788	261533	16027.0	1.54	1.56	N/A	2.29 F	90.29	3305.05	805.05		
7	1850	239292	105787	248323	14592.9	1.56	1.56	N/A	2.42 F	90.29	3305.06	805.06		
8	1950	240267	101966	249748	15117.2	1.54	1.56	N/A	2.41 F	91.30	3344.87	844.87		
9	1950	234781	101965	244223	14517.5	1.56	1.56	N/A	2.47 F	91.30	3344.87	844.87		
10	2050	230871	98395	240694	14480.4	1.55	1.56	N/A	2.51 F	92.23	3381.89	881.89		
11	2050	227794	98394	237594	14144.2	1.55	1.56	N/A	2.54 F	92.23	3381.89	881.89		
12	2300	117966	90294	127818	3024.7	1.70	1.56	N/A	4.91 F	94.35	3466.13	966.13		
13	2300	104686	90293	114432	1573.2	1.71	1.56	N/A	5.53 F	94.35	3466.14	966.14		
14	2370	102469	88077	112431	1573.2	1.71	1.56	N/A	5.65 F	94.94	3489.28	989.28		
15	2370	100817	86424	111200	1573.2	1.75	1.59	N/A	5.75 F	94.94	3489.29	1036.40		
16	2700	83660	75583	95052	882.8	1.74	1.59	N/A	6.92 F	97.73	3599.97	1152.35		
17	2700	88072	75583	99504	1365.1	1.74	1.59	N/A	6.58 F	97.73	3599.97	1152.35		
18	3100	86049	62442	98863	2580.4	1.71	1.59	N/A	6.73 F	101.11	3734.23	1293.00		
19	3100	76477	62441	89195	1534.2	1.72	1.59	N/A	7.57 F	101.11	3734.23	1293.01		
20	3700	55953	42882	70509	1428.8	1.69	1.60	N/A	10.35 F	106.15	3934.24	1502.54		
21	3700	48311	42881	62778	593.5	1.71	1.60	N/A	11.99 F	106.16	3934.25	1502.55		
22	4000	41458	33043	56865	919.9	1.69	1.60	N/A	13.97 F	108.69	4034.82	1607.91		
23	4650	26293	11655	43706	1600.1	1.63	1.60	N/A	22.03 F	114.20	4253.37	1836.86		
24	4900	32619	4156	50970	3111.2	1.59	1.60	N/A	17.76 F	116.32	4337.37	1924.87		
25	4900	21439	4155	39625	1889.2	1.61	1.60	N/A	27.02 F	116.32	4337.38	1924.87		
26	5039	15822	26	34389	1726.6	1.61	1.61	N/A	36.61 F	117.49	4383.77	1973.48		
27	5039	15822	26	34388	1726.6	1.61	1.61	N/A	36.61 F	117.49	4383.78	1973.49		
28	5600	-33912	-16743	-14286	1876.7	1.57	1.61	N/A	(14.60)	122.23	4572.11	2170.78		
29	5650	-30585	-18235	-10742	1350.0	1.58	1.61	N/A	(16.18)	122.66	4588.87	2188.34		
30														
31	F	Conn Fracture												
32	( )	Compression												
33	(V)	Vector Collapse Safety Factor												
34														

Working | Config | Min SF | Load/SF | DF Summary | VME | Wallplot

For Help, press F1 | Default Datum @ 0.00 usft | API - US Survey Feet | jgriffin2

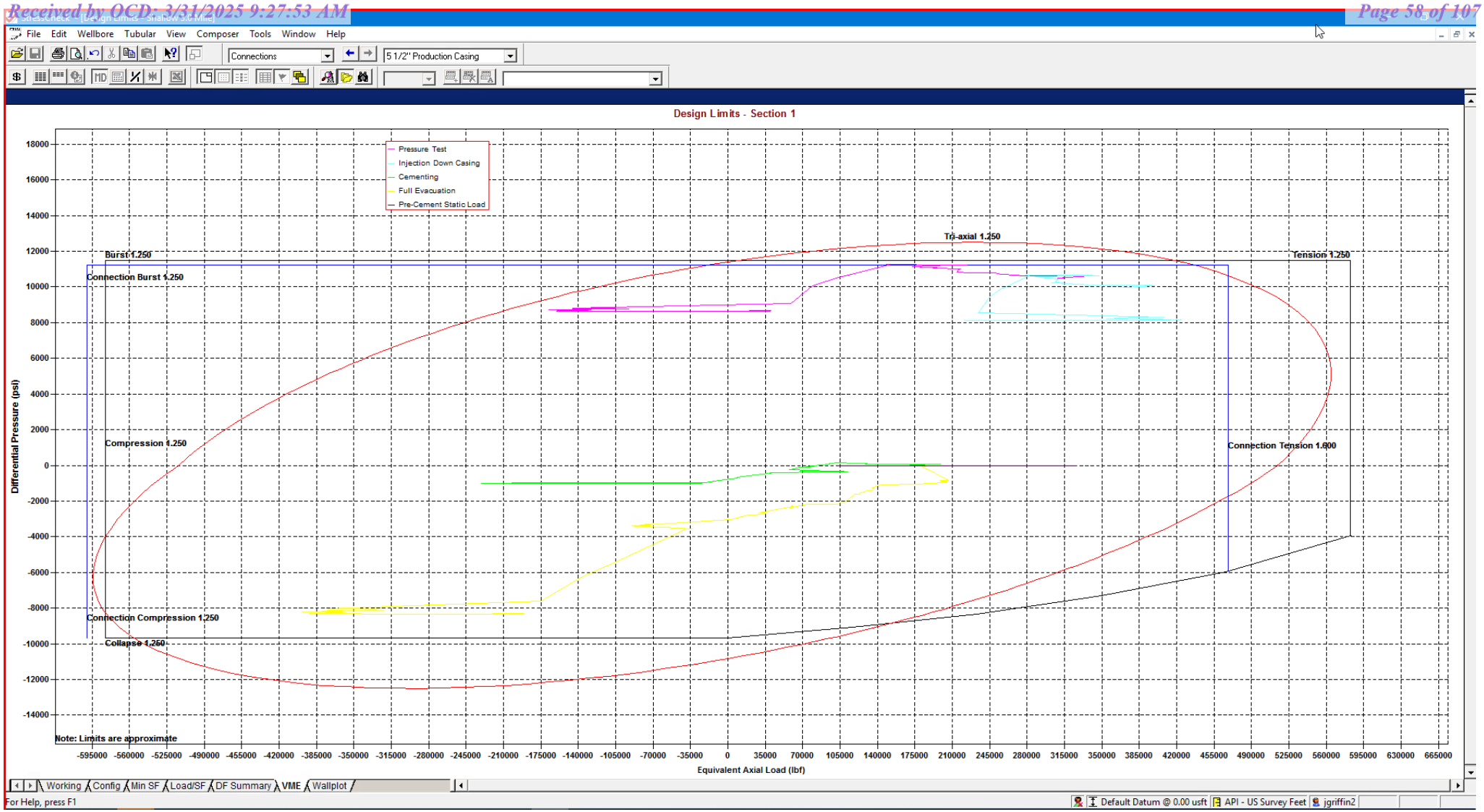
8-5/8" Intermediate Casing Pressure Test:
Internal Profile based off Surface Pressure + Hydrostatic: 4589 psi
External Profile based off Pore Pressure: 2188 psi

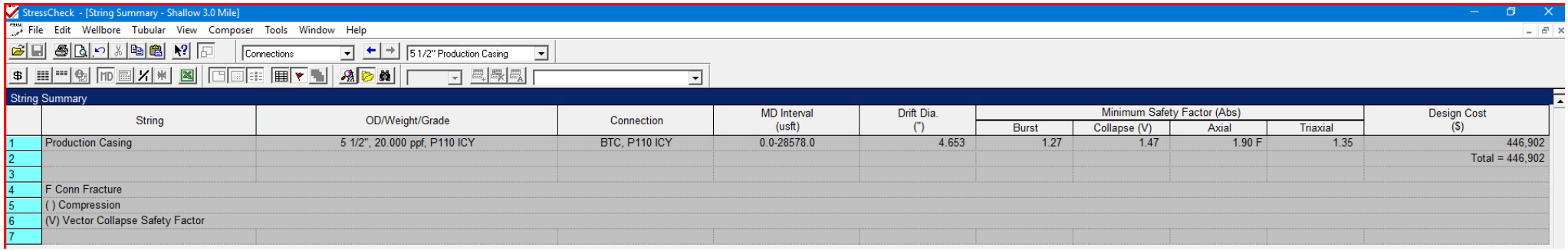




	String	OD/Weight/Grade	Connection	MD Interval (usft)	Drift Dia. (")	Minimum Safety Factor (Abs)				Design Cost ($)
						Burst	Collapse (V)	Axial	Triaxial	
1	Intermediate Casing	8 5/8", 32.000 ppf, J-55	BTC, J-55	0.0-5650.0	7.875 A	1.56	1.57	1.81 F	1.34	80,117
2										Total = 80,117
3										
4	F Conn Fracture									
5	A Alternate Drift									
6	(V) Vector Collapse Safety Factor									
7										

*Modelling done with 8-5/8" 32# Intermediate Casing. Passes all Burst, Collapse and Tensile design criteria.





	String	OD/Weight/Grade	Connection	MD Interval (usft)	Drift Dia. (")	Minimum Safety Factor (Abs)				Design Cost ($)
						Burst	Collapse (V)	Axial	Triaxial	
1	Production Casing	5 1/2", 20.000 ppf, P110 ICY	BTC, P110 ICY	0.0-28578.0	4.653	1.27	1.47	1.90 F	1.35	446,902
2										Total = 446,902
3										
4	F Conn Fracture									
5	( ) Compression									
6	(V) Vector Collapse Safety Factor									
7										

*Modelling done with 5-1/2" 20# Production Casing with a 125ksi Control Yield. Passes all Burst, Collapse and Tensile design criteria.

eog resources

Shallow Design C

4. CASING PROGRAM

Hole Size	Interval MD From (ft)	Interval MD To (ft)	Interval TVD From (ft)	Interval TVD To (ft)	Csg OD	Weight	Grade	Conn
16"	0	2,161	0	2,030	13-3/8"	54.5#	J-55	STC
11"	0	7,951	0	5,650	9-5/8"	40#	J-55	LTC
7-7/8"	0	29,353	0	12,000	6"	24.5#	P110-EC	VAM Sprint-SF

Hole will be full during casing run for well control and tensile SF factor. Casing will be kept at least half full during run for this design to meet BLM collapse SF requirement. External pressure will be reviewed prior to conducting casing pressure tests to ensure that 70% of the yield is not exceeded.

Variance is requested to waive the centralizer requirements for the 9-5/8" casing in the 11" hole size. An expansion additive will be utilized, in the cement slurry, for the entire length of the 11" hole interval to maximize cement bond and zonal isolation.

Variance is also requested to waive any centralizer requirements for the 6" casing in the 7-7/8" hole size. An expansion additive will be utilized, in the cement slurry, for the entire length of the 7-7/8" hole interval to maximize cement bond and zonal isolation.

EOG requests permission to allow deviation from the 0.422'' annulus clearance requirement for the intermediate (salt) section from Title 43 CFR Part 3170 under the following conditions:

- The variance is not applicable within the Potash Boundaries or Capitan Reef areas.
- Operator takes responsibility to get casing to set point in the event that the clearance causes stuck pipe issues.

5. CEMENTING PROGRAM:

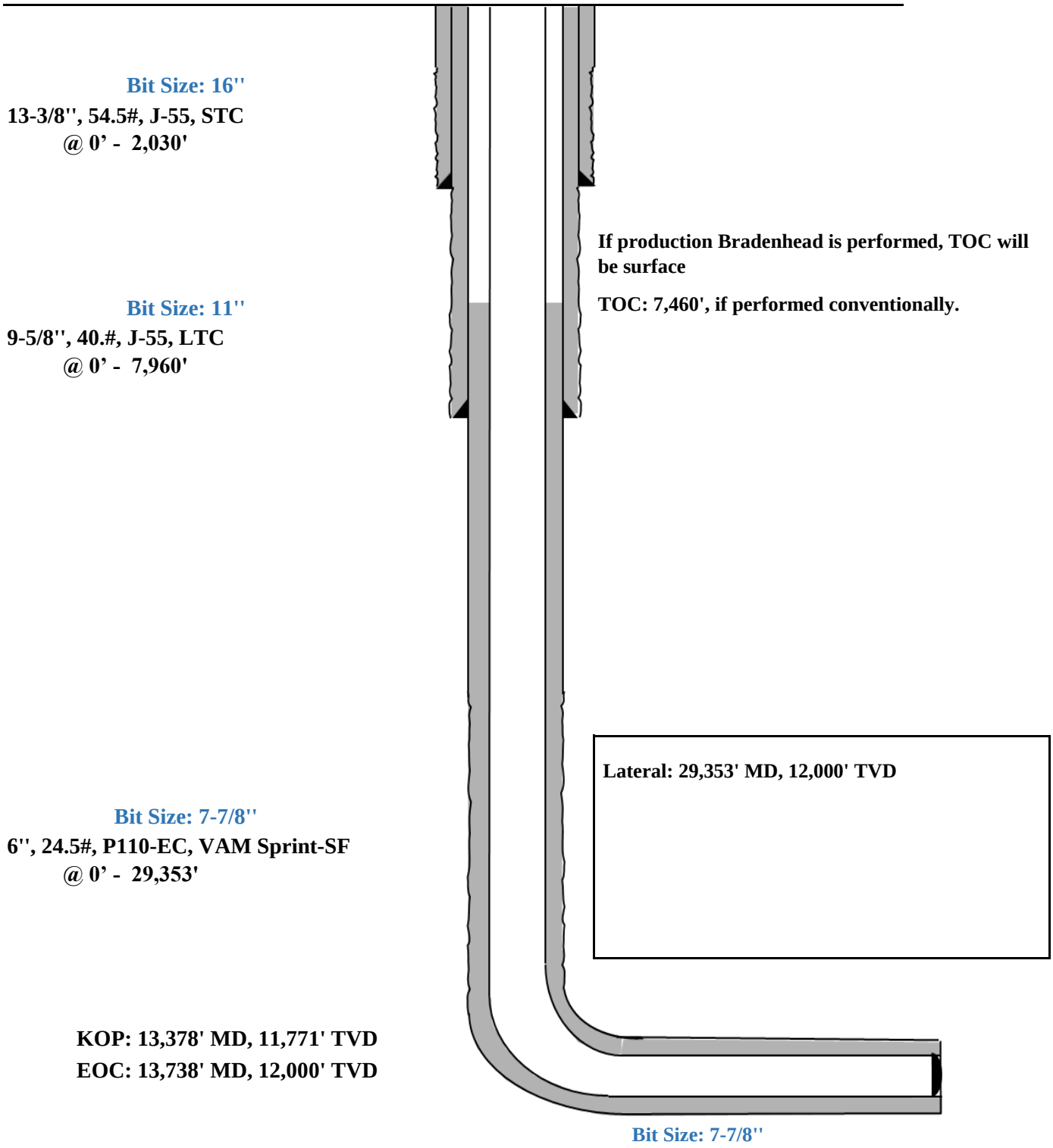
Depth	No. Sacks	Wt. ppg	Yld Ft3/sk	Slurry Description
2,030' 13-3/8"	570	13.5	1.73	Lead: Class C/H + 4.0% Bentonite Gel + 0.5% CaCl2 + 0.25 lb/sk Cello-Flake (TOC @ Surface)
	160	14.8	1.34	Tail: Class C/H + 0.6% FL-62 + 0.25 lb/sk Cello-Flake + 0.2% Sodium Metasilicate (TOC @ 1830')
8,050' 9-5/8"	760	12.7	2.22	Lead: Class C/H + 10% NaCl + 6% Bentonite Gel + 3% MagOx (TOC @ Surface)
	250	14.8	1.32	Tail: Class C/H + 10% NaCL + 3% MagOx (TOC @ 6360')
29,353' 6"	1000	14.8	1.32	Bradenhead squeeze: Class C/H + 3% Salt + 1% PreMag-M + 6% Bentonite Gel (TOC @ surface)
	2500	13.2	1.52	Tail: Class C/H + 5% NEX-020 + 0.2% NAC-102 + 0.15% NAS-725 + 0.5% NFL-549 + 0.2% NFP-703 + 1% NBE-737 + 0.3% NRT-241 (TOC @ Top of Brushy)

eog resources

Shallow Design C

Proposed Wellbore

KB: 3558'
GL: 3533'



Stresscheck - [Triaxial Results - Shallow 3.0 Mile - Big Hole]

File Edit Wellbore Tubular View Composer Tools Window Help

9 5/8" Intermediate Casing

Pressure Test

Triaxial Results

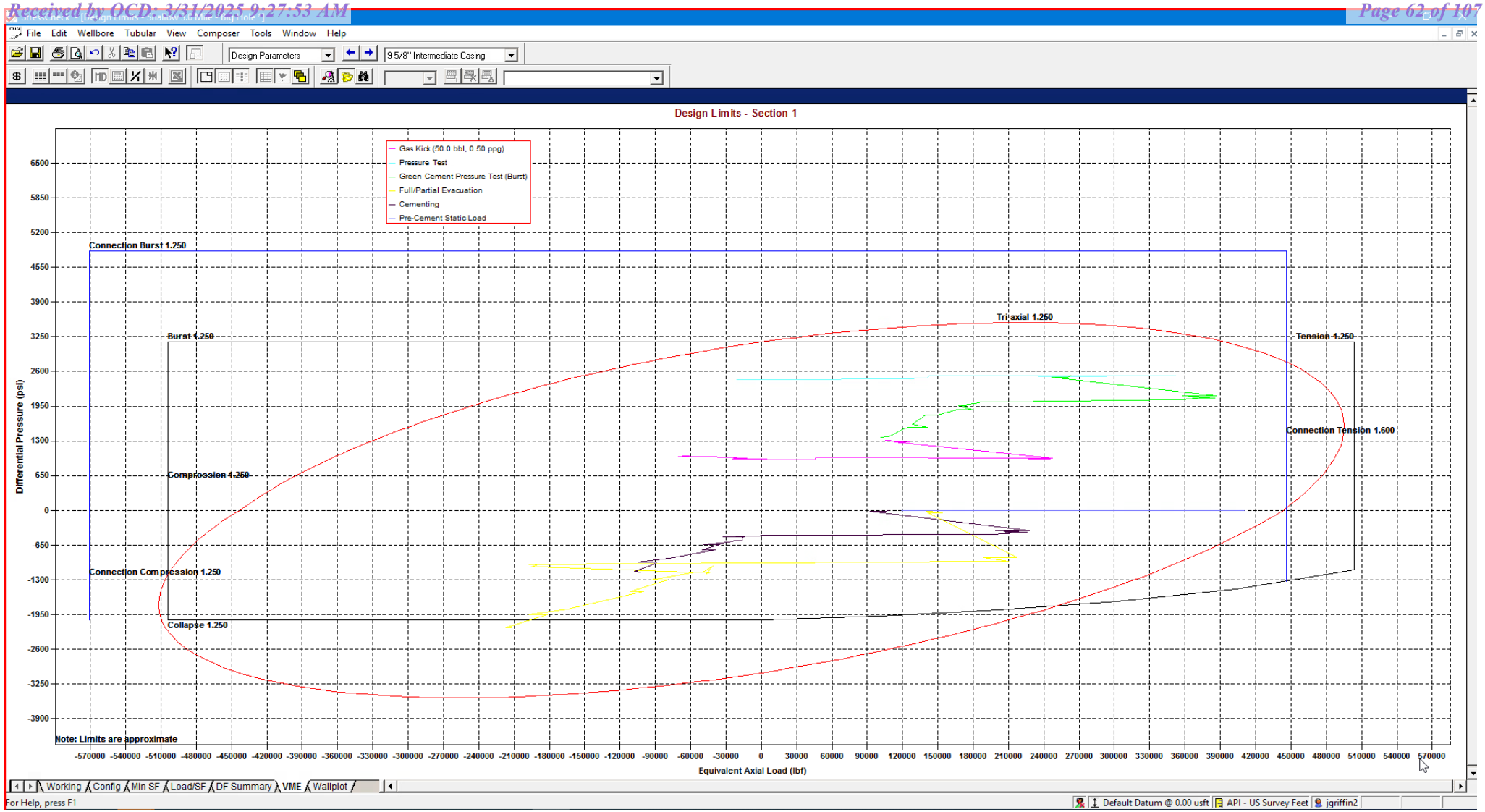
	Depth (MD) (usft)	Axial Force (lbf) Apparent (w/Bending)	Axial Force (lbf) Actual (w/o Bending)	Equivalent Axial Load (lbf)	Bending Stress at OD (psi)	Absolute Safety Factor Triaxial	Absolute Safety Factor Burst	Absolute Safety Factor Collapse (V)	Absolute Safety Factor Axial	Temperature (°F)	Pressure (psi) Internal	Pressure (psi) External	Addt'l Pickup To Prevent Buck. (lbf)	Buckled Length (usft)
1	0	252987	228954	253140	2098.2	1.69	1.58	N/A	2.82 F	70.00	2500.00	0.00	N/A	N/A
2	100	247735	223702	248466	2098.2	1.69	1.58	N/A	2.88 F	71.10	2543.63	43.63		
3	100	234996	223701	235716	986.2	1.71	1.58	N/A	3.04 F	71.10	2543.64	43.64		
4	1700	341565	139667	352253	17627.2	1.53	1.57	N/A	2.09 F	88.70	3241.64	741.64		
5	1700	312979	139666	323488	15131.5	1.58	1.57	N/A	2.28 F	88.70	3241.65	741.65		
6	1850	336881	132027	348440	17885.2	1.51	1.57	N/A	2.12 F	90.29	3305.05	805.05		
7	1850	318549	132027	329984	16284.8	1.54	1.57	N/A	2.24 F	90.29	3305.06	805.06		
8	1950	320468	127243	332475	16869.9	1.52	1.57	N/A	2.23 F	91.30	3344.87	844.87		
9	1950	312802	127243	324756	16200.7	1.53	1.57	N/A	2.28 F	91.30	3344.87	844.87		
10	2050	307858	122773	320295	16159.3	1.52	1.57	N/A	2.32 F	92.23	3381.89	881.89		
11	2050	303560	122772	315965	15784.1	1.53	1.57	N/A	2.35 F	92.23	3381.89	881.89		
12	2300	151294	112633	163658	3375.4	1.71	1.57	N/A	4.72 F	94.35	3466.13	966.13		
13	2300	132741	112633	144956	1755.6	1.72	1.57	N/A	5.38 F	94.35	3466.14	966.14		
14	2370	129966	109858	142452	1755.6	1.72	1.57	N/A	5.49 F	94.94	3489.28	989.28		
15	2370	127909	107800	140922	1755.6	1.75	1.60	N/A	5.58 F	94.94	3489.29	1036.40		
16	2700	105515	94232	119785	985.1	1.75	1.60	N/A	6.77 F	97.73	3599.97	1152.35		
17	2700	111680	94231	126006	1523.4	1.75	1.60	N/A	6.39 F	97.73	3599.97	1152.35		
18	3100	110766	77783	126839	2879.6	1.71	1.60	N/A	6.44 F	101.11	3734.23	1293.00		
19	3100	97392	77783	113331	1712.1	1.73	1.60	N/A	7.33 F	101.11	3734.23	1293.01		
20	3700	71565	53303	89806	1594.4	1.70	1.61	N/A	9.97 F	106.15	3934.24	1502.54		
21	3700	60887	53302	79004	662.3	1.71	1.61	N/A	11.72 F	106.16	3934.25	1502.55		
22	4650	34671	14219	56495	1785.6	1.64	1.61	N/A	20.59 F	114.20	4253.37	1836.86		
23	4900	44595	4828	67626	3472.0	1.59	1.61	N/A	16.01 F	116.32	4337.37	1924.87		
24	4900	28975	4828	51775	2108.2	1.62	1.61	N/A	24.64 F	116.32	4337.38	1924.87		
25	5029	22103	34	45340	1926.8	1.61	1.61	N/A	32.30 F	117.40	4380.40	1969.94		
26	5029	22102	33	45339	1926.8	1.61	1.61	N/A	32.30 F	117.40	4380.41	1969.95		
27	5600	-45329	-21341	-20805	2094.3	1.57	1.62	N/A	(13.67)	122.23	4572.11	2170.78		
28	5650	-40465	-23210	-15657	1506.5	1.58	1.62	N/A	(15.31)	122.66	4588.87	2188.34		
29														
30	F	Conn Fracture												
31	( )	Compression												
32	(V)	Vector Collapse Safety Factor												
33														

