Form 3160-3 FORM APPROVED OMB No. 1004-0137 (June 2015) Expires: January 31, 2018 **UNITED STATES** DEPARTMENT OF THE INTERIOR 5. Lease Serial No. NMNM86913 **BUREAU OF LAND MANAGEMENT** APPLICATION FOR PERMIT TO DRILL OR REENTER 6. If Indian, Allotee or Tribe Name 7. If Unit or CA Agreement, Name and No. **✓** DRILL REENTER 1a. Type of work: Oil Well 1b. Type of Well: Gas Well Other 8. Lease Name and Well No. 1c. Type of Completion: Hydraulic Fracturing Single Zone ✓ Multiple Zone BLOOMIN ONION 11/14 FED COM 715H 2. Name of Operator 9. API Well No. MEWBOURNE OIL COMPANY 30**-0**15**-5**7234 10. Field and Pool, or Exploratory 3a. Address 3b. Phone No. (include area code) P O BOX 5270, HOBBS, NM 88241 (575) 393-5905 WF/WOLFCAMP 4. Location of Well (Report location clearly and in accordance with any State requirements.\*) 11. Sec., T. R. M. or Blk. and Survey or Area SEC 2/T20S/R30E/NMP At surface NWSE / 1530 FSL / 1770 FEL / LAT 32.599187 / LONG -103.9399819 At proposed prod. zone SESE / 100 FSL / 1980 FEL / LAT 32.5663027 / LONG -103.9406744 14. Distance in miles and direction from nearest town or post office\* 12. County or Parish 13. State **EDDY** NM 20 miles 15. Distance from proposed\* 16. No of acres in lease 17. Spacing Unit dedicated to this well 185 feet location to nearest property or lease line, ft. 320.0 (Also to nearest drig. unit line, if any) 18. Distance from proposed location\* 19. Proposed Depth 20. BLM/BIA Bond No. in file to nearest well, drilling, completed, 20 feet 9890 feet / 20615 feet FED: NM1693 applied for, on this lease, ft. 21. Elevations (Show whether DF, KDB, RT, GL, etc.) 22. Approximate date work will start\* 23. Estimated duration 3227 feet 07/20/2025 60 days 24. Attachments The following, completed in accordance with the requirements of Onshore Oil and Gas Order No. 1, and the Hydraulic Fracturing rule per 43 CFR 3162.3-3 (as applicable) 1. Well plat certified by a registered surveyor. 4. Bond to cover the operations unless covered by an existing bond on file (see Item 20 above). 2. A Drilling Plan. 3. A Surface Use Plan (if the location is on National Forest System Lands, the 5. Operator certification. SUPO must be filed with the appropriate Forest Service Office). 6. Such other site specific information and/or plans as may be requested by the Name (Printed/Typed) Date 25. Signature BRADLEY BISHOP / Ph: (575) 393-5905 05/23/2025 (Electronic Submission) Title Regulatory Approved by (Signature) Date Name (Printed/Typed) (Electronic Submission) CODY LAYTON / Ph: (575) 234-5959 08/29/2025 Title Office Assistant Field Manager Lands & Minerals Carlsbad Field Office Application approval does not warrant or certify that the applicant holds legal or equitable title to those rights in the subject lease which would entitle the



Title 18 U.S.C. Section 1001 and Title 43 U.S.C. Section 1212, make it a crime for any person knowingly and willfully to make to any department or agency

applicant to conduct operations thereon. Conditions of approval, if any, are attached.

<u>C-102</u>	-		Ener			l Resources Dep				Revised J	uly 9, 2024		
	Electronica D Permittir			OIL	CONSERVAT	ION DIVISION				✓ Initial Submitt	ta1		
Via OC	D I CHIIILLII	ig						Submi		☐ Amended Rep			
								Type:		☐ As Drilled			
					WELL LOCAT	ATION INFORMATION							
API Nur	mber 8 <mark>0-015-5</mark>	57234	Pool Code	72120		ool Name VF-WFMP Big	Eddy; Wolf	fcamp	(Ga	s)			
Property	Code 35709		Property Na	BLO		ON 11/14 F	_		Well	Number	715H		
OGRID 14744	No.		Operator Na	ame	MEWBOURI	NE OIL COM	PANY		Grou	nd Level Elevation	3227'		
	Owner:	State  Fee	⊥ ]Tribal □ F∈	ederal		Mineral Owner:	☐ State ☐ Fee	 □ Tribal	<b>☑</b> Fed	leral			
					Surfa	ice Location							
UL	Section	Township	Range	Lot	Ft. from N/S	Ft. from E/W	Latitude		Longi		County		
J	2	20S	30E		1530 FSL	1770 FEL	32.59918	70°N	103.	.9399819°W	EDDY		
		T	1	1		Hole Location							
UL	Section	Township	Range	Lot	Ft. from N/S	Ft. from E/W	Latitude	08037	Longi		County		
0	14	20S	30E		100 FSL	1980 FEL	32.56630	27°N	103.	.9406744°W	EDDY		
Dedicate	ed Acres	Infill or Defi	ning Well	Defining	Well API	Overlapping Spa	cing Unit (Y/N)	Consolic	lation (	Code			
320		DEFININ	_			N C							
Order N	umbers. N/	A		•		Well setbacks are	e under Common	Ownersh	nip: 🔽	Yes □ No			
					Kick O	ff Point (KOP)							
UL	Section	Township	Range	Lot	Ft. from N/S	Ft. from E/W	Latitude		Longi	itude	County		
0	2	20S	30E		473 FSL	1980 FEL	32.59627	28°N	_	.9406749°W	EDDY		
					First Ta	ke Point (FTP)							
UL	Section	Township	Range	Lot	Ft. from N/S	Ft. from E/W	Latitude		Longi	itude	County		
В	11	20S	30E		100 FNL	1980 FEL	32.59469	82°N	103.	9406794°W	EDDY		
						ke Point (LTP)							
UL	Section	Township	Range	Lot	Ft. from N/S		Latitude		Longi		County		
0	14	20S	30E		100 FSL	1980 FEL	32.56630	27°N	103.	9406744°W	EDDY		
	l Area or Ar	rea of Uniform	Interest	Spacing	Unit Type 🛭 Hori	zontal  Vertical	Grour 3227'	nd Floor I	Elevati	on:			
N/A							3221						
OPER A	ATOR CER	TIFICATIONS	<u> </u>			SURVEYOR CER	TIFICATIONS						
		information conte ef, and , if the well			olete to the best of	I hereby certify that th	e well location show	yn on this j	olat was	s plotted from field no	tes of actual		
organiza	tion either own	is a working intere	est or unleased 1	nineral inter	est in the land	surveys made by me us my belief.	naer my supervision	and man	ne sam	e is true and correct to	o ine vesi oj		
location p	pursuant to a c		wner of a workir	ng interest or	unleased mineral			N MET					
	or to a volunta y the division.	ry pooling agreen	ient or a compu	lsory pooling	order heretofore			, 19680	)				
		al well, I further o					\\$\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\		<b>'</b>	S S			
in each ti	act (in the tar,	get pool or <mark>format</mark>	tion) in which an	y part of the			THE			4			
_	vill be located ett M	or obtained <b>a con</b>			the division.		PROPERTY OF THE STATE OF THE ST	ONAL S	3011				
Signature	ecc m	<u>ueer</u>	03/24/	2025		Signature and Seal of Prof	essional Surveyor	\					
Brett	Miller					Robert M	. Howet	,†					
Printed Na	me					Certificate Number	Date of Surve	ey					
brett	.miller@	)mewbou	rne.com			19680		0	2/1	8/2025			
Email Add	ress					10000		•	, -	-,			

#### ACREAGE DEDICATION PLATS

This grid represents a standard section. You may superimpose a non-standard section, or larger area, over this grid. Operators must outline the dedicated acreage in a red box, clearly show the well surface location and bottom hole location, if it is a directionally drilled, with the dimensions from the section lines in the cardinal directions. If this is a horizontal wellbore show on this plat the location of the First Take Point and Last Take Point, and the point within the Completed interval (other than the First Take Point or Last Take Point) that is closest to any outer boundary of the tract.

Surveyors shall use the latest United States government survey or dependent resurvey. Well locations will be in reference to the New Mexico Principal Meridian. If the land is not surveyed, contact the OCD Engineering Bureau. Independent subdivision surveys will not be acceptable.

### BLOOMIN ONION 11/14 FED COM #715H

GEODETIC DATA
NAD 83 GRID - NM EAST SURFACE LOCATION (SL) PROPOSED PENETRATION POINT 2 (PPP2) <u>' FSL & 1770' FEL (SEC.</u> 581939.0 – E: 662472.5 612' FNL & 1983' FEL (SEC.11) N: 577793.5 - E: 662273.4 2612 N: LAT: 32.5991870° N LAT: 32.5877943° N LONG: 103.9399819° W LONG: 103.9406782° W KICK OFF POINT (KOP) PROPOSED PENETRATION POINT 3 (PPP3) 473' FSL & 1980' FEL (SEC 1324' FSL & 1985' FEL (SEC.11) N: 580878.0 - E: 662263.0 N: 576470.3 - E: 662278.5 LAT: 32.5962728° N LAT: 32.5841572° N LONG: 103.9406749° W LONG: 103.9406776° W FIRST TAKE POINT (FTP) PROPOSED PENETRATION POINT 4 (PPP4) 100' FNL & 1980' FEL (SEC <u>O' FNL & 1987' FEL (SEC.14)</u> N: 575147.1 - E: 662283.6 N: 580305.1 - E: 662263.7 LAT: 32.5946982° N LAT: 32.5805201° N LONG: 103.9406794° W LONG: 103.9406769° W BOTTOM HOLE/LAST TAKE POINT (BH/LTP) 100' FSL & 1980' FEL (SEC.14) N: 569974.7 - E: 662303.4 LAT: 32.5663027° N LONG: 103.9406744° W CORNER DATA NAD 83 GRID - NM EAST A: FOUND BRASS CAP "1943" N: 569860.4 - E: 658982.8 B: FOUND BRASS CAP "1943" N: 572503.1 - E: 658972.6 C: FOUND BRASS CAP "1943" N: 575143.8 - E: 658975.3 D: FOUND BRASS CAP "1943" N: 577782.9 - E: 658969.8 E: FOUND BRASS CAP "1943" N: 580421.2 - E: 658964.9 F: FOUND BRASS CAP "1916" N: 585709.4 - E: 658995.1 G: FOUND BRASS CAP "1916" N: 585717.4 - E: 661635.9 H: CALCULATED CORNER N: 585724.1 - E: 664264.2 I: FOUND BRASS CAP "1943" N: 583088.0 - E: 664241.2 J: FOUND BRASS CAP "1943" N: 580444.6 - E: 664242.4 K: FOUND BRASS CAP "1943" N: 577799.8 - E: 664255.5 L: FOUND BRASS CAP "1943" N: 575148.7 - E: 664269.8 M: FOUND BRASS CAP "1943" N: 572497.7 - E: 664277.0

> N: FOUND BRASS CAP "1943" N: 569876.3 - E: 664283.2

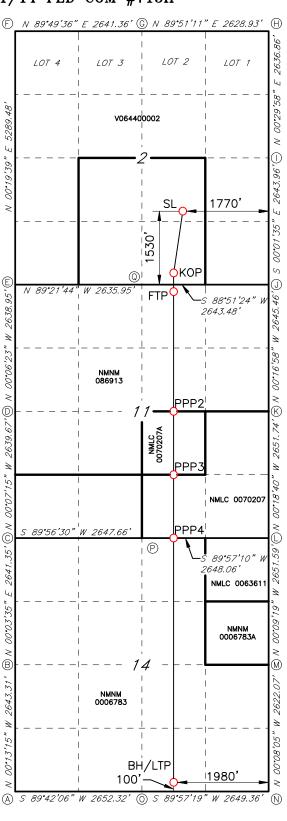
> O: FOUND BRASS CAP "1943"

N: 569874.2 - E: 661634.4 P: FOUND BRASS CAP "1943"

N: 575146.5 - E: 661622.4

Q: FOUND BRASS CAP "1943"

N: 580391.9 - E: 661600.1



### State of New Mexico Energy, Minerals and Natural Resources Department

Submit Electronically Via E-permitting

Oil Conservation Division 1220 South St. Francis Dr. Santa Fe, NM 87505

## NATURAL GAS MANAGEMENT PLAN

I. Operator:	Mev	vbourne (	Oil Co.	OGRID:	14744	Date:	,3	3/27/25
	riginal [	☐ Amendment	due to □ 19.15.23	7.9.D(6)(a) NMA	C □ 19.15.27.9.D(	(6)(b) NMAC □	Other.	
f Other, please	describe	»:						
			formation for each or connected to a		eted well or set of vooint.	wells proposed to	be dri	illed or proposed t
Well Nam	ne	API	ULSTR	Footages	Anticipated Oil BBL/D	Anticipated Gas MCF/D	P	Anticipated roduced Water BBL/D
BLOOMIN ONION 11/1	4 FED COM	715H	J 2 20S 30E	1530' FSL x 1770'	FEL 1500	1500		4000
					Y1-500 Y2-300 Y3-200	Y1-700 Y2-400 Y3-250	Y.	1-1000 Y2-600 Y3-400
IV. Central De	livery P	oint Name:	BLOOMI	N ONION 11/14 F	FED COM 715H	[See	19.15.2	7.9(D)(1) NMAC
V. Anticipated proposed to be r	Schedul recomple	le: Provide the	following inform gle well pad or co	ation for each new	w or recompleted w	vell or set of well	s propo	osed to be drilled o
V. Anticipated	Schedul recomple	le: Provide the	following inform	ation for each nev	w or recompleted w	vell or set of well	s propo	osed to be drilled o
proposed to be r	Schedul recomple ne	le: Provide the eted from a sin	following inform gle well pad or co	ation for each new	w or recompleted wral delivery point.  Completion	vell or set of well	s propo Flow Date	First Production

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Section 2 — Enhance	<u>d Plan</u>
EFFECTIVE APRIL 1,	2022

Beginning April 1, 2022, an operator that is not in compliance with its statewide natural gas capture requirement for the applicable reporting area must complete this section.

X Operator certifies that it is not required to complete this section because Operator is in compliance with its statewide natural gas capture requirement for the applicable reporting area.

### IX. Anticipated Natural Gas Production:

W	fell	API	Anticipated Average Natural Gas Rate MCF/D	Anticipated Volume of Natural Gas for the First Year MCF
X. Natural Gas Ga	thering System (NG	GS):		
Operator	System	ULSTR of Tie-in	Anticipated Gathering Start Date	Available Maximum Daily Capacity of System Segment Tie-in

**XI. Map.**  $\square$  Attach an accurate and legible map depicting the location of the well(s), the anticipated pipeline route(s) connecting the production operations to the existing or planned interconnect of the natural gas gathering system(s), and the maximum daily capacity of the segment or portion of the natural gas gathering system(s) to which the well(s) will be connected.

XII. Line Capacity. The natural gas gathering system [	$\square$ will $\square$ will not have	capacity to gather	100% of the anticipated	natural gas
production volume from the well prior to the date of first	st production.			

**XIII.** Line Pressure. Operator  $\square$  does  $\square$  does not anticipate that its existing well(s) connected to the same segment, or portion, of the natural gas gathering system(s) described above will continue to meet anticipated increases in line pressure caused by the new well(s).

Attach (	Operator's	plan to	manage	production	in res	ponse to	o the	increased	line	pressu

**XIV. Confidentiality:** □ Operator asserts confidentiality pursuant to Section 71-2-8 NMSA 1978 for the information provided in Section 2 as provided in Paragraph (2) of Subsection D of 19.15.27.9 NMAC, and attaches a full description of the specific information for which confidentiality is asserted and the basis for such assertion.

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# Section 3 - Certifications Effective May 25, 2021

Operator certifies that, after reasonable inquiry and based on the available information at the time of submittal:

🖾 Operator will be able to connect the well(s) to a natural gas gathering system in the general area with sufficient capacity to transport one hundred percent of the anticipated volume of natural gas produced from the well(s) commencing on the date of first production, taking into account the current and anticipated volumes of produced natural gas from other wells connected to the pipeline gathering system; or ☐ Operator will not be able to connect to a natural gas gathering system in the general area with sufficient capacity to transport one hundred percent of the anticipated volume of natural gas produced from the well(s) commencing on the date of first production, taking into account the current and anticipated volumes of produced natural gas from other wells connected to the pipeline gathering system. If Operator checks this box, Operator will select one of the following: Well Shut-In. ☐ Operator will shut-in and not produce the well until it submits the certification required by Paragraph (4) of Subsection D of 19.15.27.9 NMAC; or Venting and Flaring Plan. 

Operator has attached a venting and flaring plan that evaluates and selects one or more of the potential alternative beneficial uses for the natural gas until a natural gas gathering system is available, including: power generation on lease; (a) power generation for grid; (b)

- compression on lease; (c)
- liquids removal on lease: (d)
- reinjection for underground storage; (e)
- reinjection for temporary storage; **(f)**
- reinjection for enhanced oil recovery; **(g)**
- fuel cell production; and (h)
- other alternative beneficial uses approved by the division. (i)

### **Section 4 - Notices**

- 1. If, at any time after Operator submits this Natural Gas Management Plan and before the well is spud:
- Operator becomes aware that the natural gas gathering system it planned to connect the well(s) to has become (a) unavailable or will not have capacity to transport one hundred percent of the production from the well(s), no later than 20 days after becoming aware of such information, Operator shall submit for OCD's approval a new or revised venting and flaring plan containing the information specified in Paragraph (5) of Subsection D of 19.15.27.9 NMAC; or
- Operator becomes aware that it has, cumulatively for the year, become out of compliance with its baseline natural gas capture rate or natural gas capture requirement, no later than 20 days after becoming aware of such information, Operator shall submit for OCD's approval a new or revised Natural Gas Management Plan for each well it plans to spud during the next 90 days containing the information specified in Paragraph (2) of Subsection D of 19.15.27.9 NMAC, and shall file an update for each Natural Gas Management Plan until Operator is back in compliance with its baseline natural gas capture rate or natural gas capture requirement.
- 2. OCD may deny or conditionally approve an APD if Operator does not make a certification, fails to submit an adequate venting and flaring plan which includes alternative beneficial uses for the anticipated volume of natural gas produced, or if OCD determines that Operator will not have adequate natural gas takeaway capacity at the time a well will be spud.

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I certify that, after reasonable inquiry, the statements in and attached to this Natural Gas Management Plan are true and correct to the best of my knowledge and acknowledge that a false statement may be subject to civil and criminal penalties under the Oil and Gas Act.

Signature:	Bradley Bishop
Printed Name:	BRADLEY BISHOP
Title:	REGULATORY MANAGER
E-mail Address:	BBISHOP@MEWBOURNE.COM
Date:	5 <b>-26:27</b> 1/25
Phone:	575-393-5905
	OIL CONSERVATION DIVISION
	(Only applicable when submitted as a standalone form)
Approved By:	
Title:	
Approval Date:	
Conditions of App	proval:

### Mewbourne Oil Company

#### Natural Gas Management Plan – Attachment

- VI. Separation equipment will be sized by construction engineering staff based on stated manufacturer daily throughput capacities and anticipated daily production rates to ensure adequate capacity. Closed vent system piping, compression needs, and VRUs will be sized utilizing ProMax modelling software to ensure adequate capacity for anticipated production volumes and conditions.
- VII. Mewbourne Oil Company (MOC) will take following actions to comply with the regulations listed in 19.15.27.8:
  - A. MOC will maximize the recovery of natural gas by minimizing the waste, as defined by 19.15.2 NMAC, of natural gas through venting and flaring. MOC will ensure that well(s) will be connected to a natural gas gathering system with sufficient capacity to transport natural gas. If there is no adequate takeaway for the gas, well(s) will be shut in until the natural gas gathering system is available.
  - B. All drilling operations will be equipped with a rig flare located at least 100 ft from the nearest surface hole. Rig flare will be utilized to combust any natural gas that is brought to surface during normal drilling operations. In the case of emergency venting or flaring the volumes will be estimated and reported appropriately.
  - C. During completion operations any natural gas brought to surface will be flared. Immediately following the finish of completion operations, all well flow will be directed to permanent separation equipment. Produced natural gas from separation equipment will be sent to sales. It is not anticipated that gas will not meet pipeline standards. However, if natural gas does not meet gathering pipeline quality specifications, MOC will flare the natural gas for 60 days or until the natural gas meets the pipeline quality specifications, whichever is sooner. MOC will ensure that the flare is sized properly and is equipped with automatic igniter or continuous pilot. The gas sample will analyzed twice per week and the gas will be routed into a gathering system as soon as pipeline specifications are met.
  - D. Natural gas will not be flared with the exceptions and provisions listed in the 19.15.27.8 D.(1) through (4). If there is no adequate takeaway for the separator gas, well(s) will be shut in until the natural gas gathering system is available with exception of emergency or malfunction situations. Venting and/or flaring volumes will be estimated and reported appropriately.
  - E. MOC will comply with the performance standards requirements and provisions listed in 19.15.27.8 E.(1) through (8). All equipment will be designed and sized to handle maximum anticipated pressures and throughputs in order to minimize the waste. Production storage tanks constructed after May 25, 2021 will be equipped with automatic gauging system. Flares constructed after May 25, 2021 will be equipped with automatic igniter or continuous pilot. Flares will be located at least 100' from the well and storage tanks unless otherwise approved by the division. MOC will conduct AVO inspections as described in 19.15.27.8 E (5) (a) with frequencies specified in 19.15.27.8 E (5) (b) and (c). All emergencies will be resolved as quickly and safely as feasible to minimize waste.
  - F. The volume of natural gas that is vented or flared as the result of malfunction or emergency during drilling and completions operations will be estimated. The volume of natural gas that is vented, flared or beneficially used during production operations, will be measured or estimated. MOC will install equipment to measure

the volume of natural gas flared from existing process piping or a flowline piped from equipment such as high pressure separators, heater treaters, or vapor recovery units associated with a well or facility associated with a well authorized by an APD issued after May 25, 2021 that has an average daily production greater than 60 Mcf/day. If metering is not practicable due to circumstances such as low flow rate or low pressure venting and flaring, MOC will estimate the volume of vented or flared natural gas. Measuring equipment will conform to industry standards and will not be designed or equipped with a manifold that allows the diversion of natural gas around the metering element except for the sole purpose of inspecting and servicing the measurement equipment.

VIII. For maintenance activities involving production equipment and compression, venting will be limited to the depressurization of the subject equipment to ensure safe working conditions. For maintenance of production and compression equipment the associated producing wells will be shut in to eliminate venting. For maintenance of VRUs all gas normally routed to the VRU will be routed to flare to eliminate venting.



#### U.S. Department of the Interior BUREAU OF LAND MANAGEMENT

APD ID: 10400105053

Submission Date: 05/23/2025

Highlighted data reflects the most

**Operator Name: MEWBOURNE OIL COMPANY** 

recent changes

Well Name: BLOOMIN ONION 11/14 FED COM

Well Number: 715H

Well Type: OIL WELL

Well Work Type: Drill

**Show Final Text** 

### **Section 1 - Geologic Formations**

					ALC: NO.		
Formation ID	Formation Name	Elevation	True Vertical	Measured Depth	Lithologies	Mineral Resources	Producing Formatio
15662055	UNKNOWN	3245	28	28	OTHER : Top Soil	NONE	N
15662060	RUSTLER	2935	310	310	ANHYDRITE, DOLOMITE	USEABLE WATER	N
15662059	TOP SALT	2675	570	570	SALT	NONE	N
15662056	BOTTOM SALT	1585	1660	1660	SALT	NONE	N
15662063	YATES	1399	1846	1846	SANDSTONE	NATURAL GAS, OIL	N
15662064	CAPITAN REEF	1131	2114	2114	DOLOMITE, LIMESTONE	USEABLE WATER	N
15662061	DELAWARE	-420	3665	3665	LIMESTONE	NATURAL GAS, OIL	N
15662054	BONE SPRINGS	-3225	6470	6470	LIMESTONE, SHALE	NATURAL GAS, OIL	N
15662057	BONE SPRING 1ST	-4455	7700	7700	SANDSTONE	NATURAL GAS, OIL	Y
15662058	BONE SPRING 2ND	-4966	8211	8211	SANDSTONE	NATURAL GAS, OIL	N
15662069	BONE SPRING 3RD	-5540	8785	8785	LIMESTONE	NATURAL GAS, OIL	Y

### **Section 2 - Blowout Prevention**

Pressure Rating (PSI): 5M Rating Depth: 20615

Equipment: Annular, Pipe Rams, Blind Rams, Other accessories to the BOP equipment will include a Kelly cock and floor safety valve (inside BOP) and choke lines and choke manifold. See attached schematics.

