

Santa Fe Main Office
Phone: (505) 476-3441
General Information
Phone: (505) 629-6116

State of New Mexico
Energy, Minerals and Natural Resources

Form C-103
Revised July 18, 2013

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OIL CONSERVATION DIVISION
1220 South St. Francis Dr.
Santa Fe, NM 87505

SUNDRY NOTICES AND REPORTS ON WELLS (DO NOT USE THIS FORM FOR PROPOSALS TO DRILL OR TO DEEPEN OR PLUG BACK TO A DIFFERENT RESERVOIR. USE "APPLICATION FOR PERMIT" (FORM C-101) FOR SUCH PROPOSALS.)		WELL API NO. 30-015-55313
1. Type of Well: Oil Well <input type="checkbox"/> Gas Well <input checked="" type="checkbox"/> Other <input type="checkbox"/> SWD		5. Indicate Type of Lease STATE <input checked="" type="checkbox"/> FEE <input type="checkbox"/>
2. Name of Operator CHEVRON USA, INC.		6. State Oil & Gas Lease No.
3. Address of Operator 6301 DEAUVILLE BLVD, MIDLAND, TEXAS 79706		7. Lease Name or Unit Agreement Name SEVERITAS 2 STATE SWD
4. Well Location Unit Letter <u>A</u> : <u>809</u> feet from the <u>NORTH</u> line and <u>960</u> feet from the <u>EAST</u> line Section <u>2</u> Township <u>26S</u> Range <u>27E</u> NMPM County <u>EDDY</u>		8. Well Number 001
11. Elevation (Show whether DR, RKB, RT, GR, etc.)		9. OGRID Number 4323
		10. Pool name or Wildcat SWD; DELAWARE

12. Check Appropriate Box to Indicate Nature of Notice, Report or Other Data

NOTICE OF INTENTION TO: PERFORM REMEDIAL WORK <input type="checkbox"/> PLUG AND ABANDON <input type="checkbox"/> TEMPORARILY ABANDON <input type="checkbox"/> CHANGE PLANS <input type="checkbox"/> PULL OR ALTER CASING <input type="checkbox"/> MULTIPLE COMPL <input type="checkbox"/> DOWNHOLE COMMINGLE <input type="checkbox"/> CLOSED-LOOP SYSTEM <input type="checkbox"/> OTHER: <input type="checkbox"/>		SUBSEQUENT REPORT OF: REMEDIAL WORK <input type="checkbox"/> ALTERING CASING <input type="checkbox"/> COMMENCE DRILLING OPNS. <input type="checkbox"/> P AND A <input type="checkbox"/> CASING/CEMENT JOB <input type="checkbox"/> DFIT;SRT;BHL PRESSURE TESTS <input checked="" type="checkbox"/>	
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13. Describe proposed or completed operations. (Clearly state all pertinent details, and give pertinent dates, including estimated date of starting any proposed work). SEE RULE 19.15.7.14 NMAC. For Multiple Completions: Attach wellbore diagram of proposed completion or recompletion.

CHEVRON USA, INC. SUBMITS THE FINAL TEST RESULTS FOR THE DFIT; SRT AND BOTTOM HOLE PRESSURES RUN ON THE SEVERITAS 2 STATE SWD 001 / API 30-015-55313 FOR THE CHERRY CANYON AND BELL CANYON FORMATIONS

PLEASE SEE ATTACHED

Spud Date:

Rig Release Date:

I hereby certify that the information above is true and complete to the best of my knowledge and belief.

SIGNATURE Carol Adler TITLE Sr. Regulatory Affairs Coordinator DATE 12/23/2025

Type or print name Carol Adler E-mail address: caroladler@chevron.com PHONE: (432) 687-7723

For State Use Only

APPROVED

BY: _____ TITLE _____ DATE _____ Conditions
of Approval (if any):

the human energy company™

Severitas SWD DFIT Interpretations

Xinghui “Lou” Liu, Brent Kebert, and Kris Walker
12/19/2025

Severitas SWD DFIT Result Summary

Stress Measurement Results

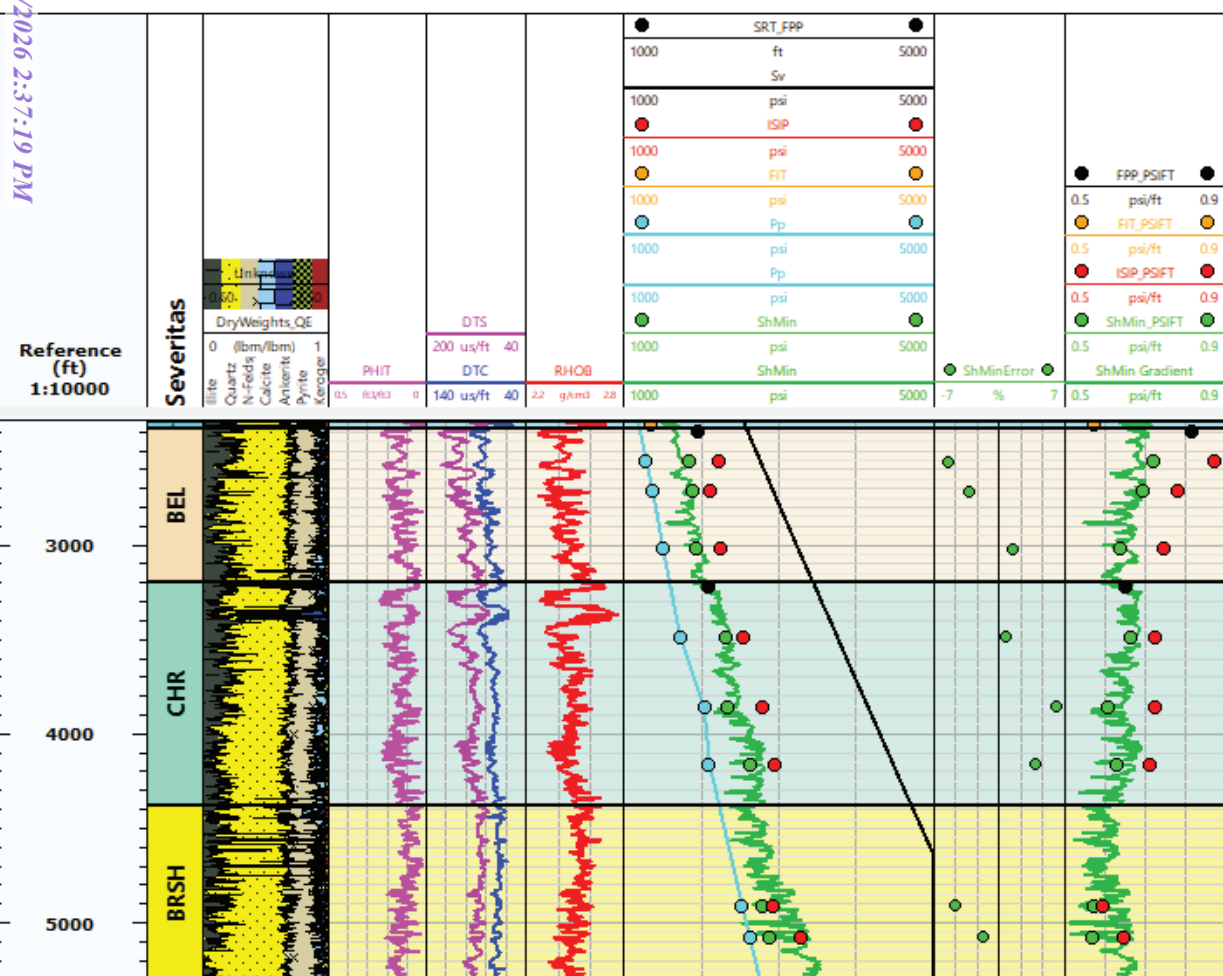
Test	Perf MD, ft	TVD, ft	Breakdown WHP, psi	ISIP, psi	Shmin, psi	ISIP Grad, psi/ft	Shmin Grad, psi/ft	Stress Confidence
Bell DFIT 3	2558.7 - 2561.7	2559.2	3579.0	2233.3	1841.0	0.87	0.72	High
Bell DFIT 2	2714.7 - 2717.7	2715.2	2674.2	2114.6	1882.6	0.78	0.69	High
Bell DFIT 1	3020.5 - 3023.5	3020.8	2880.7	2251.6	1930.9	0.75	0.64	High
Cherry DFIT 3	3487.0 - 3491.0	3488.0	1752.0	2534.2	2320.2	0.73	0.67	High
Cherry DFIT 2	3858.6 - 3861.6	3858.4	2537.0	2790.7	2337.7	0.72	0.61	Moderate
Cherry DFIT 1	4161.8 - 4164.8	4161.4	2929.0	2954.8	2624.8	0.71	0.63	High
Brushy DFIT 3	4911.0 - 4914.0	4909.7	3952.0	2919.2	2803.2	0.59	0.57	Moderate
Brushy DFIT 2	5077.0 - 5080.0	5076.1	2911.0	3281.8	2889.8	0.65	0.57	High

Pore Pressure and Frac Fluid Efficiency Results

Test	Perf MD, ft	TVD, ft	Pore Pressure, psi	Pp Grad, psi/ft	Pumped Vol (bbl)	Closure time (min)	Frac Fluid Efficiency	Permeability Level
Bell DFIT 3	2558.7 - 2561.7	2559.2	1286.9	0.50	22.0	50.0	0.74	Moderate
Bell DFIT 2	2714.7 - 2717.7	2715.2	1381.1	0.51	20.0	24.0	0.64	High
Bell DFIT 1	3020.5 - 3023.5	3020.8	1516.2	0.50	22.0	52.8	0.76	Moderate
Cherry DFIT 3	3487.0 - 3491.0	3488.0	1738.2	0.50	20.0	9.4	0.54	High
Cherry DFIT 2	3858.6 - 3861.6	3858.4	2047.7	0.53	5.0	8.5	0.72	Moderate
Cherry DFIT 1	4161.8 - 4164.8	4161.4	2095.8	0.50	20.0	9.4	0.43	High
Brushy DFIT 3	4911.0 - 4914.0	4909.7	2524.0	0.51	15.0	6.1	0.56	High
Brushy DFIT 2	5077.0 - 5080.0	5076.1	2633.8	0.52	20.0	101.8	0.85	Low



DFIT/SFT Integration with Mechanical Earth Model for Severitas



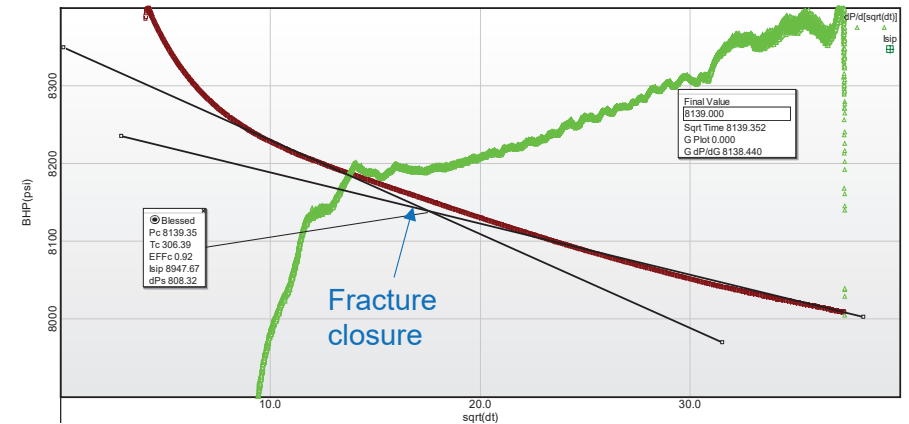
- 6 DFIT measurements measure fracture closure pressure (ShMin), instantaneous shut-in pressure (ISIP), and pore pressure (Pp)
- 2 SRT measurements estimate fracture closure pressure (FFP)
- 1 formation integrity test (FIT) at the top of the interval
- Anisotropic sonic logging was performed using Stoneley inversion guided by independent measurements of mud slowness
- Lab measurements provided correlations to get full anisotropy logs and dynamic-static conversion
- A minor constant tectonic horizontal strain of $2e-5$ is required to align ShMin measurements and logs resulting in a standard deviation of 4%
- ShMin is linear at ~ 0.66 psi/ft down to 4200 ft
- Both fracture gradient & pore pressure gradient start decreasing in the lower Cherry & Brushy to ~ 0.60 psi/ft
- ShMin comes close to pore pressure at ~ 5000 ft indicating formation is close to being critically stressed
- Petrophysical logging data reveals several ankerite bearing intervals, some as thick as 85 ft, between 4310 and 4910 ft that have porosities less than 4%. These intervals are interpreted to have extremely low permeability and may act as flow & pressure barriers that compartmentalize injection activities above 4200 ft