Working / Config / Min SF / Load/SF / DF Summary / VME / Wallplot

For Help, press F1

Default Datum @ 0.00 usft | API - US Survey Feet | jqriffin2

9-5/8" Intermediate Casing Pressure Test:
Internal Profile based off Surface Pressure + Hydrostatic: 4589 psi
External Profile based off Pore Pressure: 2188 psi



StressCheck - [String Summary - Shallow 3.0 Mile - Big Hole *]

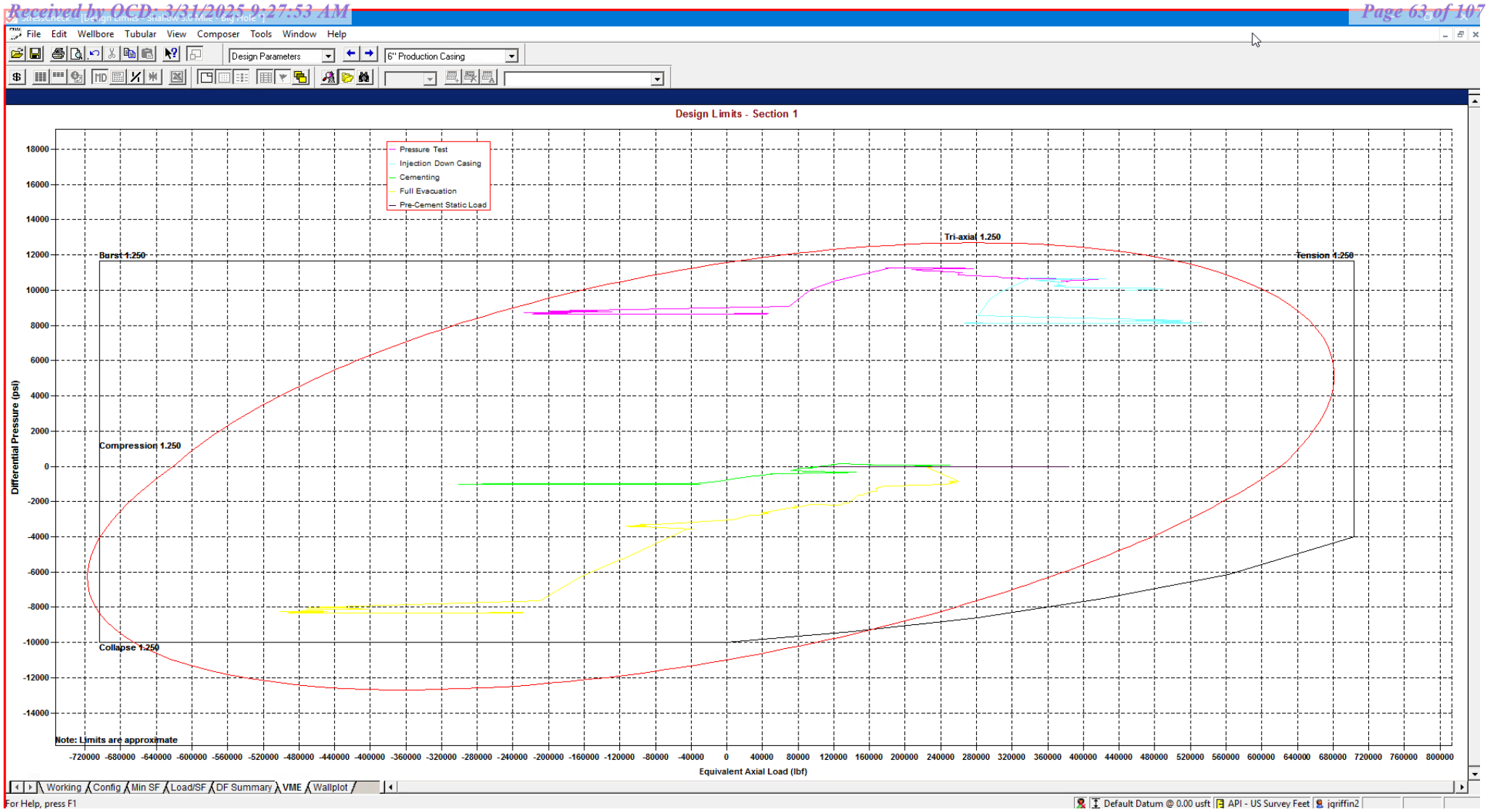
File Edit Wellbore Tubular View Composer Tools Window Help

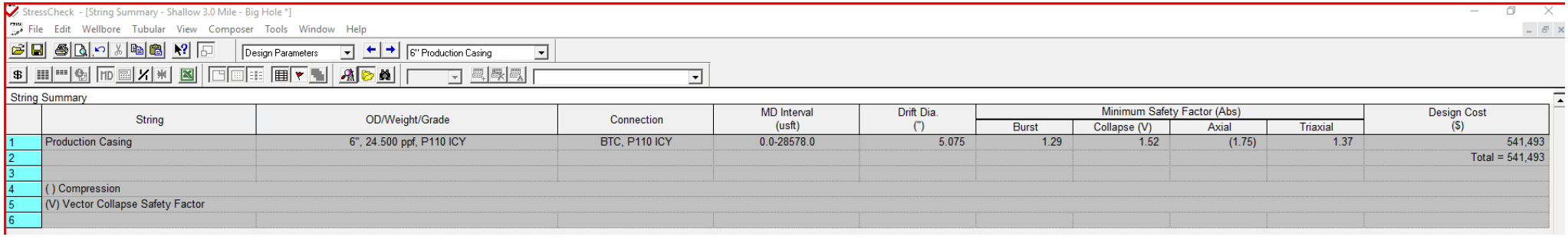
Collapse Loads | 9 5/8" Intermediate Casing

String Summary

	String	OD/Weight/Grade	Connection	MD Interval (usft)	Drift Dia. (")	Minimum Safety Factor (Abs)				Design Cost ($)
						Burst	Collapse (V)	Axial	Triaxial	
1	Intermediate Casing	9 5/8", 40.000 ppf, J-55	BTC, J-55	0.0-5650.0	8.750 A	1.57	1.59	1.80 F	1.35	98,141
2										Total = 98,141
3										
4	F Conn Fracture									
5	A Alternate Drift									
6	(V) Vector Collapse Safety Factor									
7										

*Modelling done with 9-5/8" 40# Intermediate Casing. Passes all Burst, Collapse and Tensile design criteria.





StressCheck - [String Summary - Shallow 3.0 Mile - Big Hole *]

String Summary

	String	OD/Weight/Grade	Connection	MD Interval (usft)	Drift Dia. (")	Minimum Safety Factor (Abs)				Design Cost ($)
						Burst	Collapse (V)	Axial	Triaxial	
1	Production Casing	6", 24.500 ppf, P110 ICY	BTC, P110 ICY	0.0-28578.0	5.075	1.29	1.52	(1.75)	1.37	541,493
2										Total = 541,493
3										
4	( ) Compression									
5	(V) Vector Collapse Safety Factor									
6										

*Modelling done with 6" Production Casing with a 125ksi Control Yield. Passes all Burst, Collapse and Tensile design criteria.

eog resources

Shallow Design D

4. CASING PROGRAM

Hole Size	Interval MD From (ft)	Interval MD To (ft)	Interval TVD From (ft)	Interval TVD To (ft)	Csg OD	Weight	Grade	Conn
16"	0	2,161	0	2,030	13-3/8"	54.5#	J-55	STC
11"	0	7,951	0	5,650	9-5/8"	40#	J-55	LTC
7-7/8"	0	13,278	0	11,671	6"	22.3#	P110-EC	DWC/C IS
6-3/4"	13,278	29,353	11,671	12,000	5-1/2"	20#	P110-EC	DWC/C IS MS

Hole will be full during casing run for well control and tensile SF factor. Casing will be kept at least half full during run for this design to meet BLM collapse SF requirement. External pressure will be reviewed prior to conducting casing pressure tests to ensure that 70% of the yield is not exceeded.

Variance is requested to waive the centralizer requirements for the 9-5/8" casing in the 11" hole size. An expansion additive will be utilized, in the cement slurry, for the entire length of the 11" hole interval to maximize cement bond and zonal isolation.

Variance is also requested to waive any centralizer requirements for the 6" and 5-1/2" casings in the 7-7/8" and 6-3/4" hole sizes. An expansion additive will be utilized in the cement slurry for the entire length of the 7-7/8" and 6-3/4" hole intervals to maximize cement bond and zonal isolation.

EOG requests permission to allow deviation from the 0.422'' annulus clearance requirement for the intermediate (salt) section from Title 43 CFR Part 3170 under the following conditions:

- The variance is not applicable within the Potash Boundaries or Capitan Reef areas.
- Operator takes responsibility to get casing to set point in the event that the clearance causes stuck pipe issues.

5. CEMENTING PROGRAM:

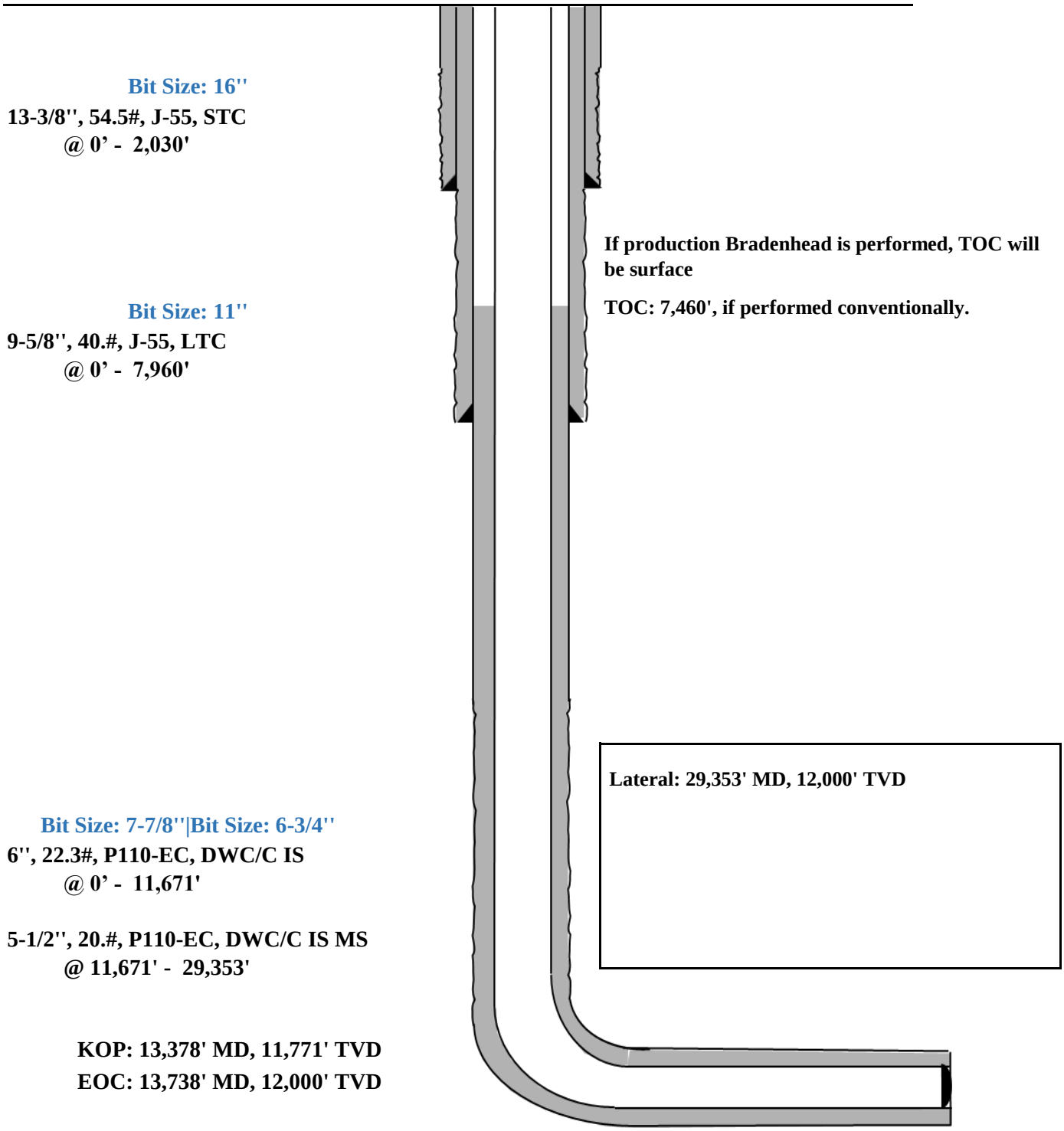
Depth	No. Sacks	Wt. ppg	Yld Ft3/sk	Slurry Description
2,030' 13-3/8"	570	13.5	1.73	Lead: Class C/H + 4.0% Bentonite Gel + 0.5% CaCl2 + 0.25 lb/sk Cello-Flake (TOC @ Surface)
	160	14.8	1.34	Tail: Class C/H + 0.6% FL-62 + 0.25 lb/sk Cello-Flake + 0.2% Sodium Metasilicate (TOC @ 1830')
8,050' 9-5/8"	760	12.7	2.22	Lead: Class C/H + 10% NaCl + 6% Bentonite Gel + 3% MagOx (TOC @ Surface)
	250	14.8	1.32	Tail: Class C/H + 10% NaCL + 3% MagOx (TOC @ 6360')
29,353' 6"	1000	14.8	1.32	Bradenhead squeeze: Class C/H + 3% Salt + 1% PreMag-M + 6% Bentonite Gel (TOC @ surface)
	2500	13.2	1.52	Tail: Class C/H + 5% NEX-020 + 0.2% NAC-102 + 0.15% NAS-725 + 0.5% NFL-549 + 0.2% NFP-703 + 1% NBE-737 + 0.3% NRT-241 (TOC @ Top of Brushy)

eog resources

Shallow Design D

Proposed Wellbore

KB: 3558'
GL: 3533'



File Edit Wellbore Tubular View Composer Tools Window Help

9 5/8" Intermediate Casing

Pressure Test

Triaxial Results

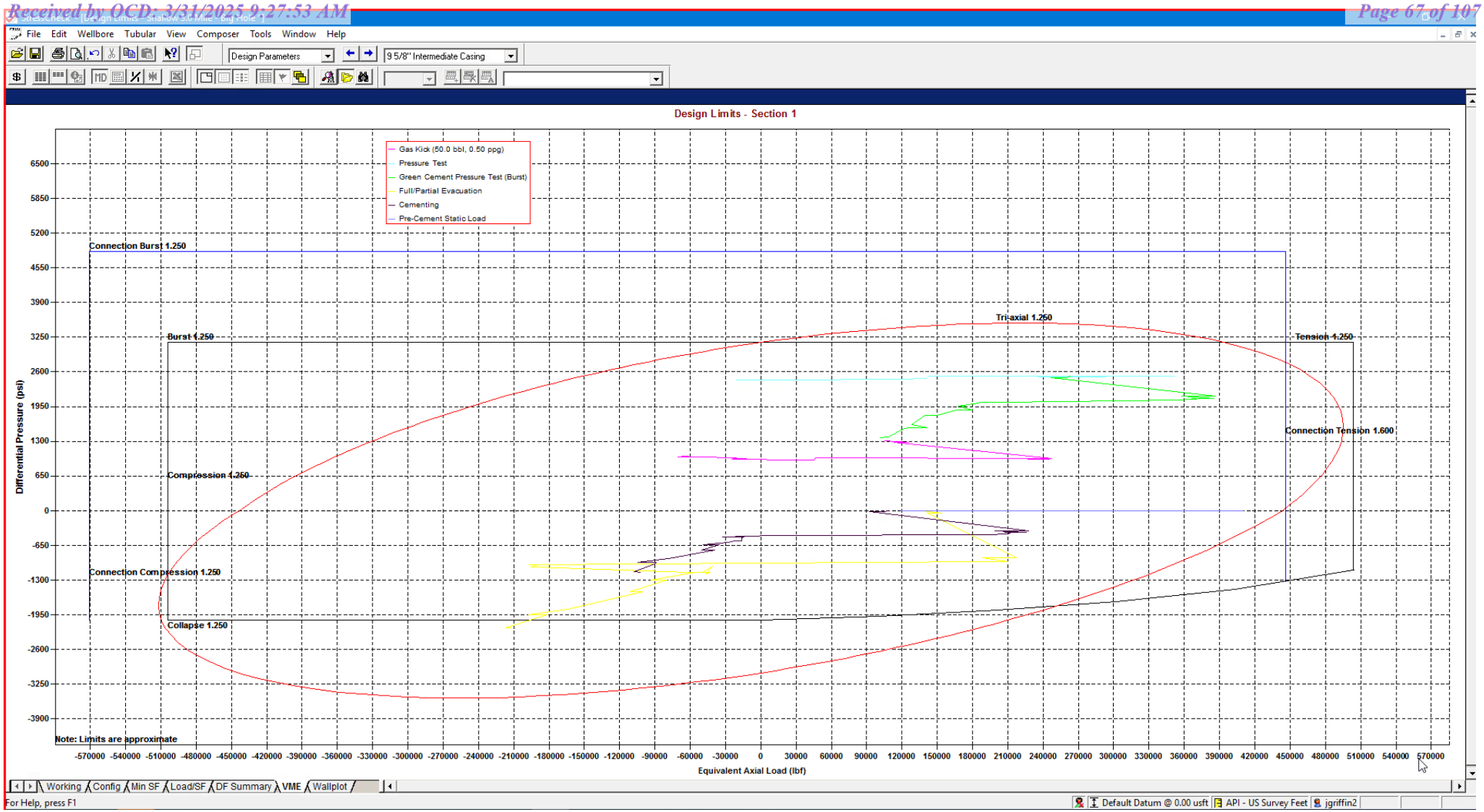
	Depth (MD) (usft)	Axial Force (lbf) Apparent (w/Bending)	Axial Force (lbf) Actual (w/o Bending)	Equivalent Axial Load (lbf)	Bending Stress at OD (psi)	Absolute Safety Factor Triaxial	Absolute Safety Factor Burst	Absolute Safety Factor Collapse (V)	Absolute Safety Factor Axial	Temperature (°F)	Pressure (psi) Internal	Pressure (psi) External	Addt'l Pickup To Prevent Buck. (lbf)	Buckled Length (usft)
1	0	252987	228954	253140	2098.2	1.69	1.58	N/A	2.82 F	70.00	2500.00	0.00	N/A	N/A
2	100	247735	223702	248466	2098.2	1.69	1.58	N/A	2.88 F	71.10	2543.63	43.63		
3	100	234996	223701	235716	986.2	1.71	1.58	N/A	3.04 F	71.10	2543.64	43.64		
4	1700	341565	139667	352253	17627.2	1.53	1.57	N/A	2.09 F	88.70	3241.64	741.64		
5	1700	312979	139666	323488	15131.5	1.58	1.57	N/A	2.28 F	88.70	3241.65	741.65		
6	1850	336881	132027	348440	17885.2	1.51	1.57	N/A	2.12 F	90.29	3305.05	805.05		
7	1850	318549	132027	329984	16284.8	1.54	1.57	N/A	2.24 F	90.29	3305.06	805.06		
8	1950	320468	127243	332475	16869.9	1.52	1.57	N/A	2.23 F	91.30	3344.87	844.87		
9	1950	312802	127243	324756	16200.7	1.53	1.57	N/A	2.28 F	91.30	3344.87	844.87		
10	2050	307858	122773	320295	16159.3	1.52	1.57	N/A	2.32 F	92.23	3381.89	881.89		
11	2050	303560	122772	315965	15784.1	1.53	1.57	N/A	2.35 F	92.23	3381.89	881.89		
12	2300	151294	112633	163658	3375.4	1.71	1.57	N/A	4.72 F	94.35	3466.13	966.13		
13	2300	132741	112633	144956	1755.6	1.72	1.57	N/A	5.38 F	94.35	3466.14	966.14		
14	2370	129966	109858	142452	1755.6	1.72	1.57	N/A	5.49 F	94.94	3489.28	989.28		
15	2370	127909	107800	140922	1755.6	1.75	1.60	N/A	5.58 F	94.94	3489.29	1036.40		
16	2700	105515	94232	119785	985.1	1.75	1.60	N/A	6.77 F	97.73	3599.97	1152.35		
17	2700	111680	94231	126006	1523.4	1.75	1.60	N/A	6.39 F	97.73	3599.97	1152.35		
18	3100	110766	77783	126839	2879.6	1.71	1.60	N/A	6.44 F	101.11	3734.23	1293.00		
19	3100	97392	77783	113331	1712.1	1.73	1.60	N/A	7.33 F	101.11	3734.23	1293.01		
20	3700	71565	53303	89806	1594.4	1.70	1.61	N/A	9.97 F	106.15	3934.24	1502.54		
21	3700	60887	53302	79004	662.3	1.71	1.61	N/A	11.72 F	106.16	3934.25	1502.55		
22	4650	34671	14219	56495	1785.6	1.64	1.61	N/A	20.59 F	114.20	4253.37	1836.86		
23	4900	44595	4828	67626	3472.0	1.59	1.61	N/A	16.01 F	116.32	4337.37	1924.87		
24	4900	28975	4828	51775	2108.2	1.62	1.61	N/A	24.64 F	116.32	4337.38	1924.87		
25	5029	22103	34	45340	1926.8	1.61	1.61	N/A	32.30 F	117.40	4380.40	1969.94		
26	5029	22102	33	45339	1926.8	1.61	1.61	N/A	32.30 F	117.40	4380.41	1969.95		
27	5600	-45329	-21341	-20805	2094.3	1.57	1.62	N/A	(13.67)	122.23	4572.11	2170.78		
28	5650	-40465	-23210	-15657	1506.5	1.58	1.62	N/A	(15.31)	122.66	4588.87	2188.34		
29														
30	F	Conn Fracture												
31	( )	Compression												
32	(V)	Vector Collapse Safety Factor												
33														