Requesting Variance? YES

Variance request: A variance is requested for the use of a flexible choke line from the BOP to the choke manifold. See attached for hydrostatic test chart. Anchors are not required by manufacturer. Variance is requested to use a multi bowl wellhead. Variance is requested to perform break testing according to attached procedure. If a breaktesting variance is approved & incorporated, API Standard 53 will be incorporated and testing annular BOP to 70% of RWP or 100% of MASP, whichever is greater, will be performed.

Well Name: BLOOMIN ONION 11/14 FED COM Well Number: 715H

**Testing Procedure:** BOP/BOPE will be tested by an independent service company to 250 psi low and the high pressure indicated above per 43 CFR Part 3172 requirements. The System may be upgraded to a higher pressure but still tested to the working pressure listed in the table above. If the system is upgraded all the components installed will be functional and tested. Pipe rams will be operationally checked each 24 hour period. Blind rams will be operationally checked on each trip out of the hole. These checks will be noted on the daily tour sheets.

#### **Choke Diagram Attachment:**

5M\_BOPE\_Choke\_Diagram\_20250520144751.pdf

Flex\_Line\_Specs\_API\_16C\_20250520144758.pdf

#### **BOP Diagram Attachment:**

5M\_BOPE\_Schematic\_20250520144809.pdf

Multi\_Bowl\_WH\_20250520144816.pdf

MOC\_Break\_Testing\_Variance\_20250520144822.pdf

### **Section 3 - Casing**

									7000		_	-										
Casing ID	String Type	Hole Size	Csg Size	Condition	Standard	Tapered String	Top Set MD	Bottom Set MD	Top Set TVD	Bottom Set TVD	Top Set MSL	Bottom Set MSL	Calculated casing length MD	Grade	Weight	Joint Type	Collapse SF	Burst SF	Joint SF Type	Joint SF	Body SF Type	Body SF
1	SURFACE	26	18.625	NEW	API	<b>Z</b>	0	385	0	385	3227	2842	385	J-55	87.5	BUTT	3.66	13.0 7	DRY	39.4 5	DRY	40.5 8
2	INTERMED IATE	17.5	13.375	NEW	API	N		1290	0	1290	3224	1937	1290	H-40	48	ST&C	1.13	2.53	DRY	3.11	DRY	5.22
3	INTERMED IATE	17.5	13.375	NEW	API	17	1290	1893	1290	1893	1938	1334	603	J-55	54.5	ST&C	1.13	2.72	DRY	12.3 1	DRY	20.4 2
	INTERMED IATE	17.5	13.375	NEW	API	N	1893	2039	1893	2039	1334	1188	146	J-55	61	ST&C	1.42	2.86	DRY	66.8 1	DRY	99.9 9
	INTERMED IATE	17.5	9.625	NEW	API	N	0	3590	0	3590	3228	-363	3590	J-55	36	LT&C	1.26	2.19	DRY	3.51	DRY	4.36
6	PRODUCTI ON	8.75	7.0	NEW	API	N	0	9385	0	9302	3635	-6075		P- 110	26	LT&C	1.33	2.12	DRY	2.84	DRY	3.4
7	LINER	6.12 5	4.5	NEW	API	N	9185	20615	9139	9890	-5912	-6663	11430	P- 110	13.5	LT&C	1.73	2.01	DRY	2.19	DRY	2.73

#### **Casing Attachments**

Well Name: BLOOMIN ONION 11/14 FED COM Well Number: 715H

Ca	sing	Яβ	tta	ch	me	nts
	;	9		•	••••	

Casing ID: 1

String

**SURFACE** 

**Inspection Document:** 

**Spec Document:** 

**Tapered String Spec:** 

Casing Design Assumptions and Worksheet(s):

18.625in\_87.5\_\_J55\_BTC\_Csg\_20250520145706.pdf

Casing ID: 2

String

**INTERMEDIATE** 

**Inspection Document:** 

**Spec Document:** 

**Tapered String Spec:** 

Casing Design Assumptions and Worksheet(s):

 $13.375 in\_48\_H40\_STC\_Csg\_20250520145051.pdf$ 

Casing ID: 3

String

INTERMEDIATE

**Inspection Document:** 

**Spec Document:** 

**Tapered String Spec:** 

Casing Design Assumptions and Worksheet(s):

13.375in\_54.5\_\_J55\_STC\_Csg\_20250520145154.pdf

Well Name: BLOOMIN ONION 11/14 FED COM Well Number: 715H

Casing Attachments	Casing	յ Attac	hments
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Casing ID: 4

String

INTERMEDIATE

**Inspection Document:** 

**Spec Document:** 

**Tapered String Spec:** 

**Casing Design Assumptions and Worksheet(s):** 

 $13.375 in\_61\_\_J55\_STC\_Csg\_20250520145620.pdf$ 

Casing ID: 5

String

**INTERMEDIATE** 

**Inspection Document:** 

**Spec Document:** 

**Tapered String Spec:** 

Casing Design Assumptions and Worksheet(s):

9.625in\_36\_\_J55\_LTC\_Csg\_20250520145006.pdf

Casing ID: 6

String

PRODUCTION

**Inspection Document:** 

**Spec Document:** 

**Tapered String Spec:** 

Casing Design Assumptions and Worksheet(s):

7in\_26\_\_P110\_LTC\_Csg\_20250520145243.pdf

Well Name: BLOOMIN ONION 11/14 FED COM Well Number: 715H

### **Casing Attachments**

Casing ID: 7

String

**LINER** 

**Inspection Document:** 

**Spec Document:** 

**Tapered String Spec:** 

Casing Design Assumptions and Worksheet(s):

4.5in\_13.5\_\_P110\_LTC\_Csg\_20250520145959.pdf

### **Section 4 - Cement**

String Type	Lead/Tail	Stage Tool Depth	Top MD	Bottom MD	Quantity(sx)	Yield	Density	Cu Ft	Excess%	Cement type	Additives
SURFACE	Lead		0	310	530	2.12	12.5	1130	100	Class C	Salt, Gel, Extender, LCM
SURFACE	Tail		310	385	200	1.34	14.8	268	100	Class C	Retarder
INTERMEDIATE	Lead	2089	0	1736	310	2.12	12.5	660	25	Class C	Salt, Gel, Extender, LCM
INTERMEDIATE	Tail		1736	2089	100	1.34	14.8	134	25	Class C	Retarder
INTERMEDIATE	Lead		0	1770	830	2.12	12.5	1760	50	CLASS C	SALT GEL EXTENDER LCM
INTERMEDIATE	Tail		1770	2039	200	1.34	14.8	268	50	CLASS C	RETARDER
INTERMEDIATE	Lead	2089	2089	2928	160	2.12	12.5	340	25	Class C	Salt, Gel Extender, LCM
INTERMEDIATE	Tail		2928	3590	200	1.34	14.8	268	25	Class C	Retarder
PRODUCTION	Lead		4590	6293	120	2.12	12.5	260	0	Class C	Gel, Retarder, Defoamer, Extender
PRODUCTION	Tail		6293	9385	400	1.18	15.6	472	0	Class H	Retarder, Fluid Loss, Defoamer
LINER	Lead		9185	2061 5	730	1.85	13.5	1360	25	CLASS H	SALT GEL FLUID LOSS RETARDER DISPERSANT DEFOAMER ANTI

Well Name: BLOOMIN ONION 11/14 FED COM Well Number: 715H

### **Section 5 - Circulating Medium**

Mud System Type: Closed

Will an air or gas system be Used? NO

Description of the equipment for the circulating system in accordance with 43 CFR 3172;

Diagram of the equipment for the circulating system in accordance with 43 CFR 3172:

**Describe what will be on location to control well or mitigate other conditions:** Formation integrity test will be performed per 43 CFR Part 3172. On Exploratory wells or on that portion of any well approved for a 5M BOPE system or greater, a pressure integrity test of each casing shoe shall be performed. Will be tested in accordance with 43 CFR Part 3172.

Describe the mud monitoring system utilized: Pason/PVT/Visual Monitoring

### **Circulating Medium Table**

Top Depth	Bottom Depth	Mud Type	Min Weight (lbs/gal)	Max Weight (Ibs/gal)	Density (lbs/cu ft)	Gel Strength (lbs/100 sqft)	РН	Viscosity (CP)	Salinity (ppm)	Filtration (cc)	Additional Characteristics
0	385	SPUD MUD	8.4	8.6		ř					
385	2039	SALT SATURATED	10	10.2	1000						
2039	3590	WATER-BASED MUD	8.4	8.6							
3590	1028 5	WATER-BASED MUD	8.6	9.7							
1028 5	2061 5	OIL-BASED MUD	10	11.5							

Well Name: BLOOMIN ONION 11/14 FED COM Well Number: 715H

### **Section 6 - Test, Logging, Coring**

List of production tests including testing procedures, equipment and safety measures:

No logs are planned based on well control or offset log information. Offset Well: Bloomin Onion 11/14 Fed Com 717H

List of open and cased hole logs run in the well:

DIRECTIONAL SURVEY, MEASUREMENT WHILE DRILLING, MUD LOG/GEOLOGIC LITHOLOGY LOG,

Coring operation description for the well:

None

#### **Section 7 - Pressure**

Anticipated Bottom Hole Pressure: 6171 Anticipated Surface Pressure: 3995

Anticipated Bottom Hole Temperature(F): 165

Anticipated abnormal pressures, temperatures, or potential geologic hazards? NO

Describe:

Contingency Plans geoharzards description:

Contingency Plans geohazards

Hydrogen Sulfide drilling operations plan required? YES

Hydrogen sulfide drilling operations

H2S\_Plan\_20250327131832.pdf

### **Section 8 - Other Information**

Proposed horizontal/directional/multi-lateral plan submission:

BLOOMIN\_ONION\_11\_14\_FED\_COM\_715H\_Dir\_Plan\_20250520150958.pdf BLOOMIN\_ONION\_11\_14\_FED\_COM\_715H\_Dir\_Plot\_20250520151003.pdf

Other proposed operations facets description:

Other proposed operations facets attachment:

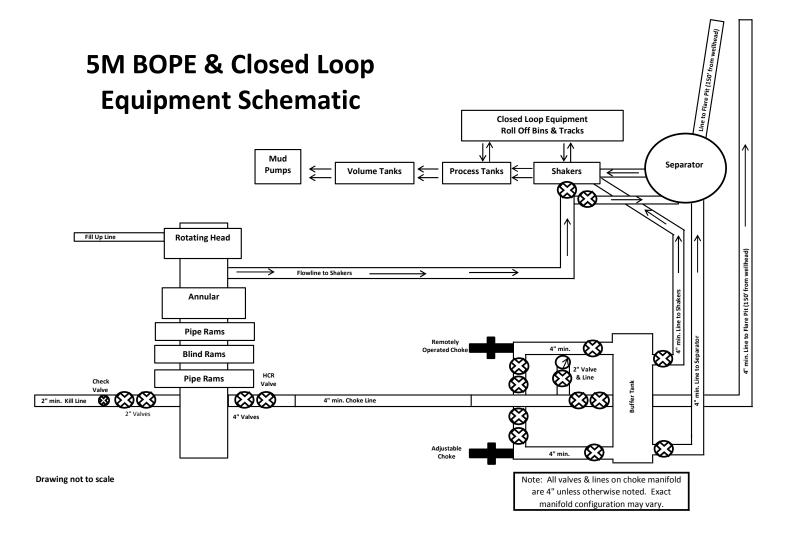
Bloomin\_Onion\_11\_14\_Fed\_Com\_715H\_Drlg\_Program\_20250520151018.pdf BLOOMIN ONION 11 14 FED COM 715H NGMP 20250520151023.pdf

Other Variance request(s)?:

Other Variance attachment:

MOC\_Offline\_Cementing\_Variance\_20250328194000.pdf MOC\_Break\_Testing\_Variance\_20250430141329.pdf







### LUOHE LETONE HYDRAULICS TECHNOLOGY CO.,LTD

### HYDROSTATIC TESTING REPORT

LTYY/QR-5.7.1-28

№: 230826015

Product Name	Cho	Choke And Kill Hose			i A	API Spec 16C 3 <sup>rd</sup> edition
Product Specification	3"×1000	0psi×60ft (18.29m	1)	Serial Num	ber	7660144
Inspection Equipment	MTU	J-BS-1600-3200-E		Test mediu	ım	Water
Inspection Department	(	C. Department		Inspection I	Date	2023.08.26
		Rate of le	ength chang	e	•	
Standard requirements	At working pr	essure, the rate of le	ngth chang	e should not n	nore than ±	2%
Testing result	10000psi (69.0	MPa) ,Rate of leng	th change 0	.7%		
		Hydrosta	atic testing			
Standard requirements		orking pressure, the ssure-holding perio				less than three minutes
Testing result	15000psi (103	.5MPa), 3 min for t	he first time	e, 60 min for th	ne second tin	ne, no leakage
100 100 30 30 30 30 30 30 30 30 30	21 5627 215421 215421 215421 215	M21 22:00:21 22:04:21	100 100 90 80 70 60 10 90 10 90 10 10 10 10 10 10 10 10 10 1	PSI 234958 2359		D1958 002958 003958 00
Conclusion	The inspec	eted items meet stan	dard requir	ements of API	Spec 16C 3 <sup>1</sup>	<sup>rd</sup> edition



### LUOHE LETONE HYDRAULICS TECHNOLOGY CO.,LTD

### CERTIFICATE OF QUALITY

### LTYY/QR-5.7.1-19B

№: LT2023-126-002

Customer Name	Austin Hose						
Product Name	Choke And Kill Hose						
Product Specification	3"×10000psi×60ft (18.29m)	Quantity	2PCS				
Serial Number	7660143~7660144	FSL	FSL3				
Temperature Range	-29°C∼+121°C	Standard	API Spec 16C 3 <sup>rd</sup> edition				
Inspection Department	Q.C. Department	Inspection date	2023.08.26				

Inspection Items				Inspection results				
Appearance Checking				In accordance with API Spec 16C 3 <sup>rd</sup> edition				
Size and Lengths				In accordance with API Spec 16C 3 <sup>rd</sup> edition				
Dimensions and Tolerances				In accordar	nce with API Spec	16C 3 <sup>rd</sup> edition		
End Connections: 4-1/16"×10000psi Integral flange for sour gas service				vice	In accordance with API Spec 6A 21st edition			
End Connections: 4-1	End Connections: 4-1/16"×10000psi Integral flange for sour gas service				In accordance with API Spec 17D 3 <sup>rd</sup> edition			
	Hydrostatic	Testing			In accordance with API Spec 16C 3 <sup>rd</sup> edition			
	product Ma	arking			In accordance with API Spec 16C 3 <sup>rd</sup> edition			
Inspection cor	Inspection conclusion The inspected items m				eet standard requirer	ments of API Spec	16C 3 <sup>rd</sup> edition	
Remarks								
Approver	Jian long C	hen	Auditor	1/1	inging Dong	Inspector	Zhansheng Wang	



### LUOHE LETONE HYDRAULICS TECHNOLOGY CO.,LTD

#### CERTIFICATE OF CONFORMANCE

№:LT230826016

Product Name: Choke And Kill Hose

Product Specification: 3"×10000psi×60ft (18.29m)

Serial Number: 7660143~7660144

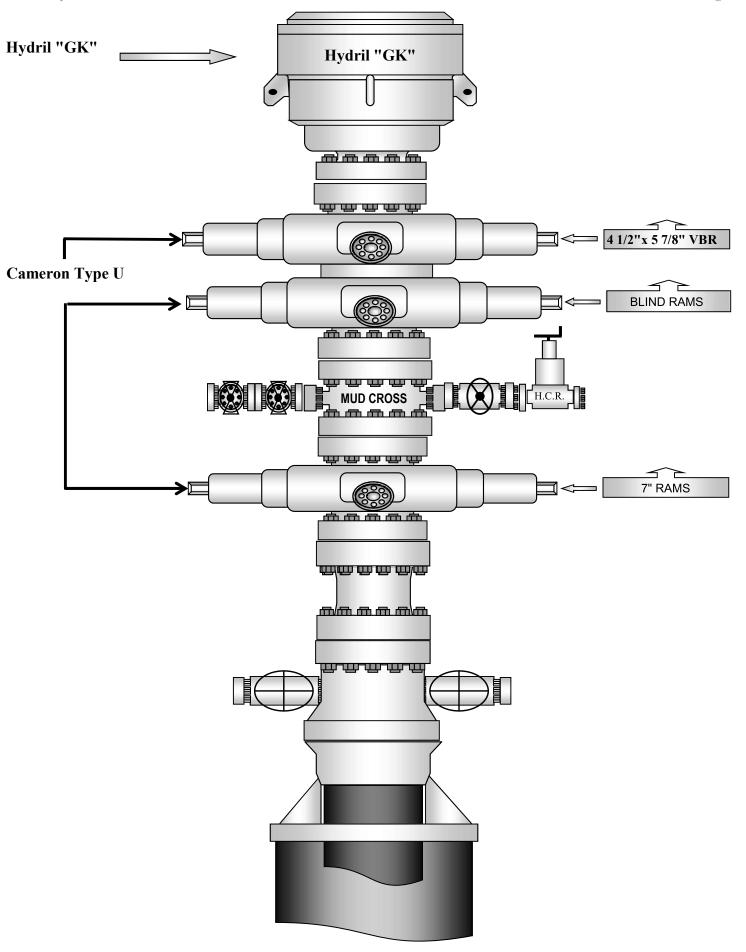
End Connections: 4-1/16"×10000psi Integral flange for sour gas service

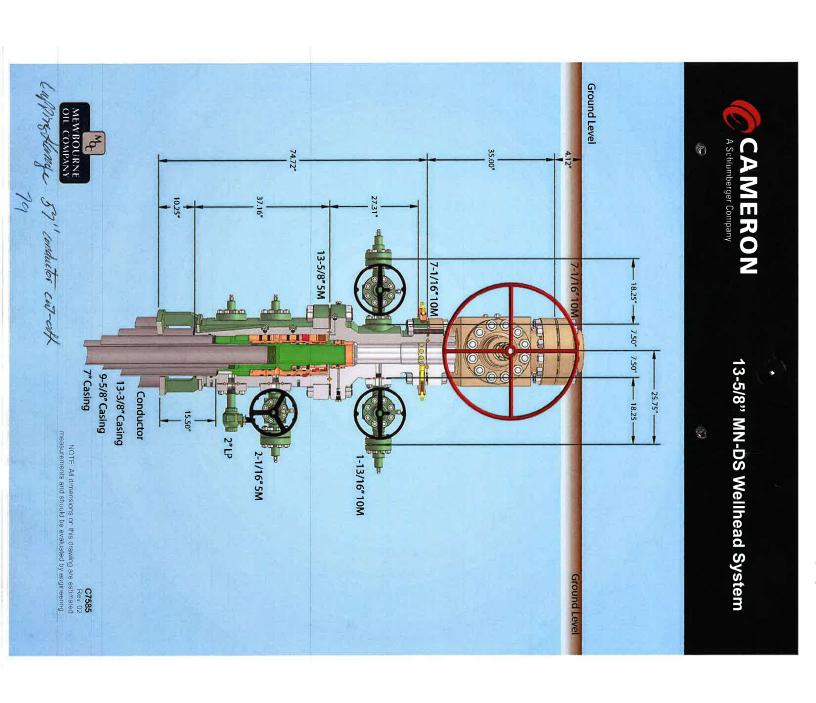
The Choke And Kill Hose assembly was produced by LUOHE LETONE HYDRAULICS TECHNOLOGY CO.,LTD . in Aug 2023, and inspected by LUOHE LETONE HYDRAULICS TECHNOLOGY CO.,LTD. according to API Spec 16C 3<sup>rd</sup> edition on Aug 26, 2023. The overall condition is good. This is to certify that the Choke And Kill Hose complies with all current standards and specifications for API Spec 16C 3<sup>rd</sup> edition.

Jian long Chen

QC Manager:

Date: Aug 26, 2023







### Mewbourne Oil Co.

### **BOP Break Testing Variance**

Mewbourne Oil Company requests a variance from the minimum standards for well control equipment testing of 43 CFR 3172 to allow a testing schedule of the blow out preventer (BOP) and blow out prevention equipment (BOPE) along with batch drilling & offline cementing operations. Modern rig upgrades which facilitate pad drilling allow the BOP stack to be moved between wells on a multi-well pad without breaking any BOP stack components apart. Widespread use of these technologies has led to break testing BOPE being endorsed as safe and reliable. American Petroleum Institute (API) best practices are frequently used by regulators to develop their regulations. API Standard 53, *Well Control Equipment Systems for Drilling Wells* (5<sup>th</sup> Ed., Dec. 2018) Section 5.3.7.1 states "A pressure test of the pressure containing component shall be performed following the disconnection or repair, limited to the affected component."

### **Procedures**

- 1. Full BOPE test at first installation on the pad.
  - Full BOPE test at least every 21 days.
  - Function test BOP elements per 43 CFR 3172.
  - Contact the BLM if a well control event occurs.
- 2. After the well section is secured and the well is confirmed to be static, the BOP will be disconnected from the wellhead and walked with the rig to another well on the pad. Two breaks on the BOPE will be made (Fig. 1).
  - Connection between the flex line and the HCR valve
  - Connection between the wellhead and the BOP quick connect (Fig. 5 & 6).
- 3. A capping flange will be installed after cementing per wellhead vendor procedure & casing pressure will be monitored via wellhead valve.
- 4. The BOP will be removed and carried by a hydraulic carrier (Fig. 3 & 4).
- 5. The rig will then walk to the next well.
- 6. Confirm that the well is static and remove the capping flange.
- 7. The connection between the flex line and HCR valve and the connection between the wellhead and the BOP quick connect will be reconnected.
- 8. Install a test plug into the wellhead.
- 9. A test will then be conducted against the upper pipe rams and choke, testing both breaks (Fig. 1 & 2).
- 10. The test will be held at 250 psi low and to the high value submitted in the APD, not to exceed 5000 psi.
- 11. The annular, blind rams and lower pipe rams will then be function tested.
- 12. If a pad consists of three or more wells, steps 4 through 11 will be repeated.



13. A break test will only be conducted if the intermediate section can be drilled and cased within 21 days of the last full BOPE test.

### **Barriers**

### **Before Nipple Down:**

- Floats in casing
- Kill weight fluid in casing
- Kill weight fluid in annulus
- Solid body mandrel and/or packoff

#### **After Nipple Down:**

- Floats in casing
- Kill weight fluid in casing
- Kill weight fluid in annulus
- Solid body mandrel and/or packoff
- Offline cementing tool and/or cement head
- Capping flange after cementing

### **Summary**

A variance is requested to only test broken pressure seals on the BOPE when moving between wells on a multi-well pad if the following conditions are met:

- A full BOPE test is conducted on the first well on the pad. API Standard 53 requires testing annular BOP to 70% of RWP or 100% of MASP, whichever is greater.
- If the first well on the pad is not the well with the deepest intermediate section, a full BOPE test will also be performed when moving to a deeper well.
- The hole section being drilled has a MASP under 5000 psi.
- If a well control event occurs, Mewbourne will contact BLM for permission to continue break testing.
- If significant (>50%) losses occur, full BOPE testing will be required going forward.
- Full BOPE test will be required prior to drilling the production hole.

While walking the rig, the BOP stack will be secured via hydraulic winch or hydraulic carrier. A full BOPE test will be performed at least every 21 days.