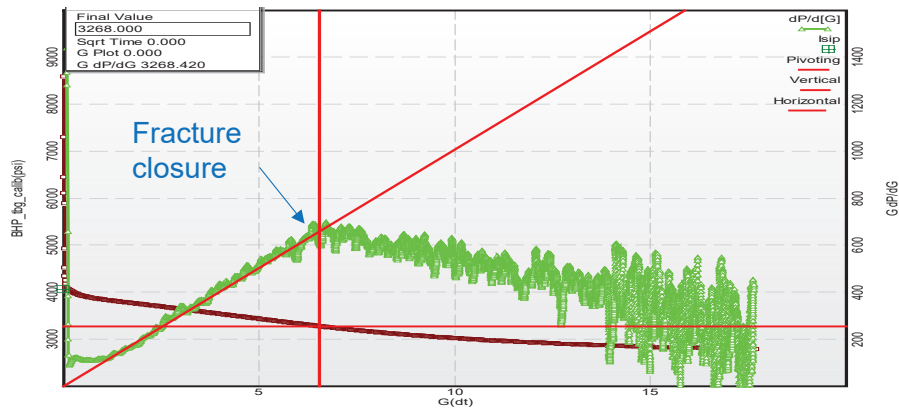
Pre-Closure Analysis Methods and Plots

- Commonly used pressure decline analysis techniques to obtain closure stress include:
 - Square-root time plot
 - G-function plot
 - Log-log plot
- Among techniques using these diagnostic plots, the G-function plot is the most popular.

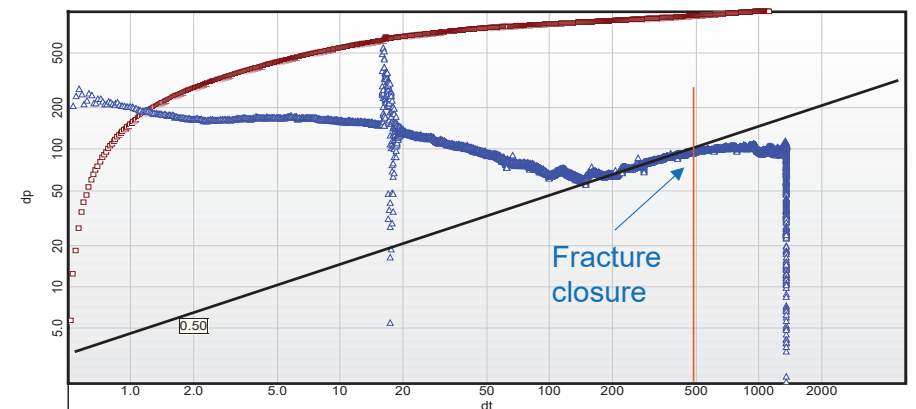
Typical Square Root Time Plot



Typical G Function Plot



Typical Log-Log Plot



G-time Function Method for Pre-Closure Analysis

- A straight-line pressure response over time during shut-in is the best way to characterize fracture closing behavior.
- A G-time function was introduced by Nolte (1979) in the paper SPE- 8341 to analyze pressure decline data:

$$\Delta P = (P_f - P_c) \propto \frac{\pi C_L \sqrt{t_p}}{2 c_f} G(\Delta t_D)$$

- Pre-closure analysis (**PCA**) is thus performed using one of the three types of plots:
 - Pressure vs G-function time
 - Pressure vs square root of time
 - Pressure vs time on log-log scale
- G-function is most popular, as it is often used to identify natural fracture opening in addition to closure stress.
- In addition to closure stress (Shmin), the following parameters can be determined from PCA:
 - Instantaneous Shut-In Pressure (ISIP)
 - Net fracture pressure
 - Fracture fluid efficiency

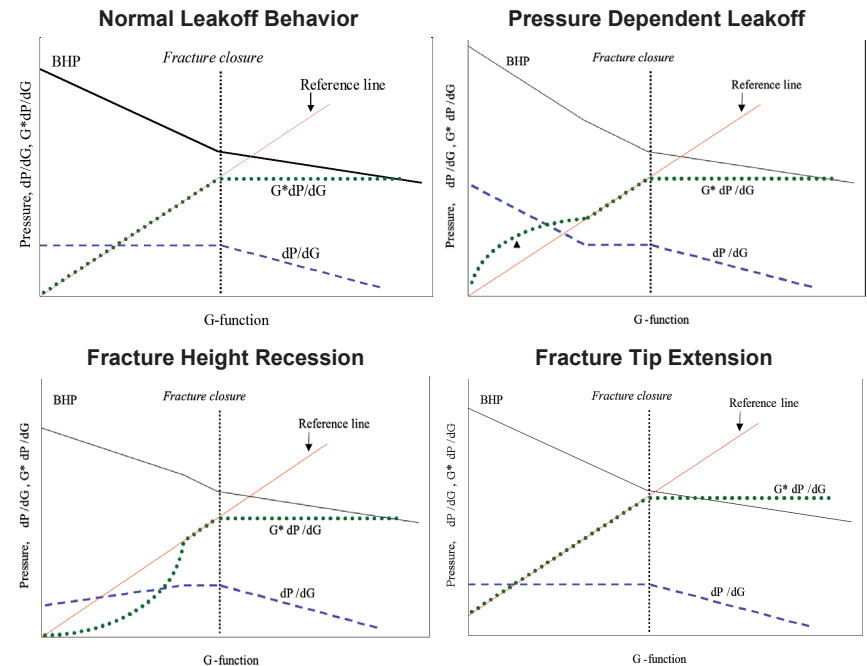
G-function Definition

$$\Delta t_D = (t - t_p) / t_p$$

$$G(\Delta t_D) = \frac{4}{\pi} (g(\Delta t_D) - g_0)$$

$$g(\Delta t_D) = \begin{cases} 4/3 \left((1 + \Delta t_D)^{1.5} - \Delta t_D^{1.5} \right) & \text{low leakoff} \\ (1 + \Delta t_D) \sin^{-1}(1 + \Delta t_D)^{-0.5} + \Delta t_D^{0.5} & \text{high leakoff} \end{cases}$$

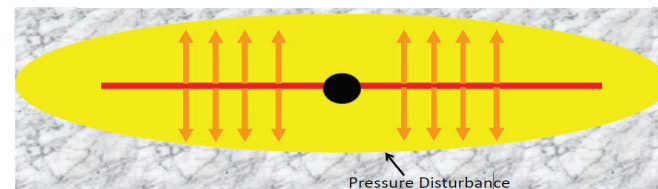
where t is total time and t_p is pumping time



After-Closure Analysis

- After-closure analysis is performed after the fracture closes.
- ACA is based on the “**impulse solution**”, which assumes a short duration of injection and depends on the injection volume.
- Traditional pressure transient analysis (PTA) is typically based on the “constant-rate solution”.
- During the pressure decline, **two linear flow regimes** can develop:
 - The first linear flow** is driven by fluid leakoff from the fracture into the formation before the fracture closure.
 - Once the fracture is closed, **the second linear flow** is the pressure fall-off behavior in the formation without any fluid coming from the fracture. It calls as pseudo linear flow (**PLF**).
- If the shut-in is long enough and the reservoir is more permeable, a pseudo radial flow (**PRF**) may develop. In this case, the fracture acts as a giant wellbore, and the reservoir pressure and permeability can be determined independent of fracture geometry.
- More uncertainty is associated with reservoir permeability estimation from PLF as it depends on fracture geometry and leakoff behavior. It is difficult to accurately determine fracture length/height for small injection tests.

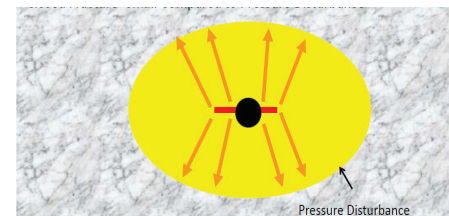
Pseudo-Linear Flow



$$p(t) - p_r = m_L F_L(t, t_c) \quad m_L = C_T \sqrt{\frac{\pi \mu}{k \phi c_t}}$$

$$F_L(t, t_c) = \frac{2}{\pi} \sin^{-1} \sqrt{\frac{t_c}{t}} \quad C_T = \frac{V_{inj}}{8 h x_f \sqrt{t_c}}$$

Pseudo-Radial Flow



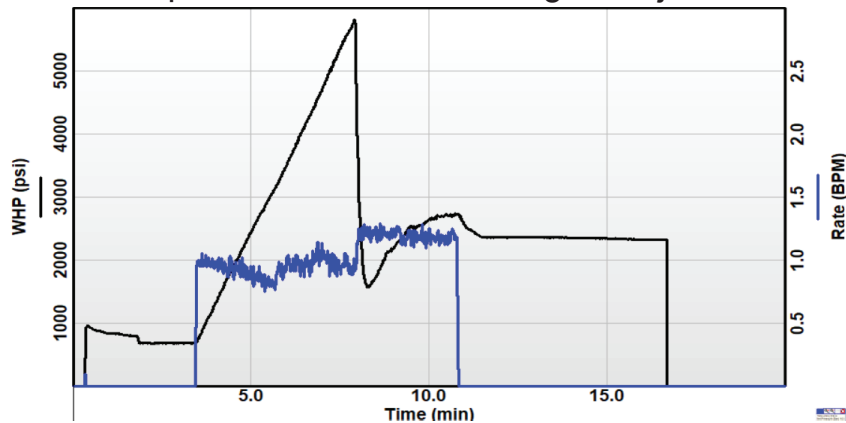
$$p(t) - p_r = m_R F_R(t, t_c) \quad m_R = \frac{\pi}{16} \frac{V_{i1} \mu}{k h t_c}$$

$$F_R(t, t_c) = \frac{1}{4} \ln\left(1 + \frac{\chi t_c}{t - t_c}\right) \quad \chi = \frac{16}{\pi^2} \cong 1.6$$



Brushy Canyon DFIT-1 Test

Pump Pressure & Rate during 1st Injection



- The shut-in pressure declined only by 35 psi in one hour and 50 minutes after the first injection. The perf interval seems very tight.
- Second injection was performed after bleeding off. The shut-in pressure remained flat.
- The ISIP for the second injection was lower by 1,237 psi compared to the first injection.
- At this point, it was clear that closure stress could not obtain from this interval.