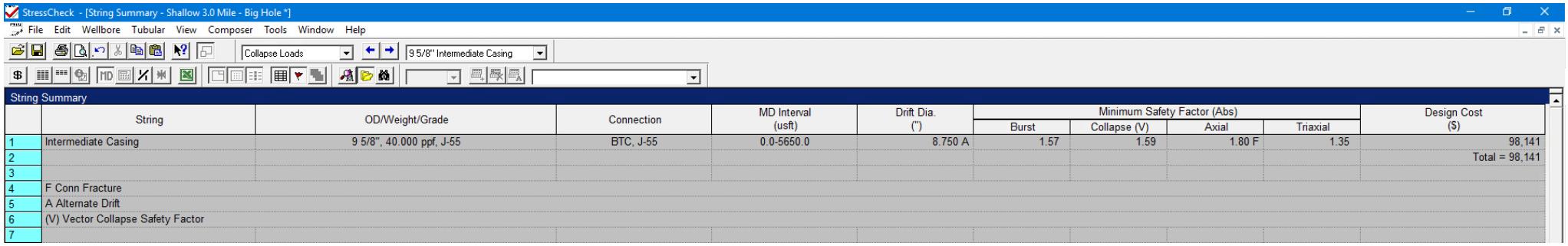
Working / Config / Min SF / Load/SF / DF Summary / VME / Wallplot

For Help, press F1

Default Datum @ 0.00 usft | API - US Survey Feet | jqriffin2

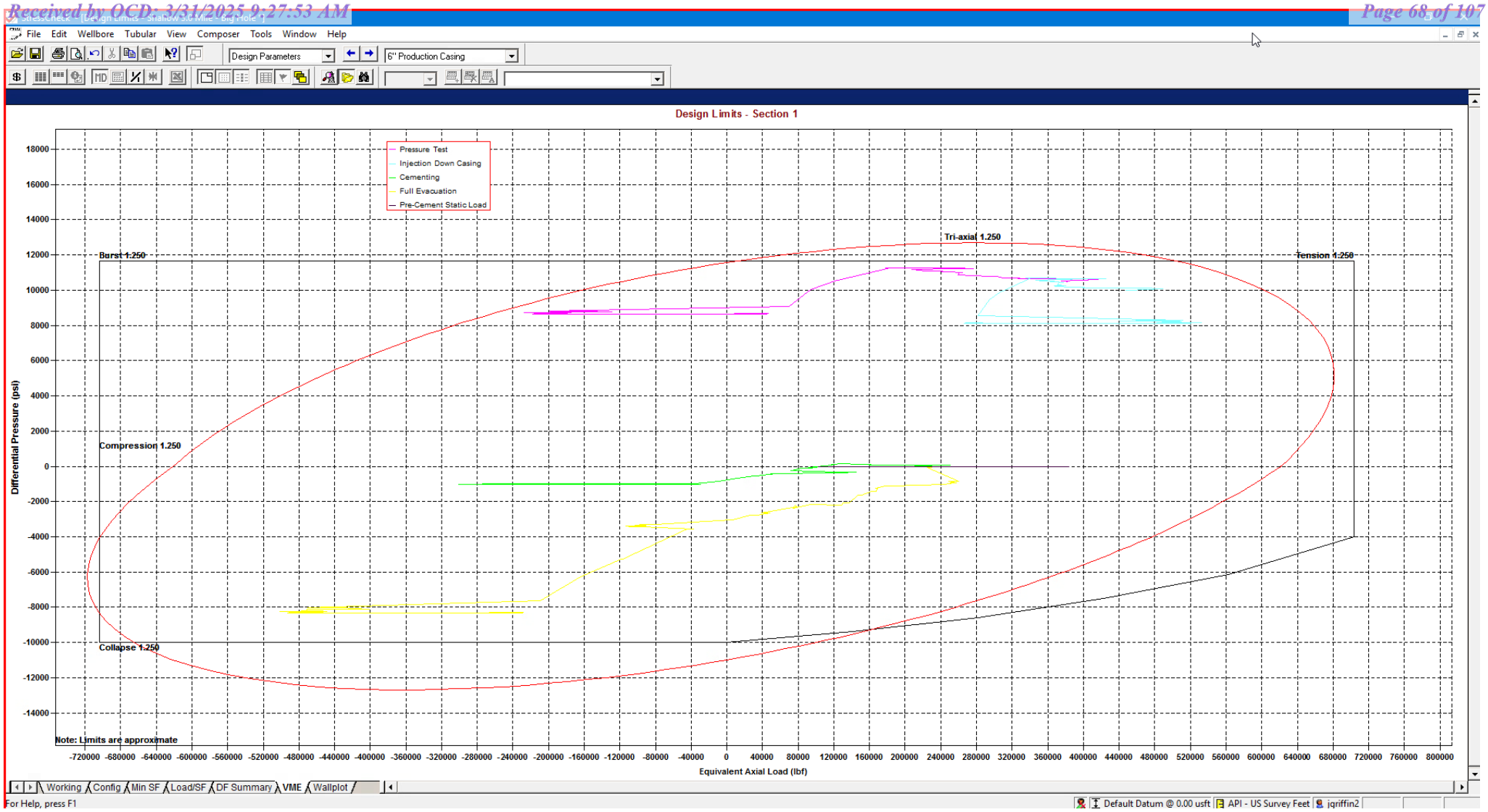
9-5/8" Intermediate Casing Pressure Test:
Internal Profile based off Surface Pressure + Hydrostatic: 4589 psi
External Profile based off Pore Pressure: 2188 psi

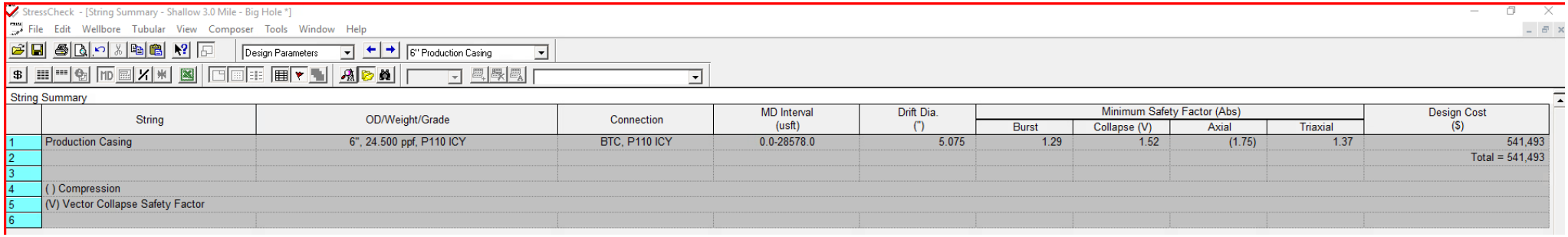




	String	OD/Weight/Grade	Connection	MD Interval (usft)	Drift Dia. (")	Minimum Safety Factor (Abs)				Design Cost ($)
						Burst	Collapse (V)	Axial	Triaxial	
1	Intermediate Casing	9 5/8", 40.000 ppf, J-55	BTC, J-55	0.0-5650.0	8.750 A	1.57	1.59	1.80 F	1.35	98,141
2										Total = 98,141
3										
4	F Conn Fracture									
5	A Alternate Drift									
6	(V) Vector Collapse Safety Factor									
7										

*Modelling done with 9-5/8" 40# Intermediate Casing. Passes all Burst, Collapse and Tensile design criteria.



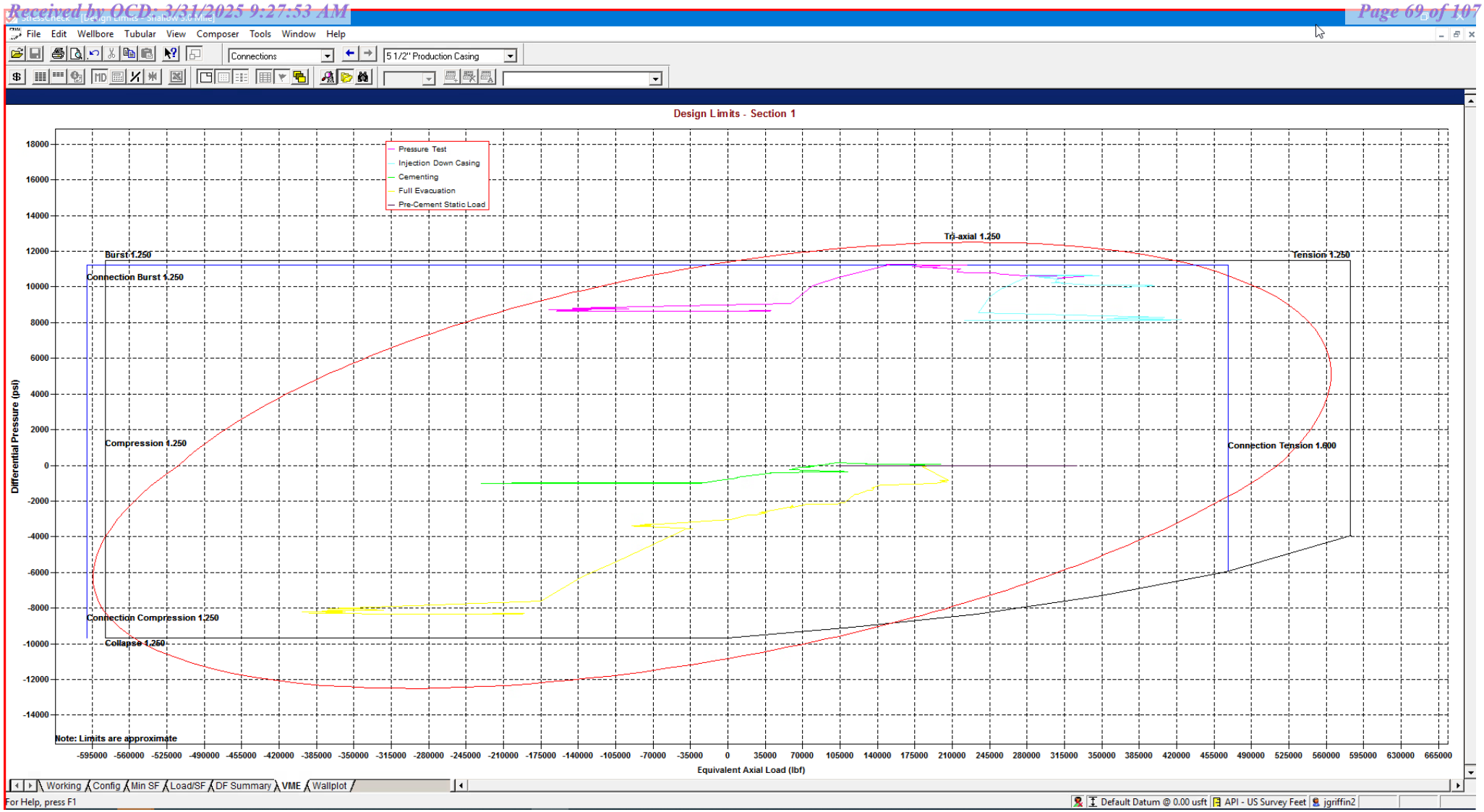


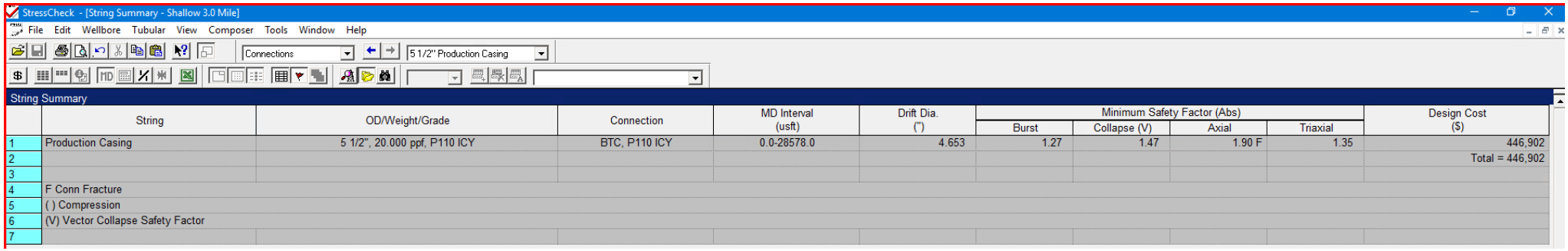
StressCheck - [String Summary - Shallow 3.0 Mile - Big Hole *]

String Summary

	String	OD/Weight/Grade	Connection	MD Interval (usft)	Drift Dia. (")	Minimum Safety Factor (Abs)				Design Cost ($)
						Burst	Collapse (V)	Axial	Triaxial	
1	Production Casing	6", 24.500 ppf, P110 ICY	BTC, P110 ICY	0.0-28578.0	5.075	1.29	1.52	(1.75)	1.37	541,493
2										Total = 541,493
3										
4	( ) Compression									
5	(V) Vector Collapse Safety Factor									
6										

*Modelling done with 6" Production Casing with a 125ksi Control Yield. Passes all Burst, Collapse and Tensile design criteria.





	String	OD/Weight/Grade	Connection	MD Interval (usft)	Drift Dia. (")	Minimum Safety Factor (Abs)				Design Cost ($)
						Burst	Collapse (V)	Axial	Triaxial	
1	Production Casing	5 1/2", 20.000 ppf, P110 ICY	BTC, P110 ICY	0.0-28578.0	4.653	1.27	1.47	1.90 F	1.35	446,902
2										Total = 446,902
3										
4	F Conn Fracture									
5	( ) Compression									
6	(V) Vector Collapse Safety Factor									
7										

*Modelling done with 5-1/2" 20# Production Casing with a 125ksi Control Yield. Passes all Burst, Collapse and Tensile design criteria.

eog resources

Shallow Casing Design E

1. CASING PROGRAM

Hole Size	Interval MD From (ft)	Interval MD To (ft)	Interval TVD From (ft)	Interval TVD To (ft)	Csg OD	Weight	Grade	Conn
13"	0	2,025	0	2,025	10-3/4"	40.5#	J-55	STC
9-7/8"	0	7,793	0	5,645	8-5/8"	32#	J-55	BTC-SC
7-7/8"	0	12,626	0	10,896	6"	24.5#	P110-EC	VAM Sprint-TC
6-3/4"	12,626	28,578	10,896	11,225	5-1/2"	20#	P110-EC	VAM Sprint SF

**For highlighted rows above, variance is requested to run entire string of either 6'' or 5-1/2'' casing string above due to availablility.

Hole will be full during casing run for well control and tensile SF factor. Casing will be kept at least half full during run for this design to meet BLM collapse SF requirement. External pressure will be reviewed prior to conducting casing pressure tests to ensure that 70% of the yield is not exceeded.

Variance is requested to waive the centralizer requirements for the 8-5/8" casing in the 9-7/8" hole size. An expansion additive will be utilized, in the cement slurry, for the entire length of the 9-7/8" hole interval to maximize cement bond and zonal isolation.

Variance is also requested to waive any centralizer requirements for the 6" and 5-1/2" casings in the 7-7/8" and 6-3/4" hole sizes. An expansion additive will be utilized in the cement slurry for the entire length of the 7-7/8" and 6-3/4" hole intervals to maximize cement bond and zonal isolation.

EOG requests permission to allow deviation from the 0.422'' annulus clearance requirement for the intermediate (salt) section from Title 43 CFR Part 3170 under the following conditions:

- The variance is not applicable within the Potash Boundaries or Capitan Reef areas.
- Operator takes responsibility to get casing to set point in the event that the clearance causes stuck pipe issues.

2. CEMENTING PROGRAM:

Depth	No. Sacks	Wt. ppg	Yld Ft3/sk	Slurry Description
2,030' 10-3/4"	450	13.5	1.73	Lead: Class C/H + 4.0% Bentonite Gel + 0.5% CaCl2 + 0.25 lb/sk Cello-Flake (TOC @ Surface)
	120	14.8	1.34	Tail: Class C/H + 0.6% FL-62 + 0.25 lb/sk Cello-Flake + 0.2% Sodium Metasilicate (TOC @ 1830')
7,890' 8-5/8"	460	12.7	2.22	Lead: Class C/H + 10% NaCl + 6% Bentonite Gel + 3% MagOx (TOC @ Surface)
	210	14.8	1.32	Tail: Class C/H + 10% NaCL + 3% MagOx (TOC @ 6234')
28,578' 6"	1000	14.8	1.32	Bradenhead squeeze: Class C/H + 3% Salt + 1% PreMag-M + 6% Bentonite Gel (TOC @ surface)
	2410	13.2	1.52	Tail: Class C/H + 5% NEX-020 + 0.2% NAC-102 + 0.15% NAS-725 + 0.5% NFL-549 + 0.2% NFP-703 + 1% NBE-737 + 0.3% NRT-241 (TOC @ 8140')

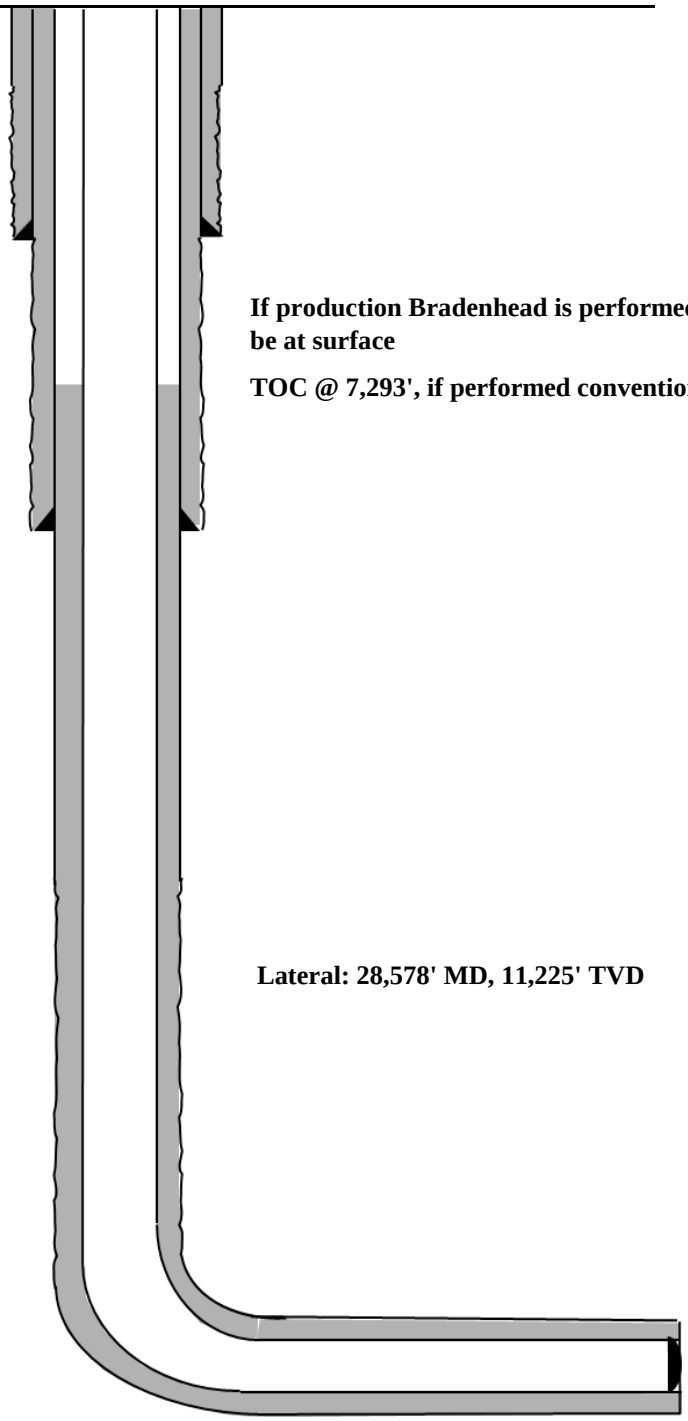
eog resources

Shallow Casing Design E

Proposed Wellbore

KB: 3558'
GL: 3533'

API: 30-025-***



Bit Size: 13''
10-3/4'', 40.5#, J-55, STC
@ 0' - 2,025'

If production Bradenhead is performed, TOC will be at surface

TOC @ 7,293', if performed conventionally.