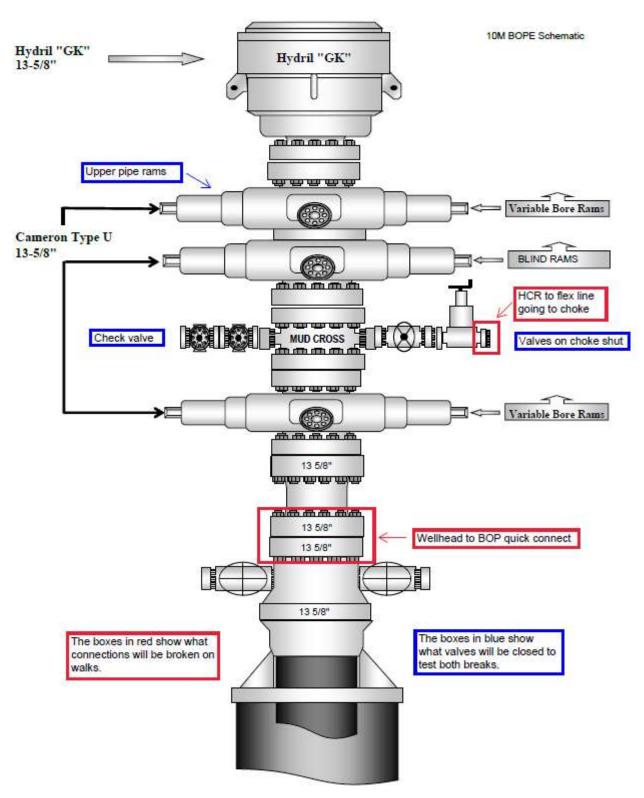


Figure 1. BOP diagram



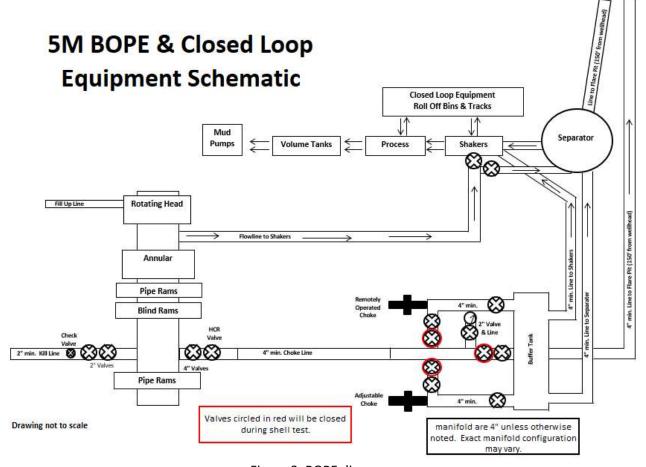


Figure 2. BOPE diagram





Figure 3. BOP handling system





Figure 4. BOP handling system



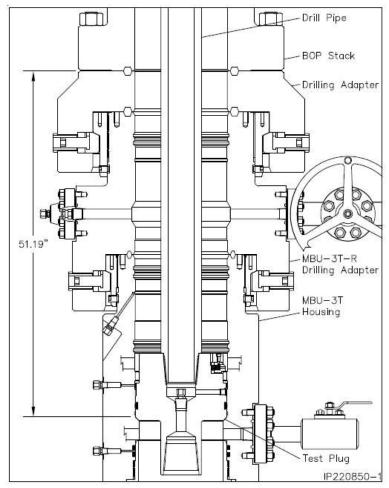


Figure 5. Cactus 5M wellhead with BOP quick connect

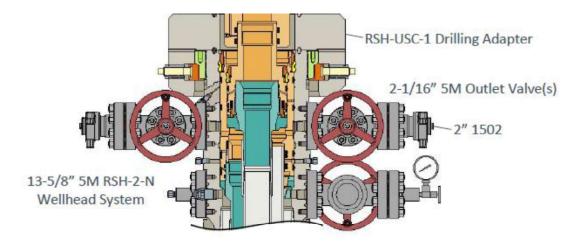


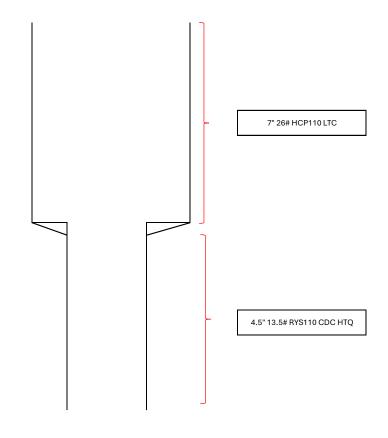
Figure 6. Vault 5M wellhead with BOP quick connect

#### Mewbourne Oil Company, Bloomin Onion 11/14 Fed Com 552H

Sec 11, T20S, R30E SHL: 205' FNL & 1110' FWL (Sec 11) BHL: 100' FSL & 990' FWL (Sec 14)

Casing Design A

	Hole Size	From	То	Csg. Size	#/ft	Grade	Conn.	SF Collapse	SF Burst	SF Jt Tension	SF Body Tension
ſ	8.75	0'	8478'	7'	7" 26# HCP110 LTC			1.82	2.33	3.14	3.77
ſ	8.5	8478'	19240'	4.5" 13	3.5# RYS	110 CDC	HTQ	1.89	2.20	2.94	2.90





Coupling Pipe Body Grade: J55 (Casing) Grade: J55 (Casing) Body: Bright Green 1st Band: Bright Green 1st Band: White 2nd Band: -2nd Band: -3rd Band: -3rd Band: -4th Band: -

Outside Diameter	9.625 in.	Wall Thickness	0.352 in.	Grade	J55 (Casing)
Min, Wall Thickness	87.50 %	Pipe Body Drift	API Standard	Туре	Casing
Connection OD Option	Regular				

#### Pipe Body Data

Geometry			
Nominal OD	9,625 in.	Drift	8.765 in.
Wall Thickness	0.352 in.	Plain End Weight	34.89 lb/ft
Nominal Weight	36 lb/ft	OD Tolerance	API
Nominal ID	8,921 in.		

Performance	
SMYS	55,000 psi
Min UTS	75,000 psi
Body Yield Strength	564 x1000 lb
Min. Internal Yield Pressure	3520 psi
Collapse Pressure	2020 psi
Max. Allowed Bending	26 °/100 ft

#### **Connection Data**

Geometry		Performance		Make-Up Torques	
Thread per In	8	Joint Strength	453 x1000 lb	Minimum Torque	3400 ft-lb
Connection OD	10,625 in,	Coupling Face Load	433 x1000 lb	Optimum Torque	4530 ft-Ib
Hand Tight Stand Off	3.500 in.	Internal Pressure Capacity	3520 psi	Maximum Torque	5660 ft-lb

#### Notes

For products according to API Standards 5CT & 5B; Performance calculated considering API Technical Report 5C3 (Sections 9 & 10) equations,
For geometrical and steel grades combinations not considered in the API Standards 5CT and/or 5B; Performance calculations indirectly derived from API Technical Report 5C3 (Sections 9 & 10) equations,

Couplings OD are shown according to current API 5CT 10th Edition.



### **API STC**

Coupling	Pipe Body
Grade: H40	Grade: H40
Body: •	1st Band: Black
1st Band: Black	2nd Band: -
2nd Band: -	3rd Band: =
3rd Band: =	4th Band: -

Outside Diameter	13.375 in.	Wall Thickness	0.330 in.	Grade	H40
Min. Wall Thickness	87.50 %	Pipe Body Drift	API Standard	Туре	Casing
Connection OD Option	Regular				

#### Pipe Body Data

Geometry			
Nominal OD	13,375 in.	Drift	12 <b>.</b> 559 in <b>.</b>
Wall Thickness	0.330 in.	Plain End Weight	46.02 lb/ft
Nominal Weight	48 lb/ft	OD Tolerance	API
Nominal ID	12,715 in.		

40,000 psi
60,000 psi
541 x1000 lb
1730 psi
740 psi
14 °/100 ft

#### **Connection Data**

Geometry		Perf
Thread per In	8	Joint S
Connection OD	14,375 in,	Couplin
Hand Tight Stand Off	3.500 in.	Interna

322 x1000 lb
377 x1000 lb
1730 psi

Make-Up Torques	
Minimum Torque	2420 ft-lb
Optimum Torque	3220 ft-lb
Maximum Torque	4030 ft-lb

#### Notes

For products according to API Standards 5CT & 5B; Performance calculated considering API Technical Report 5C3 (Sections 9 & 10) equations,
For geometrical and steel grades combinations not considered in the API Standards 5CT and/or 5B; Performance calculations indirectly derived from API Technical Report 5C3 (Sections 9 & 10) equations,

Couplings OD are shown according to current API 5CT 10th Edition.

**Tenaris** 

**API STC** 

Coupling Pipe Body Grade: J55 (Casing) Grade: J55 (Casing) Body: Bright Green 1st Band: Bright Green 1st Band: White 2nd Band: -2nd Band: -3rd Band: -3rd Band: -4th Band: -

Outside Diameter	13.375 in.	Wall Thickness	0.380 in.	Grade	J55 (Casing)
Min. Wall Thickness	87.50 %	Pipe Body Drift	API Standard	Туре	Casing
Connection OD Option	Regular				

#### Pipe Body Data

Geometry			
Nominal OD	13,375 in.	Drift	12 <b>.</b> 459 in <b>.</b>
Wall Thickness	0.380 in.	Plain End Weight	52.79 lb/ft
Nominal Weight	54.500 lb/ft	OD Tolerance	API
Nominal ID	12,615 in.		

Performance	
SMYS	55,000 psi
Min UTS	75,000 psi
Body Yield Strength	853 x1000 lb
Min. Internal Yield Pressure	2730 psi
Collapse Pressure	1130 psi
Max. Allowed Bending	19 °/100 ft

#### **Connection Data**

Geometry		Performance		Make-Up Torques	
Thread per In	8	Joint Strength	514 x1000 lb	Minimum Torque	3860 ft-lb
Connection OD	14,375 in,	Coupling Face Load	519 x1000 lb	Optimum Torque	5140 ft-lb
Hand Tight Stand Off	3.500 in.	Internal Pressure Capacity	2730 psi	Maximum Torque	6430 ft-lb

#### Notes

For products according to API Standards 5CT & 5B; Performance calculated considering API Technical Report 5C3 (Sections 9 & 10) equations,
For geometrical and steel grades combinations not considered in the API Standards 5CT and/or 5B; Performance calculations indirectly derived from API Technical Report 5C3 (Sections 9 & 10) equations,

Couplings OD are shown according to current API 5CT 10th Edition.



Coupling	Pipe Body
Grade: P110	Grade: P110
Body: White	1st Band: White
1st Band: =	2nd Band: =
2nd Band: =	3rd Band: -
3rd Band: -	4th Band: -

Outside Diameter	7.000 in.	Wall Thickness	0.362 in.	Grade	P110
Min, Wall Thickness	87.50 %	Pipe Body Drift	API Standard	Туре	Casing
Connection OD Option	Regular				

#### Pipe Body Data

Geometry			
Nominal OD	7,000 in.	Drift	6.151 in.
Wall Thickness	0.362 in.	Plain End Weight	25.69 lb/ft
Nominal Weight	26 lb/ft	OD Tolerance	API
Nominal ID	6.276 in.		

Performance	
SMYS	110,000 psi
Min UTS	125,000 psi
Body Yield Strength	830 x1000 lb
Min. Internal Yield Pressure	9960 psi
Collapse Pressure	6230 psi
Max. Allowed Bending	72 °/100 ft

#### **Connection Data**

Geometry		Performance		Make-Up Torques	
Thread per In	8	Joint Strength	693 x1000 lb	Minimum Torque	5200 ft-lb
Connection OD	7,875 in,	Coupling Face Load	799 x1000 lb	Optimum Torque	6930 ft-lb
Hand Tight Stand Off	3 in.	Internal Pressure Capacity	9960 psi	Maximum Torque	8660 ft-lb

#### Notes

For products according to API Standards 5CT & 5B; Performance calculated considering API Technical Report 5C3 (Sections 9 & 10) equations,
For geometrical and steel grades combinations not considered in the API Standards 5CT and/or 5B; Performance calculations indirectly derived from API Technical Report 5C3 (Sections 9 & 10) equations,

Couplings OD are shown according to current API 5CT 10th Edition.

**Tenaris** 

**API STC** 

Coupling Pipe Body Grade: J55 (Casing) Grade: J55 (Casing) Body: Bright Green 1st Band: Bright Green 1st Band: White 2nd Band: -2nd Band: -3rd Band: -3rd Band: -4th Band: -

Outside Diameter	13.375 in.	Wall Thickness	0.430 in.	Grade	J55 (Casing)
Min. Wall Thickness	87.50 %	Pipe Body Drift	API Standard	Туре	Casing
Connection OD Option	Regular				

#### Pipe Body Data

Geometry			
Nominal OD	13.375 in.	Drift	12 <b>.</b> 359 in.
Wall Thickness	0.430 in.	Plain End Weight	59.50 lb/ft
Nominal Weight	61 lb/ft	OD Tolerance	API
Nominal ID	12,515 in.		

Performance		
SMYS	55,000 psi	
Min UTS	75,000 psi	
Body Yield Strength	962 x1000 lb	
Min. Internal Yield Pressure	3090 psi	
Collapse Pressure	1540 psi	
Max. Allowed Bending	19 °/100 ft	

#### **Connection Data**

Geometry		Performance		Make-Up Torques	
Thread per In	8	Joint Strength	595 x1000 lb	Minimum Torque	4460 ft-lb
Connection OD	14,375 in,	Coupling Face Load	519 x1000 lb	Optimum Torque	5950 ft-lb
Hand Tight Stand Off	3.500 in.	Internal Pressure Capacity	3090 psi	Maximum Torque	7440 ft-lb

#### Notes

For products according to API Standards 5CT & 5B; Performance calculated considering API Technical Report 5C3 (Sections 9 & 10) equations,
For geometrical and steel grades combinations not considered in the API Standards 5CT and/or 5B; Performance calculations indirectly derived from API Technical Report 5C3 (Sections 9 & 10) equations,

Couplings OD are shown according to current API 5CT 10th Edition.



Coupling Pipe Body Grade: J55 (Casing) Grade: J55 (Casing) Body: Bright Green 1st Band: Bright Green 1st Band: White 2nd Band: -2nd Band: -3rd Band: -3rd Band: -4th Band: -

Outside Diameter	18.625 in.	Wall Thickness	0.435 in.	Grade	J55 (Casing)
Min. Wall Thickness	87,50 %	Pipe Body Drift	Special Drift	Туре	Casing
Connection OD Option	Regular				

#### Pipe Body Data

Geometry			
Nominal OD	18.625 in.	Plain End Weight	84 <b>.</b> 59 lb/ft
Wall Thickness	0.435 in.	OD Tolerance	API
Nominal ID	17.755 in.		
Drift	17.756 in.		

Perfe	ormance	
SMYS		55,000 psi
Min UT	s	75,000 psi
Body Y	ield Strength	1367 x1000 lb
Min. Int	ternal Yield Pressure	2250 psi
Collaps	se Pressure	630 psi
Max. A	llowed Bending	13.54 °/100 ft

#### **Connection Data**

Geometry		Performance	
Thread per In	5	Joint Strength	1328 x1000 lb
Connection OD	20 in,	Coupling Face Load	1669 x1000 lb
Hand Tight Stand Off	0.875 in.	Internal Pressure Capacity	2250 psi

#### Notes

For products according to API Standards 5CT & 5B; Performance calculated considering API Technical Report 5C3 (Sections 9 & 10) equations,
For geometrical and steel grades combinations not considered in the API Standards 5CT and/or 5B; Performance calculations indirectly derived from API Technical Report 5C3 (Sections 9 & 10) equations,

Couplings OD are shown according to current API 5CT 10th Edition.

Couplings OD are shown according to current.APISC 170th Edition.

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Coupling	Pipe Body
Grade: P110	Grade: P110
Body: White	1st Band: White
1st Band: -	2nd Band: =
2nd Band: -	3rd Band: =
3rd Band: -	4th Band: =

Outside Diameter	4.500 in.	Wall Thickness	0.290 in.	Grade	P110
Min. Wall Thickness	87.50 %	Pipe Body Drift	API Standard	Туре	Casing
Connection OD Option	Regular				

#### Pipe Body Data

Geometry			
Nominal OD	4.500 in.	Drift	3 <b>.</b> 795 in.
Wall Thickness	0.290 in.	Plain End Weight	13.05 lb/ft
Nominal Weight	13.500 lb/ft	OD Tolerance	API
Nominal ID	3,920 in.		

Performance	
SMYS	110,000 psi
Min UTS	125,000 psi
Body Yield Strength	422 x1000 lb
Min. Internal Yield Pressure	12,410 psi
Collapse Pressure	10,690 psi
Max. Allowed Bending	112 °/100 ft

#### **Connection Data**

Geometry		Performance		Make-Up Torques	
Thread per In	8	Joint Strength	338 x1000 lb	Minimum Torque	2750 ft-lb
Connection OD	5,250 in,	Coupling Face Load	473 x1000 lb	Optimum Torque	3660 ft-lb
Hand Tight Stand Off	3 in.	Internal Pressure Capacity	12,410 psi	Maximum Torque	4580 ft-lb

#### Notes

For products according to API Standards 5CT & 5B; Performance calculated considering API Technical Report 5C3 (Sections 9 & 10) equations,
For geometrical and steel grades combinations not considered in the API Standards 5CT and/or 5B; Performance calculations indirectly derived from API Technical Report 5C3 (Sections 9 & 10) equations,

Couplings OD are shown according to current API 5CT 10th Edition.

Couplings OD are shown according to current.APISC 170th Edition.

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Sec 2, T20S, R30E SHL: 1530' FSL 1770' FEL (Sec 2) BHL: 100' FSL 1980' FEL (Sec 14)

Well Location GL: 3227'

· · cm mocuron	GE: 0227										
Point	Calls	Leases	Aliquot	Section	Township	Range	County	Lat	Long	TVD	MD
SHL	SHL: 1530' FSL & 1770' FEL (Sec 2)	Fee	NWSE	2	20S	30E	Eddy	32.5991870	- 103.9399819	0'	0'
KOP	KOP: 473' FSL & 1980' FEL (Sec 2)	Fee	SESE	2	20S	30E	Eddy	32.5962728	- 103.9406749	9,302'	9,385'
FTP	FTP/LP: 100' FNL & 1980' FEL (Sec 11)	NMNM086913	NENE	11	20S	30E	Eddy	32.5946982	- 103.9406794	9,875'	10,285'
PPP2	PPP2: 2612' FNL & 1982' FEL (Sec 11)	NMLC0070207	NESE	11	20S	30E	Eddy	32.5877943	- 103.9406773	9,878'	12,797'
PPP3	PPP3: 1324' FSL & 1984' FEL (Sec 11)	NMLC0063611	NENE	11	20S	30E	Eddy	32.5841572	- 103.9406767	9,880'	14,120'
PPP4	PPP4: 0' FNL & 1986' FEL (Sec 14)	NMNM006783A	SENE	14	20S	30E	Eddy	32.5805201	- 103.9406760	9,882'	15,443'
BHL	BHL: 100' FSL & 1980' FEL (Sec 14)	NMNM0006783	SESE	14	20S	30E	Eddy	32.5663027	- 103.9406744	9,890'	20,615'

#### GEOLOGY

Formation	Est. Top (TVD)	Lithology	Mineral Resources	Formation	Est. Top (TVD)	Lithology	Mineral Resources
Rustler	310'	Dolomite/Anhydrite	Usable Water	Delaware (Lamar)	3665'	Limestone	Oil/Natural Gas
Castile				Bell Canyon			
Salt Top	570'	Salt	None	Cherry Canyon			
Marker Bed 126	991'	Salt	None	Manzanita Marker			
Salt Base	1660'	Salt	None	Basal Brushy Canyon			
Yates	1846'	Sandstone	Oil/Natural Gas	Bone Spring	6470'	Limestone/Shale	Oil/Natural Gas
Seven Rivers				1st Bone Spring Carbonate	7357'	Limestone	Oil/Natural Gas
Queen				1st Bone Spring Sand	7700'	Sandstone	Oil/Natural Gas
Capitan	2114'	Limestone/Dolomite	Usable Water	2nd Bone Spring Carbonate	7973'	Limestone	Oil/Natural Gas
Grayburg				2nd Bone Spring Sand	8211'	Sandstone	Oil/Natural Gas
San Andres				3rd Bone Spring Carbonate	8785'	Limestone	Oil/Natural Gas
Glorietta				3rd Bone Spring Sand			
Yeso				Wolfcamp			

		Casina Proara	m Docian A			BLM Minimum Safety Factors	um Safaty Factors 1 125		actors 1.125		1.6 Dry	1.6 Dry
Casing Program Design A					BLW William Salety Factors	1.123	1.0	1.8 Wet	1.8 Wet			
Surface	26"	0'	0'	385'	385'	18 5/8" 87.5# J55 BTC	3.66	13.07	39.45	40.58		
Intermediate 1	17.5"	0'	0'	1290'	1290'	13.375" 48# H40 STC	1.13	2.53	3.11	5.22		
Intermediate 1	17.5"	1290'	1290'	1893'	1893'	13.375" 54.5# J55 STC	1.13	2.72	12.31	20.42		
Intermediate 1	17.5"	1893'	1893'	2039'	2039'	13.375" 61# J55 STC	1.42	2.86	66.81	108.02		
Intermediate 2	12.25"	0'	0'	3590'	3590'	9.625" 36# J55 LTC	1.26	2.19	3.51	4.36		
Production	8.75"	0'	0'	9385'	9302'	7" 26# P110 LTC	1.33	2.12	2.84	3.40		
Liner	6.125"	9185'	9139'	20615'	9890'	4.5" 13.5# P110 LTC	1.73	2.01	2.19	2.73		

#### All casing strings will be tested in accordance with 43 CFR Part 3172. Must have table for contingency casing.

	Y or N
Is casing new? If used, attach certification as required in Onshore Order #1	Y
Is casing API approved? If no, attach casing specification sheet.	Y
Is premium or uncommon casing planned? If yes attach casing specification sheet.	N
Does the above easing design meet or exceed BLM's minimum standards? If not provide justification (loading assumptions, easing design criteria).	Y
Will the pipe be kept at a minimum 1/3 fluid filled to avoid approaching the collapse pressure rating of the casing?	Y
Is well located within Capitan Reef?	Y
If yes, does production casing cement tie back a minimum of 50' above the Reef?	Y
Is well within the designated 4 string boundary.	Y
Is well located in SOPA but not in R-111-Q?	N
If yes, are the first 2 strings cemented to surface and 3 <sup>rd</sup> string cement tied back 500° into previous casing?	
Is well located in R-111-Q and SOPA?	Y
If yes, are the first three strings cemented to surface?	Y
Is 2 <sup>nd</sup> string set 100' to 600' below the base of salt?	Y
Is an open annulus used to satisfy R-111-Q? If yes, see cement design.	
Is an engineered weak point used to satisfy R-111-Q?	Y
If yes, at what depth is the weak point planned?	
Is well located in high Cave/Karst?	N
If yes, are there two strings cemented to surface?	
(For 2 string wells) If yes, is there a contingency casing if lost circulation occurs?	
Is well located in critical Cave/Karst?	Y
If ves, are there three strings cemented to surface?	Y

Sec 2, T20S, R30E SHL: 1530' FSL 1770' FEL (Sec 2) BHL: 100' FSL 1980' FEL (Sec 14)

Design A - Cement Program

2005								
40.60	LEAD	530	12.5	2.12	0' - 310'	1130	1000/	Class C: Salt, Gel, Extender, LCM
18.625 in	TAIL	200	14.8	1.34	310' - 385'	268	100%	Class C: Retarder
13.375 in	LEAD	830	12.5	2.12	0' - 1770'	1760	50%	Class C: Salt, Gel, Extender, LCM
13.375 III	TAIL	200	14.8	1.34	1770' - 2039'	268	30%	Class C: Retarder
1st Stg 9.625 in	LEAD	160	12.5	2.12	2089' - 2928'	340	25%	Class C: Salt, Gel, Extender, LCM
18t Stg 9.025 in	TAIL	200	14.8	1.34	2928' - 3590'	268	23%	Class C: Retarder
					9 5/8" 1	DV Tool @ 2089'		
	LEAD	310	12.5	2.12	0' - 1736'	660		Class C: Salt, Gel, Extender, LCM
2nd Stg 9.625 in	TAIL	100	14.8	1.34	1736' - 2089'	134	25%	Class C: Retarder
	LEAD	120	12.5	2.12	4590' - 6293'	260	007	Class C: Salt, Gel, Extender, LCM, Defoamer
7 in	TAIL	400	15.6	1.18	6293' - 9385'	472	0%	Class H: Retarder, Fluid Loss, Defoamer
4.5 in	LEAD	730	13.5	1.85	9185' - 20615'	1360	25%	Class H: Salt, Gel, Fluid Loss, Retarder, Dispersant, Defoamer, Anti-

#### **Pressure Control Equipment**

BOP installed and tested before drilling hole, in:	Size, in	System Rated WP	Туре		Tested to:	Rating Depth
		5M	Annular	X	2500#/3500#	-
	20		Blind Ram	X		
17.5		5M	Pipe Ram	X	5000#	20,615'
			Double Ram		3000#	
			Other*			

<sup>\*</sup>Specify if additional ram is utilized.