Surface Gauge Pressure during 1st & 2nd Injections



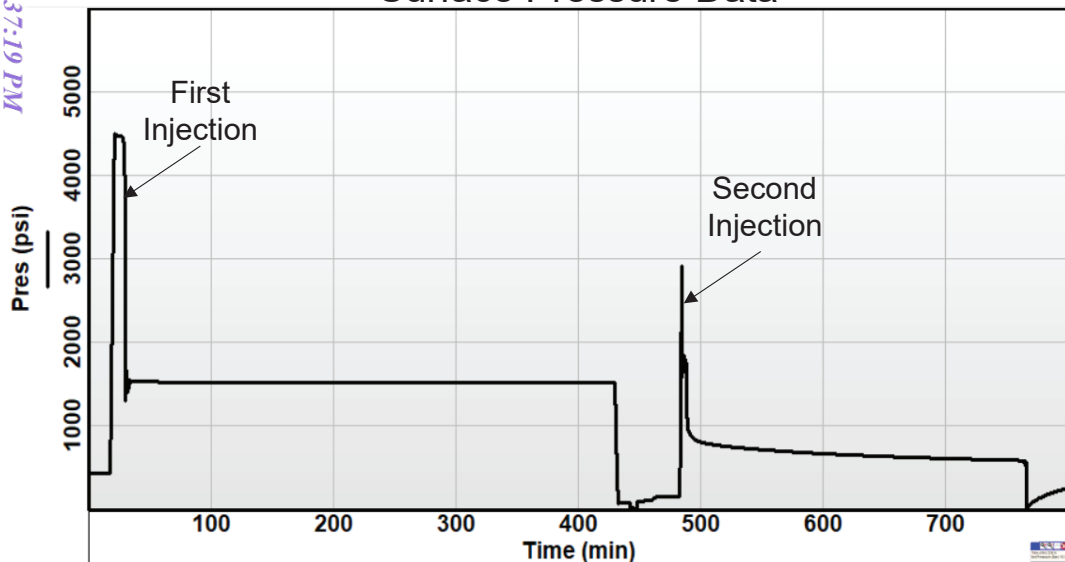
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Test date	11/6/2025	11/7/2025
Test start time, MST	10:48 PM	12:52 AM
Perforation interval MD, ft	5259-5262	5259-5262
TVD, ft	5,258.0	5,258.0
Injection cycle	1	2
Pumping time, min	7.5	3.2
Pump-in volume, bbl	7.6	3.6
Fluid density, ppg	8.4	8.4
Breakdown pressure at surface, psi	5,726	4,532
ISIP at surface, psi	2,718	1,481
BH ISIP, psi	5,011	3,774

Brushy Canyon DFIT-2 Test Data

Surface Pressure Data



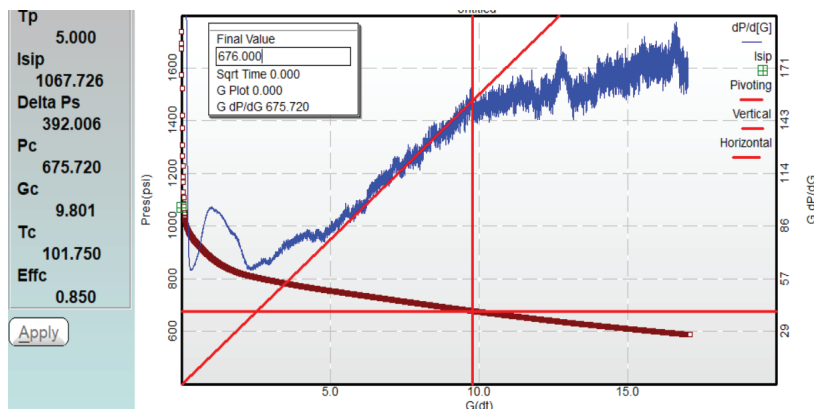
- 6 bbl was pumped during the first injection, but the pressure remained flat during the shut-in.

Test date	11/7/2025	11/7/2025
Test start time, MST	4:30 AM	12:13 PM
Perforation interval MD, ft	5077-5080	5077-5080
TVD, ft	5076.1	5076.1
Injection cycle	1	2
Pumping time, min	4.0	6.0
Pump-in volume, bbl	6.0	20.0
Fluid density, ppg	8.4	8.4
Breakdown pressure at surface, psi	4,493	2,911
ISIP at surface, psi	1,785	1,068
BH ISIP, psi	3,999	3,282

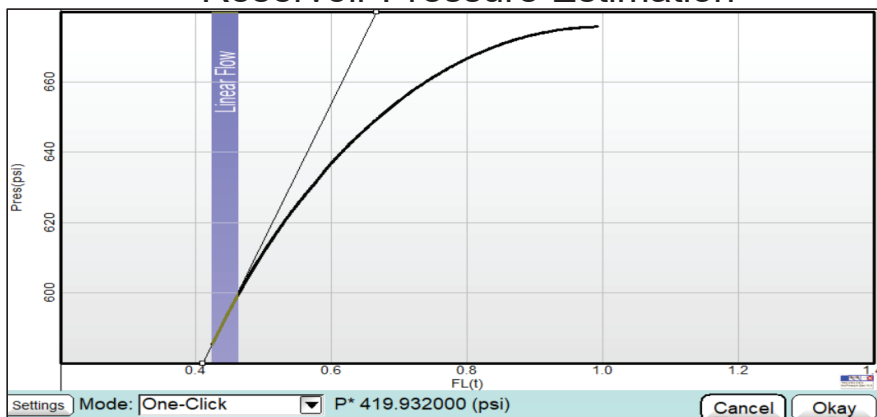
- The interval should be very permeable, which was confirmed by a geologist.
- The fracture might be closed immediately after the first injection was stopped.
- With this reason, the second injection was pumped with 20 bbl, and nice pressure decline was observed during the shut-in.

Brushy Canyon DFIT-2 Data Interpretation

Closure Analysis



Reservoir Pressure Estimation



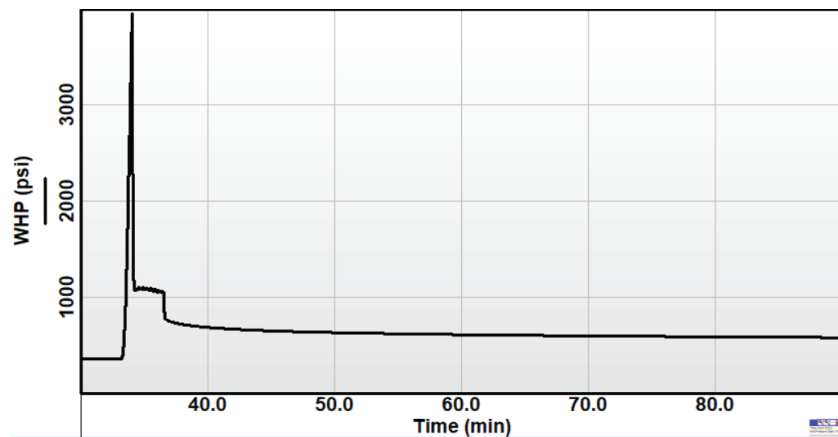
Test date	11/7/2025
Test start time, MST	12:13 PM
Perforation interval MD, ft	5077-5080
TVD, ft	5076.1
Pumping time, min	6.0
Pump-in volume, bbl	20.0
Fluid density, ppg	8.4
Breakdown pressure at surface, psi	2,911
ISIP at surface, psi	1,068
BH ISIP, psi	3,282
G-dP/dG Pc, psi	676
Shmin, psi	2,890
Frac closure time, min	101.8
After Closure Linear p*, psi	420
Reservoir pressure, psi	2,634

- Closure analysis of the second injection data indicated that the fracture created by the DFIT was in 101.8 min.
- The closure pressure or Shmin at perf interval is 2,890 psi (0.57 psi/ft).
- Reservoir pressure was estimated from linear flow analysis: 419.9 psi at surface or 2,634 psi (0.52 psi/ft) at perf interval.

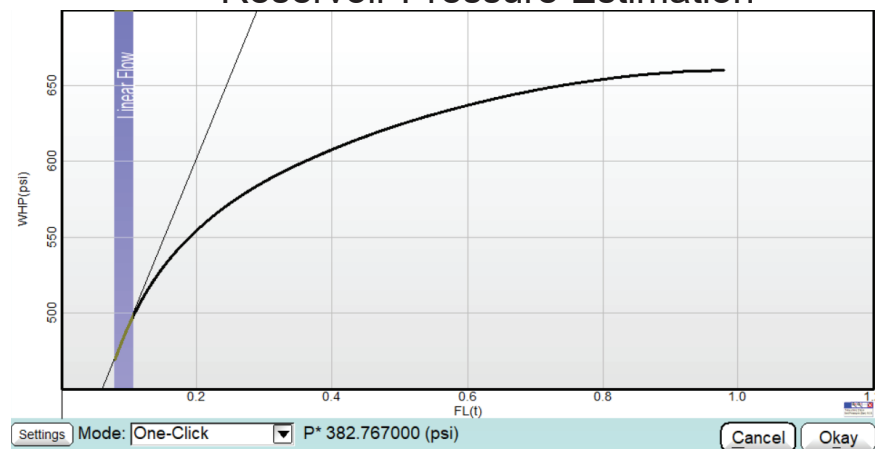


Brushy Canyon DFIT-3 Data Interpretation

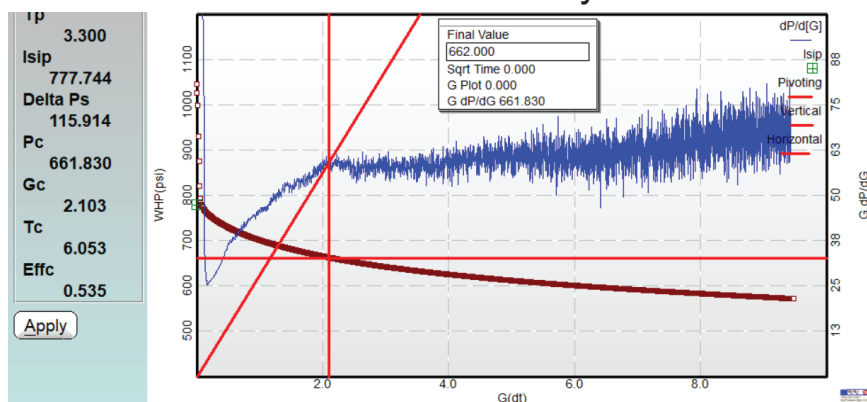
Surface Pressure Data



Reservoir Pressure Estimation



DFIT Closure Analysis

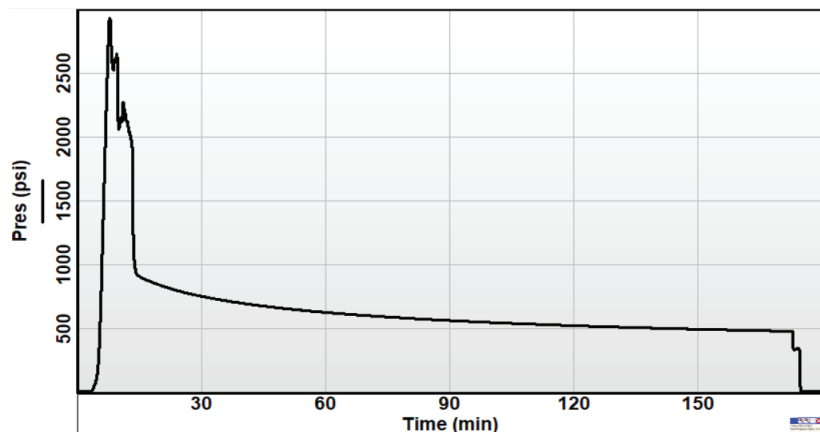


Test date	11/7/2025
Test start time, MST	7:33 PM
Perforation interval MD, ft	4911-4914
TVD, ft	4,909.7
Pumping time, min	3.3
Pump-in volume, bbl	15
Fluid density, ppg	8.4
Breakdown pressure at surface, psi	3,952
ISIP at surface, psi	778
BH ISIP, psi	2,919
G-dP/dG Pc, psi	662
Shmin, psi	2,803
Frac closure time, min	6.1
After Closure Linear p*, psi	383
Reservoir pressure, psi	2,524