Bit Size: 9-7/8''
8-5/8'', 32.#, J-55, BTC-SC
@ 0' - 7,793'

Lateral: 28,578' MD, 11,225' TVD

Bit Size: 7-7/8''|Bit Size: 6-3/4''
6'', 24.5#, P110-EC, VAM Sprint-TC
@ 0' - 10,896'

5-1/2'', 20.#, P110-EC, VAM Sprint SF
@ 10,896' - 28,578'

KOP: 12,726' MD, 10,996' TVD
EOC: 12,963' MD, 11,225' TVD

StressCheck - [Triaxial Results - Shallow 3.0 Mile *]

File Edit Wellbore Tubular View Composer Tools Window Help

Burst Design | 8 5/8" Intermediate Casing | Pressure Test

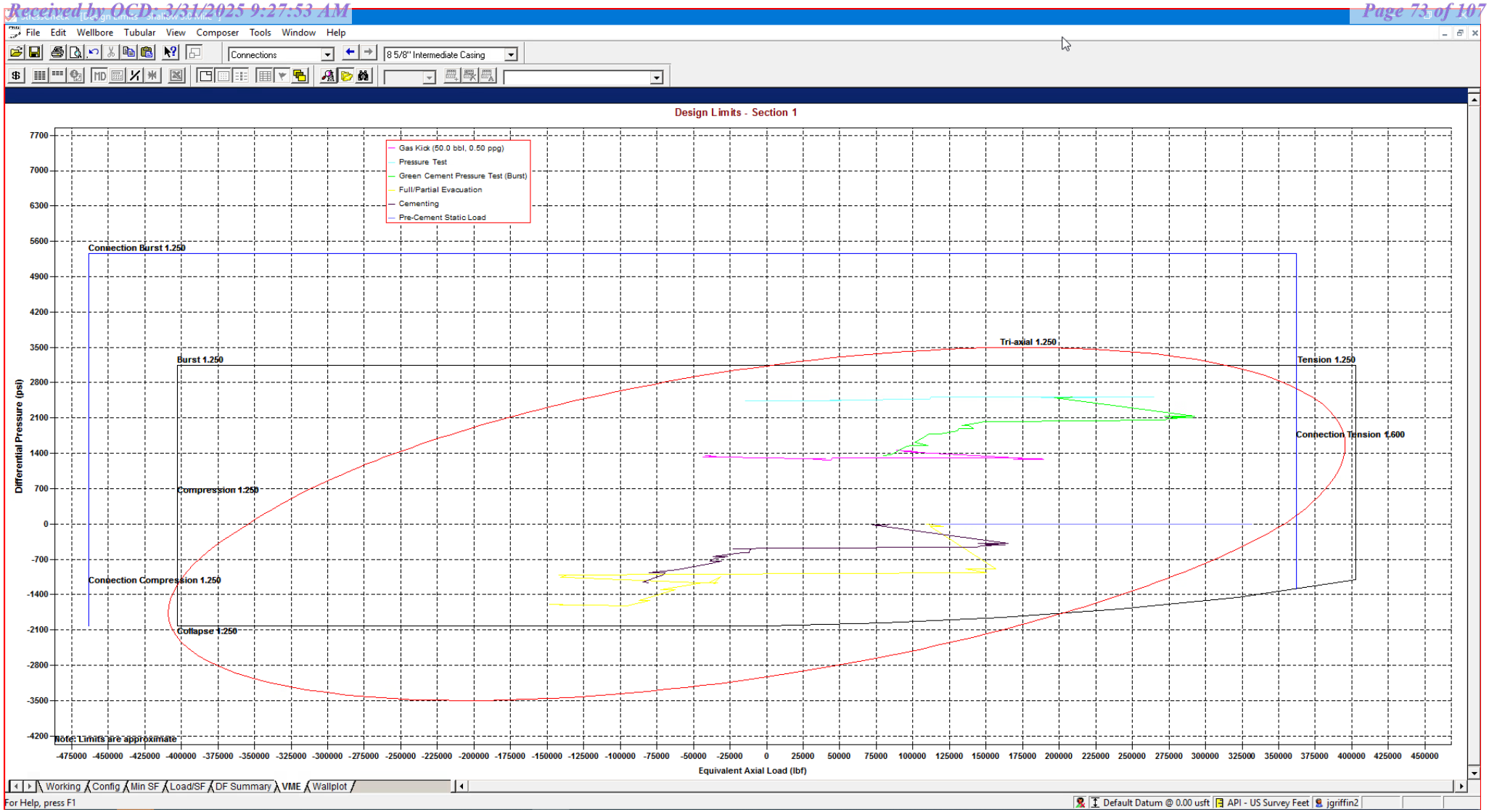
Triaxial Results

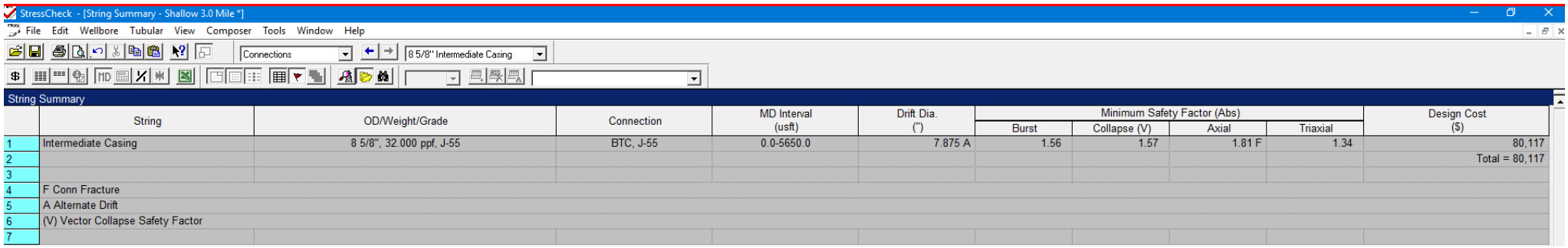
	Depth (MD) (usft)	Axial Force (lbf) Apparent (w/Bending)	Axial Force (lbf) Actual (w/o Bending)	Equivalent Axial Load (lbf)	Bending Stress at OD (psi)	Absolute Safety Factor Triaxial	Absolute Safety Factor Burst	Absolute Safety Factor Collapse (V)	Absolute Safety Factor Axial	Temperature (°F)	Pressure (psi) Internal	Pressure (psi) External	Addt'l Pickup To Prevent Buck. (lbf)	Buckled Length (usft)
1	0	200426	183224	200546	1880.2	1.68	1.57	N/A	2.89 F	70.00	2500.00	0.00	N/A	N/A
2	100	196229	179028	196812	1880.2	1.69	1.57	N/A	2.95 F	71.10	2543.63	43.63		
3	100	187111	179027	187686	883.7	1.70	1.57	N/A	3.10 F	71.10	2543.64	43.64		
4	1700	256401	111891	264835	15795.8	1.56	1.56	N/A	2.26 F	88.70	3241.64	741.64		
5	1700	235940	111891	244247	13559.4	1.60	1.56	N/A	2.45 F	88.70	3241.65	741.65		
6	1850	252413	105788	261533	16027.0	1.54	1.56	N/A	2.29 F	90.29	3305.05	805.05		
7	1850	239292	105787	248323	14592.9	1.56	1.56	N/A	2.42 F	90.29	3305.06	805.06		
8	1950	240267	101966	249748	15117.2	1.54	1.56	N/A	2.41 F	91.30	3344.87	844.87		
9	1950	234781	101965	244223	14517.5	1.56	1.56	N/A	2.47 F	91.30	3344.87	844.87		
10	2050	230871	98395	240694	14480.4	1.55	1.56	N/A	2.51 F	92.23	3381.89	881.89		
11	2050	227794	98394	237594	14144.2	1.55	1.56	N/A	2.54 F	92.23	3381.89	881.89		
12	2300	117966	90294	127818	3024.7	1.70	1.56	N/A	4.91 F	94.35	3466.13	966.13		
13	2300	104686	90293	114432	1573.2	1.71	1.56	N/A	5.53 F	94.35	3466.14	966.14		
14	2370	102469	88077	112431	1573.2	1.71	1.56	N/A	5.65 F	94.94	3489.28	989.28		
15	2370	100817	86424	111200	1573.2	1.75	1.59	N/A	5.75 F	94.94	3489.29	1036.40		
16	2700	83660	75583	95052	882.8	1.74	1.59	N/A	6.92 F	97.73	3599.97	1152.35		
17	2700	88072	75583	99504	1365.1	1.74	1.59	N/A	6.58 F	97.73	3599.97	1152.35		
18	3100	86049	62442	98863	2580.4	1.71	1.59	N/A	6.73 F	101.11	3734.23	1293.00		
19	3100	76477	62441	89195	1534.2	1.72	1.59	N/A	7.57 F	101.11	3734.23	1293.01		
20	3700	55953	42882	70509	1428.8	1.69	1.60	N/A	10.35 F	106.15	3934.24	1502.54		
21	3700	48311	42881	62778	593.5	1.71	1.60	N/A	11.99 F	106.16	3934.25	1502.55		
22	4000	41458	33043	56865	919.9	1.69	1.60	N/A	13.97 F	108.69	4034.82	1607.91		
23	4650	26293	11655	43706	1600.1	1.63	1.60	N/A	22.03 F	114.20	4253.37	1836.86		
24	4900	32619	4156	50970	3111.2	1.59	1.60	N/A	17.76 F	116.32	4337.37	1924.87		
25	4900	21439	4155	39625	1889.2	1.61	1.60	N/A	27.02 F	116.32	4337.38	1924.87		
26	5039	15822	26	34389	1726.6	1.61	1.61	N/A	36.61 F	117.49	4383.77	1973.48		
27	5039	15822	26	34388	1726.6	1.61	1.61	N/A	36.61 F	117.49	4383.78	1973.49		
28	5600	-33912	-16743	-14286	1876.7	1.57	1.61	N/A	(14.60)	122.23	4572.11	2170.78		
29	5650	-30585	-18235	-10742	1350.0	1.58	1.61	N/A	(16.18)	122.66	4588.87	2188.34		
30														
31	F	Conn Fracture												
32	( )	Compression												
33	(V)	Vector Collapse Safety Factor												
34														

Working | Config | Min SF | Load/SF | DF Summary | VME | Wallplot

For Help, press F1 | Default Datum @ 0.00 usft | API - US Survey Feet | jgriffin2

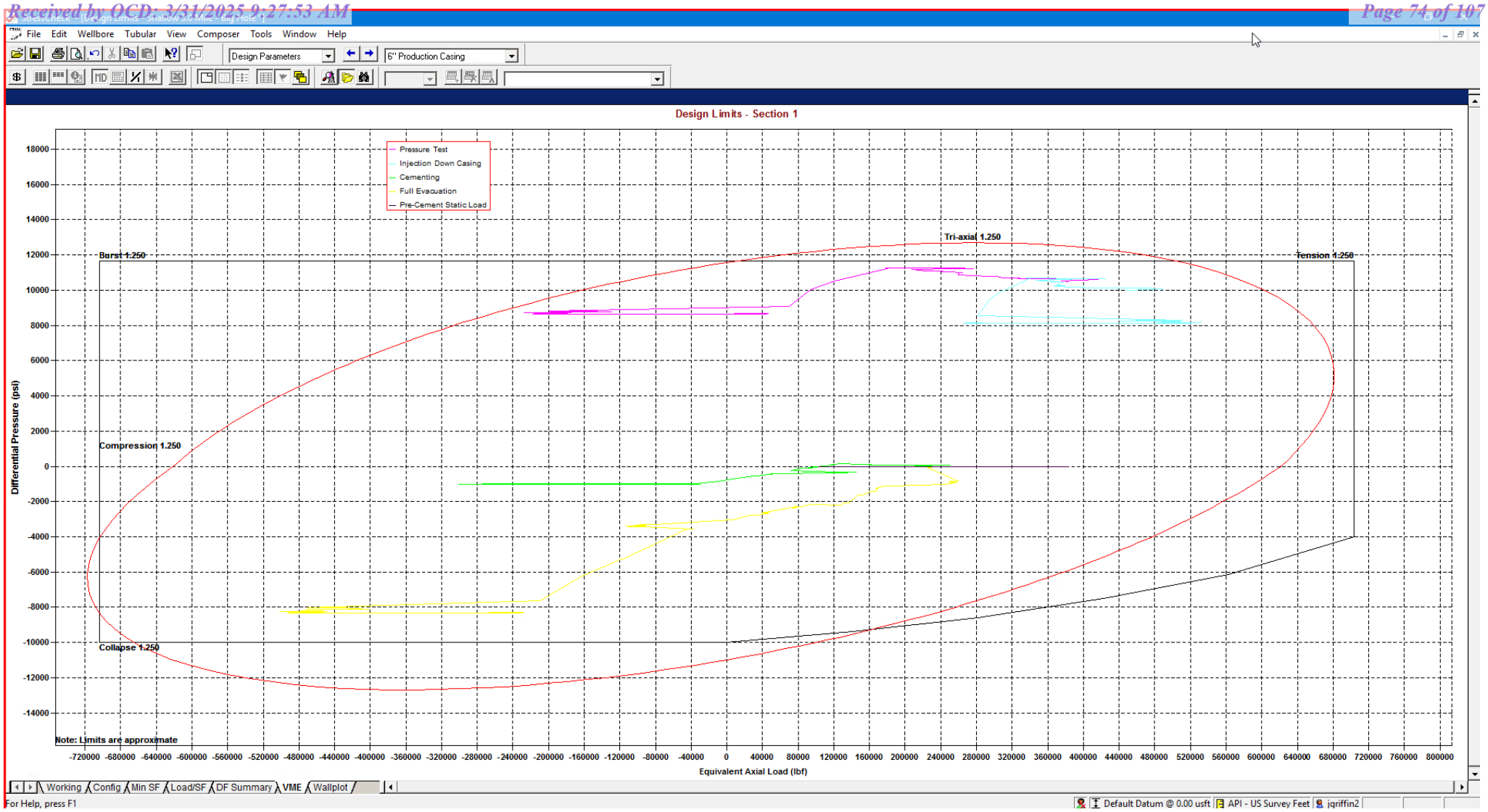
8-5/8" Intermediate Casing Pressure Test:
Internal Profile based off Surface Pressure + Hydrostatic: 4589 psi
External Profile based off Pore Pressure: 2188 psi





	String	OD/Weight/Grade	Connection	MD Interval (usft)	Drift Dia. (")	Minimum Safety Factor (Abs)				Design Cost ($)
						Burst	Collapse (V)	Axial	Triaxial	
1	Intermediate Casing	8 5/8", 32.000 ppf, J-55	BTC, J-55	0.0-5650.0	7.875 A	1.56	1.57	1.81 F	1.34	80,117
2										Total = 80,117
3										
4	F Conn Fracture									
5	A Alternate Drift									
6	(V) Vector Collapse Safety Factor									
7										

*Modelling done with 8-5/8" 32# Intermediate Casing. Passes all Burst, Collapse and Tensile design criteria.

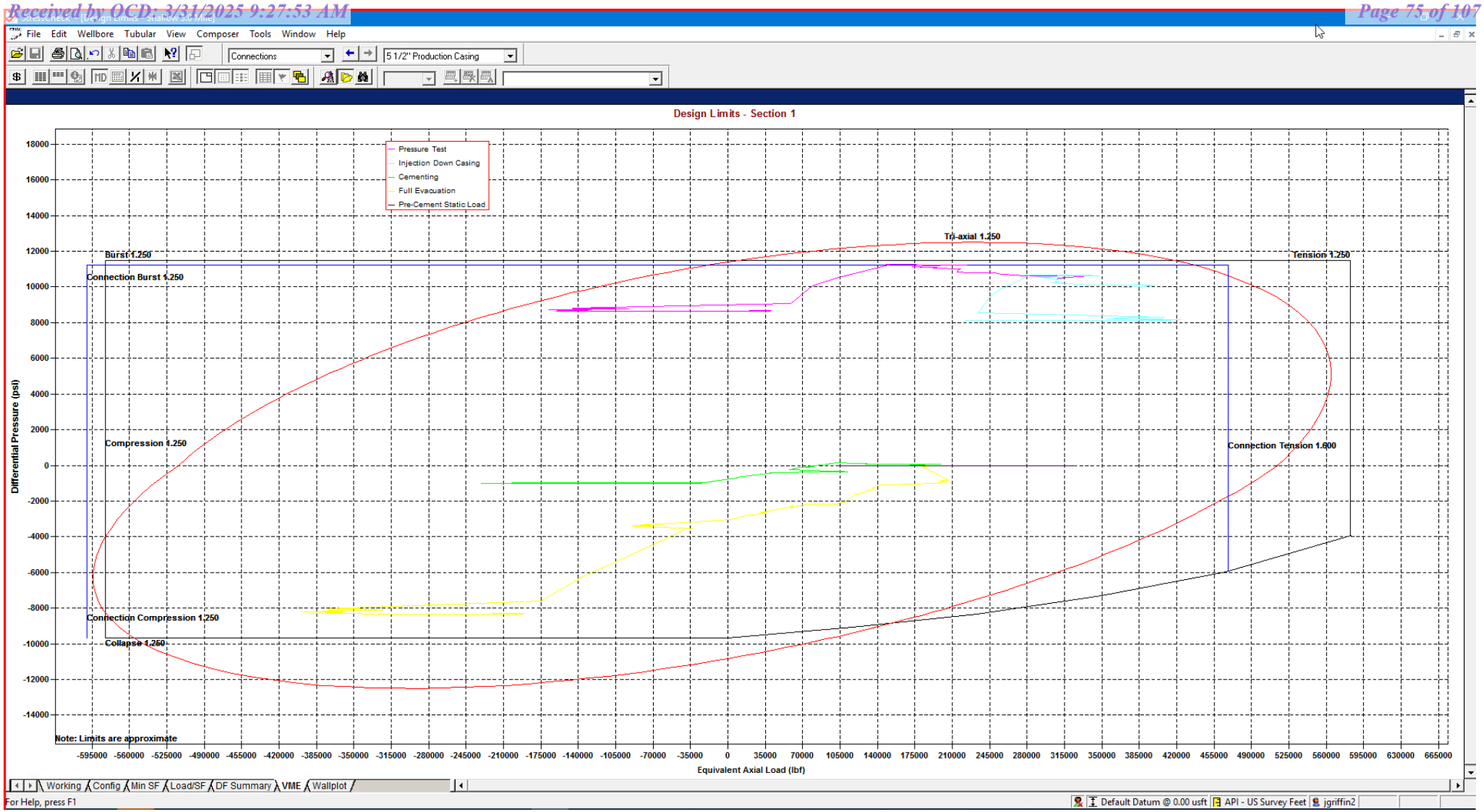


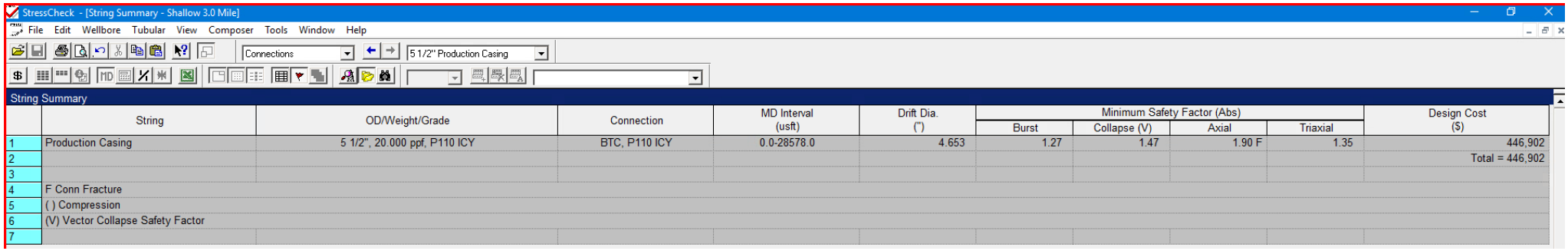
StressCheck - [String Summary - Shallow 3.0 Mile - Big Hole *]

String Summary

	String	OD/Weight/Grade	Connection	MD Interval (usft)	Drift Dia. (")	Minimum Safety Factor (Abs)				Design Cost ($)
						Burst	Collapse (V)	Axial	Triaxial	
1	Production Casing	6", 24.500 ppf, P110 ICY	BTC, P110 ICY	0.0-28578.0	5.075	1.29	1.52	(1.75)	1.37	541,493
2										Total = 541,493
3										
4	( ) Compression									
5	(V) Vector Collapse Safety Factor									
6										

*Modelling done with 6" Production Casing with a 125ksi Control Yield. Passes all Burst, Collapse and Tensile design criteria.