Equipment: Annular, Pipe Rams, Blind Rams, Other accessories to the BOP equipment will include a Kelly cock and floor safety valve (inside BOP) and choke lines and choke manifold. See attached schematics.

Variance Request: A variance is requested for the use of a flexible choke line from the BOP to the choke manifold. See attached for hydrostatic test chart. Anchors are not required by manufacturer. Variance is requested to use a multi bowl wellhead. Variance is requested to perform break testing according to attached procedure. If a breaktesting variance is approved & incorporated, API Standard 53 will be incorporated and testing annular BOP to 70% of RWP or 100% of MASP, whichever is greater, will be performed.

Testing Procedure: BOP/BOPE will be tested by an independent service company to 250 psi low and the high pressure indicated above per 43 CFR Part 3172 requirements. The System may be upgraded to a higher pressure but still tested to the working pressure listed in the table above. If the system is upgraded all the components installed will be functional and tested. Pipe rams will be operationally checked each 24 hour period. Blind rams will be operationally checked on each trip out of the hole. These checks will be noted on the daily tour sheets.

ı		Formation integrity test will be performed per 43 CFR Part 3172.
ı	Y	On Exploratory wells or on that portion of any well approved for a 5M BOPE system or greater, a pressure integrity test of each casing shoe shall be performed. Will
L		be tested in accordance with 43 CFR Part 3172.
ſ	N	Mewbourne Oil Company request a variance to use a 5000 psi annular BOP with a 10,000 psi BOP stack.

#### Mud Program

I	Depth (MD)	Mud Wt., lb/gal	Mud Type
ſ	0' - 385'	8.4 - 8.6	Fresh Water
ſ	385' - 2039'	10.0 - 10.2	Brine
ſ	2039' - 3590'	8.4 - 8.6	Fresh Water
ſ	3590' - 10285'	8.6 - 9.7	Cut-Brine
ſ	10285' - 20615'	10.0 - 12.	OBM

Sufficient mud materials to maintain mud properties and meet minimum lost circulation and weight increase requirements will be kept on location at all times.

WH - 211 1 2 4 1 2 CO 110	D DAMEST LAG S
What will be used to monitor the loss or gain of fluid?	Pason/PV1/Visual Monitoring

Sec 2, T20S, R30E SHL: 1530' FSL 1770' FEL (Sec 2) BHL: 100' FSL 1980' FEL (Sec 14)

#### **Logging and Testing Procedures**

[	Loggin	g, Coring and Testing.
	N	Will run GR/CNL from KOP (9385') to surface (horizontal well – vertical portion of hole). Stated logs run will be in the Completion Report and submitted to the BLM.
Ī	Y	No logs are planned based on well control or offset log information. Offset Well: Bloomin Onion 11/14 Fed Com 717H
	N	Coring? If yes, explain:

#### Open & Cased Hole Logs Run In the Well

Caliper		Cement Bond Log	CNL/FDC
Compensated Densilog		Compensated Neutron Log	Computer Generated Log
Dip Meter Log	V	Directional Survey	Dual Induction/Microresistivity
Dual Lateral Log/Microspherically Focused		Electric Log	Formation Density Compensated Log
Gamma Ray Log	Ø.	Measurement While Drilling	Mud Log/Geological Lithology Log
Other		Porosity-Resistivity Log	Sidewall Neutron Log
Sonic Log		Spontaneous Potential Log	Temperature Log

#### **Drilling Conditions**

Condition	Specify what type and where?
BH Pressure at deepest TVD	6171 psi
BH Temperature	165
Abnormal Temp, Pressure, or Geologic Hazards	No

Mitigation measure for abnormal conditions. Describe. Lost circulation material/s

surface hole. Weighted mud for possible over-pressure in Wolfcamp formation.

Hydrogen Sulfide (H2S) monitors will be installed prior to drilling out the surface shoe. If H2S is detected in concentrations greater than 100 ppm, the operator will comply with the provisions of Onshore Oil and Gas Order #6. If Hydrogen Sulfide is encountered, measured values and formations will be provided to the BLM.

	H2S is present
X	H2S Plan attached

Sec 2, T20S, R30E SHL: 1530' FSL 1770' FEL (Sec 2) BHL: 100' FSL 1980' FEL (Sec 14)

#### Other facets of operation

Mewbourne Oil Company also requests approval to implement additional designs as described below &/or in other attachments. BLM will be notified of elected design.

Offline Cementing Variance: Variance is requested to perform offline cementing according to the attached procedure. R-111Q: Mewbourne proposes performing Open Hole Cementing per R-111Q Guidelines if well is in Potash.

		Casing Progra	m Dosign P			BLM Minimum Safety Factors	1.125	1.0	1.6 Dry	1.6 Dry
	'	BLW William Salety Factors	1.123	1.0	1.8 Wet	1.8 Wet				
Surface	26"	0'	0'	385'	385'	18 5/8" 87.5# J55 BTC	3.66	13.07	39.45	40.58
Intermediate 1	17.5"	0'	0'	1290'	1290'	13.375" 48# H40 STC	1.13	2.53	3.11	5.22
Intermediate 1	17.5"	1290'	1290'	1893'	1893'	13.375" 54.5# J55 STC	1.13	2.72	12.31	20.42
Intermediate 1	17.5"	1893'	1893'	2039'	2039'	13.375" 61# J55 STC	1.42	2.86	66.81	108.02
Intermediate 2	12.25"	0'	0'	3590'	3590'	9.625" 36# J55 LTC	1.26	2.19	3.51	4.36
Production	8.75"	0'	0'	10285'	9875'	7" 26# P110 LTC	1.25	2.00	2.59	3.10
Liner	6.125"	9385'	9302'	20615'	9890'	4.5" 13.5# P110 LTC	1.73	2.01	2.23	2.78

#### All casing strings will be tested in accordance with 43 CFR Part 3172. Must have table for contingency casing.

se casing new? If used, attach certification as required in Onshore Order #1  y casing API approved? If no, attach casing specification sheet.  y seminum or uncommon casing planned? If yes attach casing specification sheet.  Noes the above casing design meet or exceed BLM's minimum standards? If not provide justification (loading assumptions, casing design criteria).  y Will the pipe be kept at a minimum 1/3 fluid filled to avoid approaching the collapse pressure rating of the casing?  y If yes, does production casing cement tie back a minimum of 50° above the Reef?  y If yes, does production casing cement tie back a minimum of 50° above the Reef?  y If yes, does production casing cement tie back a minimum of 50° above the Reef?  y If yes, are the first 2 strings cemented to surface and 3 <sup>rd</sup> string cement tied back 500° into previous casing?  y If yes, are the first 2 strings cemented to surface?  y If yes, are the first three strings cemented to surface?  y If yes, are the first three strings cemented to surface?  y If yes, are the first three strings cemented to surface?  y If yes, are the first three strings cement design.  s an open annulus used to satisfy R-111-Q? If yes, see cement design.  s an engineered weak point used to satisfy R-111-Q?  If yes, at what depth is the weak point planned?  y If yes, are there two strings cemented to surface?  N If yes, are there two strings cemented to surface?  N If yes, are there two strings cemented to surface?  N If yes, are there two strings cemented to surface?  N If yes, are there two strings cemented to surface?  N If yes, are there two strings cemented to surface?  Y Y If yes, see cement design if lost circulation occurs?		
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s premium or uncommon easing planned? If yes attach easing specification sheet.  Noes the above easing design meet or exceed BLM's minimum standards? If not provide justification (loading assumptions, easing design criteria).  Yill the pipe be kept at a minimum 1/3 fluid filled to avoid approaching the collapse pressure rating of the easing?  Yes well located within Capitan Reef?  If yes, does production easing cement tie back a minimum of 50° above the Reef?  Is well within the designated 4 string boundary.  Yes well located in SOPA but not in R-111-Q?  If yes, are the first 2 strings cemented to surface and 3 <sup>rd</sup> string cement tied back 500° into previous easing?  Se well located in R-111-Q and SOPA?  If yes, are the first three strings cemented to surface?  Yes an open annulus used to satisfy R-111-Q? If yes, see cement design.  Sa ne nginered weak point used to satisfy R-111-Q? If yes, see cement design.  Se well located in high Cave/Karst?  North yes, are there two strings cemented to surface?  Yes are the first three strings cemented to surface?  Yes an open annulus used to satisfy R-111-Q? If yes, see cement design.  See well located in high Cave/Karst?  North yes, are there two strings cemented to surface?  Yes are the first three are contingency casing if lost circulation occurs?  Yes well located in critical Cave/Karst?	Is casing new? If used, attach certification as required in Onshore Order #1	Y
Does the above easing design meet or exceed BLM's minimum standards? If not provide justification (loading assumptions, casing design criteria).  Y Will the pipe be kept at a minimum 1/3 fluid filled to avoid approaching the collapse pressure rating of the easing?  S well located within Capitan Reef?  If yes, does production easing cement tie back a minimum of 50' above the Reef?  Y Y  If yes, does production easing cement tie back a minimum of 50' above the Reef?  Y Y  S well located in SOPA but not in R-111-Q?  If yes, are the first 2 strings cemented to surface and 3 <sup>rd</sup> string cement tied back 500' into previous easing?  S well located in R-111-Q and SOPA?  If yes, are the first three strings cemented to surface?  Y S an open amulus used to satisfy R-111-Q? If yes, see cement design.  S an enginered weak point used to satisfy R-111-Q?  If yes, at what depth is the weak point planned?  S well located in high Cave/Karst?  N  If yes, are there two strings cemented to surface?  (For 2 string wells) If yes, is there a contingency easing if lost circulation occurs?  S well located in critical Cave/Karst?	Is casing API approved? If no, attach casing specification sheet.	Y
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If yes, does production casing eement tie back a minimum of 50° above the Reef?  Is well within the designated 4 string boundary.  S well located in SOPA but not in R-111-Q?  If yes, are the first 2 strings cemented to surface and 3° string cement tied back 500° into previous casing?  S well located in R-111-Q and SOPA?  If yes, are the first three strings cemented to surface?  Y If yes, are the first three strings cemented to surface?  Y Is 2° string set 100° to 600° below the base of salt?  S an open annulus used to satisfy R-111-Q?  Y If yes, at what depth is the weak point used to satisfy R-111-Q?  Y If yes, at what depth is the weak point planned?  S well located in high Cave/Karst?  N If yes, are there two strings cemented to surface?  (For 2 string wells) If yes, is there a contingency casing if lost circulation occurs?  S well located in critical Cave/Karst?		
Is well within the designated 4 string boundary.  s well located in SOPA but not in R-111-Q?  If yes, are the first 2 strings cemented to surface and 3 <sup>rd</sup> string cement tied back 500° into previous easing?  s well located in R-111-Q and SOPA?  If yes, are the first three strings cemented to surface?  Y Y  Is 2 <sup>rd</sup> string set 100° to 600° below the base of salt?  s an open annulus used to satisfy R-111-Q? If yes, see cement design.  s ne enginered weak point used to satisfy R-111-Q?  If yes, at what depth is the weak point planned?  s well located in high Cave/Karst?  N  If yes, are there two strings cemented to surface?  (For 2 string wells) If yes, is there a contingency casing if lost circulation occurs?  s well located in critical Cave/Karst?	Is well located within Capitan Reef?	Y
s well located in SOPA but not in R-111-Q?  If yes, are the first 2 strings cemented to surface and 3 <sup>rd</sup> string cement tied back 500' into previous casing?  s well located in R-111-Q and SOPA?  If yes, are the first three strings cemented to surface?  If yes are the first three strings cemented to surface?  Y Is 2 <sup>rd</sup> string set 100' to 600' below the base of salt?  Y an open annulus used to satisfy R-111-Q? If yes, see cement design.  s an enginered weak point used to satisfy R-111-Q?  If yes, at what depth is the weak point planned?  s well located in high Cave/Karst?  N  If yes, are there two strings cemented to surface?  (For 2 string wells) If yes, is there a contingency casing if lost circulation occurs?  s well located in critical Cave/Karst?	If yes, does production casing cement tie back a minimum of 50° above the Reef?	Y
If yes, are the first 2 strings cemented to surface and 3 <sup>rd</sup> string cement tied back 500° into previous casing?  s well located in R-111-Q and SOPA?  If yes, are the first three strings cemented to surface?  If yes, are the first three strings cemented to surface?  Y  Is 2 <sup>rd</sup> string set 100° to 600° below the base of salt?  s an open annulus used to satisfy R-111-Q? If yes, see cement design.  s an engineered weak point used to satisfy R-111-Q?  If yes, at what depth is the weak point planned?  s well located in high Cave/Karst?  N  If yes, are there two strings cemented to surface?  (For 2 string wells) If yes, is there a contingency casing if lost circulation occurs?  s well located in critical Cave/Karst?	Is well within the designated 4 string boundary.	Y
If yes, are the first 2 strings cemented to surface and 3 <sup>rd</sup> string cement tied back 500° into previous casing?  s well located in R-111-Q and SOPA?  If yes, are the first three strings cemented to surface?  If yes, are the first three strings cemented to surface?  Y  Is 2 <sup>rd</sup> string set 100° to 600° below the base of salt?  s an open annulus used to satisfy R-111-Q? If yes, see cement design.  s an engineered weak point used to satisfy R-111-Q?  If yes, at what depth is the weak point planned?  s well located in high Cave/Karst?  N  If yes, are there two strings cemented to surface?  (For 2 string wells) If yes, is there a contingency casing if lost circulation occurs?  s well located in critical Cave/Karst?		
s well located in R-111-Q and SOPA?  If yes, are the first three strings cemented to surface?  If yes, are the first three strings cemented to surface?  Is 2 <sup>nd</sup> string set 100' to 600' below the base of salt?  If yes, an open annulus used to satisfy R-111-Q? If yes, see cement design.  If yes, at what depth is the weak point planned?  If yes, at what depth is the weak point planned?  If yes, are there two strings cemented to surface?  If yes, are there two strings cemented to surface?  (For 2 string wells) If yes, is there a contingency casing if lost circulation occurs?  If yes, are there two strings cemented to surface?  (For 2 string wells) If yes, is there a contingency casing if lost circulation occurs?  If yes, are there two strings cemented to surface?  (For 2 string wells) If yes, is there a contingency casing if lost circulation occurs?  Y	Is well located in SOPA but not in R-111-Q?	N
If yes, are the first three strings cemented to surface?  Is 2 <sup>m2</sup> string set 100′ to 600′ below the base of salt?  S an open annulus used to satisfy R-111-Q² If yes, see cement design.  S an engineered weak point used to satisfy R-111-Q² If yes, see cement design.  Y  If yes, at what depth is the weak point planned?  S well located in high Cave/Karst?  N  If yes, are there two strings cemented to surface?  (For 2 string wells) If yes, is there a contingency casing if lost circulation occurs?  S well located in critical Cave/Karst?  Y	If yes, are the first 2 strings cemented to surface and 3 <sup>rd</sup> string cement tied back 500° into previous casing?	
If yes, are the first three strings cemented to surface?  Is 2 <sup>m2</sup> string set 100′ to 600′ below the base of salt?  S an open annulus used to satisfy R-111-Q² If yes, see cement design.  S an engineered weak point used to satisfy R-111-Q² If yes, see cement design.  Y  If yes, at what depth is the weak point planned?  S well located in high Cave/Karst?  N  If yes, are there two strings cemented to surface?  (For 2 string wells) If yes, is there a contingency casing if lost circulation occurs?  S well located in critical Cave/Karst?  Y		
Is 2 <sup>nd</sup> string set 100' to 600' below the base of salt?  8 an open annulus used to satisfy R-111-Q' If yes, see cement design.  8 an enginered weak point used to satisfy R-111-Q'  If yes, at what depth is the weak point planned?  8 well located in high Cave/Karst?  If yes, are there two strings cemented to surface?  (For 2 string wells) If yes, is there a contingency casing if lost circulation occurs?  8 well located in critical Cave/Karst?  Y	Is well located in R-111-Q and SOPA?	Y
s an open annulus used to satisfy R-111-Q? If yes, see cement design.  s an engineered weak point used to satisfy R-111-Q?  If yes, at what depth is the weak point planned?  s well located in high Cave/Karst?  If yes, are there two strings cemented to surface?  (For 2 string wells) If yes, is there a contingency casing if lost circulation occurs?  s well located in critical Cave/Karst?  y		Y
s an engineered weak point used to satisfy R-111-Q?  If yes, at what depth is the weak point planned?  s well located in high Cave/Karst?  If yes, are there two strings cemented to surface?  (For 2 string wells) If yes, is there a contingency casing if lost circulation occurs?  s well located in critical Cave/Karst?  Y		Y
If yes, at what depth is the weak point planned?  s well located in high Cave/Karst?  If yes, are there two strings cemented to surface?  (For 2 string wells) If yes, is there a contingency casing if lost circulation occurs?  s well located in critical Cave/Karst?  Y	Is an open annulus used to satisfy R-111-Q? If yes, see cement design.	
s well located in high Cave/Karst?  If yes, are there two strings cemented to surface?  (For 2 string wells) If yes, is there a contingency casing if lost circulation occurs?  s well located in critical Cave/Karst?  Y	Is an engineered weak point used to satisfy R-111-Q?	Y
If yes, are there two strings cemented to surface? (For 2 string wells) If yes, is there a contingency casing if lost circulation occurs? s well located in critical Cave/Karst?  Y	If yes, at what depth is the weak point planned?	
If yes, are there two strings cemented to surface? (For 2 string wells) If yes, is there a contingency casing if lost circulation occurs? s well located in critical Cave/Karst?  Y		
(For 2 string wells) If yes, is there a contingency casing if lost circulation occurs?  s well located in critical Cave/Karst?  Y	Is well located in high Cave/Karst?	N
s well located in critical Cave/Karst?		
	(For 2 string wells) If yes, is there a contingency casing if lost circulation occurs?	
If yes, are there three strings cemented to surface?	Is well located in critical Cave/Karst?	Y
	If yes, are there three strings cemented to surface?	Y

Design B - Cement Program

Design D Cen								
18.625 in	LEAD	530	12.5	2.12	0' - 310'	1130	100%	Class C: Salt, Gel, Extender, LCM
18.025 III	TAIL	200	14.8	1.34	310' - 385'	268	100%	Class C: Retarder
13.375 in	LEAD	830	12.5	2.12	0' - 1770'	1760	50%	Class C: Salt, Gel, Extender, LCM
13.373 III	TAIL	200	14.8	1.34	1770' - 2039'	268	3076	Class C: Retarder
1st Stg 9.625 in	LEAD	160	12.5	2.12	2089' - 2928'	340	25%	Class C: Salt, Gel, Extender, LCM
18t Stg 9.025 in	TAIL	200	14.8	1.34	2928' - 3590'	268	23%	Class C: Retarder
					9 5/8'	' DV Tool @ 2089'		
	LEAD	310	12.5	2.12	0' - 1736'	660		Class C: Salt, Gel, Extender, LCM
2nd Stg 9.625 in	TAIL	100	14.8	1.34	1736' - 2089'	134	25%	Class C: Retarder
7 in	LEAD	190	12.5	2.12	4590' - 7237'	410	0%	Class C: Salt, Gel, Extender, LCM, Defoamer
/ III	TAIL	400	15.6	1.18	7237' - 10285'	472	0%	Class H: Retarder, Fluid Loss, Defoamer
4.5 in	LEAD			1.85	9385' - 20615'	1320	25%	Class H: Salt, Gel, Fluid Loss, Retarder, Dispersant, Defoamer, Anti- settling Agent

### **Mewbourne Oil Company**

Eddy County, New Mexico NAD 83 Bloomin Onion 11/14 Fed Com #715H Sec 02, T20S, R30E

SHL: 1530' FSL & 1770' FEL (Sec 2) BHL: 100' FSL & 1980' FEL (Sec 14)

Plan: Design #1

### **Standard Planning Report**

24 March, 2025

Database: Hobbs

Company: Mewbourne Oil Company

Project: Eddy County, New Mexico NAD 83 Bloomin Onion 11/14 Fed Com #715H

Well: Sec 02, T20S, R30E

Wellbore: BHL: 100' FSL & 1980' FEL (Sec 14)

Design: Design #1 Local Co-ordinate Reference:

TVD Reference: MD Reference: North Reference:

Survey Calculation Method:

Site Bloomin Onion 11/14 Fed Com #715H WELL @ 3255.0usft (Original Well Elev) WELL @ 3255.0usft (Original Well Elev)

Minimum Curvature

Project Eddy County, New Mexico NAD 83

Map System: Geo Datum:

Map Zone:

Site:

US State Plane 1983 North American Datum 1983 New Mexico Eastern Zone

System Datum:

Ground Level

Bloomin Onion 11/14 Fed Com #715H Site

Northing: 581,939.00 usft Site Position: Latitude: 32.5991870 From: Мар Easting: 662,472.50 usft Longitude: -103.9399820

**Position Uncertainty:** 0.0 usft Slot Radius: 13-3/16 "

Well Sec 02, T20S, R30E

**Well Position** +N/-S 0.0 usft Northing: 581,939.00 usft Latitude: 32.5991870 +E/-W 0.0 usft Easting: 662,472.50 usft Longitude: -103.9399820

**Position Uncertainty** 0.0 usft Wellhead Elevation: 3,255.0 usft Ground Level: 3,227.0 usft

0.21° **Grid Convergence:** 

Wellbore BHL: 100' FSL & 1980' FEL (Sec 14)

Magnetics **Model Name** Sample Date Declination Dip Angle Field Strength (°) (°) (nT) 7.35 48,423.67065530 IGRF2010 12/31/2014 60.38

Design #1 Design

Audit Notes:

**PROTOTYPE** Tie On Depth: 0.0 Version: Phase:

Vertical Section: Depth From (TVD) +N/-S +E/-W Direction (usft) (usft) (usft) (°) 0.0 180.81 0.0 0.0

Plan Survey Tool Program Date 3/24/2025

**Depth From** Depth To

(usft) (usft) Survey (Wellbore) Tool Name Remarks

0.0 20,615.9 Design #1 (BHL: 100' FSL & 1980

lan Sections										
Measured Depth (usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)	TFO (°)	Target
0.0	0.00	0.00	0.0	0.0	0.0	0.00	0.00	0.00	0.00	
2,039.0	0.00	0.00	2,039.0	0.0	0.0	0.00	0.00	0.00	0.00	
2,490.1	9.02	191.17	2,488.3	<b>-</b> 34.8	<b>-6.</b> 9	2.00	2.00	0.00	191.17	
8,934.3	9.02	191.17	8,852.7	-1,026.2	-202.6	0.00	0.00	0.00	0.00	
9,385.5	0.00	0.00	9,302.0	-1,061.0	-209.5	2.00	<b>-</b> 2.00	0.00	180.00	KOP: 473' FSL & 1980
10,284.7	89.92	179.79	9,875.0	-1,633.2	-207.4	10.00	10.00	0.00	179.79	
20,615.9	89.92	179.79	9,890.0	-11,964.3	-169.1	0.00	0.00	0.00	0.00	BHL: 100' FSL & 1980

Database: Hobbs

Company: Mewbourne Oil Company

Project: Eddy County, New Mexico NAD 83
Site: Bloomin Onion 11/14 Fed Com #715H

Well: Sec 02, T20S, R30E

**Wellbore:** BHL: 100' FSL & 1980' FEL (Sec 14)

Design: Design #1

Local Co-ordinate Reference:

TVD Reference: MD Reference: North Reference:

Survey Calculation Method:

Site Bloomin Onion 11/14 Fed Com #715H WELL @ 3255.0usft (Original Well Elev) WELL @ 3255.0usft (Original Well Elev)