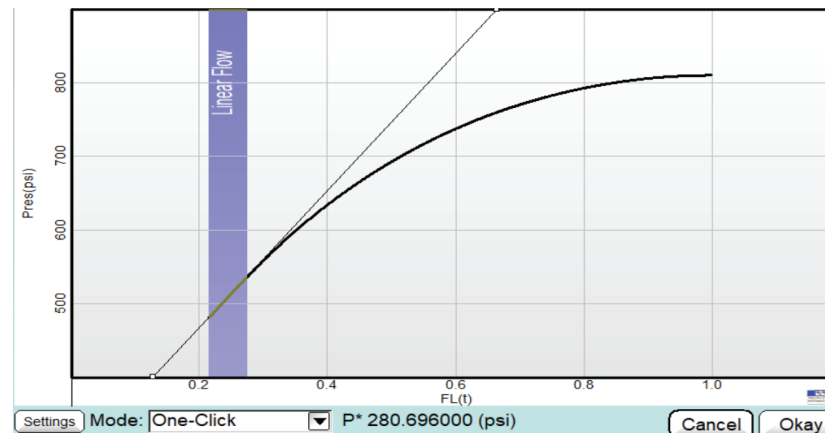


Cherry Canyon DFIT-1 Data Interpretation

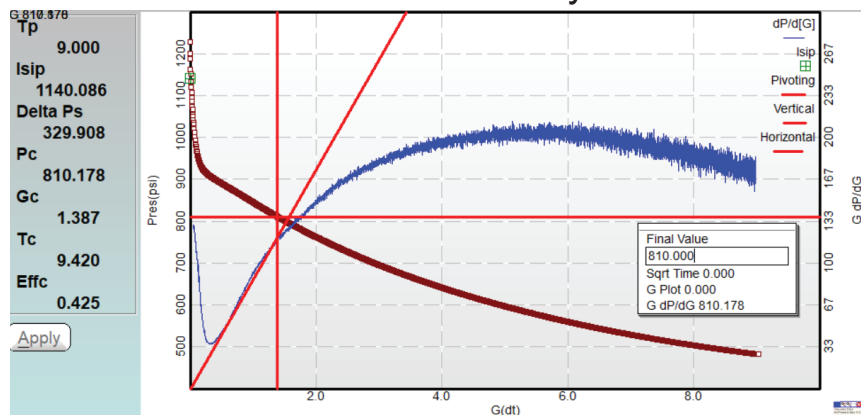
Surface Pressure Data



Reservoir Pressure Estimation



DFIT Closure Analysis

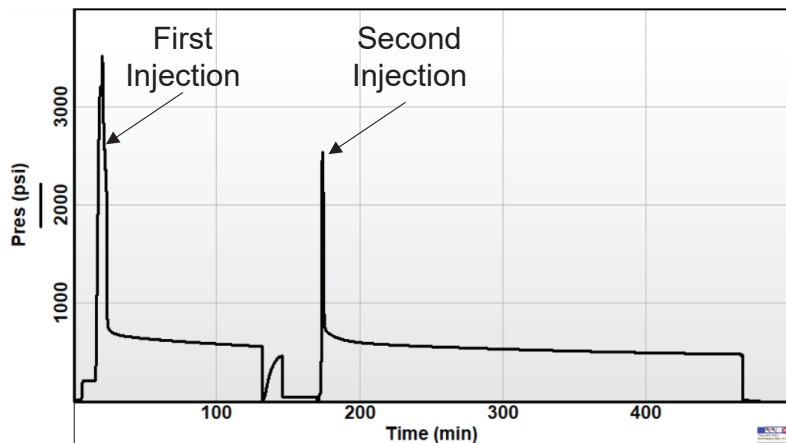


Test date	11/14/2025
Test start time, MST	1:14 AM
Perforation interval MD, ft	4161.8-4164.8
TVD, ft	4,161.4
Pumping time, min	9
Pump-in volume, bbl	20
Fluid density, ppg	8.4
Breakdown pressure at surface, psi	2,929
ISIP at surface, psi	778
BH ISIP, psi	2,919
G-dP/dG Pc, psi	810
Shmin, psi	2,625
Frac closure time, min	9.4
After Closure Linear p*, psi	218
Reservoir pressure, psi	2,096

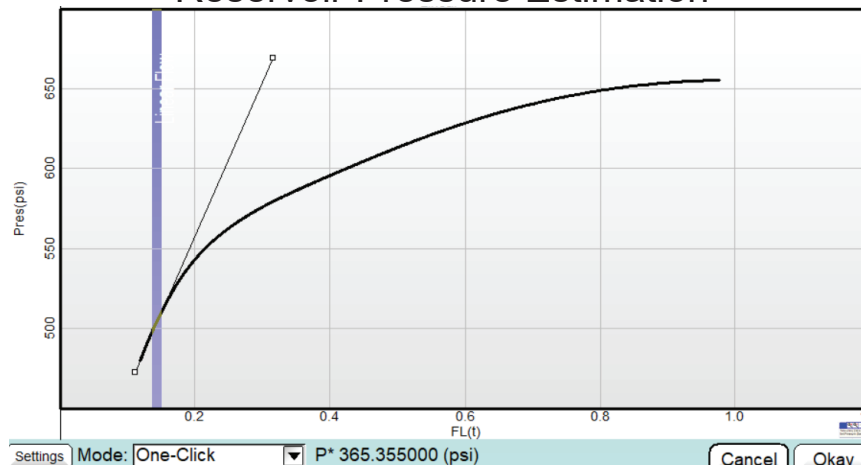


Cherry Canyon DFIT-2 Data Interpretation

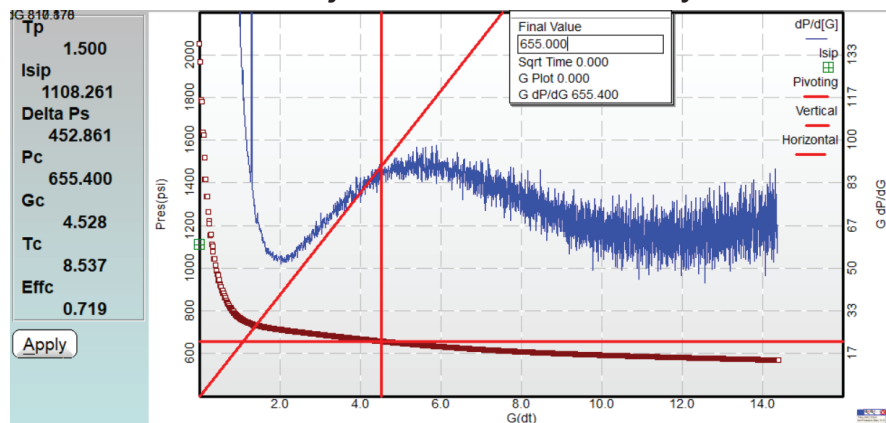
Surface Pressure Data



Reservoir Pressure Estimation



Second Injection Closure Analysis



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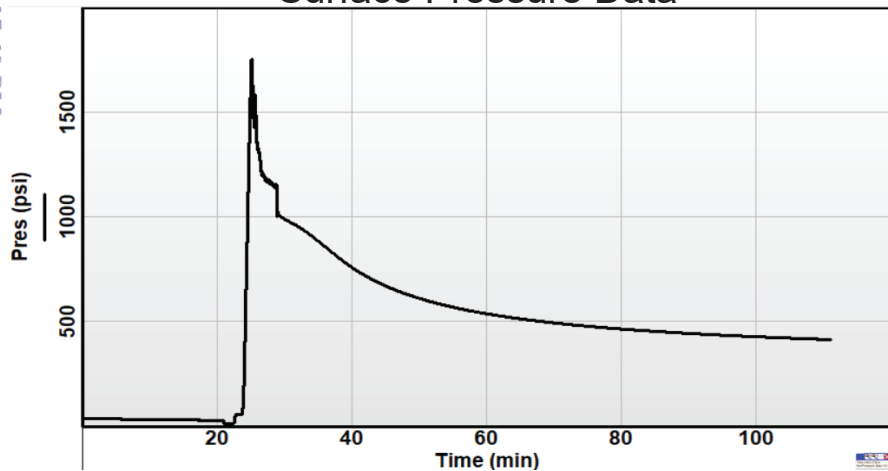


Test date	11/14/2025	11/14/2025
Test start time, MST	6:15 PM	8:51 PM
Perforation interval MD, ft	3858.6-3861.6	3858.6-3861.6
TVD, ft	3858.4	3858.4
Injection cycle	1	2
Pumping time, min	7	2
Pump-in volume, bbl	20	5
Fluid density, ppg	8.4	8.4
Breakdown WHP, psi	3,513	2,537
ISIP at surface, psi	1,191	1,108
BH ISIP, psi	2,874	2,791
G-dP/dG Pc, psi		655
Shmin, psi		2,338
Frac closure time, min		8.5
After Closure Linear p*, psi		365
Reservoir pressure, psi		2,048

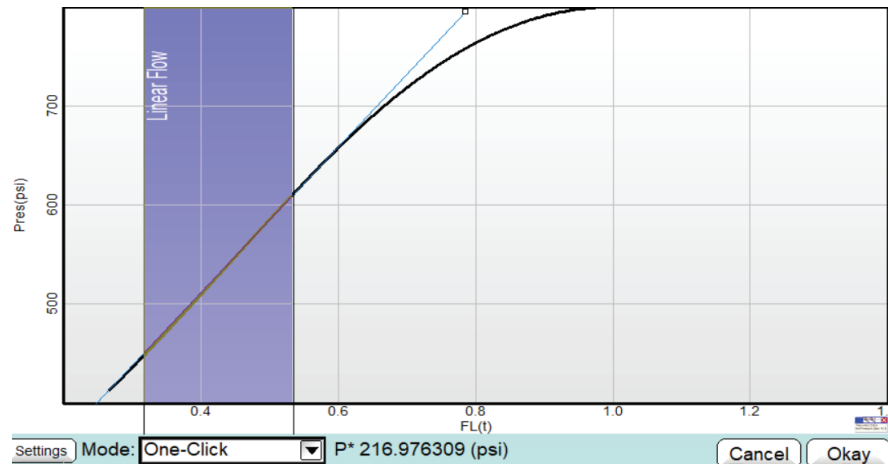
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Cherry Canyon DFIT-3 Data Interpretation

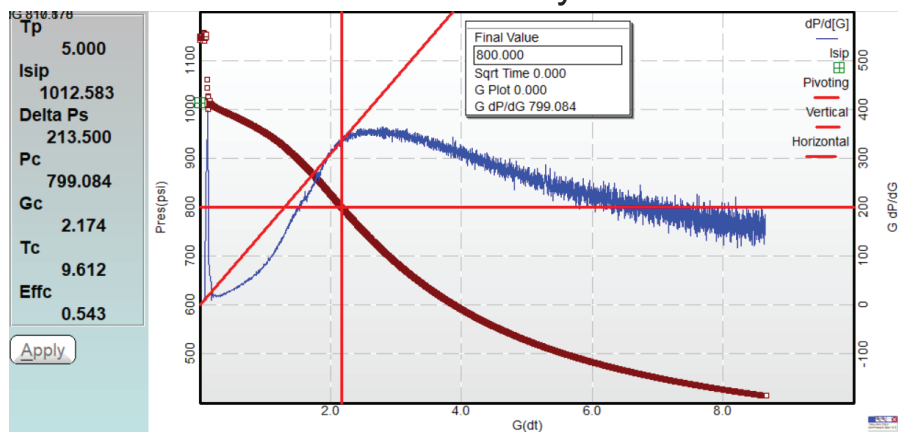
Surface Pressure Data



Reservoir Pressure Estimation



DFIT Closure Analysis



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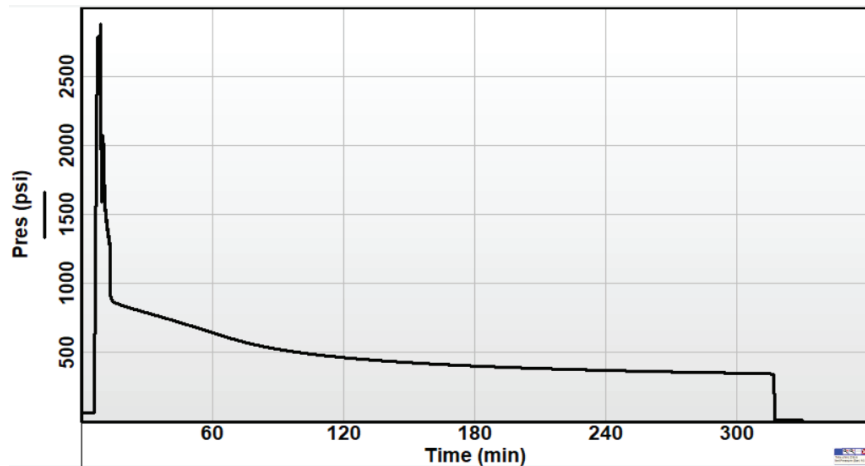


Test date	11/15/2025
Test start time, MST	8:53 PM
Perforation interval MD, ft	3487-3491
TVD, ft	3,488.0
Pumping time, min	5
Pump-in volume, bbl	20
Fluid density, ppg	8.4
Breakdown WHP, psi	1,752
ISIP at surface, psi	1,013
BH ISIP, psi	2,534
G-dP/dG Pc, psi	799
Shmin, psi	2,320
Frac closure time, min	9.6
After Closure Linear p*, psi	217
Reservoir pressure, psi	1,738