	String	OD/Weight/Grade	Connection	MD Interval (usft)	Drift Dia. (")	Minimum Safety Factor (Abs)				Design Cost ($)
						Burst	Collapse (V)	Axial	Triaxial	
1	Production Casing	5 1/2", 20.000 ppf, P110 ICY	BTC, P110 ICY	0.0-28578.0	4.653	1.27	1.47	1.90 F	1.35	446,902
2										Total = 446,902
3										
4	F Conn Fracture									
5	( ) Compression									
6	(V) Vector Collapse Safety Factor									
7										

*Modelling done with 5-1/2" 20# Production Casing with a 125ksi Control Yield. Passes all Burst, Collapse and Tensile design criteria.

eog resources

Shallow Casing Design 501H

Additive	Purpose
Bentonite Gel	Lightweight/Lost circulation prevention
Calcium Chloride	Accelerator
Cello-flake	Lost circulation prevention
Sodium Metasilicate	Accelerator
MagOx	Expansive agent
Pre-Mag-M	Expansive agent
Sodium Chloride	Accelerator
FL-62	Fluid loss control
Halad-344	Fluid loss control
Halad-9	Fluid loss control
HR-601	Retarder
Microbond	Expansive Agent

Cement integrity tests will be performed immediately following plug bump.

Note: Cement volumes based on bit size plus at least 25% excess in the open hole plus 10% excess in the cased-hole overlap section.

EOG requests variance from minimum standards to pump a two stage cement job on the production casing string with the first stage being pumped conventionally with the calculated top of cement at the top of the Brushy Canyon and the second stage performed as a 1000 sack bradenhead squeeze with planned cement from the Brushy Canyon to surface. If necessary, a top out consisting of 400 sacks of Class C cement + 3% Salt + 1% PreMag-M + 6% Bentonite Gel (1.32 yld, 14.8 ppg) will be executed as a contingency. Top will be verified by Echo-meter.

Bradenhead will be the primary option for production cementing. EOG also requests to have the conventional option in place to accommodate for logistical or wellbore conditions. The tie back requirements will be met if the cement is pumped conventionally, and cement volumes will be adjusted accordingly. TOC will be verified by CBL.

eog resources

MUD PROGRAM:

During this procedure we plan to use a Closed-Loop System and haul contents to the required disposal. The applicable depths and properties of the drilling fluid systems are as follows:

Measured Depth	Type	Weight (ppg)	Viscosity	Water Loss
0 – 2,030'	Fresh - Gel	8.6-8.8	28-34	N/c
2,030' – 7,793'	Brine	9-10.5	28-34	N/c
5,450' – 28,578' Lateral	Oil Base	8.8-9.5	58-68	N/c - 6

An electronic pit volume totalizer (PVT) will be utilized on the circulating system, to monitor pit volume, flow rate, pump pressure and stroke rate.

Sufficient mud materials to maintain mud properties and meet minimum lost circulation and weight increase requirements will be kept at the wellsite at all times.

Appendix A - Spec Sheets

Received by OCD: 3/31/2025 9:27:53 AM

Pipe Body and API Connections Performance Data

13.375 54.50/0.380 J55

PDF

New Search »

« Back to Previous List

USC Metric

6/8/2015 10:04:37 AM

Mechanical Properties	Pipe	BTC	LTC	STC	
Minimum Yield Strength	55,000	--	--	--	psi
Maximum Yield Strength	80,000	--	--	--	psi
Minimum Tensile Strength	75,000	--	--	--	psi
Dimensions	**Pipe**	**BTC**	**LTC**	**STC**	
Outside Diameter	13.375	14.375	--	14.375	in.
Wall Thickness	0.380	--	--	--	in.
Inside Diameter	12.615	12.615	--	12.615	in.
Standard Drift	12.459	12.459	--	12.459	in.
Alternate Drift	--	--	--	--	in.
Nominal Linear Weight, T&C	54.50	--	--	--	lbs/ft
Plain End Weight	52.79	--	--	--	lbs/ft
Performance	**Pipe**	**BTC**	**LTC**	**STC**	
Minimum Collapse Pressure	1,130	1,130	--	1,130	psi
Minimum Internal Yield Pressure	2,740	2,740	--	2,740	psi
Minimum Pipe Body Yield Strength	853.00	--	--	--	1000 lbs
Joint Strength	--	909	--	514	1000 lbs
Reference Length	--	11,125	--	6,290	ft
Make-Up Data	**Pipe**	**BTC**	**LTC**	**STC**	
Make-Up Loss	--	4.81	--	3.50	in.
Minimum Make-Up Torque	--	--	--	3,860	ft-lbs
Maximum Make-Up Torque	--	--	--	6,430	ft-lbs

Released to Imaging: 4/11/2025 8:22:00 AM

Received by OCD: 3/31/2025 9:27:53 AM

Pipe Body and API Connections Performance Data

9.625 40.00/0.395 J55

PDF

New Search »

« Back to Previous List

USC Metric

6/8/2015 10:23:27 AM

Mechanical Properties	Pipe	BTC	LTC	STC	
Minimum Yield Strength	55,000	--	--	--	psi
Maximum Yield Strength	80,000	--	--	--	psi
Minimum Tensile Strength	75,000	--	--	--	psi
Dimensions	**Pipe**	**BTC**	**LTC**	**STC**	
Outside Diameter	9.625	10.625	10.625	10.625	in.
Wall Thickness	0.395	--	--	--	in.
Inside Diameter	8.835	8.835	8.835	8.835	in.
Standard Drift	8.679	8.679	8.679	8.679	in.
Alternate Drift	8.750	8.750	8.750	8.750	in.
Nominal Linear Weight, T&C	40.00	--	--	--	lbs/ft
Plain End Weight	38.97	--	--	--	lbs/ft
Performance	**Pipe**	**BTC**	**LTC**	**STC**	
Minimum Collapse Pressure	2,570	2,570	2,570	2,570	psi
Minimum Internal Yield Pressure	3,950	3,950	3,950	3,950	psi
Minimum Pipe Body Yield Strength	630.00	--	--	--	1000 lbs
Joint Strength	--	714	520	452	1000 lbs
Reference Length	--	11,898	8,665	7,529	ft
Make-Up Data	**Pipe**	**BTC**	**LTC**	**STC**	
Make-Up Loss	--	4.81	4.75	3.38	in.
Minimum Make-Up Torque	--	--	3,900	3,390	ft-lbs
Maximum Make-Up Torque	--	--	6,500	5,650	ft-lbs

Released to Imaging: 4/11/2025 8:22:00 AM

VAM USA

DWC/C-IS MS™

Connection Data Sheet

OD (in.)	WEIGHT (lbs./ft.)	WALL (in.)	GRADE	API DRIFT (in.)	RBW%	CONNECTION
5.500	Nominal: 20.00 Plain End: 19.83	0.361	VST P110EC	4.653	87.5	DWC/C-IS MS

PIPE PROPERTIES		
Outside Diameter	5.500	in.
Inside Diameter	4.778	in.
Nominal Area	5.828	sq.in.
Grade Type	API 5CT	
Min. Yield Strength	125	ksi
Max. Yield Strength	140	ksi
Min. Tensile Strength	135	ksi
Yield Strength	729	klb
Ultimate Strength	787	klb
Min. Internal Yield	14,360	psi
Collapse	12,090	psi

CONNECTION PROPERTIES		
Connection Type	Semi-Premium T&C	
Connection O.D. (nom)	6.115	in.
Connection I.D. (nom)	4.778	in.
Make-Up Loss	4.125	in.
Coupling Length	9.250	in.
Critical Cross Section	5.828	sq.in.
Tension Efficiency	100.0%	of pipe
Compression Efficiency	100.0%	of pipe
Internal Pressure Efficiency	100.0%	of pipe
External Pressure Efficiency	100.0%	of pipe

CONNECTION PERFORMANCES		
Yield Strength	729	klb
Parting Load	787	klb
Compression Rating	729	klb
Min. Internal Yield	14,360	psi
External Pressure	12,090	psi
Maximum Uniaxial Bend Rating	104.2	°/100 ft
Reference String Length w 1.4 Design Factor	26,040	ft

FIELD END TORQUE VALUES		
Min. Make-up torque	16,100	ft.lb
Opti. Make-up torque	17,350	ft.lb
Max. Make-up torque	18,600	ft.lb
Min. Shoulder Torque	1,610	ft.lb
Max. Shoulder Torque	12,880	ft.lb
Min. Delta Turn	-	Turns
Max. Delta Turn	0.200	Turns
Maximum Operational Torque	21,100	ft.lb
Maximum Torsional Value (MTV)	23,210	ft.lb

Need Help? Contact: tech.support@vam-usa.com

Reference Drawing: 8136PP Rev.01 & 8136BP Rev.01

Date: 12/03/2019

Time: 06:19:27 PM

For detailed information on performance properties, refer to DWC Connection Data Notes on following page(s).

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Tech Support Email: tech.support@vam-usa.com

DWC Connection Data Sheet Notes:
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2. All standard DWC/C connections are interchangeable for a given pipe OD. DWC connections are interchangeable with DWC/C-SR connections of the same OD and wall.
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8. The torque values listed are recommended. The actual torque required may be affected by field conditions such as temperature, thread compound, speed of make-up, weather conditions, etc.
9. Connection yield torque is not to be exceeded.
10. Reference string length is calculated by dividing the joint strength by both the nominal weight in air and a design factor (DF) of 1.4. These values are offered for reference only and do not include load factors such as bending, buoyancy, temperature, load dynamics, etc.
11. DWC connections will accommodate API standard drift diameters.
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Received by OCD: 3/31/2025 9:27:53 AM

Pipe Body and API Connections Performance Data

10.750 40.50/0.350 J55

PDF

New Search »

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USC Metric

6/8/2015 10:14:05 AM

Mechanical Properties	Pipe	BTC	LTC	STC	
Minimum Yield Strength	55,000	--	--	--	psi
Maximum Yield Strength	80,000	--	--	--	psi
Minimum Tensile Strength	75,000	--	--	--	psi
Dimensions	**Pipe**	**BTC**	**LTC**	**STC**	
Outside Diameter	10.750	11.750	--	11.750	in.
Wall Thickness	0.350	--	--	--	in.
Inside Diameter	10.050	10.050	--	10.050	in.
Standard Drift	9.894	9.894	--	9.894	in.
Alternate Drift	--	--	--	--	in.
Nominal Linear Weight, T&C	40.50	--	--	--	lbs/ft
Plain End Weight	38.91	--	--	--	lbs/ft
Performance	**Pipe**	**BTC**	**LTC**	**STC**	
Minimum Collapse Pressure	1,580	1,580	--	1,580	psi
Minimum Internal Yield Pressure	3,130	3,130	--	3,130	psi
Minimum Pipe Body Yield Strength	629.00	--	--	--	1000 lbs
Joint Strength	--	700	--	420	1000 lbs
Reference Length	--	11,522	--	6,915	ft
Make-Up Data	**Pipe**	**BTC**	**LTC**	**STC**	
Make-Up Loss	--	4.81	--	3.50	in.
Minimum Make-Up Torque	--	--	--	3,150	ft-lbs
Maximum Make-Up Torque	--	--	--	5,250	ft-lbs

Released to Imaging: 4/11/2025 8:22:00 AM

VALLOUREC STAR 8.625 32# J55 S S2L2 DA 7.875 W/O# SLN # PO# MADE IN USA FT LB

vallourec

API 5CT, 10th Ed. Connection Data Sheet

O.D. (in)	WEIGHT (lb/ft)		WALL (in)	GRADE	*API DRIFT (in)	RBW %
8.625	Nominal:	32.00	0.352	J55	7.796	87.5
	Plain End:	31.13				

Material Properties (PE)

Pipe	
Minimum Yield Strength:	55 ksi
Maximum Yield Strength:	80 ksi
Minimum Tensile Strength:	75 ksi
Coupling	
Minimum Yield Strength:	55 ksi
Maximum Yield Strength:	80 ksi
Minimum Tensile Strength:	75 ksi

Pipe Body Data (PE)

Geometry	
Nominal ID:	7.92 inch
Nominal Area:	9.149 in^2
*Special/Alt. Drift:	7.875 inch
Performance	
Pipe Body Yield Strength:	503 kips
Collapse Resistance:	2,530 psi
Internal Yield Pressure: (API Historical)	3,930 psi

API Connection Data

Coupling OD: 9.625"

STC Performance	
STC Internal Pressure:	3,930 psi
STC Joint Strength:	372 kips
LTC Performance	
LTC Internal Pressure:	3,930 psi
LTC Joint Strength:	417 kips
SC-BTC Performance - Cplg OD = 9.125"	
BTC Internal Pressure:	3,930 psi
BTC Joint Strength:	503 kips

API Connection Torque

STC Torque (ft-lbs)

Min:	2,793	Opti:	3,724	Max:	4,655

LTC Torque (ft-lbs)

Min:	3,130	Opti:	4,174	Max:	5,217

BTC Torque (ft-lbs)

follow API guidelines regarding positional make up

*Alt. Drift will be used unless API Drift is specified on order.

**If above API connections do not suit your needs, VAM® premium connections are available up to 100% of pipe body ratings.

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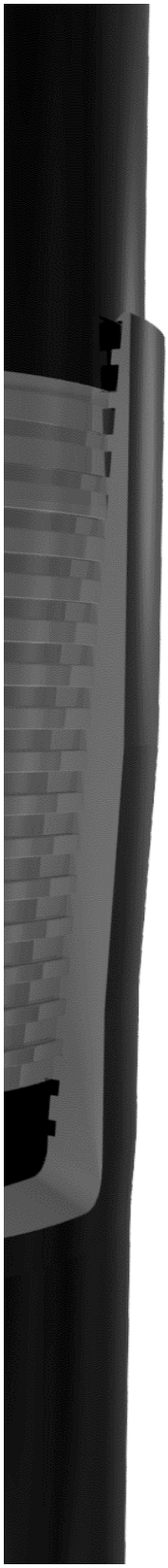


Issued on: 10 Feb. 2021 by Wesley Ott

VAM® SPRINT-SF
Connection Data Sheet

OD	Weight (lb/ft)	Wall Th.	Grade	API Drift:	Connection
6 in.	Nominal: 24.50 Plain End: 23.95	0.400 in.	P110EC	5.075 in.	**VAM® SPRINT-SF**

PIPE PROPERTIES		
Nominal OD	6.000	in.
Nominal ID	5.200	in.
Nominal Cross Section Area	7.037	sqin.
Grade Type		High Yield
Min. Yield Strength	125	ksi
Max. Yield Strength	140	ksi
Min. Ultimate Tensile Strength	135	ksi

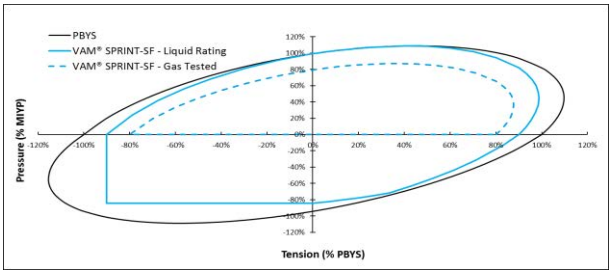
CONNECTION PROPERTIES		
Connection Type		Integral Semi-Flush
Connection OD (nom):	6.277	in.
Connection ID (nom):	5.146	in.
Make-Up Loss	5.386	in.
Critical Cross Section	6.417	sqin.
Tension Efficiency	91.0	% of pipe
Compression Efficiency	91.0	% of pipe
Internal Pressure Efficiency	100	% of pipe
External Pressure Efficiency	100	% of pipe

CONNECTION PERFORMANCES		
Tensile Yield Strength	801	klb
Compression Resistance	801	klb
Internal Yield Pressure	14,580	psi
Collapse Resistance	12,500	psi
Max. Structural Bending	83	°/100ft
Max. Bending with ISO/API Sealability	30	°/100ft

* 87.5% RBW

TORQUE VALUES		
Min. Make-up torque	21,750	ft.lb
Opt. Make-up torque	24,250	ft.lb
Max. Make-up torque	26,750	ft.lb
Max. Torque with Sealability (MTS)	53,000	ft.lb

VAM® SPRINT-SF is a semi-flush connection innovatively designed for extreme shale applications. Its high tension rating and ultra high torque capacity make it ideal to run a fill string length as production casing in shale wells with extended horizontal sections and tight clearance requirements.



Do you need help on this product? - Remember no one knows VAM® like VAM®

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Over 140 VAM® Specialists available worldwide 24/7 for Rig Site Assistance

DWC/C-IS™

Connection Data Sheet

OD (in.)	WEIGHT (lbs./ft.)	WALL (in.)	GRADE	API DRIFT (in.)	RBW%	CONNECTION
6.000	Nominal: 22.30 Plain End: 21.70	0.360	VST P110EC	5.155	92.5	DWC/C-IS

PIPE PROPERTIES

Nominal OD	6.000	in.
Nominal ID	5.280	in.
Nominal Area	6.379	sq.in.
Grade Type	API 5CT	
Min. Yield Strength	125	ksi
Max. Yield Strength	140	ksi
Min. Tensile Strength	135	ksi
Yield Strength	797	klb
Ultimate Strength	861	klb
Min. Internal Yield Pressure	13,880	psi
Collapse Pressure	9,800	psi

CONNECTION PROPERTIES

Connection Type	Semi-Premium T&C	
Connection OD (nom)	6.650	in.
Connection ID (nom)	5.280	in.
Make-Up Loss	4.313	in.
Coupling Length	9.625	in.
Critical Cross Section	6.379	sq.in.
Tension Efficiency	100.0%	of pipe
Compression Efficiency	100.0%	of pipe
Internal Pressure Efficiency	100.0%	of pipe
External Pressure Efficiency	100.0%	of pipe

CONNECTION PERFORMANCES

Yield Strength	797	klb
Parting Load	861	klb
Compression Rating	797	klb
Min. Internal Yield	13,880	psi
External Pressure	9,800	psi
Maximum Uniaxial Bend Rating	47.7	°/100 ft
Reference String Length w 1.4 Design Factor	25,530	ft.