Grid

ed Survey									
Measured Depth (usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Vertical Section (usft)	Dogleg Rate (°/100usft)	Bui <b>l</b> d Rate (°/100usft)	Turn Rate (°/100usft)
0.0	0.00 SL & 1770' FEL	0.00	0.0	0.0	0.0	0.0	0.00	0.00	0.00
		, ,	50.0				0.00	0.00	2.22
50.0	0.00	0.00	50.0	0.0	0.0	0.0	0.00	0.00	0.00
100.0	0.00	0.00	100.0	0.0	0.0	0.0	0.00	0.00	0.00
150.0	0.00	0.00	150.0	0.0	0.0	0.0	0.00	0.00	0.00
200.0	0.00	0.00	200.0	0.0	0.0	0.0	0.00	0.00	0.00
250.0	0.00	0.00	250.0	0.0	0.0	0.0	0.00	0.00	0.00
300.0	0.00	0.00	300.0	0.0	0.0	0.0	0.00	0.00	0.00
350.0	0.00	0.00	350.0	0.0	0.0	0.0	0.00	0.00	0.00
400.0	0.00	0.00	400.0	0.0	0.0	0.0	0.00	0.00	0.00
450.0	0.00	0.00	450.0	0.0	0.0	0.0	0.00	0.00	0.00
500.0	0.00	0.00	500.0	0.0	0.0	0.0	0.00	0.00	0.00
550.0	0.00	0.00	550.0	0.0	0.0	0.0	0.00	0.00	0.00
600.0	0.00	0.00	600.0	0.0	0.0	0.0	0.00	0.00	0.00
650.0	0.00	0.00	650.0	0.0	0.0	0.0	0.00	0.00	0.00
700.0	0.00	0.00	700.0	0.0	0.0	0.0	0.00	0.00	0.00
750.0	0.00	0.00	750.0	0.0	0.0	0.0	0.00	0.00	0.00
800.0	0.00	0.00	800.0	0.0	0.0	0.0	0.00	0.00	0.00
850.0	0.00	0.00	850.0	0.0	0.0	0.0	0.00	0.00	0.00
900.0				0.0	0.0	0.0	0.00		
900 <u>.</u> 0 950.0	0.00	0.00	900.0	0.0			0.00	0.00	0.00
	0.00	0.00	950.0		0.0	0.0		0.00	0.00
1,000.0	0.00	0.00	1,000.0	0.0	0.0	0.0	0.00	0.00	0.00
1,050.0	0.00	0.00	1,050.0	0.0	0.0	0.0	0.00	0.00	0.00
1,100.0	0.00	0.00	1,100.0	0.0	0.0	0.0	0.00	0.00	0.00
1,150.0	0.00	0.00	1,150.0	0.0	0.0	0.0	0.00	0.00	0.00
1,200.0	0.00	0.00	1,200.0	0.0	0.0	0.0	0.00	0.00	0.00
1,250.0	0.00	0.00	1,250.0	0.0	0.0	0.0	0.00	0.00	0.00
1,300.0	0.00	0.00	1,300.0	0.0	0.0	0.0	0.00	0.00	0.00
1,350.0	0.00	0.00	1,350.0	0.0	0.0	0.0	0.00	0.00	0.00
1,400.0	0.00	0.00	1,400.0	0.0	0.0	0.0	0.00	0.00	0.00
1,450.0	0.00	0.00	1,450.0	0.0	0.0	0.0	0.00	0.00	0.00
1,500.0	0.00	0.00	1,500.0	0.0	0.0	0.0	0.00	0.00	0.00
1,550.0	0.00	0.00	1,550.0	0.0	0.0	0.0	0.00	0.00	0.00
1,600.0	0.00	0.00	1,600.0	0.0	0.0	0.0	0.00	0.00	0.00
1,650.0	0.00	0.00	1,650.0	0.0	0.0	0.0	0.00	0.00	0.00
1,700.0	0.00	0.00	1,700.0	0.0	0.0	0.0	0.00	0.00	0.00
			,						
1,750.0	0.00	0.00	1,750.0	0.0	0.0	0.0	0.00	0.00	0.00
1,800.0	0.00	0.00	1,800.0	0.0	0.0	0.0	0.00	0.00	0.00
1,850.0	0.00	0.00	1,850.0	0.0	0.0	0.0	0.00	0.00	0.00
1,900.0	0.00	0.00	1,900.0	0.0	0.0	0.0	0.00	0.00	0.00
1,950.0	0.00	0.00	1,950.0	0.0	0.0	0.0	0.00	0.00	0.00
2,000.0	0.00	0.00	2,000.0	0.0	0.0	0.0	0.00	0.00	0.00
2,039.0	0.00	0.00	2,039.0	0.0	0.0	0.0	0.00	0.00	0.00
2,050.0	0.22	191.17	2,050.0	0.0	0.0	0.0	2.00	2.00	0.00
2,100.0	1.22	191.17	2,100.0	-0.6	-0.1	0.6	2.00	2.00	0.00
2,150.0	2.22	191.17	2,150.0	-2.1	-0.4	2.1	2.00	2.00	0.00
2,200.0	3.22	191.17	2,199.9	<b>-</b> 4.4	-0.9	4.4	2.00	2.00	0.00
2,250.0	4.22	191.17	2,249.8	<del>-</del> 7.6	<b>-</b> 1.5	7.6	2.00	2.00	0.00
2,300.0	5.22	191.17	2,299.6	<b>-</b> 11.7	<b>-</b> 2.3	11.7	2.00	2.00	0.00
2,350.0	6.22	191.17	2,349.4	<b>-</b> 16.5	-3.3	16.6	2.00	2.00	0.00
2,400.0	7.22	191.17	2,399.0	<del>-</del> 22.3	-4.4	22.3	2.00	2.00	0.00
2,450.0	8.22	191.17	2.448.6	-28.9	-5.7	29.0	2.00	2.00	0.00
2,450.0 2,490.1	9.02	191.17	2,446.6 2,488.3	-26.9 -34.8	-5.7 -6.9	29.0 34.9	2.00	2.00 2.00	0.00
/ 49U. l	9.02	191.17	۷,400.3	-34.0	-0.9	34.9	∠.00	∠.00	0.00

Database: Hobbs

Company: Mewbourne Oil Company

Project: Eddy County, New Mexico NAD 83
Site: Bloomin Onion 11/14 Fed Com #715H

Well: Sec 02, T20S, R30E

**Wellbore:** BHL: 100' FSL & 1980' FEL (Sec 14)

Design: Design #1

Local Co-ordinate Reference:

TVD Reference: MD Reference: North Reference:

Survey Calculation Method:

Site Bloomin Onion 11/14 Fed Com #715H WELL @ 3255.0usft (Original Well Elev) WELL @ 3255.0usft (Original Well Elev)

Grid

Planned Survey									
Measured Depth (usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Vertical Section (usft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)
2,550.0	9.02	191.17	2,547.4	<b>-</b> 44.0	<b>-</b> 8.7	44.1	0.00	0.00	0.00
2,600.0	9.02	191.17	2,596.8	<b>-</b> 51.7	<del>-</del> 10.2	51.8	0.00	0.00	0.00
2,650.0	9.02	191.17	2,646.2	-59.4	-11.7	59.5	0.00	0.00	0.00
2,700.0	9.02	191.17	2,695.5	-67.1	-13.2	67.2	0.00	0.00	0.00
2,750.0	9.02	191.17	2,744.9	-74.8	-14.8	75.0	0.00	0.00	0.00
2,800.0	9.02	191.17	2,794.3	-82.4	-16.3	82.7	0.00	0.00	0.00
2,850.0	9.02	191.17	2,843.7	-90.1	-17.8	90.4	0.00	0.00	0.00
2,900.0	9.02	191.17	2,893.1	<b>-</b> 97.8	<b>-</b> 19.3	98.1	0.00	0.00	0.00
2,950.0	9.02	191.17	2,942.4	<b>-</b> 105.5	<del>-</del> 20.8	105.8	0.00	0.00	0.00
3,000.0	9.02	191.17	2,991.8	-113.2	-22.4	113.5	0.00	0.00	0.00
3,050.0	9.02	191.17	3,041.2	-120.9	-23.9	121.2	0.00	0.00	0.00
3,100.0	9.02	191.17	3,090.6	<b>-</b> 128.6	<b>-</b> 25.4	129.0	0.00	0.00	0.00
3,150.0	9.02	191.17	3,140.0	-136.3	-26.9	136.7	0.00	0.00	0.00
3,200.0	9.02	191.17	3,189.4	-144.0	-28.4	144.4	0.00	0.00	0.00
3,250.0	9.02	191.17	3,238.7	-151.7	-30.0	152.1	0.00	0.00	0.00
3,300.0	9.02	191.17	3,288.1	-159.4	-31.5	159.8	0.00	0.00	0.00
3,350.0	9.02	191.17	3,337.5	-167.1	-33.0	167.5	0.00	0.00	0.00
3,400.0	9.02	191.17	3,386.9	<b>-</b> 174.8	<b>-</b> 34.5	175.2	0.00	0.00	0.00
3,450.0	9.02	191.17	3,436.3	<del>-</del> 182.5	<b>-</b> 36.0	182.9	0.00	0.00	0.00
3,500.0	9.02	191.17	3,485.6	-190.1	<b>-</b> 37.5	190.7	0.00	0.00	0.00
3,550.0	9.02	191.17	3,535.0	-197.8	-39.1	198.4	0.00	0.00	0.00
3,600.0	9.02	191.17	3,584.4	<b>-</b> 205.5	<b>-</b> 40.6	206.1	0.00	0.00	0.00
3,650.0	9.02	191.17	3,633.8	-213.2	-42.1	213.8	0.00	0.00	0.00
3,700.0	9.02	191.17	3,683.2	-220.9	-43.6	221.5	0.00	0.00	0.00
3,750.0	9.02	191.17	3,732.5	-228.6	-45.1	229.2	0.00	0.00	0.00
3,800.0	9.02	191.17	3,781.9	-236.3	-46.7	236.9	0.00	0.00	0.00
3,850.0	9.02	191.17	3,831.3	-244.0	-48.2	244.7	0.00	0.00	0.00
3,900.0	9.02	191.17	3,880.7	<b>-</b> 251.7	<b>-</b> 49.7	252.4	0.00	0.00	0.00
3,950.0	9.02	191.17	3,930.1	<b>-</b> 259.4	<b>-</b> 51.2	260.1	0.00	0.00	0.00
4,000.0	9.02	191.17	3,979.5	-267.1	<b>-</b> 52.7	267.8	0.00	0.00	0.00
4,050.0	9.02	191.17	4,028.8	-274.8	<b>-</b> 54.3	275.5	0.00	0.00	0.00
4,100.0	9.02	191.17	4,078.2	-282.5	<b>-</b> 55.8	283.2	0.00	0.00	0.00
4,150.0	9.02	191.17	4,127.6	-290.1	-57.3	290.9	0.00	0.00	0.00
4,200.0	9.02	191.17	4,177.0	-297.8	-58.8	298.6	0.00	0.00	0.00
4,250.0	9.02	191.17	4,226.4	-305.5	-60.3	306.4	0.00	0.00	0.00
4,300.0	9.02	191.17	4,275.7	-313.2	-61.8	314.1	0.00	0.00	0.00
4,350.0	9.02	191.17	4,325.1	-320.9	-63.4	321.8	0.00	0.00	0.00
4,400.0	9.02	191.17	4,374.5	-328.6	-64.9	329.5	0.00	0.00	0.00
4,450.0	9.02	191.17	4,423.9	-336.3	-66.4	337.2	0.00	0.00	0.00
4,500.0	9.02	191.17	4,473.3	<b>-</b> 344.0	<b>-</b> 67.9	344.9	0.00	0.00	0.00
4,550.0	9.02	191.17	4,522.7	-351.7	-69.4	352.6	0.00	0.00	0.00
4,600.0	9.02	191.17	4,572.0	<b>-</b> 359.4	<del>-</del> 71.0	360.3	0.00	0.00	0.00
4,650.0	9.02	191.17	4,621.4	-367.1	-72.5	368.1	0.00	0.00	0.00
4,700.0	9.02	191.17	4,670.8	-374.8	-74.0	375.8	0.00	0.00	0.00
4,750.0	9.02	191.17	4,720.2	-382.5	-75.5	383.5	0.00	0.00	0.00
4,800.0	9.02	191.17	4,769.6	-390.2	-77.0	391.2	0.00	0.00	0.00
4,850.0	9.02	191.17	4,818.9	-397.8	-78.6	398.9	0.00	0.00	0.00
4,900.0	9.02	191.17	4,868.3	-405.5	<b>-</b> 80.1	406.6	0.00	0.00	0.00
4,950.0	9.02	191.17	4,917.7	-413.2	<b>-</b> 81.6	414.3	0.00	0.00	0.00
5,000.0	9.02	191.17	4,967.1	<b>-</b> 420.9	<b>-</b> 83.1	422.1	0.00	0.00	0.00
5,050.0	9.02	191.17	5,016.5	-428.6	<b>-</b> 84.6	429.8	0.00	0.00	0.00
5,100.0	9.02	191.17	5,065.8	<b>-</b> 436.3	<b>-</b> 86.2	437.5	0.00	0.00	0.00
5,150.0	9.02	191.17	5,115.2	-444.0	-87.7	445.2	0.00	0.00	0.00
5,200.0	9.02	191.17	5,164.6	-451.7	-89.2	452.9	0.00	0.00	0.00

Hobbs Database: Company:

Project:

Site:

Mewbourne Oil Company

Eddy County, New Mexico NAD 83 Bloomin Onion 11/14 Fed Com #715H

Well: Sec 02, T20S, R30E

BHL: 100' FSL & 1980' FEL (Sec 14) Wellbore:

Design: Design #1 Local Co-ordinate Reference:

TVD Reference: MD Reference: North Reference:

Survey Calculation Method:

Site Bloomin Onion 11/14 Fed Com #715H WELL @ 3255.0usft (Original Well Elev) WELL @ 3255.0usft (Original Well Elev)

Planned Survey									
Measured Depth (usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Vertical Section (usft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)
5,250.0	9.02	191.17	5,214.0	<del>-</del> 459.4	<b>-</b> 90.7	460.6	0.00	0.00	0.00
5,300.0	9.02	191.17	5,263.4	<b>-</b> 467.1	<b>-</b> 92.2	468.3	0.00	0.00	0.00
5,350.0	9.02	191.17	5,312.8	<b>-</b> 474.8	<b>-</b> 93.7	476.0	0.00	0.00	0.00
5,400.0	9.02	191.17	5,362.1	-482.5	-95.3	483.8	0.00	0.00	0.00
5,450.0	9.02	191.17	5,411.5	-490.2	-96.8	491.5	0.00	0.00	0.00
5,500.0	9.02	191.17	5,460.9	-497.8	-98.3	499.2	0.00	0.00	0.00
5,550.0	9.02	191.17	5,510.3	-505.5	-99.8	506.9	0.00	0.00	0.00
5,600.0	9.02	191.17	5,559.7	-513.2	-101.3	514.6	0.00	0.00	0.00
5,650.0	9.02	191.17	5,609.0	<b>-</b> 520.9	<b>-</b> 102.9	522.3	0.00	0.00	0.00
5,700.0	9.02	191.17	5,658.4	<b>-</b> 528.6	-104.4 105.0	530.0	0.00	0.00	0.00
5,750.0 5,800.0	9.02 9.02	191.17 191.17	5,707.8 5,757.2	<b>-</b> 536.3 <b>-</b> 544.0	-105.9 -107.4	537.8 545.5	0.00 0.00	0.00 0.00	0.00 0.00
	9.02 9.02	191.17		-544.0 -551.7		553.2	0.00	0.00	0.00
5,850.0			5,806.6		-108.9				
5,900.0	9.02	191.17	5,855.9	-559.4	-110.5	560.9	0.00	0.00	0.00
5,950.0	9.02	191.17	5,905.3	-567.1	-112.0	568.6	0.00	0.00	0.00
6,000 <b>.</b> 0	9.02	191.17	5,954.7	-574.8	-113.5	576.3	0.00	0.00	0.00
6,050.0	9.02	191.17	6,004.1	-582.5	-115.0	584.0	0.00	0.00	0.00
6,100.0	9.02	191.17	6,053.5	-590.2	-116.5	591.7	0.00	0.00	0.00
6,150.0	9.02	191.17	6,102.9	<b>-</b> 597.9	-118.0	599.5	0.00	0.00	0.00
6,200.0	9.02	191.17	6,152.2	-605.5	-119.6	607.2	0.00	0.00	0.00
6,250.0	9.02	191.17	6,201.6	-613.2	-121.1	614.9	0.00	0.00	0.00
6,300.0	9.02	191.17	6,251.0	-620.9	-122.6	622.6	0.00	0.00	0.00
6,350.0	9.02	191.17	6,300.4	<del>-</del> 628.6	-124.1	630.3	0.00	0.00	0.00
0.400.0	0.00	101 17	0.040.0	000.0	105.0	620.0	0.00	0.00	0.00
6,400 <b>.</b> 0 6,450 <b>.</b> 0	9.02 9.02	191.17 191.17	6,349.8 6,399.1	-636.3 -644.0	-125.6 -127.2	638.0 645.7	0.00 0.00	0.00 0.00	0.00 0.00
6,500.0	9.02	191.17	6,448.5	-644.0 -651.7	-127.2 -128.7	653.5	0.00	0.00	0.00
6,550.0	9.02	191.17	6,497.9	-659.4	-130.2	661.2	0.00	0.00	0.00
6,600.0	9.02	191.17	6,547.3	-667.1	-131.7	668.9	0.00	0.00	0.00
6,650.0	9.02	191.17	6,596.7	<b>-</b> 674.8	-133.2	676.6	0.00	0.00	0.00
6,700.0	9.02	191.17	6,646.0	<b>-</b> 682.5	-134.8	684.3	0.00	0.00	0.00
6,750.0	9.02	191.17	6,695.4	<b>-</b> 690.2	-136.3	692.0	0.00	0.00	0.00
6,800.0	9.02	191.17	6,744.8	<b>-</b> 697.9	-137.8	699.7	0.00	0.00	0.00
6,850.0	9.02	191.17	6,794.2	<del>-</del> 705.5	-139.3	707.4	0.00	0.00	0.00
6,900.0	9.02	191.17	6,843.6	-713.2	-140.8	715.2	0.00	0.00	0.00
6,950 <b>.</b> 0	9.02	191.17	6,893.0	-720.9	-142.4	722.9	0.00	0.00	0.00
7,000.0	9.02	191.17	6,942.3	-728.6	-143.9	730.6	0.00	0.00	0.00
7,050.0	9.02	191.17	6,991.7	-736.3	-145.4	738.3	0.00	0.00	0.00
7,100.0	9.02	191.17	7,041.1	-744.0	-146.9	746.0	0.00	0.00	0.00
7,150.0	9.02	191.17	7,090.5	<b>-</b> 751.7	-148.4	753.7	0.00	0.00	0.00
7,200.0	9.02	191.17	7,139.9	-759.4	-149.9	761.4	0.00	0.00	0.00
7,250.0	9.02	191.17	7,189.2	<b>-</b> 767.1	-151.5	769.2	0.00	0.00	0.00
7,300.0	9.02	191.17	7,238.6	-774.8	-153.0	776.9	0.00	0.00	0.00
7,350.0	9.02	191.17	7,288.0	<del>-</del> 782.5	-154.5	784.6	0.00	0.00	0.00
7,400.0	9.02	191.17	7,337.4	-790.2	-156.0	792.3	0.00	0.00	0.00
7,400 <b>.</b> 0 7,450 <b>.</b> 0	9.02 9.02	191.17	7,337 <b>.</b> 4 7,386 <b>.</b> 8	-790.2 -797.9	-156.0 -157.5	792.3 800.0	0.00	0.00	0.00
7,430 <b>.</b> 0 7,500 <b>.</b> 0	9.02	191.17	7,366.6 7,436.2	-797.9 -805.6	-157.5 -159.1	807.7	0.00	0.00	0.00
7,550 <b>.</b> 0	9.02	191.17	7,436.2 7,485.5	-813.2	-160.6	815.4	0.00	0.00	0.00
7,600.0	9.02	191.17	7,534.9	-820.9	-162.1	823.1	0.00	0.00	0.00
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7,650.0	9.02	191.17	7,584.3	<b>-</b> 828.6	-163.6	830.9	0.00	0.00	0.00
7,700.0	9.02	191.17	7,633.7	<b>-</b> 836.3	<b>-</b> 165.1	838.6	0.00	0.00	0.00
7,750.0	9.02	191.17	7,683.1	<b>-</b> 844.0	<b>-</b> 166.7	846.3	0.00	0.00	0.00
7,800.0	9.02	191.17	7,732.4	<b>-</b> 851.7	<b>-</b> 168.2	854.0 864.7	0.00	0.00	0.00
7,850.0	9.02	191.17	7,781.8	<b>-</b> 859.4	-169.7	861.7	0.00	0.00	0.00
7,900.0	9.02	191.17	7,831.2	-867.1	-171.2	869.4	0.00	0.00	0.00

Database: Hobbs

Company: Mewbourne Oil Company

Project: Eddy County, New Mexico NAD 83
Site: Bloomin Onion 11/14 Fed Com #715H

Well: Sec 02, T20S, R30E

Wellbore: BHL: 100' FSL & 1980' FEL (Sec 14)

Design: Design #1

Local Co-ordinate Reference:

TVD Reference: MD Reference: North Reference:

Survey Calculation Method:

Site Bloomin Onion 11/14 Fed Com #715H WELL @ 3255.0usft (Original Well Elev) WELL @ 3255.0usft (Original Well Elev)

Grid

ın:	Design #1								
ned Survey									
Measured Depth (usft)	d Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Vertical Section (usft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)
7,950	0.0 9.02	191.17	7,880.6	<b>-</b> 874.8	-172.7	877.1	0.00	0.00	0.00
8,000	0.0 9.02	191.17	7,930.0	-882.5	-174.2	884.9	0.00	0.00	0.00
8,050	0.0 9.02	191.17	7,979.3	-890.2	-175.8	892.6	0.00	0.00	0.00
8,100	0.0 9.02	191.17	8,028.7	<b>-</b> 897.9	<b>-</b> 177.3	900.3	0.00	0.00	0.00
8,150	0.0 9.02	191.17	8,078.1	-905.6	-178.8	908.0	0.00	0.00	0.00
8,200		191.17	8,127.5	-913.2	-180.3	915.7	0.00	0.00	0.00
8,250		191.17	8,176.9	-920.9	-181.8	923.4	0.00	0.00	0.00
8,300		191.17	8,226.3	-928.6	-183.4	931.1	0.00	0.00	0.00
8,350		191.17	8,275.6	-936.3	-184.9	938.8	0.00	0.00	0.00
8,400		191.17	8,325.0	<b>-</b> 944.0	<b>-</b> 186.4	946.6	0.00	0.00	0.00
8,450		191.17	8,374.4	<b>-</b> 951.7	<b>-</b> 187.9	954.3	0.00	0.00	0.00
8,500		191.17	8,423.8	<b>-</b> 959.4	<b>-</b> 189.4	962.0	0.00	0.00	0.00
8,550		191.17	8,473.2	<b>-</b> 967.1	<b>-</b> 191.0	969.7	0.00	0.00	0.00
8,600	0.0 9.02	191.17	8,522.5	<b>-</b> 974.8	<b>-</b> 192.5	977.4	0.00	0.00	0.00
8,650	0.0 9.02	191.17	8,571.9	-982.5	-194.0	985.1	0.00	0.00	0.00
8,700	0.0 9.02	191.17	8,621.3	-990.2	-195.5	992.8	0.00	0.00	0.00
8,750		191.17	8,670.7	-997.9	-197.0	1,000.5	0.00	0.00	0.00
8,800		191.17	8,720.1	-1,005.6	-198.6	1,008.3	0.00	0.00	0.00
8,850		191.17	8,769.4	-1,013.2	-200.1	1,016.0	0.00	0.00	0.00
8,900	0.0 9.02	191.17	8,818.8	<b>-</b> 1,020.9	-201.6	1,023.7	0.00	0.00	0.00
8,934		191.17	8,852.7	-1,026.2	-202.6	1,029.0	0.00	0.00	0.00
8,950		191.17	8,868.2	-1,028.6	-203.1	1,031.4	2.00	-2.00	0.00
9,000		191.17	8,917.7	-1,035.6	-204.5	1,038.4	2.00	-2.00 -2.00	0.00
9,050		191.17	8,967.3	-1,041.8	-205.7	1,044.6	2.00	-2.00 -2.00	0.00
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9,100		191.17	9,017.0	-1,047.1	-206.7	1,049.9	2.00	-2.00	0.00
9,150		191.17	9,066.8	-1,051.5	-207.6	1,054.3	2.00	-2.00	0.00
9,200		191.17	9,116.7	-1,055 <b>.</b> 1	-208.3	1,058.0	2.00	-2.00	0.00
9,250		191.17	9,166.6	-1,057 <b>.</b> 9	-208.9	1,060.7	2.00	-2.00	0.00
9,300	0.0 1.71	191.17	9,216.6	-1,059.7	-209.3	1,062.6	2.00	-2.00	0.00
9,350		191.17	9,266.5	<b>-</b> 1,060.8	<b>-</b> 209.5	1,063.6	2.00	-2.00	0.00
9,385		0.00	9,302.0	<b>-</b> 1,061.0	-209.5	1,063.9	2.00	<del>-</del> 2.00	0.00
	3' FSL & 1980' FEL (	•							
9,400		179.79	9,316.5	-1,061 <b>.</b> 2	-209.5	1,064.0	10.00	10.00	0.00
9,450		179.79	9,366.4	-1,064.6	-209.5	1,067.5	10.00	10.00	0.00
9,500	0.0 11.45	179.79	9,415.8	-1,072.4	-209.5	1,075.3	10.00	10.00	0.00
9,550	0.0 16.45	179.79	9,464.3	-1,084.5	-209.4	1,087.3	10.00	10.00	0.00
9,600		179.79	9,511.6	-1,100.7	-209.4	1,103.5	10.00	10.00	0.00
9,650		179.79	9,557.2	-1,121.0	-209.3	1,123,8	10.00	10.00	0.00
9,700		179.79	9,601.0	-1,145.2	209.2	1,148.0	10.00	10.00	0.00
9,750		179.79	9,642.4	-1,173.1	-209.1	1,175.9	10.00	10.00	0.00
9,800	0.0 41.45	179.79	9,681.3	-1,204.5	-209.0	1,207.4	10.00	10.00	0.00
9,850		179.79	9,717.3	-1,239.2	-203.0	1,242.0	10.00	10.00	0.00
9,900		179.79	9,750.1	-1,239.2 -1,276.9	-208.7	1,242.0	10.00	10.00	0.00
9,950		179.79	9,779.5	-1,276.9 -1,317.3	-208.7 -208.6	1,320.1	10.00	10.00	0.00
10,000		179.79	9,805.3	-1,360.1	-208.4	1,363.0	10.00	10.00	0.00
10,050		179.79	9,827.3	-1,405.0	-208.2	1,407.9	10.00	10.00	0.00
10,100		179.79	9,845.2	<b>-</b> 1,451 <b>.</b> 7	-208.1	1,454,5	10.00	10,00	0.00
10,150	76.45	179.79	9,859.0	<b>-</b> 1,499 <b>.</b> 7	-207.9	1,502.5	10.00	10.00	0.00
10,200	0.0 81.45	179.79	9,868.6	<b>-</b> 1,548 <b>.</b> 8	-207.7	1,551.6	10.00	10.00	0.00
10,250	0.0 86.45	179.79	9,873.9	-1,598.5	-207.5	1,601.3	10.00	10.00	0.00
10,284	1.7 89.92	179.79	9,875.0	-1,633.2	-207.4	1,635,9	10.00	10.00	0.00
10,285		179.79	9,875.0	-1,633.9	-207.4	1,636.7	0.00	0.00	0.00
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FTP/I P·	100' FNL & 1980' FE	EL (Sec 11)							