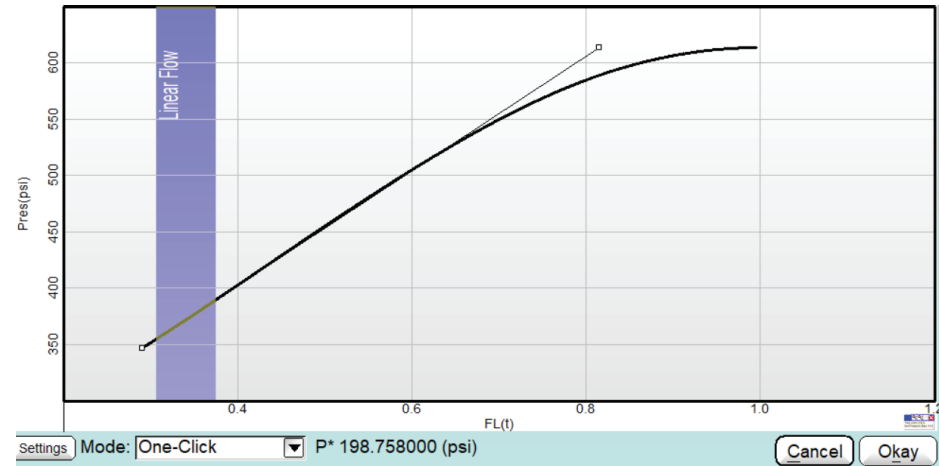
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Bell Canyon DFIT-1 Data Interpretation

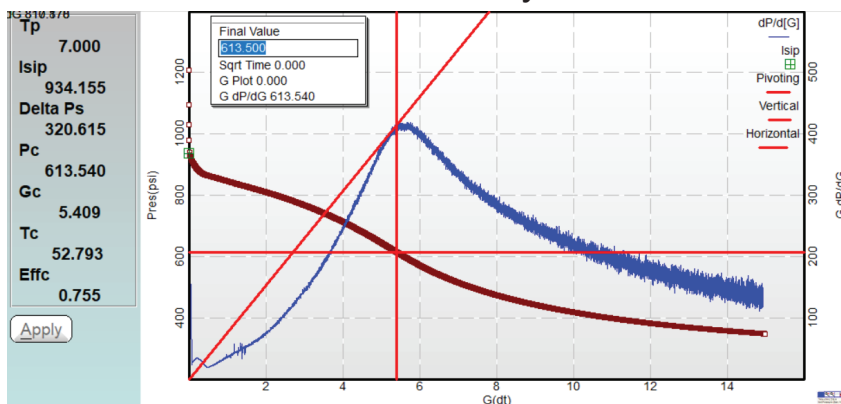
Surface Pressure Data



Reservoir Pressure Estimation



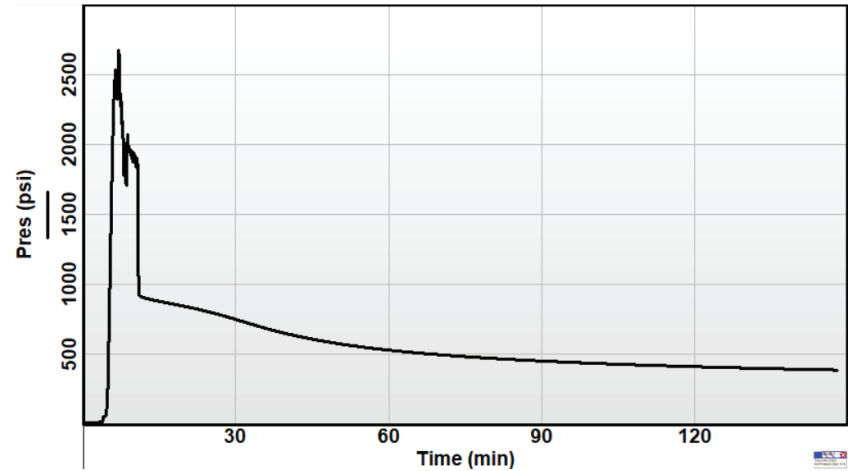
DFIT Closure Analysis



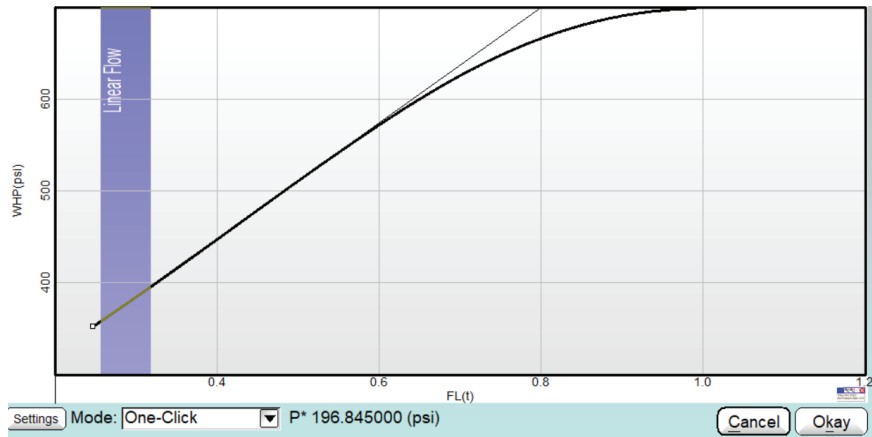
Test date	11/18/2025
Test start time, MST	10:35 PM
Perforation interval MD, ft	3020.5-3023.5
TVD, ft	3,020.8
Pumping time, min	7
Pump-in volume, bbl	22
Fluid density, ppg	8.4
Breakdown WHP, psi	2,881
ISIP at surface, psi	934
BH ISIP, psi	2,252
G-dP/dG Pc, psi	613.5
Shmin, psi	1,931
Frac closure time, min	52.8
After Closure Linear p*, psi	199
Reservoir pressure, psi	1,516

Bell Canyon DFIT-2 Data Interpretation

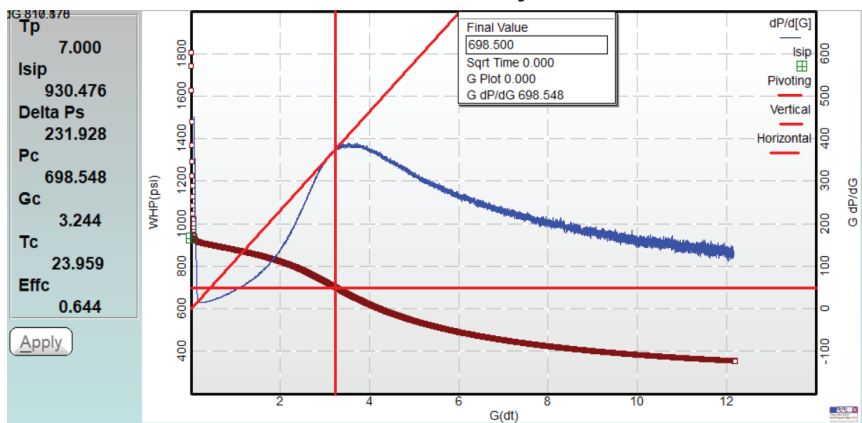
Surface Pressure Data



Reservoir Pressure Estimation



DFIT Closure Analysis

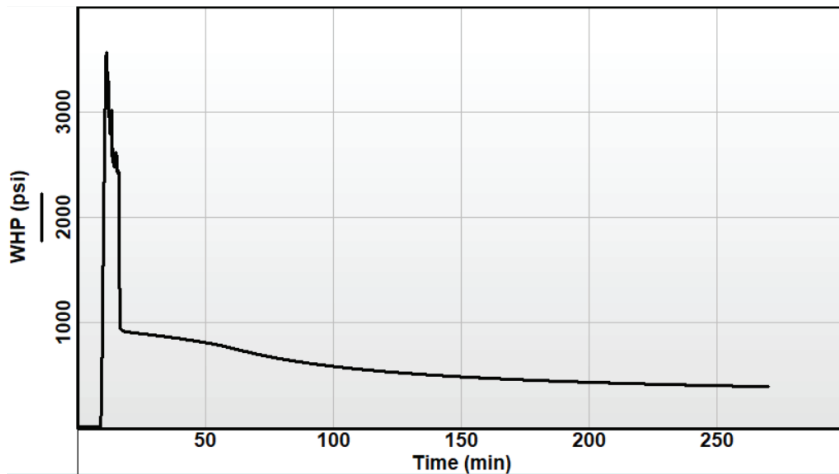


Test date	11/19/2025
Test start time, MST	11:24 AM
Perforation interval MD, ft	2714.7-2717.7
TVD, ft	2,715.2
Pumping time, min	6.3
Pump-in volume, bbl	20
Fluid density, ppg	8.4
Breakdown WHP, psi	2,674
ISIP at surface, psi	1,013
BH ISIP, psi	2,534
G-dP/dG Pc, psi	930.5
Shmin, psi	1,883
Frac closure time, min	24.0
After Closure Linear p*, psi	197
Reservoir pressure, psi	1,381

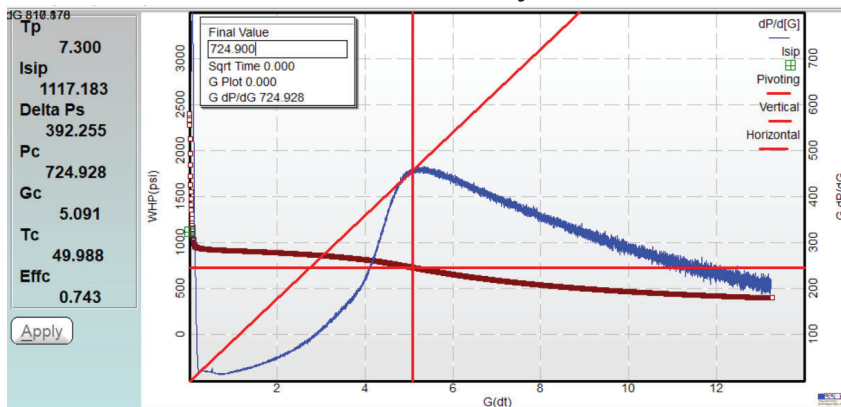


Bell Canyon DFIT-3 Data Interpretation

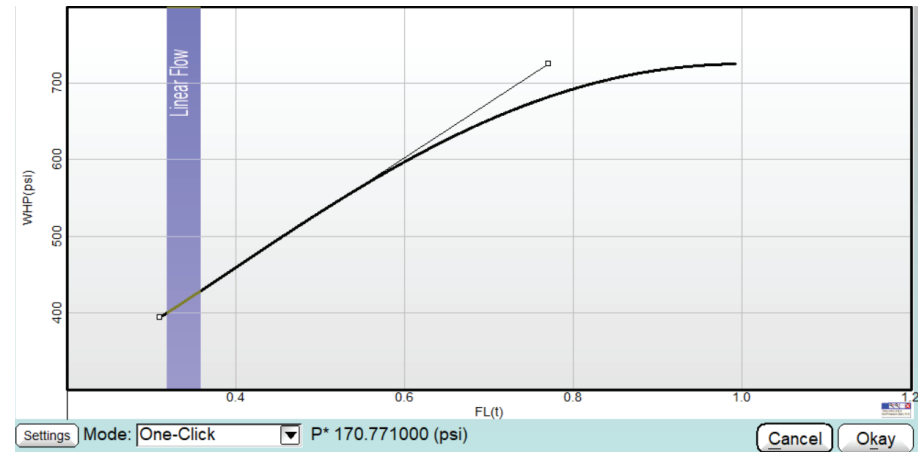
Surface Pressure Data



DFIT Closure Analysis



Reservoir Pressure Estimation



Test date	11/19/2025
Test start time, MST	10:39 PM
Perforation interval MD, ft	2558.7-2561.7
TVD, ft	2,559.2
Pumping time, min	7.3
Pump-in volume, bbl	22
Fluid density, ppg	8.4
Breakdown WHP, psi	3,579
ISIP at surface, psi	1,117
BH ISIP, psi	2,233
G-dP/dG Pc, psi	725
Shmin, psi	1,841
Frac closure time, min	50.0
After Closure Linear p*, psi	171
Reservoir pressure, psi	1,287



Key Takeaways

- DFIT testing pressure was measured at surface with high-precision pressure gauges. During shut-in period without wellbore fluid friction, surface gauge pressure plus hydrostatic pressure becomes the bottom-hole pressure, which is used for DFIT analysis.
- Nine DFITs were conducted, with 3 tests in each Canyon formation. Fracture closure pressure or minimum horizontal stress values for 8 out of 9 tests were successfully obtained.
- Stress gradients range from 0.57 to 0.72 psi/ft, and stress confidence is labeled as higher or lower based on fracture closure signatures.
- Reservoir or pore pressure was estimated from linear flow pressure behavior after the fracture is closed. Pore pressure (Pp) gradients range from 0.50 to 0.53 psi/ft.
- Fracture fluid efficiency for 8 DFIT tests was estimated by a frac model. Fluid efficiency is defined as the ratio of the volume of the fracture created at the end of pumping to the volume of fluid pumped, and is affected by reservoir permeability, pumping volume and pumping rate.
 - Higher fracture fluid efficiency indicates lower formation permeability.
 - Lower fracture fluid efficiency indicates higher formation permeability.
 - DFIT results with similar fluid volume (20 – 22 bbl) pumped show that the testing intervals in the Cherry Canyon is more permeable than those in the Bell Canyon.