FIELD END TORQUE VALUES

Min. Make-up torque	17,000	ft.lb
Opti. Make-up torque	18,250	ft.lb
Max. Make-up torque	19,500	ft.lb
Min. Shoulder Torque	1,700	ft.lb
Max. Shoulder Torque	13,600	ft.lb
Min. Delta Turn	-	Turns
Max. Delta Turn	0.200	Turns
Maximum Operational Torque	24,200	ft.lb
Maximum Torsional Value (MTV)	26,620	ft.lb

Need Help? Contact: tech.support@vam-usa.com
Reference Drawing: 8135PP Rev.02 & 8135BP Rev.02
Date: 07/30/2020
Time: 07:50:47 PM

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Midland

Lea County, NM (NAD 83 NME)
Lacey Swiss 1 Fed Com
#2H

OH

Plan: Plan #0.2

Standard Planning Report

03 March, 2025

eog resources

Planning Report

Database:	PEDMB	**Local Co-ordinate Reference:**	Well #2H
Company:	Midland	**TVD Reference:**	KB = 26' @ 3485.0usft
Project:	Lea County, NM (NAD 83 NME)	**MD Reference:**	KB = 26' @ 3485.0usft
Site:	Lacey Swiss 1 Fed Com	**North Reference:**	Grid
Well:	#2H	**Survey Calculation Method:**	Minimum Curvature
Wellbore:	OH		
Design:	Plan #0.2		

Project Lea County, NM (NAD 83 NME)

Map System:	US State Plane 1983	**System Datum:**	Mean Sea Level
Geo Datum:	North American Datum 1983		
Map Zone:	New Mexico Eastern Zone		

Site Lacey Swiss 1 Fed Com

Site Position:		**Northing:**	425,128.00 usft	**Latitude:**	32° 9' 58.098 N
From:	Map	**Easting:**	793,117.00 usft	**Longitude:**	103° 31' 10.745 W
Position Uncertainty:	0.0 usft	**Slot Radius:**	13-3/16 "		

Well #2H

Well Position	**+N/-S**	0.0 usft	**Northing:**	424,479.00 usft	**Latitude:**	32° 9' 51.741 N
	+E/-W	0.0 usft	**Easting:**	792,246.00 usft	**Longitude:**	103° 31' 20.935 W
Position Uncertainty		0.0 usft	**Wellhead Elevation:**	usft	**Ground Level:**	3,459.0 usft
Grid Convergence:		0.43 °				

Wellbore OH

Magnetics	**Model Name**	**Sample Date**	**Declination (°)**	**Dip Angle (°)**	**Field Strength (nT)**
	IGRF2025	3/3/2025	6.25	59.72	47,029.25062085

Design Plan #0.2

Audit Notes:

Version:		**Phase:**	PLAN	**Tie On Depth:**	0.0

Vertical Section:	**Depth From (TVD) (usft)**	**+N/-S (usft)**	**+E/-W (usft)**	**Direction (°)**
	0.0	0.0	0.0	187.97

Plan Survey Tool Program **Date** 3/3/2025

	Depth From (usft)	**Depth To (usft)**	**Survey (Wellbore)**	**Tool Name**	**Remarks**
1	0.0	22,266.5	Plan #0.2 (OH)	EOG MWD+IFR1 MWD + IFR1	

eog resources

Planning Report

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Company:	Midland	**TVD Reference:**	KB = 26' @ 3485.0usft
Project:	Lea County, NM (NAD 83 NME)	**MD Reference:**	KB = 26' @ 3485.0usft
Site:	Lacey Swiss 1 Fed Com	**North Reference:**	Grid
Well:	#2H	**Survey Calculation Method:**	Minimum Curvature
Wellbore:	OH		
Design:	Plan #0.2		

Plan Sections

Measured Depth (usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)	TFO (°)	Target
0.0	0.00	0.00	0.0	0.0	0.0	0.00	0.00	0.00	0.00	
1,400.0	0.00	0.00	1,400.0	0.0	0.0	0.00	0.00	0.00	0.00	
2,259.7	17.19	294.57	2,246.8	53.2	-116.4	2.00	2.00	0.00	294.57	
8,089.0	17.19	294.57	7,815.7	769.8	-1,683.6	0.00	0.00	0.00	0.00	
8,948.7	0.00	0.00	8,662.5	823.0	-1,800.0	2.00	-2.00	0.00	180.00	KOP(Lacey Swiss 1 F
9,169.2	26.46	178.85	8,875.2	773.0	-1,799.0	12.00	12.00	81.13	178.85	FTP(Lacey Swiss 1 F
9,698.6	90.00	179.66	9,139.9	345.6	-1,794.6	12.00	12.00	0.15	0.90	
11,807.3	90.00	179.66	9,140.0	-1,763.0	-1,782.0	0.00	0.00	0.00	0.00	Fed Perf #1(Lacey Sv
14,447.3	90.00	179.56	9,140.0	-4,403.0	-1,764.0	0.00	0.00	0.00	-87.36	Fed Perf #2(Lacey Sv
19,725.4	90.00	179.68	9,140.0	-9,681.0	-1,729.0	0.00	0.00	0.00	92.16	Fed Perf #3(Lacey Sv
19,729.7	90.00	179.59	9,140.0	-9,685.3	-1,729.0	2.00	0.05	-2.00	-88.50	
22,266.5	90.00	179.59	9,140.0	-12,222.0	-1,711.0	0.00	0.00	0.00	0.00	PBHL(Lacey Swiss 1

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Planning Report

Database:	PEDMB	**Local Co-ordinate Reference:**	Well #2H
Company:	Midland	**TVD Reference:**	KB = 26' @ 3485.0usft
Project:	Lea County, NM (NAD 83 NME)	**MD Reference:**	KB = 26' @ 3485.0usft
Site:	Lacey Swiss 1 Fed Com	**North Reference:**	Grid
Well:	#2H	**Survey Calculation Method:**	Minimum Curvature
Wellbore:	OH		
Design:	Plan #0.2		

Planned Survey

Measured Depth (usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Vertical Section (usft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)
0.0	0.00	0.00	0.0	0.0	0.0	0.0	0.00	0.00	0.00
100.0	0.00	0.00	100.0	0.0	0.0	0.0	0.00	0.00	0.00
200.0	0.00	0.00	200.0	0.0	0.0	0.0	0.00	0.00	0.00
300.0	0.00	0.00	300.0	0.0	0.0	0.0	0.00	0.00	0.00
400.0	0.00	0.00	400.0	0.0	0.0	0.0	0.00	0.00	0.00
500.0	0.00	0.00	500.0	0.0	0.0	0.0	0.00	0.00	0.00
600.0	0.00	0.00	600.0	0.0	0.0	0.0	0.00	0.00	0.00
700.0	0.00	0.00	700.0	0.0	0.0	0.0	0.00	0.00	0.00
800.0	0.00	0.00	800.0	0.0	0.0	0.0	0.00	0.00	0.00
900.0	0.00	0.00	900.0	0.0	0.0	0.0	0.00	0.00	0.00
1,000.0	0.00	0.00	1,000.0	0.0	0.0	0.0	0.00	0.00	0.00
1,100.0	0.00	0.00	1,100.0	0.0	0.0	0.0	0.00	0.00	0.00
1,200.0	0.00	0.00	1,200.0	0.0	0.0	0.0	0.00	0.00	0.00
1,300.0	0.00	0.00	1,300.0	0.0	0.0	0.0	0.00	0.00	0.00
1,400.0	0.00	0.00	1,400.0	0.0	0.0	0.0	0.00	0.00	0.00
1,500.0	2.00	294.57	1,500.0	0.7	-1.6	-0.5	2.00	2.00	0.00
1,600.0	4.00	294.57	1,599.8	2.9	-6.3	-2.0	2.00	2.00	0.00
1,700.0	6.00	294.57	1,699.5	6.5	-14.3	-4.5	2.00	2.00	0.00
1,800.0	8.00	294.57	1,798.7	11.6	-25.4	-8.0	2.00	2.00	0.00
1,900.0	10.00	294.57	1,897.5	18.1	-39.6	-12.4	2.00	2.00	0.00
2,000.0	12.00	294.57	1,995.6	26.0	-56.9	-17.9	2.00	2.00	0.00
2,100.0	14.00	294.57	2,093.1	35.4	-77.4	-24.3	2.00	2.00	0.00
2,200.0	16.00	294.57	2,189.6	46.1	-100.9	-31.7	2.00	2.00	0.00
2,259.7	17.19	294.57	2,246.8	53.2	-116.4	-36.6	2.00	2.00	0.00
2,300.0	17.19	294.57	2,285.4	58.2	-127.3	-40.0	0.00	0.00	0.00
2,400.0	17.19	294.57	2,380.9	70.5	-154.2	-48.4	0.00	0.00	0.00
2,500.0	17.19	294.57	2,476.4	82.8	-181.0	-56.9	0.00	0.00	0.00
2,600.0	17.19	294.57	2,571.9	95.1	-207.9	-65.3	0.00	0.00	0.00
2,700.0	17.19	294.57	2,667.5	107.4	-234.8	-73.8	0.00	0.00	0.00
2,800.0	17.19	294.57	2,763.0	119.6	-261.7	-82.2	0.00	0.00	0.00
2,900.0	17.19	294.57	2,858.5	131.9	-288.6	-90.7	0.00	0.00	0.00
3,000.0	17.19	294.57	2,954.1	144.2	-315.5	-99.1	0.00	0.00	0.00
3,100.0	17.19	294.57	3,049.6	156.5	-342.3	-107.6	0.00	0.00	0.00
3,200.0	17.19	294.57	3,145.1	168.8	-369.2	-116.0	0.00	0.00	0.00
3,300.0	17.19	294.57	3,240.7	181.1	-396.1	-124.4	0.00	0.00	0.00
3,400.0	17.19	294.57	3,336.2	193.4	-423.0	-132.9	0.00	0.00	0.00
3,500.0	17.19	294.57	3,431.7	205.7	-449.9	-141.3	0.00	0.00	0.00
3,600.0	17.19	294.57	3,527.3	218.0	-476.8	-149.8	0.00	0.00	0.00
3,700.0	17.19	294.57	3,622.8	230.3	-503.6	-158.2	0.00	0.00	0.00
3,800.0	17.19	294.57	3,718.3	242.6	-530.5	-166.7	0.00	0.00	0.00
3,900.0	17.19	294.57	3,813.9	254.9	-557.4	-175.1	0.00	0.00	0.00
4,000.0	17.19	294.57	3,909.4	267.2	-584.3	-183.6	0.00	0.00	0.00
4,100.0	17.19	294.57	4,004.9	279.4	-611.2	-192.0	0.00	0.00	0.00
4,200.0	17.19	294.57	4,100.4	291.7	-638.1	-200.5	0.00	0.00	0.00
4,300.0	17.19	294.57	4,196.0	304.0	-664.9	-208.9	0.00	0.00	0.00
4,400.0	17.19	294.57	4,291.5	316.3	-691.8	-217.3	0.00	0.00	0.00
4,500.0	17.19	294.57	4,387.0	328.6	-718.7	-225.8	0.00	0.00	0.00
4,600.0	17.19	294.57	4,482.6	340.9	-745.6	-234.2	0.00	0.00	0.00
4,700.0	17.19	294.57	4,578.1	353.2	-772.5	-242.7	0.00	0.00	0.00
4,800.0	17.19	294.57	4,673.6	365.5	-799.4	-251.1	0.00	0.00	0.00
4,900.0	17.19	294.57	4,769.2	377.8	-826.2	-259.6	0.00	0.00	0.00
5,000.0	17.19	294.57	4,864.7	390.1	-853.1	-268.0	0.00	0.00	0.00
5,100.0	17.19	294.57	4,960.2	402.4	-880.0	-276.5	0.00	0.00	0.00
5,200.0	17.19	294.57	5,055.8	414.7	-906.9	-284.9	0.00	0.00	0.00

eog resources

Planning Report

Database:	PEDMB	**Local Co-ordinate Reference:**	Well #2H
Company:	Midland	**TVD Reference:**	KB = 26' @ 3485.0usft
Project:	Lea County, NM (NAD 83 NME)	**MD Reference:**	KB = 26' @ 3485.0usft
Site:	Lacey Swiss 1 Fed Com	**North Reference:**	Grid
Well:	#2H	**Survey Calculation Method:**	Minimum Curvature
Wellbore:	OH		
Design:	Plan #0.2		

Planned Survey

Measured Depth (usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Vertical Section (usft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)
5,300.0	17.19	294.57	5,151.3	426.9	-933.8	-293.4	0.00	0.00	0.00
5,400.0	17.19	294.57	5,246.8	439.2	-960.7	-301.8	0.00	0.00	0.00
5,500.0	17.19	294.57	5,342.3	451.5	-987.5	-310.3	0.00	0.00	0.00
5,600.0	17.19	294.57	5,437.9	463.8	-1,014.4	-318.7	0.00	0.00	0.00
5,700.0	17.19	294.57	5,533.4	476.1	-1,041.3	-327.1	0.00	0.00	0.00
5,800.0	17.19	294.57	5,628.9	488.4	-1,068.2	-335.6	0.00	0.00	0.00
5,900.0	17.19	294.57	5,724.5	500.7	-1,095.1	-344.0	0.00	0.00	0.00
6,000.0	17.19	294.57	5,820.0	513.0	-1,122.0	-352.5	0.00	0.00	0.00
6,100.0	17.19	294.57	5,915.5	525.3	-1,148.8	-360.9	0.00	0.00	0.00
6,200.0	17.19	294.57	6,011.1	537.6	-1,175.7	-369.4	0.00	0.00	0.00
6,300.0	17.19	294.57	6,106.6	549.9	-1,202.6	-377.8	0.00	0.00	0.00
6,400.0	17.19	294.57	6,202.1	562.2	-1,229.5	-386.3	0.00	0.00	0.00
6,500.0	17.19	294.57	6,297.7	574.4	-1,256.4	-394.7	0.00	0.00	0.00
6,600.0	17.19	294.57	6,393.2	586.7	-1,283.3	-403.2	0.00	0.00	0.00
6,700.0	17.19	294.57	6,488.7	599.0	-1,310.2	-411.6	0.00	0.00	0.00
6,800.0	17.19	294.57	6,584.3	611.3	-1,337.0	-420.0	0.00	0.00	0.00
6,900.0	17.19	294.57	6,679.8	623.6	-1,363.9	-428.5	0.00	0.00	0.00
7,000.0	17.19	294.57	6,775.3	635.9	-1,390.8	-436.9	0.00	0.00	0.00
7,100.0	17.19	294.57	6,870.8	648.2	-1,417.7	-445.4	0.00	0.00	0.00
7,200.0	17.19	294.57	6,966.4	660.5	-1,444.6	-453.8	0.00	0.00	0.00
7,300.0	17.19	294.57	7,061.9	672.8	-1,471.5	-462.3	0.00	0.00	0.00
7,400.0	17.19	294.57	7,157.4	685.1	-1,498.3	-470.7	0.00	0.00	0.00
7,500.0	17.19	294.57	7,253.0	697.4	-1,525.2	-479.2	0.00	0.00	0.00
7,600.0	17.19	294.57	7,348.5	709.7	-1,552.1	-487.6	0.00	0.00	0.00
7,700.0	17.19	294.57	7,444.0	721.9	-1,579.0	-496.1	0.00	0.00	0.00
7,800.0	17.19	294.57	7,539.6	734.2	-1,605.9	-504.5	0.00	0.00	0.00
7,900.0	17.19	294.57	7,635.1	746.5	-1,632.8	-513.0	0.00	0.00	0.00
8,000.0	17.19	294.57	7,730.6	758.8	-1,659.6	-521.4	0.00	0.00	0.00
8,089.0	17.19	294.57	7,815.7	769.8	-1,683.6	-528.9	0.00	0.00	0.00
8,100.0	16.97	294.57	7,826.2	771.1	-1,686.5	-529.8	2.00	-2.00	0.00
8,200.0	14.97	294.57	7,922.3	782.5	-1,711.5	-537.7	2.00	-2.00	0.00
8,300.0	12.97	294.57	8,019.3	792.6	-1,733.5	-544.6	2.00	-2.00	0.00
8,400.0	10.97	294.57	8,117.1	801.2	-1,752.4	-550.5	2.00	-2.00	0.00
8,500.0	8.97	294.57	8,215.6	808.4	-1,768.1	-555.5	2.00	-2.00	0.00
8,600.0	6.97	294.57	8,314.7	814.2	-1,780.7	-559.4	2.00	-2.00	0.00
8,700.0	4.97	294.57	8,414.1	818.5	-1,790.2	-562.4	2.00	-2.00	0.00
8,800.0	2.97	294.57	8,513.9	821.4	-1,796.5	-564.4	2.00	-2.00	0.00
8,900.0	0.97	294.57	8,613.8	822.8	-1,799.6	-565.4	2.00	-2.00	0.00
8,948.7	0.00	0.00	8,662.5	823.0	-1,800.0	-565.5	2.00	-2.00	0.00
8,950.0	0.16	178.85	8,663.8	823.0	-1,800.0	-565.5	12.00	12.00	0.00
8,975.0	3.16	178.85	8,688.8	822.3	-1,800.0	-564.8	12.00	12.00	0.00
9,000.0	6.16	178.85	8,713.7	820.2	-1,799.9	-562.8	12.00	12.00	0.00
9,025.0	9.16	178.85	8,738.5	816.9	-1,799.9	-559.5	12.00	12.00	0.00
9,050.0	12.16	178.85	8,763.0	812.3	-1,799.8	-554.9	12.00	12.00	0.00
9,075.0	15.16	178.85	8,787.3	806.4	-1,799.7	-549.1	12.00	12.00	0.00
9,100.0	18.16	178.85	8,811.3	799.2	-1,799.5	-542.0	12.00	12.00	0.00
9,125.0	21.16	178.85	8,834.8	790.8	-1,799.4	-533.7	12.00	12.00	0.00
9,150.0	24.16	178.85	8,857.9	781.2	-1,799.2	-524.2	12.00	12.00	0.00
9,169.2	26.46	178.85	8,875.2	773.0	-1,799.0	-516.1	12.00	12.00	0.00
9,175.0	27.16	178.88	8,880.4	770.4	-1,798.9	-513.5	12.00	12.00	0.41
9,200.0	30.16	178.97	8,902.4	758.4	-1,798.7	-501.7	12.00	12.00	0.36
9,225.0	33.16	179.05	8,923.6	745.3	-1,798.5	-488.7	12.00	12.00	0.30
9,250.0	36.16	179.11	8,944.2	731.0	-1,798.3	-474.7	12.00	12.00	0.26
9,275.0	39.16	179.17	8,964.0	715.8	-1,798.0	-459.6	12.00	12.00	0.22

eog resources

Planning Report

Database:	PEDMB	**Local Co-ordinate Reference:**	Well #2H
Company:	Midland	**TVD Reference:**	KB = 26' @ 3485.0usft
Project:	Lea County, NM (NAD 83 NME)	**MD Reference:**	KB = 26' @ 3485.0usft
Site:	Lacey Swiss 1 Fed Com	**North Reference:**	Grid
Well:	#2H	**Survey Calculation Method:**	Minimum Curvature
Wellbore:	OH		
Design:	Plan #0.2		

Planned Survey

Measured Depth (usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Vertical Section (usft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)
9,300.0	42.16	179.22	8,982.9	699.5	-1,797.8	-443.5	12.00	12.00	0.20
9,325.0	45.16	179.26	9,001.0	682.2	-1,797.6	-426.4	12.00	12.00	0.18
9,350.0	48.16	179.30	9,018.2	664.0	-1,797.4	-408.4	12.00	12.00	0.16
9,375.0	51.16	179.34	9,034.4	645.0	-1,797.1	-389.6	12.00	12.00	0.14
9,400.0	54.16	179.37	9,049.5	625.1	-1,796.9	-370.0	12.00	12.00	0.13
9,425.0	57.16	179.40	9,063.6	604.5	-1,796.7	-349.5	12.00	12.00	0.12
9,450.0	60.16	179.43	9,076.6	583.1	-1,796.5	-328.4	12.00	12.00	0.11
9,475.0	63.16	179.46	9,088.5	561.1	-1,796.2	-306.7	12.00	12.00	0.11
9,500.0	66.16	179.48	9,099.2	538.5	-1,796.0	-284.3	12.00	12.00	0.10
9,525.0	69.16	179.51	9,108.7	515.4	-1,795.8	-261.5	12.00	12.00	0.10
9,550.0	72.16	179.53	9,117.0	491.8	-1,795.6	-238.1	12.00	12.00	0.09
9,575.0	75.16	179.55	9,124.0	467.8	-1,795.4	-214.4	12.00	12.00	0.09
9,600.0	78.16	179.57	9,129.8	443.5	-1,795.3	-190.3	12.00	12.00	0.09
9,625.0	81.16	179.60	9,134.2	418.9	-1,795.1	-166.0	12.00	12.00	0.09
9,650.0	84.16	179.62	9,137.4	394.1	-1,794.9	-141.5	12.00	12.00	0.09
9,675.0	87.16	179.64	9,139.3	369.2	-1,794.7	-116.8	12.00	12.00	0.08
9,698.6	90.00	179.66	9,139.9	345.6	-1,794.6	-93.4	12.00	12.00	0.08
9,700.0	90.00	179.66	9,139.9	344.2	-1,794.6	-92.1	0.00	0.00	0.00
9,800.0	90.00	179.66	9,139.9	244.2	-1,794.0	6.9	0.00	0.00	0.00
9,900.0	90.00	179.66	9,139.9	144.2	-1,793.4	105.8	0.00	0.00	0.00
10,000.0	90.00	179.66	9,139.9	44.2	-1,792.8	204.8	0.00	0.00	0.00
10,100.0	90.00	179.66	9,139.9	-55.8	-1,792.2	303.7	0.00	0.00	0.00
10,200.0	90.00	179.66	9,139.9	-155.8	-1,791.6	402.7	0.00	0.00	0.00
10,300.0	90.00	179.66	9,139.9	-255.8	-1,791.0	501.6	0.00	0.00	0.00
10,400.0	90.00	179.66	9,139.9	-355.8	-1,790.4	600.5	0.00	0.00	0.00
10,500.0	90.00	179.66	9,139.9	-455.8	-1,789.8	699.5	0.00	0.00	0.00
10,600.0	90.00	179.66	9,140.0	-555.8	-1,789.2	798.4	0.00	0.00	0.00
10,700.0	90.00	179.66	9,140.0	-655.8	-1,788.6	897.4	0.00	0.00	0.00
10,800.0	90.00	179.66	9,140.0	-755.8	-1,788.0	996.3	0.00	0.00	0.00
10,900.0	90.00	179.66	9,140.0	-855.8	-1,787.4	1,095.3	0.00	0.00	0.00
11,000.0	90.00	179.66	9,140.0	-955.7	-1,786.8	1,194.2	0.00	0.00	0.00
11,100.0	90.00	179.66	9,140.0	-1,055.7	-1,786.2	1,293.2	0.00	0.00	0.00
11,200.0	90.00	179.66	9,140.0	-1,155.7	-1,785.6	1,392.1	0.00	0.00	0.00
11,300.0	90.00	179.66	9,140.0	-1,255.7	-1,785.0	1,491.1	0.00	0.00	0.00
11,400.0	90.00	179.66	9,140.0	-1,355.7	-1,784.4	1,590.0	0.00	0.00	0.00
11,500.0	90.00	179.66	9,140.0	-1,455.7	-1,783.8	1,689.0	0.00	0.00	0.00
11,600.0	90.00	179.66	9,140.0	-1,555.7	-1,783.2	1,787.9	0.00	0.00	0.00
11,700.0	90.00	179.66	9,140.0	-1,655.7	-1,782.6	1,886.9	0.00	0.00	0.00
11,807.3	90.00	179.66	9,140.0	-1,763.0	-1,782.0	1,993.0	0.00	0.00	0.00
11,900.0	90.00	179.65	9,140.0	-1,855.7	-1,781.4	2,084.8	0.00	0.00	0.00
12,000.0	90.00	179.65	9,140.0	-1,955.7	-1,780.8	2,183.7	0.00	0.00	0.00
12,100.0	90.00	179.65	9,140.0	-2,055.7	-1,780.2	2,282.7	0.00	0.00	0.00
12,200.0	90.00	179.64	9,140.0	-2,155.7	-1,779.6	2,381.6	0.00	0.00	0.00
12,300.0	90.00	179.64	9,140.0	-2,255.7	-1,779.0	2,480.6	0.00	0.00	0.00
12,400.0	90.00	179.64	9,140.0	-2,355.7	-1,778.3	2,579.5	0.00	0.00	0.00
12,500.0	90.00	179.63	9,140.0	-2,455.7	-1,777.7	2,678.5	0.00	0.00	0.00
12,600.0	90.00	179.63	9,140.0	-2,555.7	-1,777.1	2,777.4	0.00	0.00	0.00
12,700.0	90.00	179.62	9,140.0	-2,655.7	-1,776.4	2,876.4	0.00	0.00	0.00
12,800.0	90.00	179.62	9,140.0	-2,755.7	-1,775.8	2,975.3	0.00	0.00	0.00
12,900.0	90.00	179.62	9,140.0	-2,855.7	-1,775.1	3,074.2	0.00	0.00	0.00
13,000.0	90.00	179.61	9,140.0	-2,955.7	-1,774.4	3,173.2	0.00	0.00	0.00
13,100.0	90.00	179.61	9,140.0	-3,055.7	-1,773.7	3,272.1	0.00	0.00	0.00
13,200.0	90.00	179.61	9,140.0	-3,155.7	-1,773.1	3,371.1	0.00	0.00	0.00
13,300.0	90.00	179.60	9,140.0	-3,255.7	-1,772.4	3,470.0	0.00	0.00	0.00

eog resources

Planning Report

Database:	PEDMB	**Local Co-ordinate Reference:**	Well #2H
Company:	Midland	**TVD Reference:**	KB = 26' @ 3485.0usft
Project:	Lea County, NM (NAD 83 NME)	**MD Reference:**	KB = 26' @ 3485.0usft
Site:	Lacey Swiss 1 Fed Com	**North Reference:**	Grid
Well:	#2H	**Survey Calculation Method:**	Minimum Curvature
Wellbore:	OH		
Design:	Plan #0.2		