Database: H Company: N

Project:

Site:

Hobbs

Mewbourne Oil Company

Eddy County, New Mexico NAD 83
Bloomin Onion 11/14 Fed Com #715H

Well: Sec 02, T20S, R30E

Wellbore: BHL: 100' FSL & 1980' FEL (Sec 14)

Design: Design #1

Local Co-ordinate Reference:

TVD Reference:
MD Reference:
North Reference:

Survey Calculation Method:

Site Bloomin Onion 11/14 Fed Com #715H WELL @ 3255.0usft (Original Well Elev) WELL @ 3255.0usft (Original Well Elev)

Grid

anned Survey									
Measured Depth (usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Vertical Section (usft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)
10,350.0	89.92	179.79	9,875.1	<b>-</b> 1,698.5	-207.1	1,701.2	0.00	0.00	0.00
10,400.0	89.92	179.79	9,875.2	<b>-</b> 1,748.5	<b>-</b> 207.0	1,751.2	0.00	0.00	0.00
10,450.0	89.92	179.79	9,875.2	-1,798.5	-206.8	1,801.2	0.00	0.00	0.00
10,500.0	89.92	179.79	9,875.3	-1,848.5	-206.6	1,851.2	0.00	0.00	0.00
10,550 <b>.</b> 0	89.92	179.79	9,875.4	-1,898.5	-206.4	1,901.2	0.00	0.00	0.00
10,600.0	89.92	179.79	9,875.5	-1,948.5	-206.2	1,951.2	0.00	0.00	0.00
10,650.0	89.92	179.79	9,875.5	-1,998.5	-206.0	2,001.2	0.00	0.00	0.00
10,700.0	89.92	179.79	9,875.6	-2,048.5	-205.8	2,051.2	0.00	0.00	0.00
10,750.0	89.92	179.79	9,875.7	-2,098.5	-205.7	2,101.2	0.00	0.00	0.00
10,800.0	89.92	179.79	9,875.7	-2,148.5	-205.5	2,151.2	0.00	0.00	0.00
10,850.0	89.92	179.79	9,875.8	-2,198.5	-205.3	2,201.1	0.00	0.00	0.00
10,900.0	89.92	179.79	9,875.9	-2,248.5	-205.1	2,251.1	0.00	0.00	0.00
10,950.0	89.92	179.79	9,876.0	-2,298.5	-204.9	2,301.1	0.00	0.00	0.00
11,000.0	89.92	179.79	9,876.0	-2,298.5 -2,348.5	-204.9 -204.7	2,351.1	0.00	0.00	0.00
11,050.0	89.92	179.79	9,876.1	-2,398.5	-204.7	2,401.1	0.00	0.00	0.00
11,100.0	89.92	179.79	9,876.2	-2,448.5	-204.4	2,451.1	0.00	0.00	0.00
11,150.0	89.92	179.79	9,876.3	-2,498.5	-204.2	2,501.1	0.00	0.00	0.00
11,200.0	89.92	179.79	9,876.3	-2,548.5	-204.0	2,551.1	0.00	0.00	0.00
11,250.0	89.92	179.79	9,876.4	-2,598.5	-203.8	2,601.1	0.00	0.00	0.00
11,300.0	89.92	179.79	9,876.5	-2,648.5	-203.6	2,651.1	0.00	0.00	0.00
11,350.0	89.92	179.79	9,876.5	<b>-</b> 2,698.5	-203.4	2,701.1	0.00	0.00	0.00
11,400.0	89.92	179.79	9,876.6	<b>-</b> 2,748.5	<b>-</b> 203.2	2,751.1	0.00	0.00	0.00
11,450.0	89.92	179.79	9,876.7	-2,798.5	-203.1	2,801.1	0.00	0.00	0.00
11,500.0	89.92	179.79	9,876.8	-2,848.5	-202.9	2,851.0	0.00	0.00	0.00
11,550.0	89.92	179.79	9,876.8	-2,898.5	-202.7	2,901.0	0.00	0.00	0.00
11,600.0	89.92	179.79	9,876.9	-2,948.5	-202.5	2,951.0	0.00	0.00	0.00
11,650.0	89.92	179.79	9,877.0	-2,998.5	-202.3	3,001.0	0.00	0.00	0.00
11,700.0	89.92	179.79	9,877.1	-3,048.5	-202.1	3,051.0	0.00	0.00	0.00
11,750.0	89.92	179.79	9,877.1	-3,098.5	-202.0	3,101.0	0.00	0.00	0.00
11,800.0	89.92	179.79	9,877.2	-3,148.5	-201.8	3,151.0	0.00	0.00	0.00
11,850.0	89.92	179.79	9,877.3	-3,198.5	-201.6	3,201.0	0.00	0.00	0.00
11,900.0	89.92	179.79	9,877.3	-3,248.5	-201.4	3,251.0	0.00	0.00	0.00
11,950.0	89.92	179.79	9,877.4	-3,298.5	-201.2	3,301.0	0.00	0.00	0.00
12,000.0	89.92	179.79	9,877.5	-3,298.5 -3,348.5	-201.2	3,351.0	0.00	0.00	0.00
12,050.0	89.92	179.79	9.877.6	-3,398.5	-200.8	3,401.0	0.00	0.00	0.00
12,100.0	89.92	179.79	9,877.6	-3,448.5	-200.7	3,450.9	0.00	0.00	0.00
12,150.0	89.92	179.79	9,877.7	-3,498.5	-200.7	3,500.9	0.00	0.00	0.00
12,200.0	89.92	179.79	9,877.8	<b>-</b> 3,548.5	-200.3	3,550.9	0.00	0.00	0.00
12,250.0	89.92	179.79	9,877.9	<b>-</b> 3,598.5	-200.1	3,600.9	0.00	0.00	0.00
12,300.0	89.92	179.79	9,877.9	-3,648.5	-199.9 100.7	3,650.9	0.00	0.00	0.00
12,350.0 12,400.0	89.92	179.79 179.79	9,878.0 9,878.1	<b>-</b> 3,698.5	-199.7 -199.5	3,700.9 3,750.9	0.00	0.00	0.00
12,400.0	89.92	179.79	9,878.1	-3,748.5	-199.5	3,750.9	0.00	0.00	0.00
12,450.0	89.92	179.79	9,878.1	-3,798.5	-199.4	3,800.9	0.00	0.00	0.00
12,500.0	89.92	179.79	9,878.2	-3,848.5	-199.2	3,850.9	0.00	0.00	0.00
12,550.0	89.92	179.79	9,878.3	-3,898.5	-199.0	3,900.9	0.00	0.00	0.00
12,600.0	89.92	179.79	9,878.4	-3,948.5	-198.8	3,950.9	0.00	0.00	0.00
12,650.0	89.92	179.79	9,878.4	-3,998.5	-198.6	4,000.9	0.00	0.00	0.00
12,700.0	89.92	179.79	9,878.5	-4,048.5	-198.4	4,050.9	0.00	0.00	0.00
12,750.0	89.92	179.79	9,878.6	-4,098.5	-198.2	4,100.8	0.00	0.00	0.00
12,797.0	89.92	179.79	9,878.6	-4,145.5	-198.1	4,147.9	0.00	0.00	0.00
	' FNL & 1982' FE								
12,800,0	89,92	179.79	9,878.7	-4,148.5	-198.1	4,150.8	0.00	0.00	0.00
12,850.0	89.92	179.79	9,878.7	-4,198.4	197.9	4,200.8	0.00	0.00	0.00

Database: Hobbs

Company: Mewbourne Oil Company

Project: Eddy County, New Mexico NAD 83
Site: Bloomin Onion 11/14 Fed Com #715H

Well: Sec 02, T20S, R30E

**Wellbore:** BHL: 100' FSL & 1980' FEL (Sec 14)

Design: Design #1

Local Co-ordinate Reference:

TVD Reference:
MD Reference:
North Reference:

Survey Calculation Method:

Site Bloomin Onion 11/14 Fed Com #715H WELL @ 3255.0usft (Original Well Elev) WELL @ 3255.0usft (Original Well Elev)

Grid

lanned Survey									
Measured Depth	Inclination	Azimuth	Vertica <b>l</b> Depth	+N/-S	+E/-W	Vertical Section	Dogleg Rate	Build Rate	Turn Rate
(usft)	(°)	(°)	(usft)	(usft)	(usft)	(usft)	(°/100usft)	(°/100usft)	(°/100usft)
12 000 0	89.92	179.79	9,878.8	-4,248.4	107.7	4 250 9	0.00	0.00	0.00
12,900.0					<b>-</b> 197.7	4,250.8	0.00		0.00
12,950.0	89.92	179.79	9,878.9	<b>-</b> 4,298.4	-197.5	4,300.8	0.00	0.00	0.00
13,000.0	89.92	179.79	9,878.9	-4,348.4	<b>-</b> 197.3	4,350.8	0.00	0.00	0.00
13,050.0	89.92	179.79	9,879.0	-4,398.4	-197.1	4,400.8	0.00	0.00	0.00
13,100.0	89.92	179.79	9,879.1	-4,448.4	-196.9	4,450.8	0.00	0.00	0.00
13,150.0	89.92	179.79	9,879.2	-4,498.4	-196.8	4,500.8	0.00	0.00	0.00
13,200.0	89.92	179.79	9,879.2	-4,548.4	-196.6	4,550.8	0.00	0.00	0.00
13.250.0	89.92	179.79	9,879.3	-4,598.4	-196.4	4,600.8	0.00	0.00	0.00
13,300.0	89.92	179.79	9,879.4	-4,648.4	-196.2	4,650.8	0.00	0.00	0.00
13,350.0	89.92	179.79	9,879.5	-4,698.4	-196.0	4,700.7	0.00	0.00	0.00
13,330.0	09.92	175.75	9,079.5	-4,030.4	-130.0	4,700.7	0.00	0.00	0.00
13,400.0	89.92	179.79	9,879.5	-4,748.4	-195.8	4,750.7	0.00	0.00	0.00
13,450.0	89.92	179.79	9,879.6	<b>-</b> 4,798.4	-195.7	4,800.7	0.00	0.00	0.00
	89.92						0.00		0.00
13,500.0		179.79	9,879.7	-4,848.4	-195.5	4,850.7		0.00	
13,550.0	89.92	179.79	9,879.7	-4,898.4	-195.3	4,900.7	0.00	0.00	0.00
13,600.0	89.92	179.79	9,879.8	-4,948.4	<b>-</b> 195.1	4,950.7	0.00	0.00	0.00
40.050.0	00.00	470.70	0.070.0	4.000.4	4040	F 000 7	0.00	0.00	0.00
13,650.0	89.92	179.79	9,879.9	-4,998.4	-194.9	5,000.7	0.00	0.00	0.00
13,700.0	89.92	179.79	9,880.0	-5,048 <b>.</b> 4	-194.7	5,050.7	0.00	0.00	0.00
13,750.0	89.92	179.79	9,880.0	-5,098.4	-194.5	5,100.7	0.00	0.00	0.00
13,800.0	89.92	179.79	9.880.1	-5,148.4	-194.4	5,150.7	0.00	0.00	0.00
13,850.0	89.92	179.79	9,880.2	-5,198.4	-194.2	5,200.7	0.00	0.00	0.00
10,000.0	00.02	. , 0., , 0	3,000.2	3, 100.4	10412	3,200.7		0.00	0.00
13,900.0	89.92	179.79	9,880.2	-5,248.4	<b>-</b> 194.0	5,250.7	0.00	0.00	0.00
13,950.0	89.92	179.79	9,880.3	-5,298.4	-193.8	5,300.7	0.00	0.00	0.00
14,000.0	89.92	179.79	9.880.4	5.348.4	-193.6	5,350.6	0.00	0.00	0.00
			,	,		,			
14,050.0	89.92	179.79	9,880.5	-5,398.4	-193.4	5,400.6	0.00	0.00	0.00
14,100.0	89.92	179.79	9,880.5	<b>-</b> 5,448.4	-193.2	5,450.6	0.00	0.00	0.00
14 100 0	89.92	170.70	9,880.6	-5,468.7	-193.2	5,470.9	0.00	0.00	0.00
14,120.3		179.79	9,000.0	-3,408.7	-193.2	5,470.9	0.00	0.00	0.00
PPP3: 1324'	FSL & 1984' FEI	L (Sec 11)							
14,150.0	89.92	179.79	9,880.6	-5,498.4	-193.1	5,500.6	0.00	0.00	0.00
14,200.0	89.92	179.79	9,880.7	-5,548.4	-192.9	5,550.6	0.00	0.00	0.00
14,250.0	89.92	179,79	9,880.8	5,598.4	-192.7	5,600,6	0.00	0.00	0.00
				,					
14,300.0	89.92	179.79	9,880.8	-5,648.4	-192.5	5,650,6	0.00	0.00	0.00
14,350,0	89.92	179,79	9,880.9	-5,698,4	-192.3	5,700.6	0.00	0.00	0.00
14,400.0	89.92	179,79	9,881.0			5,750,6	0.00	0.00	0.00
			,	-5,748.4	-192.1				
14,450.0	89.92	179.79	9,881.0	-5,798 <b>.</b> 4	-191.9	5,800.6	0.00	0.00	0.00
14,500.0	89.92	179.79	9,881.1	-5,848.4	-191.8	5,850.6	0.00	0.00	0.00
14,550.0	89.92	179.79	9,881.2	-5,898.4	-191.6	5,900.6	0.00	0.00	0.00
14,600.0	89.92	179.79	9,881.3	-5,948.4	-191.4	5,950.5	0.00	0.00	0.00
14,650.0	89.92	179.79	9,881.3	-5,998.4	-191.2	6,000.5	0.00	0.00	0.00
14,700.0	89.92	179.79	9,881.4	-6,048.4	-191.0	6,050.5	0.00	0.00	0.00
14,750.0	89.92	179.79	9,881.5	-6,098.4	-190.8	6,100.5	0.00	0.00	0.00
14,800.0	89.92	179.79	9,881.6	-6,148.4	-190.6	6,150.5	0.00	0.00	0.00
14,600.0	05.52	1/8./8	3,001.0	-0,140.4	-190.0	0,100,0	0.00	0.00	0.00
14,850.0	89.92	179.79	9,881.6	-6,198.4	-190.5	6,200,5	0.00	0.00	0.00
14,900.0	89.92	179.79	9,881.7	-6,248.4	-190.3	6,250,5	0.00	0.00	0.00
14,950.0						6,300.5			
	89.92	179.79	9,881.8	-6,298.4	-190.1		0.00	0.00	0.00
15,000.0	89.92	179.79	9,881 <b>.</b> 8	-6,348 <b>.</b> 4	-189.9	6,350.5	0.00	0.00	0.00
15,050.0	89.92	179.79	9,881.9	-6,398.4	-189.7	6,400.5	0.00	0.00	0.00
45 400 5	20.0-	470.70	0 000 5	0.440.4	100 5	0 450 5	2.25	2.25	2 22
15,100.0	89.92	179.79	9,882.0	-6,448.4	-189.5	6,450.5	0.00	0.00	0.00
15,150 <b>.</b> 0	89.92	179.79	9,882.1	-6,498.4	-189.4	6,500.5	0.00	0.00	0.00
15,200.0	89.92	179.79	9,882.1	-6,548.4	-189.2	6,550.5	0.00	0.00	0.00
15,250.0	89.92	179.79	9,882.2	6,598.4	189.0	6,600,4	0.00	0.00	0.00
15,300.0	89.92	179.79	9,882.3	-6,648.4	-188.8	6,650.4	0.00	0.00	0.00
15,350.0	89.92	179.79	9,882.4	-6,698.4	-188.6	6,700.4	0.00	0.00	0.00
15,400.0	89.92	179.79	9,882.4	-6,748.4	-188.4	6,750.4	0.00	0.00	0.00
15,443.5	89.92	179.79	9,882.5	-6,791.9	-188.3	6,793.9	0.00	0.00	0.00

Database: Hobbs Company: Mewbo

Project:

Mewbourne Oil Company

Eddy County, New Mexico NAD 83

Site: Bloomin Onion 11/14 Fed Com #715H

**Well:** Sec 02, T20S, R30E

**Wellbore:** BHL: 100' FSL & 1980' FEL (Sec 14)

Design: Design #1

Local Co-ordinate Reference:

TVD Reference: MD Reference: North Reference:

Survey Calculation Method:

Site Bloomin Onion 11/14 Fed Com #715H WELL @ 3255.0usft (Original Well Elev) WELL @ 3255.0usft (Original Well Elev)

Grid

ın:	Design #1								
ned Survey									
Measured Depth (usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Vertical Section (usft)	Dogleg Rate (°/100usft)	Bui <b>l</b> d Rate (°/100usft)	Turn Rate (°/100usft)
PPP4: 0' FNI	_ & 1986' FEL (S	ec 14)							
15,450.0	89.92	179.79	9,882.5	-6,798.4	-188.2	6,800.4	0.00	0.00	0.00
15,500.0	89.92	179.79	9,882.6	-6,848.4	-188.1	6,850.4	0.00	0.00	0.00
15,550.0	89.92	179,79	9,882,6	-6,898,4	-187.9	6,900,4	0.00	0.00	0.00
15,600.0	89.92	179.79	9,882.7	-6,948.4	-187.7	6,950.4	0.00	0.00	0.00
15,650.0	89.92	179.79	9,882.8	-6,998.4	-187.5	7,000.4	0.00	0.00	0.00
15,700.0	89.92	179.79	9,882.9	-7,048.4	-187.3	7,050.4	0.00	0.00	0.00
15,750.0	89.92	179.79	9,882.9	-7,098.4	-187.1	7,100.4	0.00	0.00	0.00
15,800.0	89.92	179.79	9,883.0	-7,148.4	-186.9	7,150.4	0.00	0.00	0.00
15,850.0	89.92	179.79	9,883.1	-7,198.4	-186.8	7,200.3	0.00	0.00	0.00
15,900.0	89.92	179.79	9,883.2	-7,248.4	-186.6	7,250.3	0.00	0.00	0.00
15,950.0	89.92	179.79	9,883.2	-7,298.4	-186.4	7,300.3	0.00	0.00	0.00
16,000.0	89.92	179.79	9,883.3	-7,348.4	-186.2	7,350.3	0.00	0.00	0.00
16,050.0	89.92	179.79	9,883.4	-7,398.4	-186.0	7,400.3	0.00	0.00	0.00
16,100.0	89.92	179.79	9,883.4	-7,448.4	-185.8	7,450.3	0.00	0.00	0.00
16,150.0	89.92	179.79	9,883.5	-7,498.4	-185.6	7,500.3	0.00	0.00	0.00
16,200.0	89.92	179.79	9,883.6	-7,548.4	<b>-</b> 185.5	7,550.3	0.00	0.00	0.00
16,250.0	89.92	179.79	9,883.7	-7,598.4	-185.3	7,600.3	0.00	0.00	0.00
16,300.0	89.92	179.79	9,883.7	-7,648.4	-185.1	7,650.3	0.00	0.00	0.00
16,350.0	89.92	179.79	9,883.8	<b>-</b> 7,698 <b>.</b> 4	<b>-</b> 184.9	7,700.3	0.00	0.00	0.00
16,400.0	89.92	179.79	9,883.9	-7,748.4	-184.7	7,750.3	0.00	0.00	0.00
16,450.0	89.92	179.79	9,884.0	-7,798.4	<b>-</b> 184.5	7,800.3	0.00	0.00	0.00
16,500.0	89.92	179.79	9,884.0	<b>-</b> 7,848 <b>.</b> 4	<b>-</b> 184 <b>.</b> 4	7,850.2	0.00	0.00	0.00
16,550.0	89.92	179.79	9,884.1	<b>-</b> 7,898.4	<b>-</b> 184.2	7,900.2	0.00	0.00	0.00
16,600.0	89.92	179.79	9,884.2	<b>-</b> 7,948.4	<b>-</b> 184.0	7,950.2	0.00	0.00	0.00
16,650.0	89.92	179.79	9,884.2	<b>-</b> 7,998.4	-183.8	8,000.2	0.00	0.00	0.00
16,700.0	89.92	179.79	9,884.3	-8,048.4	-183.6	8,050.2	0.00	0.00	0.00
16,750.0	89.92	179.79	9,884.4	-8,098.4	-183.4	8,100.2	0.00	0.00	0.00
16,800.0	89.92	179.79	9,884.5	-8,148.4	-183.2	8,150.2	0.00	0.00	0.00
16,850.0	89.92	179.79	9,884.5	-8,198.4	-183.1	8,200.2	0.00	0.00	0.00
16,900.0	89.92	179.79	9,884.6	-8,248.4	-182.9	8,250.2	0.00	0.00	0.00
16,950.0	89.92	179.79	9,884.7	-8,298.4	-182.7	8,300.2	0.00	0.00	0.00
17,000.0	89.92	179.79	9,884.7	-8,348.4	-182.5	8,350.2	0.00	0.00	0.00
17,050.0	89.92	179.79	9,884.8	-8,398.4	-182.3	8,400.2	0.00	0.00	0.00
17,100.0	89.92	179.79	9,884.9	-8,448.4	-182.1	8,450.1	0.00	0.00	0.00
17,150.0	89.92	179.79	9,885.0	-8,498.4	-181.9	8,500.1	0.00	0.00	0.00
17,200 <b>.</b> 0 17,250 <b>.</b> 0	89 <u>.</u> 92 89 <u>.</u> 92	179.79 179.79	9,885.0 9,885.1	-8,548.4 -8,598.4	-181.8 -181.6	8,550,1 8,600,1	0.00 0.00	0.00 0.00	0.00 0.00
17,300.0	89.92	179.79	9,885.2	-8,648.4	-181.4	8,650.1	0.00	0.00	0.00
17,350.0	89.92	179.79	9,885.3	-8,698 <b>.</b> 4	-181.2	8,700.1	0.00	0.00	0.00
17,400 <b>.</b> 0 17,450 <b>.</b> 0	89 <u>.</u> 92	179 <b>.</b> 79 179 <b>.</b> 79	9,885.3	-8,748 <b>.</b> 4	-181.0 180.8	8,750.1	0.00 0.00	0.00 0.00	0.00 0.00
17,450.0 17,500.0	89.92 89.92	179.79	9,885.4 9,885.5	-8,798.4 -8,848.4	-180.8 -180.6	8,800.1 8,850.1	0.00	0.00	0.00
17,550.0	89.92	179.79	9,885.5	-8,898.4	-180.5	8,900.1	0.00	0.00	0.00
17,600.0	89.92	179.79	9,885.6	-8,948.4	-180.3	8,950,1	0.00	0.00	0.00
17,650 <b>.</b> 0 17,700 <b>.</b> 0	89 <u>.</u> 92 89 <u>.</u> 92	179 <b>.</b> 79 179 <b>.</b> 79	9,885.7 9,885.8	-8,998.4 -9,048.4	-180.1 -179.9	9,000.1 9,050.1	0.00 0.00	0.00 0.00	0.00 0.00
17,700.0 17,750.0	89.92 89.92	179.79	9,885.8 9,885.8	-9,048.4 -9,098.4	-179.9 -179.7	9,050.1	0.00	0.00	0.00
•									
17,800.0	89.92	179.79	9,885.9	-9,148.4	-179.5	9,150.0	0.00	0.00	0.00
17,850.0	89.92	179.79	9,886.0	-9,198.4 0.248.4	-179.3	9,200.0	0.00	0.00	0.00
17,900 <b>.</b> 0 17,950 <b>.</b> 0	89.92 89.92	179 <b>.</b> 79 179 <b>.</b> 79	9,886.1	-9,248.4 9,298.4	-179.2 -179.0	9,250.0 9,300.0	0.00 0.00	0.00 0.00	0.00 0.00
18,000.0	89.92	179.79	9,886.1 9,886.2	-9,298.4 -9,348.4	-179.0 -178.8	9,350.0	0.00	0.00	0.00