SEVERITAS 2 STATE SWD #001 Step Rate Test Report – Bell Canyon & Cherry Canyon

Executive Summary

Two step rate tests (SRTs) were conducted on the Severitas 2 State SWD #001, one targeting the Cherry Canyon and the other targeting the Bell Canyon. The Cherry Canyon SRT was conducted on 11/17/25-11/18/25 while the Bell Canyon SRT was conducted on 11/21/25. Prior to the SRTs, the well was circulated with 9.1 ppg brine with the SRTs conducted with 9.1 ppg brine (to reflect operating conditions). Downhole pressures were collected via memory gauge.

Cherry Canyon fracturing occurred at 2100.6 psia at the gauge depth of 3227 ft, for a fracture gradient of 0.651 psi/ft, while pumping at 0.514 bpm. Bell Canyon fracturing occurred at 1960.4 psia at the gauge depth of 2405 ft, for a fracture gradient of 0.815 psi/ft, while pumping at 0.500 bpm. These fracture gradients are consistent with DFIT measurements of fracture stresses taken in the well.

Surface pressure for the Cherry Canyon under fracturing conditions is 559.1 psig. Surface pressure for the Bell Canyon under fracturing conditions is 807.8 psig. Using a 90% safety factor on the Cherry Canyon result gives a maximum surface injection pressure limit of **503 psig** or a **0.212** psi/ft surface pressure gradient to the top of the permitted interval at 2377 ft.

SRT Analysis

Procedure

The SRTs were conducted separately on isolated Cherry Canyon and Bell Canyon. The Cherry Canyon injection interval was perforated and its SRT followed. Once the Cherry Canyon SRT was completed a plug was set on top of the Cherry Canyon injection interval. The Bell Canyon injection interval was subsequently perforated and its SRT followed. After both SRTs were complete, the plug was retrieved, and the well was completed with permanent tubing, packer and downhole gauge.

The SRTs were conducted by pump trucks with memory gauges conveyed downhole on 5.5” tubing to measure BHP. The gauge for the Cherry Canyon SRT was set at 3227 ft. while the gauge for the Bell Canyon SRT was set at 2405 ft. The top of the injection interval was permitted at 2377 ft.

Prior to each SRT the wellbore was circulated until it was filled with 9.1 ppg fluid. Each SRT pumped 9.1 ppg fluid throughout the test, which is the same density as the brine that will be injected during normal operations.

The design steps/rates and the measured formation tops in the well are as follows:

SEVERITAS 2 STATE SWD #001 Step Rate Test Report – Bell Canyon & Cherry Canyon

Cherry Canyon SRT			
Step	% of Max Rate	Rate (BPM)	Duration (min)
1	12%	0.5	60
2	20%	0.9	60
3	30%	1.3	60
4	40%	1.7	60
5	60%	2.6	60
6	80%	3.4	60
7	100%	4.3	60

Table 1: Cherry Canyon SRT Designed Steps/Rates

Bell Canyon SRT			
Step	% of Max Rate	Rate (BPM)	Duration (min)
1	29%	0.5	60
2	35%	0.6	60
3	40%	0.7	60
4	50%	0.9	60
5	65%	1.1	60
6	80%	1.4	60
7	100%	1.7	60

Table 2: Bell Canyon SRT Designed Steps/Rates

Well Name	SEVERITAS 2 STATE SWD 001	
API	30015553130000	
GL	3173.0	
KB	3201.5	
Surface	MD	TVD
Salado	311	311
Castille	514	514
Top of Salt	1622	1622
Base of Salt	2151	2151
Lamar	2341	2341
Bell Canyon	2399	2399
Cherry Canyon	3196	3196
Brushy Canyon	4825	4825

Table 3: Formation Tops

SEVERITAS 2 STATE SWD #001 Step Rate Test Report – Bell Canyon & Cherry Canyon

Observations

Surface and BHP measurements show the same pressure response trends to the injection and match when applying the 9.1 ppg brine hydrostatic pressure. Both the Cherry and the Bell appear to fracture during the first injection step.

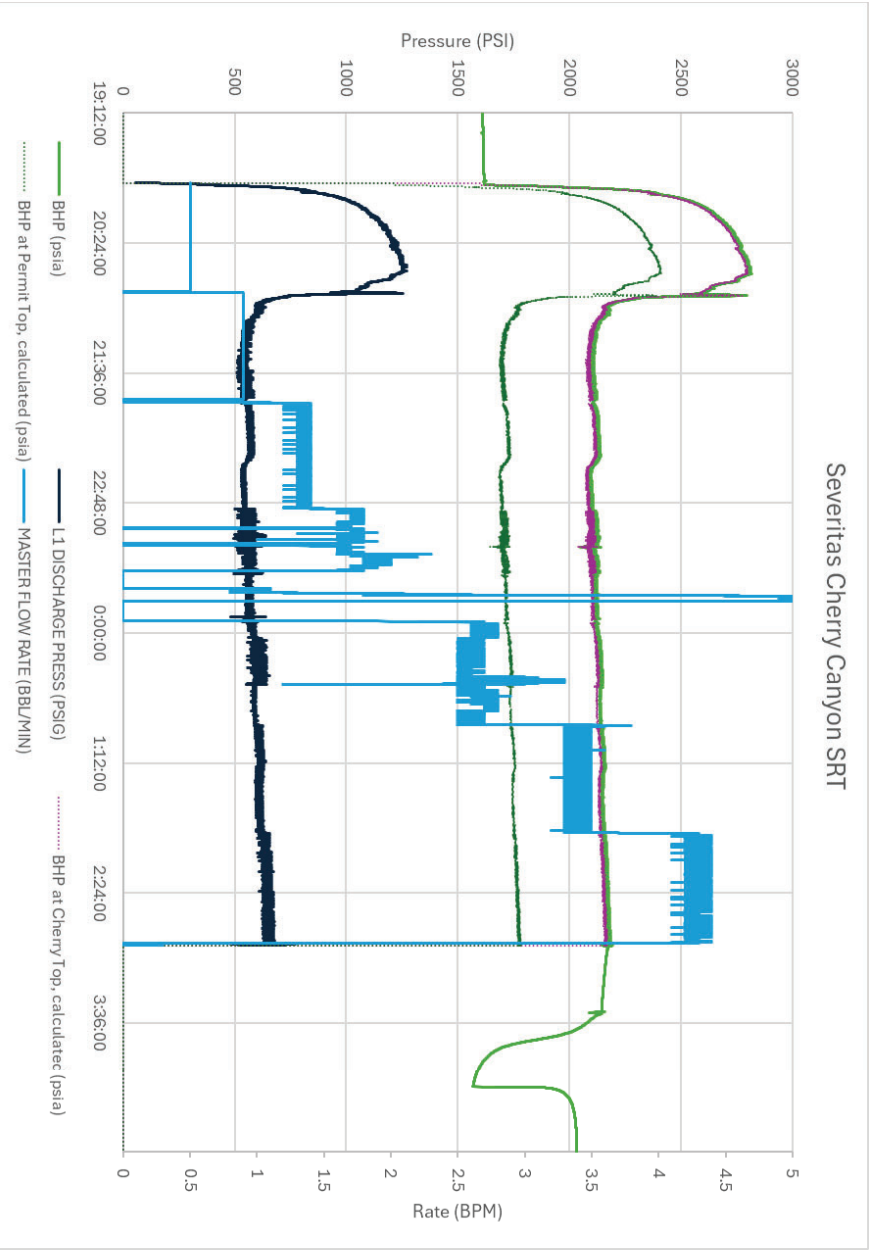


Figure 1: Cherry Canyon SRT Data. BHP at Cherry Top and at Permit Top are calculated from the BHP data using 9.1 ppg brine and assuming no friction. During the fourth rate-step (1.7 bpm) the pump tripped which resulted in downtime.

SEVERITAS 2 STATE SWD #001 Step Rate Test Report – Bell Canyon & Cherry Canyon

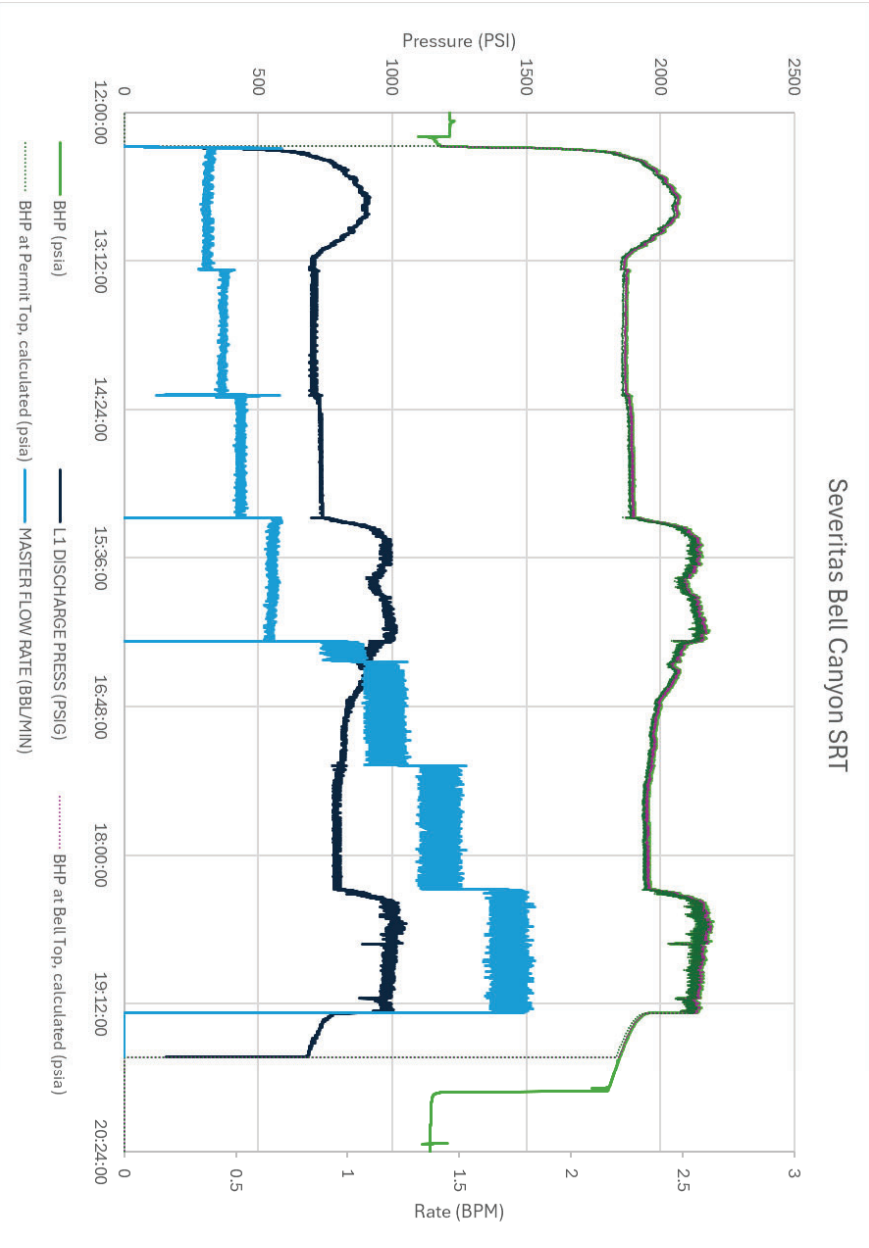


Figure 2: Bell Canyon SRT Data. BHP at Bell Canyon Top and at Permit Top are calculated from the BHP data using 9.1 ppg brine and assuming no friction. Since the gauge, permit top, and Bell Canyon top are so close, the pressure data practically overlaps.