Planned Survey

Measured Depth (usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Vertical Section (usft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)
13,400.0	90.00	179.60	9,140.0	-3,355.7	-1,771.7	3,568.9	0.00	0.00	0.00
13,500.0	90.00	179.60	9,140.0	-3,455.7	-1,771.0	3,667.9	0.00	0.00	0.00
13,600.0	90.00	179.59	9,140.0	-3,555.7	-1,770.3	3,766.8	0.00	0.00	0.00
13,700.0	90.00	179.59	9,140.0	-3,655.7	-1,769.5	3,865.7	0.00	0.00	0.00
13,800.0	90.00	179.58	9,140.0	-3,755.7	-1,768.8	3,964.7	0.00	0.00	0.00
13,900.0	90.00	179.58	9,140.0	-3,855.7	-1,768.1	4,063.6	0.00	0.00	0.00
14,000.0	90.00	179.58	9,140.0	-3,955.7	-1,767.4	4,162.5	0.00	0.00	0.00
14,100.0	90.00	179.57	9,140.0	-4,055.7	-1,766.6	4,261.4	0.00	0.00	0.00
14,200.0	90.00	179.57	9,140.0	-4,155.7	-1,765.9	4,360.4	0.00	0.00	0.00
14,300.0	90.00	179.57	9,140.0	-4,255.7	-1,765.1	4,459.3	0.00	0.00	0.00
14,400.0	90.00	179.56	9,140.0	-4,355.7	-1,764.4	4,558.2	0.00	0.00	0.00
14,447.3	90.00	179.56	9,140.0	-4,403.0	-1,764.0	4,605.0	0.00	0.00	0.00
14,500.0	90.00	179.56	9,140.0	-4,455.7	-1,763.6	4,657.1	0.00	0.00	0.00
14,600.0	90.00	179.56	9,140.0	-4,555.7	-1,762.8	4,756.1	0.00	0.00	0.00
14,700.0	90.00	179.57	9,140.0	-4,655.7	-1,762.1	4,855.0	0.00	0.00	0.00
14,800.0	90.00	179.57	9,140.0	-4,755.7	-1,761.3	4,953.9	0.00	0.00	0.00
14,900.0	90.00	179.57	9,140.0	-4,855.7	-1,760.6	5,052.9	0.00	0.00	0.00
15,000.0	90.00	179.57	9,140.0	-4,955.7	-1,759.8	5,151.8	0.00	0.00	0.00
15,100.0	90.00	179.58	9,140.0	-5,055.7	-1,759.1	5,250.7	0.00	0.00	0.00
15,200.0	90.00	179.58	9,140.0	-5,155.7	-1,758.3	5,349.6	0.00	0.00	0.00
15,300.0	90.00	179.58	9,140.0	-5,255.6	-1,757.6	5,448.6	0.00	0.00	0.00
15,400.0	90.00	179.58	9,140.0	-5,355.6	-1,756.9	5,547.5	0.00	0.00	0.00
15,500.0	90.00	179.58	9,140.0	-5,455.6	-1,756.2	5,646.4	0.00	0.00	0.00
15,600.0	90.00	179.59	9,140.0	-5,555.6	-1,755.4	5,745.4	0.00	0.00	0.00
15,700.0	90.00	179.59	9,140.0	-5,655.6	-1,754.7	5,844.3	0.00	0.00	0.00
15,800.0	90.00	179.59	9,140.0	-5,755.6	-1,754.0	5,943.2	0.00	0.00	0.00
15,900.0	90.00	179.59	9,140.0	-5,855.6	-1,753.3	6,042.2	0.00	0.00	0.00
16,000.0	90.00	179.60	9,140.0	-5,955.6	-1,752.6	6,141.1	0.00	0.00	0.00
16,100.0	90.00	179.60	9,140.0	-6,055.6	-1,751.9	6,240.0	0.00	0.00	0.00
16,200.0	90.00	179.60	9,140.0	-6,155.6	-1,751.2	6,339.0	0.00	0.00	0.00
16,300.0	90.00	179.60	9,140.0	-6,255.6	-1,750.5	6,437.9	0.00	0.00	0.00
16,400.0	90.00	179.60	9,140.0	-6,355.6	-1,749.8	6,536.8	0.00	0.00	0.00
16,500.0	90.00	179.61	9,140.0	-6,455.6	-1,749.1	6,635.8	0.00	0.00	0.00
16,600.0	90.00	179.61	9,140.0	-6,555.6	-1,748.4	6,734.7	0.00	0.00	0.00
16,700.0	90.00	179.61	9,139.9	-6,655.6	-1,747.7	6,833.6	0.00	0.00	0.00
16,800.0	90.00	179.61	9,139.9	-6,755.6	-1,747.1	6,932.6	0.00	0.00	0.00
16,900.0	90.00	179.62	9,139.9	-6,855.6	-1,746.4	7,031.5	0.00	0.00	0.00
17,000.0	90.00	179.62	9,139.9	-6,955.6	-1,745.7	7,130.5	0.00	0.00	0.00
17,100.0	90.00	179.62	9,139.9	-7,055.6	-1,745.1	7,229.4	0.00	0.00	0.00
17,200.0	90.00	179.62	9,139.9	-7,155.6	-1,744.4	7,328.3	0.00	0.00	0.00
17,300.0	90.00	179.62	9,139.9	-7,255.6	-1,743.7	7,427.3	0.00	0.00	0.00
17,400.0	90.00	179.63	9,139.9	-7,355.6	-1,743.1	7,526.2	0.00	0.00	0.00
17,500.0	90.00	179.63	9,139.9	-7,455.6	-1,742.4	7,625.2	0.00	0.00	0.00
17,600.0	90.00	179.63	9,140.0	-7,555.6	-1,741.8	7,724.1	0.00	0.00	0.00
17,700.0	90.00	179.63	9,140.0	-7,655.6	-1,741.1	7,823.1	0.00	0.00	0.00
17,800.0	90.00	179.64	9,140.0	-7,755.6	-1,740.5	7,922.0	0.00	0.00	0.00
17,900.0	90.00	179.64	9,140.0	-7,855.6	-1,739.9	8,020.9	0.00	0.00	0.00
18,000.0	90.00	179.64	9,140.0	-7,955.6	-1,739.2	8,119.9	0.00	0.00	0.00
18,100.0	90.00	179.64	9,140.0	-8,055.6	-1,738.6	8,218.8	0.00	0.00	0.00
18,200.0	90.00	179.64	9,140.0	-8,155.6	-1,738.0	8,317.8	0.00	0.00	0.00
18,300.0	90.00	179.65	9,140.0	-8,255.6	-1,737.4	8,416.7	0.00	0.00	0.00
18,400.0	90.00	179.65	9,140.0	-8,355.6	-1,736.8	8,515.7	0.00	0.00	0.00
18,500.0	90.00	179.65	9,140.0	-8,455.6	-1,736.2	8,614.6	0.00	0.00	0.00
18,600.0	90.00	179.65	9,140.0	-8,555.6	-1,735.6	8,713.6	0.00	0.00	0.00

eog resources

Planning Report

Database:	PEDMB	**Local Co-ordinate Reference:**	Well #2H
Company:	Midland	**TVD Reference:**	KB = 26' @ 3485.0usft
Project:	Lea County, NM (NAD 83 NME)	**MD Reference:**	KB = 26' @ 3485.0usft
Site:	Lacey Swiss 1 Fed Com	**North Reference:**	Grid
Well:	#2H	**Survey Calculation Method:**	Minimum Curvature
Wellbore:	OH		
Design:	Plan #0.2		

Planned Survey

Measured Depth (usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Vertical Section (usft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)
18,700.0	90.00	179.66	9,140.0	-8,655.6	-1,734.9	8,812.5	0.00	0.00	0.00
18,800.0	90.00	179.66	9,140.0	-8,755.6	-1,734.4	8,911.5	0.00	0.00	0.00
18,900.0	90.00	179.66	9,140.0	-8,855.6	-1,733.8	9,010.4	0.00	0.00	0.00
19,000.0	90.00	179.66	9,140.0	-8,955.6	-1,733.2	9,109.4	0.00	0.00	0.00
19,100.0	90.00	179.67	9,140.0	-9,055.6	-1,732.6	9,208.3	0.00	0.00	0.00
19,200.0	90.00	179.67	9,140.0	-9,155.6	-1,732.0	9,307.3	0.00	0.00	0.00
19,300.0	90.00	179.67	9,140.0	-9,255.6	-1,731.4	9,406.2	0.00	0.00	0.00
19,400.0	90.00	179.67	9,140.0	-9,355.6	-1,730.8	9,505.2	0.00	0.00	0.00
19,500.0	90.00	179.67	9,140.0	-9,455.6	-1,730.3	9,604.1	0.00	0.00	0.00
19,600.0	90.00	179.68	9,140.0	-9,555.6	-1,729.7	9,703.1	0.00	0.00	0.00
19,700.0	90.00	179.68	9,140.0	-9,655.6	-1,729.1	9,802.0	0.00	0.00	0.00
19,725.4	90.00	179.68	9,140.0	-9,681.0	-1,729.0	9,827.2	0.00	0.00	0.00
19,729.7	90.00	179.59	9,140.0	-9,685.3	-1,729.0	9,831.4	2.00	0.05	-2.00
19,800.0	90.00	179.59	9,140.0	-9,755.6	-1,728.5	9,901.0	0.00	0.00	0.00
19,900.0	90.00	179.59	9,140.0	-9,855.6	-1,727.8	9,999.9	0.00	0.00	0.00
20,000.0	90.00	179.59	9,140.0	-9,955.5	-1,727.1	10,098.8	0.00	0.00	0.00
20,100.0	90.00	179.59	9,140.0	-10,055.5	-1,726.3	10,197.8	0.00	0.00	0.00
20,200.0	90.00	179.59	9,140.0	-10,155.5	-1,725.6	10,296.7	0.00	0.00	0.00
20,300.0	90.00	179.59	9,140.0	-10,255.5	-1,724.9	10,395.6	0.00	0.00	0.00
20,400.0	90.00	179.59	9,140.0	-10,355.5	-1,724.2	10,494.6	0.00	0.00	0.00
20,500.0	90.00	179.59	9,140.0	-10,455.5	-1,723.5	10,593.5	0.00	0.00	0.00
20,600.0	90.00	179.59	9,140.0	-10,555.5	-1,722.8	10,692.4	0.00	0.00	0.00
20,700.0	90.00	179.59	9,140.0	-10,655.5	-1,722.1	10,791.4	0.00	0.00	0.00
20,800.0	90.00	179.59	9,140.0	-10,755.5	-1,721.4	10,890.3	0.00	0.00	0.00
20,900.0	90.00	179.59	9,140.0	-10,855.5	-1,720.7	10,989.2	0.00	0.00	0.00
21,000.0	90.00	179.59	9,140.0	-10,955.5	-1,720.0	11,088.2	0.00	0.00	0.00
21,100.0	90.00	179.59	9,140.0	-11,055.5	-1,719.3	11,187.1	0.00	0.00	0.00
21,200.0	90.00	179.59	9,140.0	-11,155.5	-1,718.6	11,286.0	0.00	0.00	0.00
21,300.0	90.00	179.59	9,140.0	-11,255.5	-1,717.8	11,385.0	0.00	0.00	0.00
21,400.0	90.00	179.59	9,140.0	-11,355.5	-1,717.1	11,483.9	0.00	0.00	0.00
21,500.0	90.00	179.59	9,140.0	-11,455.5	-1,716.4	11,582.9	0.00	0.00	0.00
21,600.0	90.00	179.59	9,140.0	-11,555.5	-1,715.7	11,681.8	0.00	0.00	0.00
21,700.0	90.00	179.59	9,140.0	-11,655.5	-1,715.0	11,780.7	0.00	0.00	0.00
21,800.0	90.00	179.59	9,140.0	-11,755.5	-1,714.3	11,879.7	0.00	0.00	0.00
21,900.0	90.00	179.59	9,140.0	-11,855.5	-1,713.6	11,978.6	0.00	0.00	0.00
22,000.0	90.00	179.59	9,140.0	-11,955.5	-1,712.9	12,077.5	0.00	0.00	0.00
22,100.0	90.00	179.59	9,140.0	-12,055.5	-1,712.2	12,176.5	0.00	0.00	0.00
22,200.0	90.00	179.59	9,140.0	-12,155.5	-1,711.5	12,275.4	0.00	0.00	0.00
22,266.5	90.00	179.59	9,140.0	-12,222.0	-1,711.0	12,341.2	0.00	0.00	0.00

eog resources

Planning Report

Database:	PEDMB	**Local Co-ordinate Reference:**	Well #2H
Company:	Midland	**TVD Reference:**	KB = 26' @ 3485.0usft
Project:	Lea County, NM (NAD 83 NME)	**MD Reference:**	KB = 26' @ 3485.0usft
Site:	Lacey Swiss 1 Fed Com	**North Reference:**	Grid
Well:	#2H	**Survey Calculation Method:**	Minimum Curvature
Wellbore:	OH		
Design:	Plan #0.2		

Design Targets

Target Name - hit/miss target - Shape	Dip Angle (°)	Dip Dir. (°)	TVD (usft)	+N/-S (usft)	+E/-W (usft)	Northing (usft)	Easting (usft)	Latitude	Longitude
KOP(Lacey Swiss 1 Fed - plan hits target center - Point	0.00	0.00	8,662.5	823.0	-1,800.0	425,302.00	790,446.00	32° 10' 0.019 N	103° 31' 41.802 W
FTP(Lacey Swiss 1 Fed - plan hits target center - Point	0.00	0.00	8,875.2	773.0	-1,799.0	425,252.00	790,447.00	32° 9' 59.524 N	103° 31' 41.795 W
Fed Perf #2(Lacey Swis - plan hits target center - Point	0.00	0.00	9,140.0	-4,403.0	-1,764.0	420,076.00	790,482.00	32° 9' 8.304 N	103° 31' 41.838 W
PBHL(Lacey Swiss 1 Fe - plan hits target center - Point	0.00	0.00	9,140.0	-12,222.0	-1,711.0	412,257.00	790,535.00	32° 7' 50.929 N	103° 31' 41.902 W
Fed Perf #3(Lacey Swis - plan hits target center - Point	0.00	0.00	9,140.0	-9,681.0	-1,729.0	414,798.00	790,517.00	32° 8' 16.074 N	103° 31' 41.890 W
Fed Perf #1(Lacey Swis - plan hits target center - Point	0.00	0.00	9,140.0	-1,763.0	-1,782.0	422,716.00	790,464.00	32° 9' 34.429 N	103° 31' 41.818 W

Received by OCD: 3/31/2025 9:27:53 AM

eog resources

Lea County, NM (NAD 83 NME)

Lacey Swiss 1 Fed Com #2H

Plan #0.2

Azimuths to Grid North
True North: -0.43°
Magnetic North: 5.81°

Magnetic Field
Strength: 47029.3nT
Dip Angle: 59.72°
Date: 3/3/2025
Model: IGRF2025

To convert a Magnetic Direction to a Grid Direction, Add 5.81°
To convert a Magnetic Direction to a True Direction, Add 6.25° East
To convert a True Direction to a Grid Direction, Subtract 0.43°

PROJECT DETAILS: Lea County, NM (NAD 83 NME)

Geodetic System: US State Plane 1983
Datum: North American Datum 1983
Ellipsoid: GRS 1980
Zone: New Mexico Eastern Zone
System Datum: Mean Sea Level

WELL DETAILS: #2H

3459.0
KB = 26' @ 3485.0usft

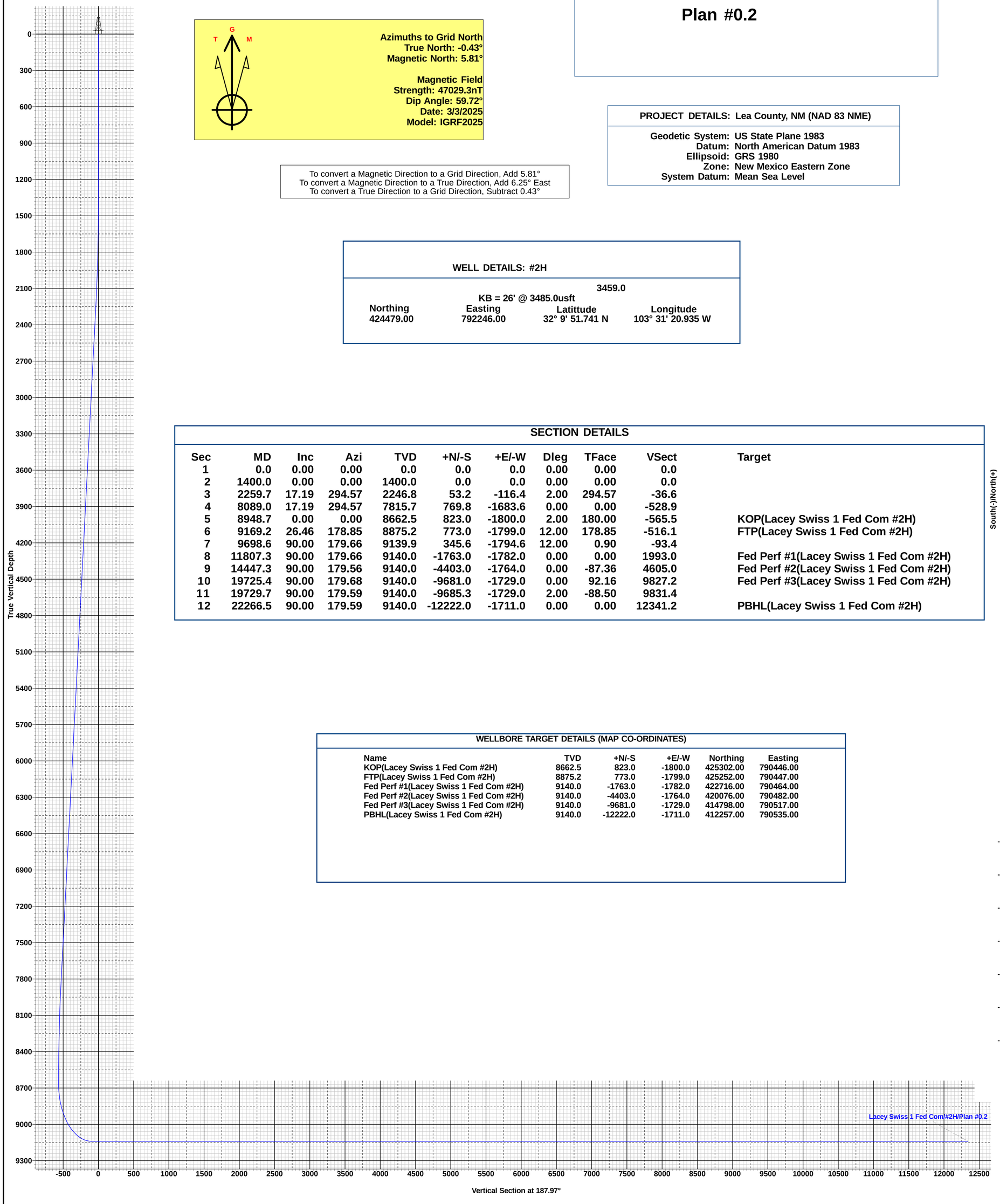
Northing	Easting	Latittude	Longitude
424479.00	792246.00	32° 9' 51.741 N	103° 31' 20.935 W