Database: Hobbs Company:

Project:

Site:

Mewbourne Oil Company

Eddy County, New Mexico NAD 83 Bloomin Onion 11/14 Fed Com #715H

Well: Sec 02, T20S, R30E

BHL: 100' FSL & 1980' FEL (Sec 14) Wellbore:

Design: Design #1 Local Co-ordinate Reference:

TVD Reference: MD Reference: North Reference:

Survey Calculation Method:

Site Bloomin Onion 11/14 Fed Com #715H WELL @ 3255.0usft (Original Well Elev) WELL @ 3255.0usft (Original Well Elev)

agn:	Design #1								
nned Survey									
Measured Depth (usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Vertical Section (usft)	Dogleg Rate (°/100usft)	Bui <b>l</b> d Rate (°/100usft)	Turn Rate (°/100usft)
18,050.0	89.92	179.79	9,886.3	-9,398.4	<b>-</b> 178.6	9,400.0	0.00	0.00	0.00
18,100.0	89.92	179.79	9,886.3	-9,448.4	-178.4	9,450.0	0.00	0.00	0.00
18,150.0	89.92	179.79	9,886.4	-9,498.4	-178.2	9,500.0	0.00	0.00	0.00
18,200.0	89.92	179.79	9,886.5	9,548.4	-178.1	9,550.0	0.00	0.00	0.00
18,250.0	89.92	179.79	9,886.6	<b>-</b> 9,598 <b>.</b> 4	<b>-</b> 177.9	9,600.0	0.00	0.00	0.00
18,300.0	89.92	179.79	9,886.6	-9,648.4	-177.7	9,650.0	0.00	0.00	0.00
18,350.0	89.92	179.79	9,886.7	-9,698.4	-177.5	9,699.9	0.00	0.00	0.00
18,400.0	89.92	179.79	9.886.8	-9,748.4	-177.3	9,749.9	0.00	0.00	0.00
18,450.0	89.92	179.79	9,886.9	-9,798.4	-177.1	9,799.9	0.00	0.00	0.00
18,500.0	89.92	179.79	9,886.9	-9,848.4	-176.9	9,849.9	0.00	0.00	0.00
18,550.0	89.92	179.79	9,887.0	<b>-</b> 9,898.4	<b>-</b> 176.8	9,899.9	0.00	0.00	0.00
18,600.0	89.92	179.79	9,887.1	-9,948.4	<b>-</b> 176.6	9,949.9	0.00	0.00	0.00
18,650.0	89.92	179.79	9,887.1	-9,998.4	<b>-</b> 176.4	9,999.9	0.00	0.00	0.00
18,700.0	89.92	179.79	9,887.2	-10,048.4	<b>-</b> 176.2	10,049.9	0.00	0.00	0.00
18,750.0	89.92	179.79	9,887.3	-10,098.4	-176.0	10,099.9	0.00	0.00	0.00
			,	,					
18,800 <b>.</b> 0	89.92	179.79	9,887 <b>.</b> 4	-10,148.4	-175.8	10,149.9	0.00	0.00	0.00
18,850.0	89.92	179.79	9,887.4	-10,198.4	-175.6	10,199.9	0.00	0.00	0.00
18,900.0	89.92	179.79	9,887.5	-10,248.4	-175.5	10,249.9	0.00	0.00	0.00
18,950.0	89.92	179.79	9,887.6	-10,298.4	-175.3	10,299.9	0.00	0.00	0.00
19,000.0	89.92	179.79	9,887.7	-10,348.4	-175.1	10,349.8	0.00	0.00	0.00
10.050.0	90.00	170.70	0.007.7	10 200 4	174.0	10 200 9	0.00	0.00	0.00
19,050.0	89.92	179.79	9,887.7	-10,398.4	-174.9	10,399.8	0.00	0.00	0.00
19,100.0	89.92	179.79	9,887.8	-10,448.4	-174.7	10,449.8	0.00	0.00	0.00
19,150.0	89.92	179.79	9,887.9	<b>-</b> 10,498.4	<b>-</b> 174.5	10,499.8	0.00	0.00	0.00
19,200.0	89.92	179.79	9,887.9	-10,548.4	-174.3	10,549.8	0.00	0.00	0.00
19,250.0	89.92	179.79	9,888.0	-10,598.4	-174.2	10,599.8	0.00	0.00	0.00
19,300.0	89.92	179.79	9,888.1	-10,648.4	-174.0	10,649.8	0.00	0.00	0.00
,									
19,350.0	89.92	179.79	9,888.2	-10,698.4	-173.8	10,699.8	0.00	0.00	0.00
19,400.0	89.92	179.79	9,888.2	-10,748.4	-173.6	10,749.8	0.00	0.00	0.00
19,450.0	89.92	179.79	9,888.3	-10,798.4	-173.4	10,799.8	0.00	0.00	0.00
19,500.0	89.92	179.79	9,888.4	-10,848.4	-173.2	10,849.8	0.00	0.00	0.00
19,550.0	89.92	179.79	9,888.5	<b>-</b> 10,898.4	<b>-</b> 173.0	10,899.8	0.00	0.00	0.00
			,						
19,600.0	89.92	179.79	9,888.5	-10,948.4	<b>-</b> 172.9	10,949.7	0.00	0.00	0.00
19,650.0	89.92	179.79	9,888.6	-10,998.4	<b>-</b> 172.7	10,999.7	0.00	0.00	0.00
19,700.0	89.92	179.79	9,888.7	-11,048.4	-172.5	11,049.7	0.00	0.00	0.00
19,750.0	89.92	179.79	9,888.7	-11,098.4	<b>-</b> 172.3	11,099.7	0.00	0.00	0.00
19,800.0	89.92	179.79	9,888.8	-11,148.4	-172.1	11,149.7	0.00	0.00	0.00
19,850.0	89.92	179.79	9.888.9	-11,198.4	-171.9	11,199.7	0.00	0.00	0.00
19,900.0	89.92	179.79	9,889.0	-11,248.4	-171.8	11,199.7	0.00	0.00	0.00
,									
19,950.0	89.92	179.79	9,889.0	-11,298.4	-171.6	11,299.7	0.00	0.00	0.00
20,000.0	89.92	179.79	9,889.1	-11,348.4	-171.4	11,349.7	0.00	0.00	0.00
20,050.0	89.92	179.79	9,889.2	-11,398.4	-171.2	11,399.7	0.00	0.00	0.00
20,100.0	89.92	179.79	9,889.3	-11,448.4	-171.0	11,449.7	0.00	0.00	0.00
20,150.0	89.92	179.79	9,889.3	-11,498.4	-170.8	11,499.7	0.00	0.00	0.00
20,200.0	89.92	179.79	9,889.4	-11,548.4	-170.6	11,549.6	0.00	0.00	0.00
20,250.0	89.92	179.79	9,889.5	-11,598.4	<b>-</b> 170.5	11,599.6	0.00	0.00	0.00
20,300.0	89.92	179.79	9,889.5	-11,648.4	-170.3	11,649.6	0.00	0.00	0.00
20,350.0	89.92	179.79	9,889.6	-11,698.4	-170.1	11,699.6	0.00	0.00	0.00
20,400.0	89.92	179.79	9,889.7	-11,748.4	-169.9	11,749.6	0.00	0.00	0.00
20,450.0	89.92	179.79	9,889.8	-11,798.4	-169.7	11,799.6	0.00	0.00	0.00
20,450.0	89.92 89.92	179.79		-11,798.4 -11,848.4		11,799.6	0.00		0.00
20,300.0	09.92	119.19	9,889.8	-11,040.4	-169.5	11,049.0	0.00	0.00	0.00
20,550.0	89.92	179.79	9,889.9	-11,898.4	<b>-</b> 169.3	11,899.6	0.00	0.00	0.00
20,600.0	89.92	179.79	9,890.0	-11,948.4	<b>-</b> 169.2	11,949.6	0.00	0.00	0.00
			the state of the s						
20,615.9	89.92	179.79	9,890.0	-11,964.3	-169.1	11,965.5	0.00	0.00	0.00

Database: Hobbs

Company: Mewbourne Oil Company

Project: Eddy County, New Mexico NAD 83
Site: Bloomin Onion 11/14 Fed Com #715H

Well: Sec 02, T20S, R30E

**Wellbore:** BHL: 100' FSL & 1980' FEL (Sec 14)

Design: Design #1

Local Co-ordinate Reference:

TVD Reference: MD Reference: North Reference:

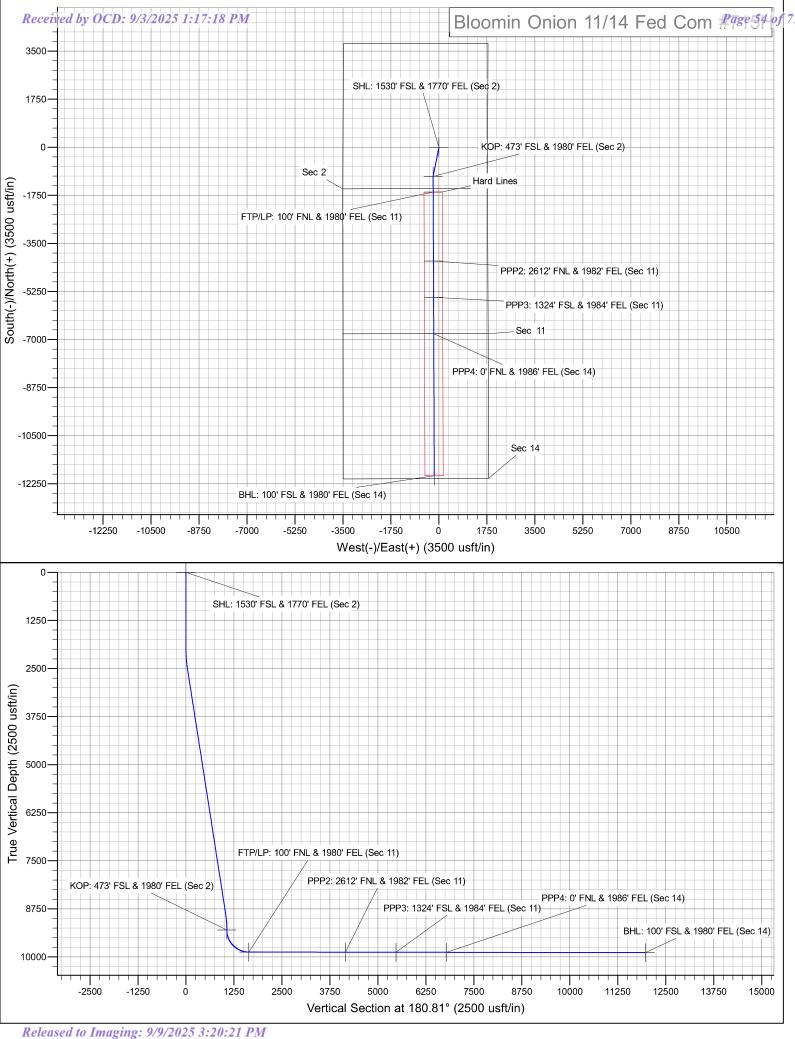
Survey Calculation Method:

Site Bloomin Onion 11/14 Fed Com #715H WELL @ 3255.0usft (Original Well Elev) WELL @ 3255.0usft (Original Well Elev)

Grid

Planned Survey										
Measured			Vertical			Vertical	Dogleg	Build	Turn	
Depth	Inclination	Azimuth	Depth	+N/-S	+E/-W	Section	Rate	Rate	Rate	
(usft)	(°)	(°)	(usft)	(usft)	(usft)	(usft)	(°/100usft)	(°/100usft)	(°/100usft)	

Design Targets									
Target Name - hit/miss target - Shape	Dip Angle (°)	Dip Dir. (°)	TVD (usft)	+N/-S (usft)	+E/-W (usft)	Northing (usft)	Easting (usft)	Latitude	Longitude
SHL: 1530' FSL & 1770' - plan hits target cen - Point	0.00 ter	0.00	0.0	0.0	0.0	581,939.00	662,472.50	32.5991870	-103.9399820
KOP: 473' FSL & 1980' F - plan hits target cen - Point	0.00 ter	0.00	9,302.0	-1,061.0	-209.5	580,878.00	662,263.00	32.5962728	-103.9406750
FTP/LP: 100' FNL & 198 - plan hits target cen - Point	0.00 ter	0.00	9,875.0	-1,633.9	-207.4	580,305.10	662,265.13	32,5946981	-103.9406749
PPP2: 2612' FNL & 1982 - plan hits target cen - Point	0.00 ter	0.00	9,878.6	<b>-</b> 4,145.5	<b>-</b> 198.1	577,793.50	662,274.43	32.5877944	<b>-</b> 103.9406748
PPP3: 1324' FSL & 1984 - plan hits target cen - Point	0.00 ter	0.00	9,880.6	-5,468.7	-193.2	576,470.30	662,279.34	32.5841573	-103.9406748
PPP4: 0' FNL & 1986' FE - plan hits target cen - Point	0 <u>.</u> 00 ter	0.00	9,882.5	-6,791.9	<b>-</b> 188.3	575,147.10	662,284.24	32.5805202	<b>-</b> 103 <u>.</u> 9406747
BHL: 100' FSL & 1980' F - plan hits target cen - Point	0.00 ter	0.00	9,890.0	-11,964.3	-169.1	569,974.70	662,303.40	32.5663027	-103.9406744



## PECOS DISTRICT DRILLING CONDITIONS OF APPROVAL

**OPERATOR'S NAME:** MEWBOURNE OIL COMPANY

WELL NAME & NO.: BLOOMIN ONION 11/14 FED COM 715H

**APD ID:** 10400105053

**LOCATION:** Section 2, T20S, R30E. NMP.

**COUNTY:** Eddy County, New Mexico

COA

$H_2S$	○ No		Yes	
Potash /	None	Secretary	<b>⊙</b> R-111-Q	Open Annulus
WIPP	4-String Design: Open	2nd Int x Production Casing	g (ICP 2 above Relief Z	one) 🔲 WIPP
Cave / Karst	C Low	Medium	□ High	Critical
Wellhead	Conventional	• Multibowl	Both	© Diverter
Cementing	Primary Squeeze	Cont. Squeeze	EchoMeter	DV Tool
Special Req	Capitan Reef	Water Disposal	<b>▼</b> COM	Unit
Waste Prev.	Self-Certification	Waste Min. Plan	C APD Submitted pr	rior to 06/10/2024
Additional	▼ Flex Hose	Casing Clearance	Pilot Hole	Break Testing
Language	Four-String	Offline Cementing	Fluid-Filled	

#### A. HYDROGEN SULFIDE

A Hydrogen Sulfide (H<sub>2</sub>S) Drilling Plan shall be activated **at spud**. As a result, the Hydrogen Sulfide area must meet all requirements from 43 CFR 3176, which includes equipment and personnel/public protection items. If Hydrogen Sulfide is encountered, please provide measured values and formations to the BLM.

APD is within the R-111-Q defined boundary. Operator must follow all applicable procedures and requirements listed within the Order No. R-111-Q.

#### **B. CASING**

#### **Primary Casing Design**

**Note:** The surface casing set depth was adjusted per BLM geologist's recommendation. "The operator proposes to set surface casing at 385 feet which will be in or above the Magenta Dolomite Aquifer and will not adequately protect all usable water zones. Instead, set surface casing at a depth of approximately 440 feet."

- 1. The 18-5/8-inch surface casing shall be set at approximately 440 ft. (a minimum of 70 ft. into the Rustler Anhydrite, above the salt, and below usable fresh water) and cemented to the surface. If salt is encountered set casing at least 25 ft. above the salt.
  - a. If cement does not circulate to the surface, the appropriate BLM office shall be notified and a temperature survey utilizing an electronic-type temperature survey with surface log readout will be used or a cement bond log shall be run to verify the top of the cement. Temperature survey will be run a minimum of six hours after pumping cement and ideally between 8-10 hours after completing the cement job.
  - b. Wait on cement (WOC) time for a primary cement job will be a minimum of **8 hours** or **500 psi compressive strength**, whichever is greater. (This is to include the lead cement)
  - c. Wait on cement (WOC) time for a remedial job will be a minimum of 4 hours after bringing cement to surface or 500 pounds compressive strength, whichever is greater.
  - d. If cement falls back, remedial cementing will be done prior to drilling out that string.
- 2. The 13-3/8 inch 1<sup>st</sup> intermediate casing shall be set in a competent bed at approximately 2,039 ft. The minimum required fill of cement behind the 13-3/8 inch intermediate casing is:
  - Cement to surface. If cement does not circulate see B.1.a, c-d above. Wait on cement (WOC) time for a primary cement job is to include the lead cement slurry due to cave/karst, Capitan Reef, and Potash.

**Note:** The 2<sup>nd</sup> intermediate casing set depth was adjusted per BLM geologist's recommendation. "The operator proposes to set second intermediate casing at 3590 feet which will potentially be in the Delaware Sands and is not competent bedrock for setting casing. BLM recommends setting casing in the base of the Capitan Reef at approximately 3418 feet."

3. The 9-5/8 inch 2<sup>nd</sup> intermediate casing shall be set in a competent bed at approximately 3,418 ft. The minimum required fill of cement behind the 9-5/8 inch intermediate casing is:

**Option 1 (Single Stage): Cement to surface.** If cement does not circulate see B.1.a, c-d above. Wait on cement (WOC) time for a primary cement job is to include the lead cement slurry due to cave/karst, Capitan Reef, and Potash.

**Option 2 (Two-Stage):** The operator has proposed to utilize a DV tool. Operator may adjust depth of DV tool if needed, adjust cement volumes accordingly. The DV tool may be cancelled if cement circulates to surface on the first stage.

- a. **First stage to DV tool:** Cement to circulate. If cement does not circulate off the DV tool, contact the appropriate BLM office before proceeding with second stage cement job.
- b. Second stage above DV tool: Cement to surface. If cement does not circulate see B.1.a, c-d above. Wait on cement (WOC) time for a primary cement job is to include the lead cement slurry due to cave/karst, Capitan Reef, and Potash.

❖ Special Capitan Reef Requirement: Ensure freshwater based mud is used across the Capitan interval.

**Note:** Excess cement for the 2<sup>nd</sup> stage is below %25. More cement might be needed.

- **4.** Operator has proposed to set 7 inch production casing at approximately **9,385 ft.** (9,302 ft. TVD). The minimum required fill of cement behind the production casing is:
  - Operator has proposed to cement the production casing in two stages by conventionally cementing the first stage and performing a bradenhead squeeze on the second stage within 180 days after well completion in accordance with the R-111-Q guidelines.
    - a. First stage: Operator will cement production casing with intent to bring cement to top of Brushy Canyon formation.
    - b. Second stage: Operator will perform bradenhead squeeze within 180 days after completion per R-111-Q requirements. Cement shall be tie-back at least 500 ft. into the 2<sup>nd</sup> intermediate casing and below the Marker Bed 126. If cement does not circulate, the appropriate BLM office shall be notified.
  - ❖ Operator has proposed an open annulus completion in R-111-Q. Operator shall provide a method of verification pre-completion top of cement. **Submit results to the BLM.**
  - ❖ Operator must verify top of cement per R-111-Q requirements. Submit results to the BLM. If cement does not circulate, contact the appropriate BLM office. If cement does not tie-back at least 500 ft. into the previous casing shoe, the appropriate BLM office shall be notified.
  - A monitored open annulus will be incorporated during completion by leaving the 2<sup>nd</sup> Intermediate Casing x Production Casing annulus un-cemented and monitored. Operator must follow <u>all</u> monitoring requirements listed within R-111-Q. Tieback shall be met within 180 days.
  - ❖ In the event of a casing failure during completion, the operator must contact the BLM engineer at (575-706-2779) and inspection staff (575-361-2822 Eddy County).
  - ❖ Pressure monitoring device and Pressure Safety Valves must be installed at surface on the open annulus for the life of the well.
- 5. The minimum required fill of cement behind the 4-1/2 inch production liner is:
  - Cement should tie-back **100 feet** into the previous casing. Operator shall provide method of verification.

#### **Alternate Casing Design**

**Note:** The surface casing set depth was adjusted per BLM geologist's recommendation. "The operator proposes to set surface casing at 385 feet which will be in or above the Magenta Dolomite Aquifer and will not adequately protect all usable water zones. Instead, set surface casing at a depth of approximately 440 feet."

- 1. The 18-5/8-inch surface casing shall be set at approximately 440 ft. (a minimum of 70 ft. into the Rustler Anhydrite, above the salt, and below usable fresh water) and cemented to the surface. If salt is encountered set casing at least 25 ft. above the salt.
  - a. If cement does not circulate to the surface, the appropriate BLM office shall be notified and a temperature survey utilizing an electronic-type temperature survey with surface log readout will be used or a cement bond log shall be run to verify the top of the cement. Temperature survey will be run a minimum of six hours after pumping cement and ideally between 8-10 hours after completing the cement job.
  - b. Wait on cement (WOC) time for a primary cement job will be a minimum of **8 hours** or **500 psi compressive strength**, whichever is greater. (This is to include the lead cement)
  - c. Wait on cement (WOC) time for a remedial job will be a minimum of 4 hours after bringing cement to surface or 500 pounds compressive strength, whichever is greater.
  - d. If cement falls back, remedial cementing will be done prior to drilling out that string.
- 2. The 13-3/8 inch 1<sup>st</sup> intermediate casing shall be set in a competent bed at approximately 2,039 ft. The minimum required fill of cement behind the 13-3/8 inch intermediate casing is:
  - Cement to surface. If cement does not circulate see B.1.a, c-d above. Wait on cement (WOC) time for a primary cement job is to include the lead cement slurry due to cave/karst, Capitan Reef, and Potash.

**Note:** The 2<sup>nd</sup> intermediate casing set depth was adjusted per BLM geologist's recommendation. "The operator proposes to set second intermediate casing at 3590 feet which will potentially be in the Delaware Sands and is not competent bedrock for setting casing. BLM recommends setting casing in the base of the Capitan Reef at approximately 3418 feet."

3. The 9-5/8 inch 2<sup>nd</sup> intermediate casing shall be set in a competent bed at approximately 3,418 ft. The minimum required fill of cement behind the 9-5/8 inch intermediate casing is:

**Option 1 (Single Stage): Cement to surface.** If cement does not circulate see B.1.a, c-d above. Wait on cement (WOC) time for a primary cement job is to include the lead cement slurry due to cave/karst, Capitan Reef, and Potash.