Analysis

Due to fracturing occurring during the first step of each SRT, datapoints prior to initial fracturing, early in the step, were selected to help establish pre-fracture trends. With these trends the fracture propagation pressures (FPP) were calculated. The Cherry Canyon FPP was 2100.6 psia at the gauge depth of 3227 ft, for a fracture gradient of 0.650 psi/ft, while pumping at 0.514 bpm. Bell Canyon fracturing occurred at 1960.4 psia at the gauge depth of 2405 ft, for a fracture gradient of 0.815 psi/ft, while pumping at 0.500 bpm. These fracture gradients are consistent with DFIT ISIP measurements which more closely represent the FPPs measured by the SRTs.

SEVERITAS 2 STATE SWD #001 Step Rate Test Report – Bell Canyon & Cherry Canyon

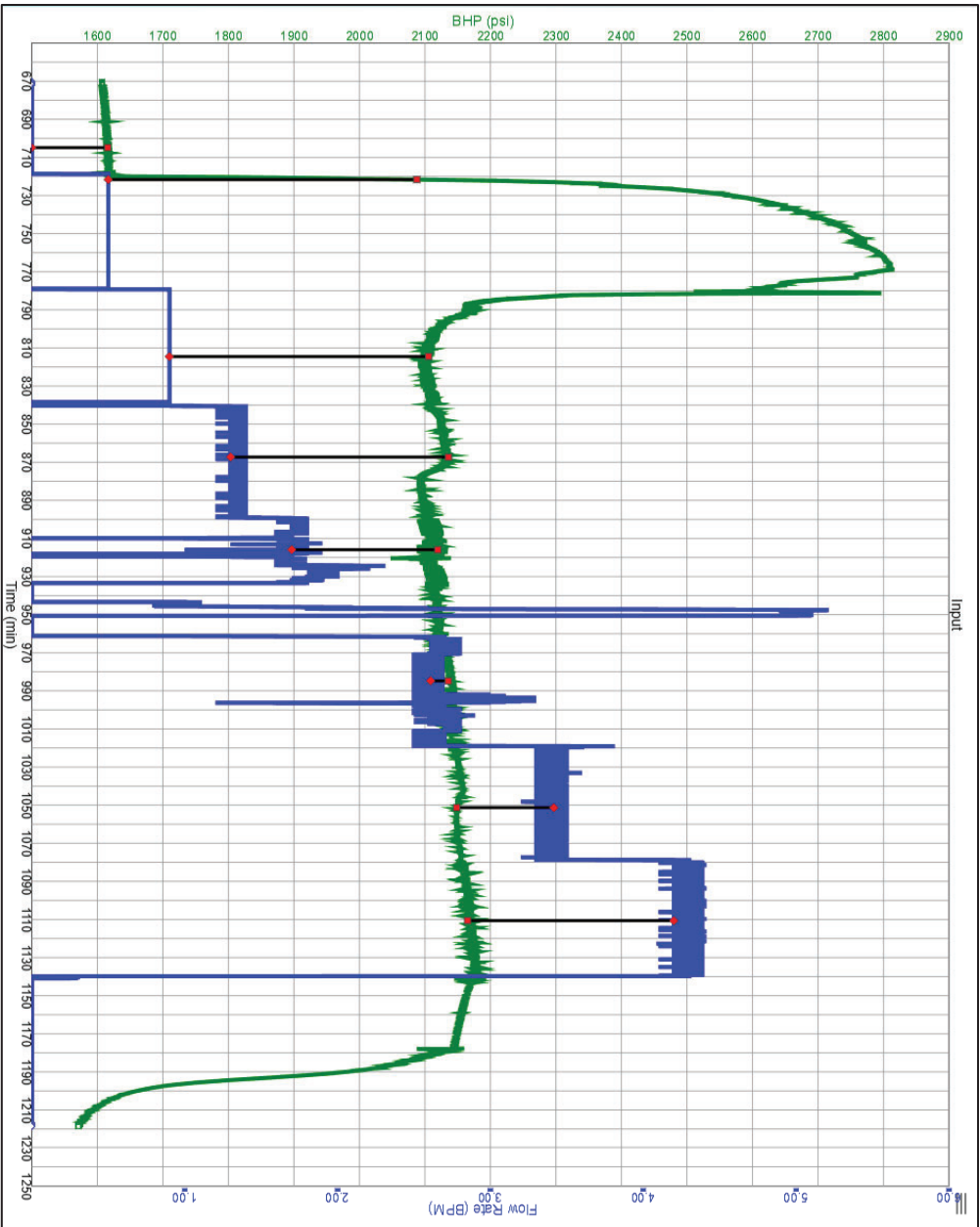
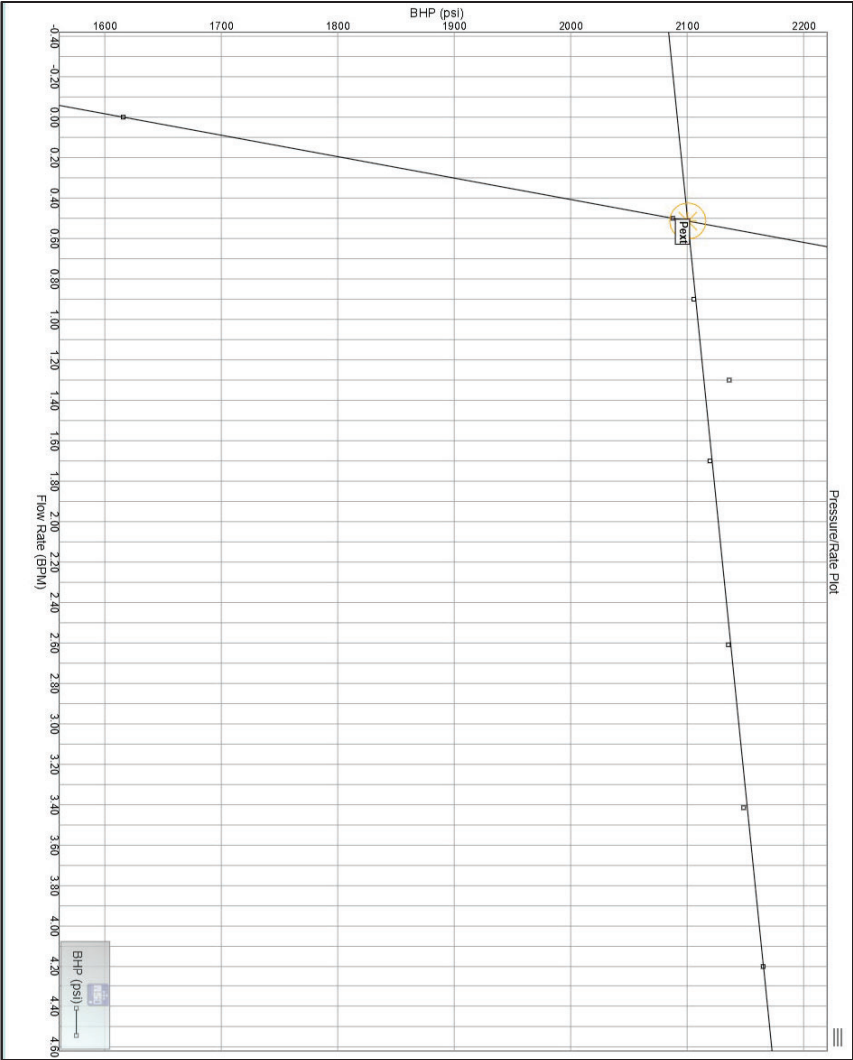


Figure 3: Cherry Canyon Pressure-Rate Plot with selected SRT Test Points. BHP gauge at 3227 ft. Pumping at the initial rate of 0.5 bpm caused the formation to break down at ~2800 psi

SEVERITAS 2 STATE SWD #001 Step Rate Test Report – Bell Canyon & Cherry Canyon



CHERRY CANYON			
FPP (psi)	Qext (bpm)	Grad (psi/ft)	Depth (ft)
2100.552	0.514	0.651	3,227ft (gauge depth)
2085.883	0.514	0.653	3,196ft (top perf)
1698.332	0.514	0.714	2,377ft (permit top)

Figure 4: Cherry Canyon SRT Interpretation. FPP and associate gradient calculated at different key depths: gauge depth, top of the formation, and the permit top.

Pressure (psi)	Rate (bpm)
1615.79	0.01
2087.55	0.50
2105.73	0.90
2136.18	1.30
2119.51	1.70
2135.41	2.61
2148.55	3.41
2165.22	4.20