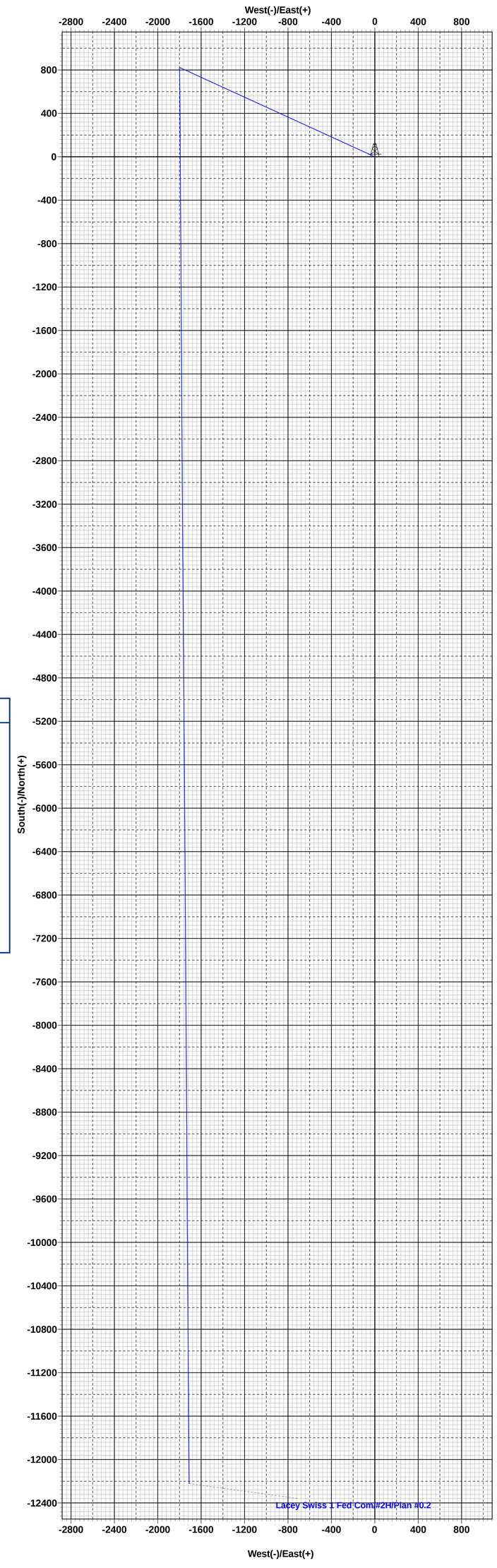
SECTION DETAILS

Sec	MD	Inc	Azi	TVD	+N/-S	+E/-W	Dleg	TFace	VSect	Target
1	0.0	0.00	0.00	0.0	0.0	0.0	0.00	0.00	0.0	
2	1400.0	0.00	0.00	1400.0	0.0	0.0	0.00	0.00	0.0	
3	2259.7	17.19	294.57	2246.8	53.2	-116.4	2.00	294.57	-36.6	
4	8089.0	17.19	294.57	7815.7	769.8	-1683.6	0.00	0.00	-528.9	
5	8948.7	0.00	0.00	8662.5	823.0	-1800.0	2.00	180.00	-565.5	KOP(Lacey Swiss 1 Fed Com #2H)
6	9169.2	26.46	178.85	8875.2	773.0	-1799.0	12.00	178.85	-516.1	FTP(Lacey Swiss 1 Fed Com #2H)
7	9698.6	90.00	179.66	9139.9	345.6	-1794.6	12.00	0.90	-93.4	
8	11807.3	90.00	179.66	9140.0	-1763.0	-1782.0	0.00	0.00	1993.0	Fed Perf #1(Lacey Swiss 1 Fed Com #2H)
9	14447.3	90.00	179.56	9140.0	-4403.0	-1764.0	0.00	-87.36	4605.0	Fed Perf #2(Lacey Swiss 1 Fed Com #2H)
10	19725.4	90.00	179.68	9140.0	-9681.0	-1729.0	0.00	92.16	9827.2	Fed Perf #3(Lacey Swiss 1 Fed Com #2H)
11	19729.7	90.00	179.59	9140.0	-9685.3	-1729.0	2.00	-88.50	9831.4	
12	22266.5	90.00	179.59	9140.0	-12222.0	-1711.0	0.00	0.00	12341.2	PBHL(Lacey Swiss 1 Fed Com #2H)

WELLBORE TARGET DETAILS (MAP CO-ORDINATES)

Name	TVD	+N/-S	+E/-W	Northing	Easting
KOP(Lacey Swiss 1 Fed Com #2H)	8662.5	823.0	-1800.0	425302.00	790446.00
FTP(Lacey Swiss 1 Fed Com #2H)	8875.2	773.0	-1799.0	425252.00	790447.00
Fed Perf #1(Lacey Swiss 1 Fed Com #2H)	9140.0	-1763.0	-1782.0	422716.00	790464.00
Fed Perf #2(Lacey Swiss 1 Fed Com #2H)	9140.0	-4403.0	-1764.0	420076.00	790482.00
Fed Perf #3(Lacey Swiss 1 Fed Com #2H)	9140.0	-9681.0	-1729.0	414798.00	790517.00
PBHL(Lacey Swiss 1 Fed Com #2H)	9140.0	-12222.0	-1711.0	412257.00	790535.00





Lea County, NM (NAD 83 NME)
Lacey Swiss 1 Fed Com
#2H
OH
Plan #0.2
16:22, March 03 2025

Released to Imaging: 4/11/2025 8:22:00 AM

eog resources

Lacey Swiss 1 Fed Com #2H

Revised Permit Information 01/23/2025:

Well Name: Lacey Swiss 1 Fed Com #2H; FKA Lacey Swiss 1 Fed Com 403H

Location: SHL: 884' FNL & 1540' FEL, Section 1, T-25-S, R-33-E, LEA Co., N.M.

BHL: 2541' FNL & 1950' FWL, Section 13, T-25-S, R-33-E, LEA Co., N.M.

1. CASING PROGRAM

Hole Size	Interval MD From (ft)	Interval MD To (ft)	Interval TVD From (ft)	Interval TVD To (ft)	Csg OD	Weight	Grade	Conn
16"	0	1,272	0	1,272	13-3/8"	54.5#	J-55	STC
11"	0	5,553	0	5,240	9-5/8"	40#	J-55	LTC
8-3/4"	0	8,949	0	8,663	7"	32#	P110-HP	BTC
7-7/8"	8,949	22,267	8,663	9,140	5-1/2"	20#	P110-EC	DWC/C IS MS

**For highlighted rows above, variance is requested to run entire string of either 7" or 5-1/2" casing string above due to availablility.

Variance is requested to waive the centralizer requirements for the 9-5/8" casing in the 11" hole size. An expansion additive will be utilized, in the cement slurry, for the entire length of the 11" hole interval to maximize cement bond and zonal isolation.

Variance is also requested to waive any centralizer requirements for the 7" and 5-1/2" casings in the 8-3/4" and 7-7/8" hole sizes. An expansion additive will be utilized, in the cement slurry, for the entire length of the 8-3/4" and 7-7/8" hole intervals to maximize cement bond and zonal isolation.

EOG requests permission to allow deviation from the 0.422'' annulus clearance requirement for the intermediate (salt) section from Title 43 CFR Part 3170 under the following conditions:

- The variance is not applicable within the Potash Boundaries or Capitan Reef areas.
- Operator takes responsibility to get casing to set point in the event that the clearance causes stuck pipe issues.

2. CEMENTING PROGRAM:

Depth TVD	No. Sacks	Wt. ppg	Yld Ft3/sk	Slurry Description
1,272' 13-3/8"	340	13.5	1.73	Lead: Class C/H + additives (TOC @ Surface)
	160	14.8	1.34	Tail: Class C/H + additives (TOC @ 1080')
5,240' 9-5/8"	520	12.7	2.22	Lead: Class C/H + additives + expansion additives (TOC @ Surface)
	180	14.8	1.32	Tail: Class C/H + additives + expansion additives (TOC @ 4442')
22,267' 7" 5-1/2"	1000	14.8	1.32	Bradenhead squeeze: Class C/H + additives + expansion additives (TOC @ surface)
	1810	13.2	1.52	Tail: Class C/H + additives (TOC @ 7,752')

eog resources

Lacey Swiss 1 Fed Com #2H

Additive	Purpose
Bentonite Gel	Lightweight/Lost circulation prevention
Calcium Chloride	Accelerator
Cello-flake	Lost circulation prevention
Sodium Metasilicate	Accelerator
MagOx	Expansive agent
Pre-Mag-M	Expansive agent
Sodium Chloride	Accelerator
FL-62	Fluid loss control
Halad-344	Fluid loss control
Halad-9	Fluid loss control
HR-601	Retarder
Microbond	Expansive Agent

Cement integrity tests will be performed immediately following plug bump.

Note: Cement volumes based on bit size plus at least 25% excess in the open hole plus 10% excess in the cased-hole overlap section.

EOG requests variance from minimum standards to pump a two stage cement job on the 7" and 5-1/2" production casing strings with the first stage being pumped conventionally with the calculated top of cement at the Brushy Canyon (7,752') and the second stage performed as a 1000 sack bradenhead squeeze with planned cement from the Brushy Canyon to surface. If necessary, a top out consisting of 400 sacks of Class C/H cement + 3% Salt + 1% PreMag-M + 6% Bentonite Gel (1.32 yld, 14.8 ppg) will be executed as a contingency. Top will be verified by Echo-meter.

Bradenhead will be the primary option for production cementing. EOG also requests to have the conventional option in place to accommodate for logistical or wellbore conditions. The tie back requirements will be met if the cement is pumped conventionally, and cement volumes will be adjusted accordingly. TOC will be verified by CBL.

3. MUD PROGRAM:

Depth (TVD)	Type	Weight (ppg)	Viscosity	Water Loss
0 – 1,272'	Fresh - Gel	8.6-8.8	28-34	N/c
1,272' – 5,240'	Brine	9.0-10.5	28-34	N/c
5,240' – 22,267'	Oil Base	8.8-9.5	58-68	N/c - 6

eog resources

Lacey Swiss 1 Fed Com #2H

4. VARIANCE REQUESTS:

EOG requests the additional variance(s) in the attached document(s):

Variances requested include (supporting documents attached):

- BOP Break Testing for 5M Intermediate Intervals (EOG BLM Variance 3a_b)
- Offline Cementing for Surface and Intermediate Intervals (EOG BLM Variance 3a_b)
- Production Offline Cement (EOG BLM Variance 3_d)
- Salt Interval Washout Annular Clearnace (EOG BLM Variance 4a)
- Alternate Shallow Casing Designs (EOG BLM Variance 5a)

eog resources

Lacey Swiss 1 Fed Com #2H

8. TUBING REQUIREMENTS:

EOG respectively requests an exception to the following NMOCD rule:

- 19.15.16.10 Casing AND TUBING RQUIREMENTS:
  J (3): "The operator shall set tubing as near the bottom as practical and tubing perforations shall not be more than 250 feet above top of pay zone."

With horizontal flowing and gas lifted wells an end of tubing depth placed at or slightly above KOP is a conservative way to ensure the tubing stays clean from debris, plugging, and allows for fewer well interventions post offset completion. The deeper the tubulars are run into the curve, the higher the probability is that the tubing will become stuck in sand and or well debris as the well produces over time. An additional consideration for EOT placement during artificial lift installations is avoiding the high dog leg severity and inclinations found in the curve section of the wellbore to help improve reliability and performance. Dog leg severity and inclinations tend not to hamper gas lifted or flowing wells, but they do effect other forms of artificial lift like rod pump or ESP (electric submersible pump). Keeping the EOT above KOP is an industry best practice for those respective forms of artificial lift.

eog resources

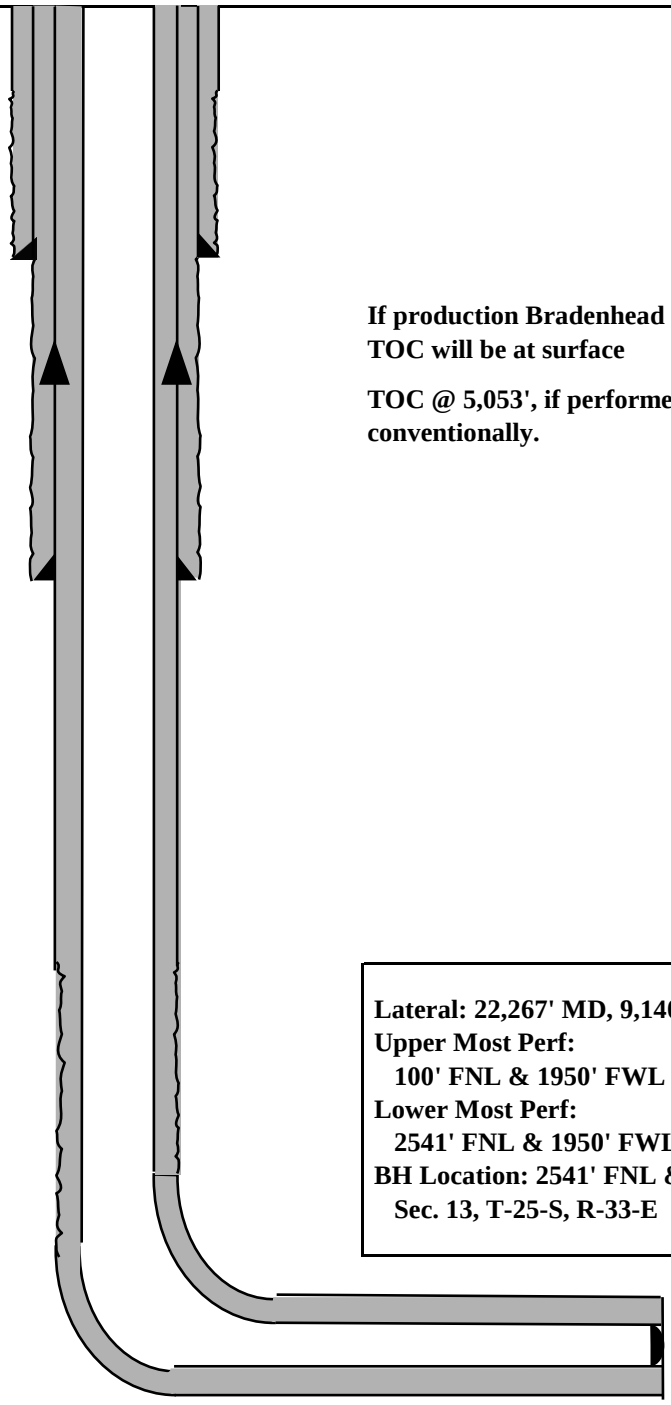
Lacey Swiss 1 Fed Com #2H

884' FNL
1540' FEL
Section 1
T-25-S, R-33-E

Proposed Wellbore

API: 30-025-53508

KB: 3484'
GL: 3459'



Bit Size: 16''
13-3/8'', 54.5#, J-55, STC
@ 0' - 1,272' MD
@ 0' - 1,272' TVD

Bit Size: 11''
9-5/8'', 40#, J-55, LTC
@ 0' - 5,553' MD
@ 0' - 5,240' TVD

Bit Size: 8-3/4''|Bit Size: 7-7/8''
7'', 32.#, P110-HP, BTC
@ 0' - 8,949' MD
@ 0' - 8,663' TVD
5-1/2'', 20.#, P110-EC, DWC/C IS MS
@ 8,949' - 22,267' MD
@ 8,663' - 9,140' TVD

KOP: 8,949' MD, 8,663' TVD
EOC: 9,699' MD, 9,140' TVD

If production Bradenhead is performed, TOC will be at surface

TOC @ 5,053', if performed conventionally.

Lateral: 22,267' MD, 9,140' TVD
Upper Most Perf:
100' FNL & 1950' FWL Sec. 1
Lower Most Perf:
2541' FNL & 1950' FWL Sec. 13
BH Location: 2541' FNL & 1950' FWL Sec. 13, T-25-S, R-33-E

eog resources

Lacey Swiss 1 Fed Com #2H

1. GEOLOGIC NAME OF SURFACE FORMATION:

Permian

2. ESTIMATED TOPS OF IMPORTANT GEOLOGICAL MARKERS:

Rustler	1,159'
Tamarisk Anhydrite	1,247'
Top of Salt	1,652'
Base of Salt	5,140'
Lamar	5,180'
Bell Canyon	5,197'
Cherry Canyon	6,236'
Brushy Canyon	7,752'
Bone Spring Lime	9,204'
Leonard (Avalon) Shale	9,279'
1st Bone Spring Sand	10,169'
2nd Bone Spring Shale	10,489'
2nd Bone Spring Sand	10,777'
3rd Bone Spring Carb	11,303'
TD	9,140'

3. ESTIMATED DEPTHS OF ANTICIPATED FRESH WATER, OIL OR GAS:

Upper Permian Sands	0- 400’	Fresh Water
Bell Canyon	5,197'	Oil
Cherry Canyon	6,236'	Oil
Brushy Canyon	7,752'	Oil
Leonard (Avalon) Shale	9,279'	Oil
1st Bone Spring Sand	10,169'	Oil
2nd Bone Spring Shale	10,489'	Oil
2nd Bone Spring Sand	10,777'	Oil

eog resources

EOG Batch Casing

Pad Name: Lacey Swiss 1 Fed Com SHALLOW Sundry
SHL: Section 2, Township 25-S, Range 33-E, LEA County, NM

EOG requests for the below wells to be approved for all designs listed in the Blanket Casing Design ('EOG BLM Variance 5a - Alternate Shallow Casing Designs.pdf' OR 'EOG BLM Variance 5b - Alternate Deep Casing Designs.pdf') document. The MDs and TVDs for all intervals are within the boundary conditions. The max inclination and DLS are also within the boundary conditions. The directional plans for the wells are attached separately.

Well Name	API #	Surface		Intermediate		Production	
		MD	TVD	MD	TVD	MD	TVD
Lacey Swiss 1 Fed Com #111H (516H)	30-025-54360	1,272	1,272	5,302	5,240	22,327	9,426
Lacey Swiss 1 Fed Com #112H (404H)	30-025-53434	1,272	1,272	5,720	5,240	22,722	9,455
Lacey Swiss 1 Fed Com #113H (303H)	30-025-53429	1,272	1,272	5,409	5,240	22,454	9,454
Lacey Swiss 1 Fed Com #1H (306H)	30-025-53431	1,272	1,272	5,406	5,240	21,908	8,911
Lacey Swiss 1 Fed Com #221H (304H)	30-025-53430	1,272	1,272	5,521	5,240	20,300	9,839
Lacey Swiss 1 Fed Com #222H (101H)	30-025-52765	1,272	1,272	5,575	5,240	20,346	9,837
Lacey Swiss 1 Fed Com #2H (403H)	30-025-53508	1,272	1,272	5,553	5,240	22,267	9,140
Lacey Swiss 1 Fed Com #311H (515H)	30-025-54361	1,272	1,272	5,478	5,240	20,651	10,227
Lacey Swiss 1 Fed Com #312H (203H)	30-025-52775	1,272	1,272	5,466	5,240	20,669	10,256
Lacey Swiss 1 Fed Com #411H (204H)	30-025-52776	1,272	1,272	5,573	5,240	21,072	10,563
Lacey Swiss 1 Fed Com #412H (201H)	30-025-52773	1,272	1,272	5,543	5,240	21,043	10,560
Lacey Swiss 1 Fed Com #504H (405H)	30-025-53435	1,272	1,272	5,459	5,240	21,270	10,862
Lacey Swiss 1 Fed Com #525H (402H)	30-025-53433	1,272	1,272	5,678	5,240	21,489	10,888
Lacey Swiss 1 Fed Com #551H (104H)	30-025-52768	1,272	1,272	5,541	5,240	21,637	11,155
Lacey Swiss 1 Fed Com #552H (102H)	30-025-52766	1,272	1,272	5,521	5,240	21,661	11,196
Lacey Swiss 1 Fed Com #582H (202H)	30-025-52774	1,272	1,272	5,638	5,240	22,103	11,534
Lacey Swiss 1 Fed Com #591H (103H)	30-025-52767	1,272	1,272	5,508	5,240	22,252	11,798

EOG Batch Casing

Variances

EOG requests the additional variance(s) in the attached document(s):

- EOG BLM Variance 2a - Intermediate Bradenhead Cement
- EOG BLM Variance 3d - Production Offline Cement
- EOG BLM Variance 3a_b - BOP Break-test and Offline Intermediate Cement
- EOG BLM Variance 4a - Salt Section Annular Clearance
- EOG BLM Variance 5a - Alternate Shallow Casing Designs

eog resources

EOG Batch Casing

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2nd Bone Spring Shale	10,489'	Oil
2nd Bone Spring Sand	10,777'	Oil

No other Formations are expected to give up oil, gas or fresh water in measurable quantities. Surface fresh water sands will be protected by setting surface casing at 1,280' and circulating cement back to surface.

Sante Fe Main Office
Phone: (505) 476-3441

General Information
Phone: (505) 629-6116

Online Phone Directory
https://www.emnrd.nm.gov/ocd/contact-us

State of New Mexico
Energy, Minerals and Natural Resources
Oil Conservation Division
1220 S. St Francis Dr.
Santa Fe, NM 87505

CONDITIONS

Action 447058

CONDITIONS

Operator: EOG RESOURCES INC 5509 Champions Drive Midland, TX 79706	OGRID: 7377
	Action Number: 447058
	Action Type: [C-103] NOI Change of Plans (C-103A)

CONDITIONS

Created By	Condition	Condition Date
matthew.gomez	Any previous COA's not addressed within the updated COA's still apply.	4/11/2025