**Option 2 (Two-Stage):** The operator has proposed to utilize a DV tool. Operator may adjust depth of DV tool if needed, adjust cement volumes accordingly. The DV tool may be cancelled if cement circulates to surface on the first stage.

- a. **First stage to DV tool:** Cement to circulate. If cement does not circulate off the DV tool, contact the appropriate BLM office before proceeding with second stage cement job.
- b. Second stage above DV tool: Cement to surface. If cement does not circulate see B.1.a, c-d above. Wait on cement (WOC) time for a primary cement job is to include the lead cement slurry due to cave/karst, Capitan Reef, and Potash.

❖ Special Capitan Reef Requirement: Ensure freshwater based mud is used across the Capitan interval.

**Note:** Excess cement for the 2<sup>nd</sup> stage is below %25. More cement might be needed.

- **4.** Operator has proposed to set 7 inch production casing at approximately **10,285 ft.** (9,875 ft. TVD). The minimum required fill of cement behind the production casing is:
  - Operator has proposed to cement the production casing in two stages by conventionally cementing the first stage and performing a bradenhead squeeze on the second stage within 180 days after well completion in accordance with the R-111-Q guidelines.
    - a. First stage: Operator will cement production casing with intent to bring cement to top of Brushy Canyon formation.
    - b. Second stage: Operator will perform bradenhead squeeze within 180 days after completion per R-111-Q requirements. Cement shall be tie-back at least 500 ft. into the 2<sup>nd</sup> intermediate casing and below the Marker Bed 126. If cement does not circulate, the appropriate BLM office shall be notified.
  - ❖ Operator has proposed an open annulus completion in R-111-Q. Operator shall provide a method of verification pre-completion top of cement. **Submit results to the BLM.**
  - ❖ Operator must verify top of cement per R-111-Q requirements. Submit results to the BLM. If cement does not circulate, contact the appropriate BLM office. If cement does not tieback at least 500 ft. into the previous casing shoe, the appropriate BLM office shall be notified.
  - A monitored open annulus will be incorporated during completion by leaving the 2<sup>nd</sup> Intermediate Casing x Production Casing annulus un-cemented and monitored. Operator must follow <u>all</u> monitoring requirements listed within R-111-Q. Tieback shall be met within 180 days.
  - ❖ In the event of a casing failure during completion, the operator must contact the BLM engineer at (575-706-2779) and inspection staff (575-361-2822 Eddy County).
  - ❖ Pressure monitoring device and Pressure Safety Valves must be installed at surface on the open annulus for the life of the well.
- 5. The minimum required fill of cement behind the 4-1/2 inch production liner is:
  - Cement should tie-back **100 feet** into the previous casing. Operator shall provide method of verification.

#### **Offline Cementing**

Operator has been (**Approved**) to pump the proposed cement program offline in the **Surface and intermediate(s) intervals**. Offline cementing should commence within 24 hours of landing the casing for the interval. Notify the BLM 4hrs prior to the commencement of any offline cementing procedure at **Eddy County:** 575-361-2822.

#### C. PRESSURE CONTROL

- 1. Variance approved to use flex line from BOP to choke manifold. Manufacturer's specification to be readily available. No external damage to flex line. Flex line to be installed as straight as possible (no hard bends).
- 2. Operator has proposed a multi-bowl wellhead assembly. Minimum working pressure of the blowout preventer (BOP) and related equipment (BOPE) required for drilling below the surface casing shoe shall be 5000 (5M) psi. Before drilling the surface casing shoe out, the BOP/BOPE shall be pressure-tested in accordance with title 43 CFR 3172.
  - a. Wellhead shall be installed by manufacturer's representatives, submit documentation with subsequent sundry.
  - b. If the welding is performed by a third party, the manufacturer's representative shall monitor the temperature to verify that it does not exceed the maximum temperature of the seal.
  - c. Manufacturer representative shall install the test plug for the initial BOP test.
  - d. If the cement does not circulate and one-inch operations would have been possible with a standard wellhead, the well head shall be cut off, cementing operations performed and another wellhead installed.
  - e. Whenever any seal subject to test pressure is broken, all the tests in 43 CFR 3172 must be followed.

#### **BOPE Break Testing Variance**

- BOPE Break Testing is ONLY permitted for intervals utilizing a 5M BOPE or less. (Annular preventer must be tested to a minimum of 70% of BOPE working pressure and shall be higher than the MASP.)
- BOPE Break Testing is NOT permitted to drilling the production hole section.
- Variance only pertains to the intermediate hole-sections and no deeper than the Bone Springs formation.
- While in transfer between wells, the BOPE shall be secured by the hydraulic carrier or cradle.
- Any well control event while drilling require notification to the BLM Petroleum Engineer (575-706-2779) prior to the commencement of any BOPE Break Testing operations.
- A full BOPE test is required prior to drilling the first deep intermediate hole section. If any subsequent hole interval is deeper than the first, a full BOPE test will be required. (200' TVD tolerance between intermediate shoes is allowable).
- The BLM is to be contacted (575-361-2822 Eddy County) 4 hours prior to BOPE tests.
- As a minimum, a full BOPE test shall be performed at 21-day intervals.
- In the event any repairs or replacement of the BOPE is required, the BOPE shall test as per 43 CFR 3172.
- If in the event break testing is not utilized, then a full BOPE test would be conducted.

#### D. SPECIAL REQUIREMENT (S)

#### **Communitization Agreement**

- The operator will submit a Communitization Agreement to the Santa Fe Office, 301 Dinosaur Trail Santa Fe, New Mexico 87508, at least 90 days before the anticipated date of first production from a well subject to a spacing order issued by the New Mexico Oil Conservation Division. The Communitization Agreement will include the signatures of all working interest owners in all Federal and Indian leases subject to the Communitization Agreement (i.e., operating rights owners and lessees of record), or certification that the operator has obtained the written signatures of all such owners and will make those signatures available to the BLM immediately upon request.
- If the operator does not comply with this condition of approval, the BLM may take enforcement actions that include, but are not limited to, those specified in 43 CFR 3163.1.
- In addition, the well sign shall include the surface and bottom hole lease numbers. When the Communitization Agreement number is known, it shall also be on the sign.

#### GENERAL REQUIREMENTS

The BLM is to be notified in advance for a representative to witness:

- a. Spudding well (minimum of 24 hours)
- b. Setting and/or Cementing of all casing strings (minimum of 4 hours)
- c. BOPE tests (minimum of 4 hours)

#### **Contact Eddy County Petroleum Engineering Inspection Staff:**

Email or call the Carlsbad Field Office, 620 East Greene St., Carlsbad, NM 88220; **BLM NM CFO DrillingNotifications@BLM.GOV**; (575) 361-2822.

- 1. Unless the production casing has been run and cemented or the well has been properly plugged, the drilling rig shall not be removed from over the hole without prior approval.
  - a. In the event the operator has proposed to drill multiple wells utilizing a skid/walking rig. Operator shall secure the wellbore on the current well, after installing and testing the wellhead, by installing a blind flange of like pressure rating to the wellhead and a pressure gauge that can be monitored while drilling is performed on the other well(s).
  - b. When the operator proposes to set surface casing with Spudder Rig
    - i. Notify the BLM when moving in and removing the Spudder Rig.
    - ii. Notify the BLM when moving in the 2<sup>nd</sup> Rig. Rig to be moved in within 90 days of notification that Spudder Rig has left the location.
    - iii. BOP/BOPE test to be conducted per **43 CFR 3172** as soon as 2<sup>nd</sup> Rig is rigged up on well.
- 2. Floor controls are required for 3M or Greater systems. These controls will be on the rig floor, unobstructed, readily accessible to the driller and will be operational at all times during drilling

Page 7 of 11

- and/or completion activities. Rig floor is defined as the area immediately around the rotary table; the area immediately above the substructure on which the draw works are located, this does not include the doghouse or stairway area.
- **3.** For intervals in which cement to surface is required, cement to surface should be verified with a visual check and density or pH check to differentiate cement from spacer and drilling mud. The results should be documented in the driller's log and daily reports.

#### A. CASING

- 1. Changes to the approved APD casing program need prior approval if the items substituted are of lesser grade or different casing size or are Non-API. The Operator can exchange the components of the proposal with that of superior strength (i.e. changing from J-55 to N-80, or from 36# to 40#). Changes to the approved cement program need prior approval if the altered cement plan has less volume or strength or if the changes are substantial (i.e. Multistage tool, ECP, etc.). The initial wellhead installed on the well will remain on the well with spools used as needed.
- 2. Wait on cement (WOC) for Potash Areas: After cementing but before commencing any tests, the casing string shall stand cemented under pressure until both of the following conditions have been met: 1) cement reaches a minimum compressive strength of 500 psi for all cement blends of both lead and tail cement, 2) until cement has been in place at least 8 hours. WOC time will be recorded in the driller's log. The casing integrity test can be done (prior to the cement setting up) immediately after bumping the plug.
- 3. Wait on cement (WOC) for Water Basin: After cementing but before commencing any tests, the casing string shall stand cemented under pressure until both of the following conditions have been met: 1) cement reaches a minimum compressive strength of 500 psi at the shoe, 2) until cement has been in place at least 8 hours. WOC time will be recorded in the driller's log. See individual casing strings for details regarding lead cement slurry requirements. The casing integrity test can be done (prior to the cement setting up) immediately after bumping the plug.
- **4.** Provide compressive strengths including hours to reach required 500 pounds compressive strength prior to cementing each casing string. Have well specific cement details onsite prior to pumping the cement for each casing string.
- **5.** No pea gravel permitted for remedial or fall back remedial without prior authorization from the BLM engineer.
- **6.** On that portion of any well approved for a 5M BOPE system or greater, a pressure integrity test of each casing shoe shall be performed. Formation at the shoe shall be tested to a minimum of the mud weight equivalent anticipated to control the formation pressure to the next casing depth or at total depth of the well. This test shall be performed before drilling more than 20 feet of new hole.
- 7. If hardband drill pipe is rotated inside casing, returns will be monitored for metal. If metal is found in samples, drill pipe will be pulled and rubber protectors which have a larger

- diameter than the tool joints of the drill pipe will be installed prior to continuing drilling operations.
- **8.** Whenever a casing string is cemented in the R-111-Q potash area, the NMOCD requirements shall be followed.

#### **B. PRESSURE CONTROL**

- 1. All blowout preventer (BOP) and related equipment (BOPE) shall comply with well control requirements as described in 43 CFR 3172.
- 2. If a variance is approved for a flexible hose to be installed from the BOP to the choke manifold, the following requirements apply: The flex line must meet the requirements of API 16C. Check condition of flexible line from BOP to choke manifold, replace if exterior is damaged or if line fails test. Line to be as straight as possible with no hard bends and is to be anchored according to Manufacturer's requirements. The flexible hose can be exchanged with a hose of equal size and equal or greater pressure rating. Anchor requirements, specification sheet and hydrostatic pressure test certification matching the hose in service, to be onsite for review. These documents shall be posted in the company man's trailer and on the rig floor.
- **3.** 5M or higher system requires an HCR valve, remote kill line and annular to match. The remote kill line is to be installed prior to testing the system and tested to stack pressure.
- **4.** If the operator has proposed a multi-bowl wellhead assembly in the APD. The following requirements must be met:
  - i. Wellhead shall be installed by manufacturer's representatives, submit documentation with subsequent sundry.
  - ii. If the welding is performed by a third party, the manufacturer's representative shall monitor the temperature to verify that it does not exceed the maximum temperature of the seal.
  - iii. Manufacturer representative shall install the test plug for the initial BOP test.
  - iv. Whenever any seal subject to test pressure is broken, all the tests in 43 CFR 3172.6(b)(9) must be followed.
  - v. If the cement does not circulate and one-inch operations would have been possible with a standard wellhead, the well head shall be cut off, cementing operations performed and another wellhead installed.
- **5.** The appropriate BLM office shall be notified a minimum of 4 hours in advance for a representative to witness the tests.
  - i. In a water basin, for all casing strings utilizing slips, these are to be set as soon as the crew and rig are ready and any fallback cement remediation has been done. The casing cut-off and BOP installation can be initiated four hours after installing the slips, which will be approximately six hours after bumping the plug. For those casing strings not using slips, the minimum wait time before cut-off is eight hours after bumping the plug. BOP/BOPE testing can begin after cut-off or once cement reaches

- 500 psi compressive strength (including lead cement), whichever is greater. However, if the float does not hold, cut-off cannot be initiated until cement reaches 500 psi compressive strength (including lead when specified).
- ii. In potash areas, for all casing strings utilizing slips, these are to be set as soon as the crew and rig are ready and any fallback cement remediation has been done. For all casing strings, casing cut-off and BOP installation can be initiated at twelve hours after bumping the cement plug. The BOPE test can be initiated after bumping the cement plug with the casing valve open. (Only applies to single stage cement jobs, prior to the cement setting up.)
- iii. The tests shall be done by an independent service company utilizing a test plug not a cup or J-packer and can be initiated immediately with the casing valve open. The operator also has the option of utilizing an independent tester to test without a plug (i.e. against the casing) pursuant to **43 CFR 3172** with the pressure not to exceed 70% of the burst rating for the casing. Any test against the casing must meet the WOC time for 8 hours or 500 pounds compressive strength, whichever is greater, prior to initiating the test (see casing segment as lead cement may be critical item).
- iv. The test shall be run on a 5000-psi chart for a 2-3M BOP/BOP, on a 10000 psi chart for a 5M BOP/BOPE and on a 15000 psi chart for a 10M BOP/BOPE. If a linear chart is used, it shall be a one-hour chart. A circular chart shall have a maximum 2-hour clock. If a twelve hour or twenty-four-hour chart is used, tester shall make a notation that it is run with a two hour clock.
- v. The results of the test shall be reported to the appropriate BLM office.
- vi. All tests are required to be recorded on a calibrated test chart. A copy of the BOP/BOPE test chart and a copy of independent service company test will be submitted to the appropriate BLM office.
- vii. The BOP/BOPE test shall include a low-pressure test from 250 to 300 psi. The test will be held for a minimum of 10 minutes if test is done with a test plug and 30 minutes without a test plug. This test shall be performed prior to the test at full stack pressure.
- viii. BOP/BOPE must be tested by an independent service company within 500 feet of the top of the Wolfcamp formation if the time between the setting of the intermediate casing and reaching this depth exceeds 20 days. This test does not exclude the test prior to drilling out the casing shoe as per 43 CFR 3172.

#### C. DRILLING MUD

Mud system monitoring equipment, with derrick floor indicators and visual and audio alarms, shall be operating before drilling into the Wolfcamp formation, and shall be used until production casing is run and cemented.

#### D. WASTE MATERIAL AND FLUIDS

All waste (i.e. drilling fluids, trash, salts, chemicals, sewage, gray water, etc.) created as a result of drilling operations and completion operations shall be safely contained and disposed of properly at a waste disposal facility. No waste material or fluid shall be disposed of on the well location or surrounding area. Porto-johns and trash containers will be on-location during fracturing operations or any other crew-intensive operations.

SA 08/28/2025

#### Hydrogen Sulfide Drilling Operations Plan Mewbourne Oil Company

#### 1. General Requirements

Rule 118 does not apply to this well because MOC has researched this area and no high concentrations of H2S were found. MOC will have on location and working all H2S safety equipment before the Delaware formation for purposes of safety and insurance requirements.

#### 2. Hydrogen Sulfide Training

All personnel, whether regularly assigned, contracted, or employed on an unscheduled basis, will have received training from a qualified instructor in the following areas prior to entering the drilling pad area of the well:

- 1. The hazards and characteristics of hydrogen sulfide gas.
- 2. The proper use of personal protective equipment and life support systems.
- 3. The proper use of hydrogen sulfide detectors, alarms, warning systems, briefing areas, evacuation procedures.
- 4. The proper techniques for first aid and rescue operations.

Additionally, supervisory personnel will be trained in the following areas:

- The effects of hydrogen sulfide on metal components. If high tensile tubular systems are utilized, supervisory personnel will be trained in their special maintenance requirements.
- 2 Corrective action and shut in procedures, blowout prevention, and well control procedures while drilling a well.
- The contents of the Hydrogen Sulfide Drilling Operations Plan.

There will be an initial training session prior to encountering a know hydrogen sulfide source. The initial training session shall include a review of the site specific Hydrogen Sulfide Drilling Operations Plan.

#### 3. Hydrogen Sulfide Safety Equipment and Systems

All hydrogen sulfide safety equipment and systems will be installed, tested, and operational prior to drilling below the 9 5/8" intermediate casing.

#### 1. Well Control Equipment

- A. Choke manifold with minimum of one adjustable choke/remote choke.
- B. Blowout preventers equipped with blind rams and pipe rams to accommodate all pipe sizes with properly sized closing unit
- C. Auxiliary equipment including annular type blowout preventer.
- 2. Protective Equipment for Essential Personnel

Thirty minute self contained work unit located in the dog house and at briefing areas.

Additionally: If H2S is encountered in concentrations less than 10 ppm, fans will be placed in work areas to prevent the accumulation of hazardous amounts of poisonous gas. If higher concentrations of H2S are detected the well will be shut in and a rotating head, mud/gas separator, remote choke and flare line with igniter will be installed.

#### 3. Hydrogen Sulfide Protection and Monitoring Equipment

Two portable hydrogen sulfide monitors positioned on location for optimum coverage and detection. The units shall have audible sirens to notify personnel when hydrogen sulfide levels exceed 20 PPM.

#### 4. <u>Visual Warning Systems</u>

- A. Wind direction indicators as indicated on the wellsite diagram.
- B. Caution signs shall be posted on roads providing access to location. Signs shall be painted a high visibility color with lettering of sufficient size to be readable at reasonable distances from potentially contaminated areas.

#### 4. Mud Program

The mud program has been designed to minimize the amount of hydrogen sulfide entrained in the mud system. Proper mud weight, safe drilling practices, and the use of hydrogen sulfide scavengers will minimize hazards while drilling the well.

#### 5. Metallurgy

All tubular systems, wellheads, blowout preventers, drilling spools, kill lines, choke manifolds, and valves shall be suitable for service in a hydrogen sulfide environment when chemically treated.

#### 6. Communications

State & County Officials phone numbers are posted on rig floor and supervisors trailer. Communications in company vehicles and toolpushers are either two way radios or cellular phones.

#### 7. Well Testing

Drill stem testing is not an anticipated requirement for evaluation of this well. If a drill stem test is required, it will be conducted with a minimum number of personnel in the immediate vicinity. The test will be conducted during daylight hours only.

#### 8. Emergency Phone Numbers

<b>Eddy County Sheriff's Office</b>	911 or 575-887-7551
Ambulance Service	911 or 575-885-2111
Carlsbad Fire Dept	911 or 575-885-2111
Loco Hills Volunteer Fire Dept.	911 or 575-677-3266
<b>Closest Medical Facility - Columbia Medical Center</b>	of Carlsbad 575-492-5000

Mewbourne Oil Company	Hobbs District Office Fax 2 <sup>nd</sup> Fax	575-393-5905 575-397-6252 575-393-7259
District Manager	Robin Terrell	575-390-4816
<b>Drilling Superintendent</b>	Frosty Lathan	575-390-4103
•	Bradley Bishop	575-390-6838
<b>Drilling Foreman</b>	Wesley Noseff	575-441-0729

**Operator Name: MEWBOURNE OIL COMPANY** 

Well Name: BLOOMIN ONION 11/14 FED COM Well Number: 715H

#### **Section 7 - Methods for Handling**

Waste type: SEWAGE

Waste content description: Human waste & grey water

Amount of waste: 1500 gallons

Waste disposal frequency: Weekly

Safe containment description: 2,000 gallon plastic container

Safe containment attachment:

Waste disposal type: HAUL TO COMMERCIAL Disposal location ownership: PRIVATE

**FACILITY** 

Disposal type description:

Disposal location description: City of Carlsbad Water Treatment facility

Waste type: GARBAGE

Waste content description: Garbage & trash

Amount of waste: 1500 pounds

Waste disposal frequency : One Time Only

Safe containment description: Enclosed trash trailer

Safe containmant attachment:

Waste disposal type: HAUL TO COMMERCIAL Disposal location ownership: PRIVATE

FACILITY

Disposal type description:

**Disposal location description:** Waste Management facility in Carlsbad.

Waste type: DRILLING

Waste content description: Drill cuttings

Amount of waste: 3510 barrels

Waste disposal frequency : One Time Only

Safe containment description: Drill cuttings will be properly contained in steel tanks (20 yard roll off bins.)

Safe containment attachment:

Waste disposal type: HAUL TO COMMERCIAL Disposal location ownership: PRIVATE

FACILITY

Disposal type description:

Disposal location description: NMOCD approved waste disposal locations are CRI or Lea Land, both facilities are located

on HWY 62/180, Sec. 27 T20S R32E.

#### **Reserve Pit**

Reserve Pit being used? NO

**Operator Name: MEWBOURNE OIL COMPANY** 

Well Name: BLOOMIN ONION 11/14 FED COM Well Number: 715H

Temporary disposal of produced water into reserve pit? NO

Reserve pit length (ft.) Reserve pit width (ft.)

Reserve pit depth (ft.) Reserve pit volume (cu. yd.)

Is at least 50% of the reserve pit in cut?

Reserve pit liner

Reserve pit liner specifications and installation description

#### **Cuttings Area**

Cuttings Area being used? NO

Are you storing cuttings on location? N

**Description of cuttings location** 

Cuttings area length (ft.) Cuttings area width (ft.)

Cuttings area depth (ft.) Cuttings area volume (cu. yd.)

Is at least 50% of the cuttings area in cut?

**Cuttings area liner** 

Cuttings area liner specifications and installation description

#### **Section 8 - Ancillary**

Are you requesting any Ancillary Facilities?: N

**Ancillary Facilities** 

Comments:

**Section 9 - Well Site** 

Well Site Layout Diagram:

BLOOMIN\_ONION\_11\_14\_FED\_COM\_715H\_WellSiteLayout\_20250520151300.pdf

Comments: NONE

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Sante Fe Main Office Phone: (505) 476-3441

General Information Phone: (505) 629-6116

Online Phone Directory https://www.emnrd.nm.gov/ocd/contact-us

# State of New Mexico Energy, Minerals and Natural Resources Oil Conservation Division 1220 S. St Francis Dr. Santa Fe, NM 87505

ACKNOWLEDGMENTS

Action 502447

#### **ACKNOWLEDGMENTS**

Operator:	OGRID:
MEWBOURNE OIL CO	14744
P.O. Box 5270	Action Number:
Hobbs, NM 88241	502447
	Action Type:
	[C-101] BLM - Federal/Indian Land Lease (Form 3160-3)

#### ACKNOWLEDGMENTS

I hereby certify that no additives containing PFAS chemicals will be added to the completion or recompletion of this well.

Sante Fe Main Office Phone: (505) 476-3441

General Information Phone: (505) 629-6116

Online Phone Directory https://www.emnrd.nm.gov/ocd/contact-us

# State of New Mexico Energy, Minerals and Natural Resources Oil Conservation Division 1220 S. St Francis Dr. Santa Fe, NM 87505

CONDITIONS

Action 502447

#### **CONDITIONS**

Operator:	OGRID:
MEWBOURNE OIL CO	14744
P.O. Box 5270	Action Number:
Hobbs, NM 88241	502447
	Action Type:
	[C-101] BLM - Federal/Indian Land Lease (Form 3160-3)

#### CONDITIONS

Created By	Condition	Condition Date
mleal	Cement is required to circulate on both surface and intermediate1 strings of casing.	9/3/2025
mleal	If cement does not circulate on any string, a Cement Bond Log (CBL) is required for that string of casing.	9/3/2025
ward.rikala	Notify the OCD 24 hours prior to casing & cement.	9/9/2025
ward.rikala	File As Drilled C-102 and a directional Survey with C-104 completion packet.	9/9/2025
ward.rikala	Once the well is spud, to prevent ground water contamination through whole or partial conduits from the surface, the operator shall drill without interruption through the fresh water zone or zones and shall immediately set in cement the water protection string.	9/9/2025
ward.rikala	Oil base muds are not to be used until fresh water zones are cased and cemented providing isolation from the oil or diesel. This includes synthetic oils. Oil based mud, drilling fluids and solids must be contained in a steel closed loop system.	9/9/2025
ward.rikala	This well is within the Capitan Reef. The first intermediate casing string shall be sat and cemented back to surface immediately above the Capitan Reef. The second intermediate string shall be set and cemented back to surface immediately below the base of the Capitan Reef.	9/9/2025
ward.rikala	Operator must comply with all of the R-111-Q requirements.	9/9/2025