Table 4: Pressure and rate values of Cherry Canyon SRT test points

SEVERITAS 2 STATE SWD #001 Step Rate Test Report – Bell Canyon & Cherry Canyon

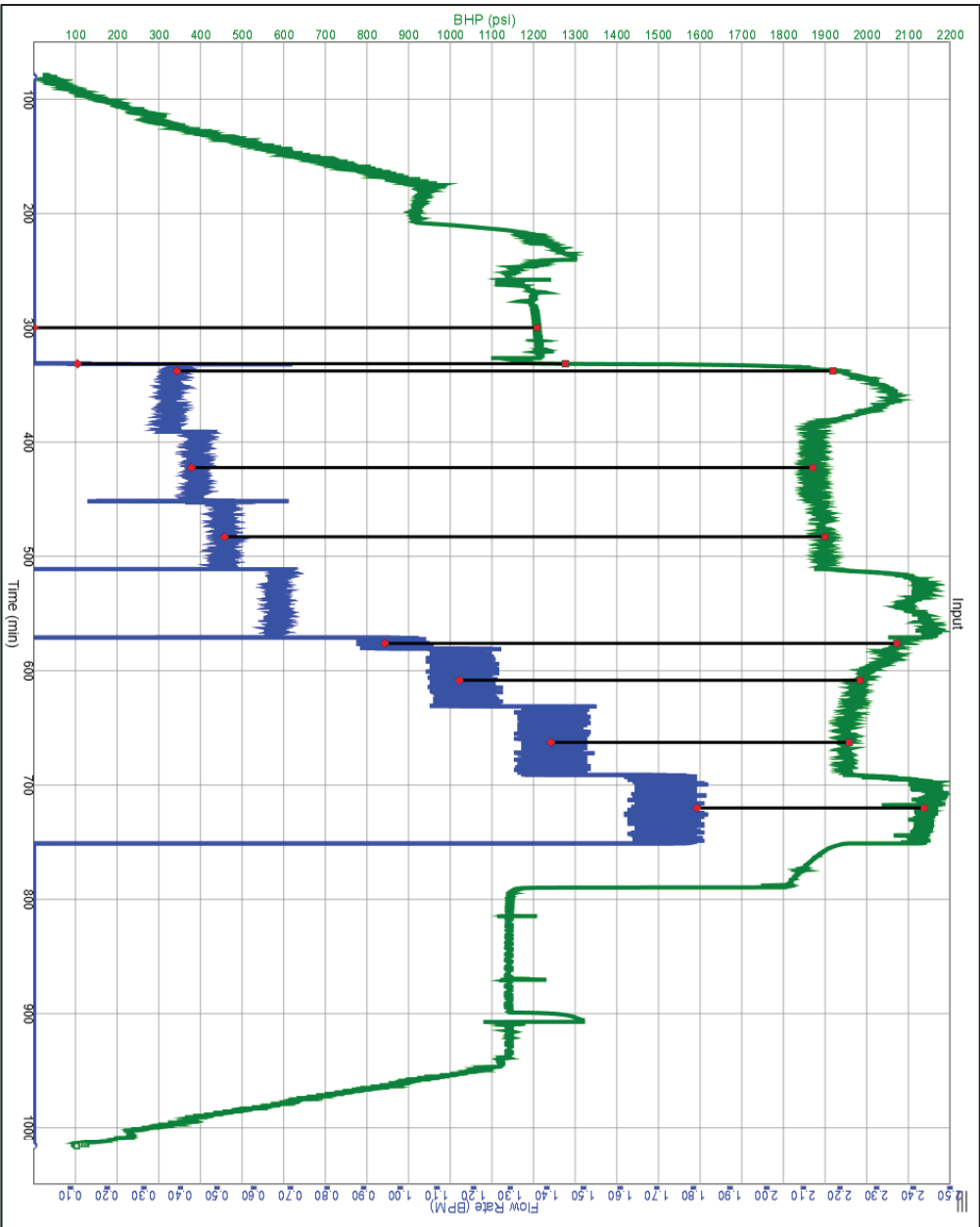
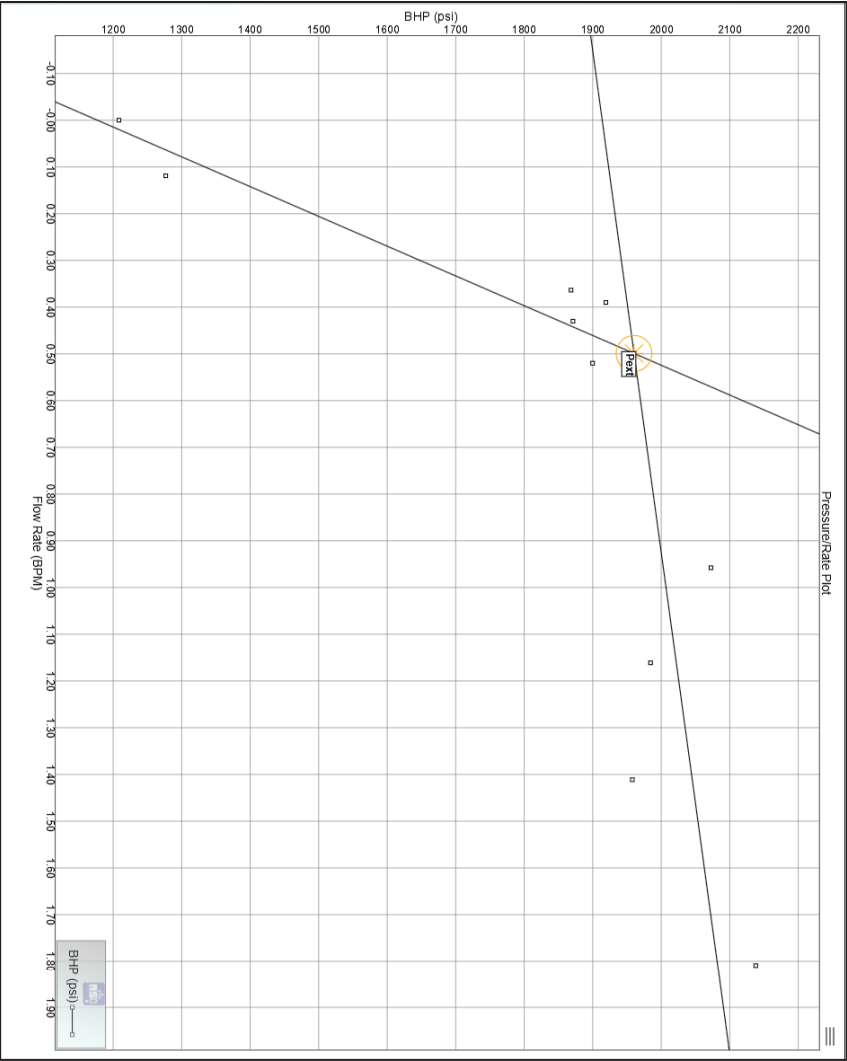


Figure 5: Bell Canyon Pressure-Rate Plot with selected SRT Test Points. BHP gauge at 2405 ft. Pumping at the initial rate of 0.5 bpm caused the formation to break down at ~2000 psi.

SEVERITAS 2 STATE SWD #001 Step Rate Test Report – Bell Canyon & Cherry Canyon



BELL CANYON			
FPP (psi)	Qext (bpm)	Grad (psi/ft)	Depth (ft)
1960.363	0.5	0.815	2,405ft (gauge depth)
1957.524	0.5	0.816	2,399ft (top perf)
1947.113	0.5	0.819	2,377ft (permit top)

Figure 6: Bell Canyon SRT Interpretation. FPP and associate gradient calculated at different key depths: gauge depth, top of the formation, and the permit top.

Pressure (psi)	Rate (bpm)
1208.40	0.01
1276.77	0.12
1919.27	0.39
1871.18	0.43
1899.84	0.52
2072.60	0.96
1984.45	1.16
1957.84	1.41
2138.00	1.81

Table 5: Pressure and rate values of Bell Canyon SRT test points

SEVERITAS 2 STATE SWD #001 Step Rate Test Report – Bell Canyon & Cherry Canyon

Surface Injection Pressure Limit Calculation

To determine the surface injection pressure limit, we first calculated wellhead injection pressure corresponding to BHP fracturing conditions, then multiplied it by a 0.9 safety factor. To calculate the surface injection pressure gradient, we divided the surface pressure limit by the top of the permitted interval.

The Cherry Canyon surface pressure limit and corresponding surface pressure gradient were 503 psig and 0.212 psi/ft. The Bell Canyon surface pressure limit and corresponding surface pressure gradient were 727 psig and 0.306 psi/ft. The Cherry Canyon, being the lower of the two values, is the limiting pressure for the well.

Cherry Canyon Calculation

Well parameters:

Injected Fluid Specific Gravity	1.093 (9.1 ppG)
Depth of BHP gauge, ft.	3227
q (flowrate), bbl/day	740.16
D (pipe ID), in	4.75
Mu (viscosity), cp	1
Tubing Roughness, in	0.0006
L (tubing length), ft	3227
Fracture Pressure (from SRT), psia	2100.6
Fracture Pressure (from SRT), psig	2085.9

Reynolds number calculation:

$$Re = \frac{92.207 q \times SG}{D \mu} = \frac{92.207 \times 740.16 \times 1.093}{4.75 \times 1} = 15704.2$$

Where:

- Re – Reynolds number (dimensionless)
- q – flow rate in bbl/day
- D – pipe internal diameter in inches
- μ – fluid viscosity in centipoise
- SG – specific gravity

Swamee-Jain Friction Factor for $Re > 5000$

$$f = \frac{0.25}{\left[\log_{10} \left(\frac{\epsilon}{3.7D} + \frac{5.74}{Re^{0.9}} \right) \right]^2} = \frac{0.25}{\left[\log_{10} \left(\frac{0.0006}{3.7 \times 4.75} + \frac{5.74}{15704.2^{0.9}} \right) \right]^2} = 0.02773$$

Where:

- f – Swamee-Jain Friction Factor

SEVERITAS 2 STATE SWD #001 Step Rate Test Report – Bell Canyon & Cherry Canyon

- ϵ – pipe roughness
- D – pipe internal diameter in inches
- Re – Reynolds number (dimensionless)

Fluid density calculation:

$$\rho = SG \times 62.4 = 1.093 \times 62.4 = 68.2 \frac{lbs}{ft^3}$$

Where:

- ρ – fluid density in $\frac{lbs}{ft^3}$
- SG – specific gravity

Flow velocity calculation:

$$v = 0.011915 \times \frac{q}{D^2} = 0.011915 \times \frac{740.16}{4.75^2} = 0.3909 \frac{ft}{s}$$

Where:

- v – flow velocity in $\frac{ft}{s}$
- q – flow rate in bbl/day
- D – pipe internal diameter in inches

Darcy-Weisbach friction equation:

$$\Delta P_{friction} = f \frac{L}{D_{ft}} \frac{\rho v^2}{2g_c} = 0.02773 \times \frac{3227}{4.75} \times \frac{68.2 \times 0.3909^2}{2 \times 32.174} = 36.6 \frac{lbs}{ft^2} = 0.254 \text{ psi}$$

Where:

- f – Swamee-Jain Friction Factor
- ρ – fluid density in $\frac{lbs}{ft^3}$
- L – pipe length in ft
- D_{ft} – pipe internal diameter in feet
- v – flow velocity in $\frac{ft}{s}$
- g_c – gravitational constant $32.174 \frac{lbs \cdot ft}{s^2}$

Hydrostatic pressure calculation:

$$\Delta P_{hydrostatic} = 0.433 \times SG \times TVD = 0.433 \times 1.093 \times 3227 = 1527.2 \text{ psi}$$

Where:

- SG – specific gravity

SEVERITAS 2 STATE SWD #001 Step Rate Test Report – Bell Canyon & Cherry Canyon

- $TV D$ – true vertical depth (top of Bell Canyon) in feet

Surface injection pressure calculation:

$P_{surface} = P_{BHP} - \Delta P_{hydrostatic} + \Delta P_{friction} = 2085.9 - 1527.2 + 0.254 = 559 \text{ psig}$

Surface injection pressure gradient calculation – 0.9 safety factor

$P_{max} = P_{surface} \times Safety\ Factor = 559 \times 0.9 = 503 \text{ psig}$

$Gradient_{SIP-top\ permit} = \frac{P_{max}}{Depth_{permit\ Top}} = \frac{503}{2377} = 0.212 \frac{psi}{ft}$

Bell Canyon Calculation

Well parameters:

Injected Fluid Specific Gravity	1.093 (9.1 ppG)
Depth of BHP gauge, ft.	2405
q (flowrate), bbl/day	720
D (pipe ID), in	4.75
Mu (viscosity), cp	1
Tubing Roughness, in	0.0006
L (tubing length), ft	2405
Fracture Pressure (from SRT), psia	1960.4
Fracture Pressure (from SRT), psig	1945.7

Reynolds number calculation:

$Re = \frac{92.207 q \times SG}{D \mu} = \frac{92.207 \times 720 \times 1.093}{4.75 \times 1} = 15276.5$

Where:

- Re – Reynolds number (dimensionless)
- q – flow rate in bbl/day
- D – pipe internal diameter in inches
- μ – fluid viscosity in centipoise
- SG – specific gravity

Swamee-Jain Friction Factor for $Re > 5000$

$f = \frac{0.25}{\left[\log_{10} \left(\frac{\epsilon}{3.7D} + \frac{5.74}{Re^{0.9}} \right) \right]^2} = \frac{0.25}{\left[\log_{10} \left(\frac{0.0006}{3.7 \times 4.75} + \frac{5.74}{15276.5^{0.9}} \right) \right]^2} = 0.02793$

Where:

- f – Swamee-Jain Friction Factor
- ϵ – pipe roughness

SEVERITAS 2 STATE SWD #001 Step Rate Test Report – Bell Canyon & Cherry Canyon

- D – pipe internal diameter in inches
- Re – Reynolds number (dimensionless)

Fluid density calculation:

$$\rho = SG \times 62.4 = 1.093 \times 62.4 = 68.2 \frac{lbs}{ft^3}$$

Where:

- ρ – fluid density in $\frac{lbs}{ft^3}$
- SG – specific gravity

Flow velocity calculation:

$$v = 0.011915 \times \frac{q}{D^2} = 0.011915 \times \frac{720}{4.75^2} = 0.3802 \frac{ft}{s}$$

Where:

- v – flow velocity in $\frac{ft}{s}$
- q – flow rate in bbl/day
- D – pipe internal diameter in inches

Darcy-Weisbach friction equation:

$$\Delta P_{friction} = f \frac{L}{D_{ft}} \frac{\rho v^2}{2g_c} = 0.02793 \times \frac{2405}{4.75} \times \frac{68.2 \times 0.3802^2}{2 \times 32.174} = 26 \frac{lbs}{ft^2} = 0.181 \text{ psi}$$

Where:

- f – Swamee-Jain Friction Factor
- ρ – fluid density in $\frac{lbs}{ft^3}$
- L – pipe length in ft
- D_{ft} – pipe internal diameter in feet
- v – flow velocity in $\frac{ft}{s}$
- g_c – gravitational constant $32.174 \frac{lbs \cdot ft}{s^2}$

Hydrostatic pressure calculation:

$$\Delta P_{hydrostatic} = 0.433 \times SG \times TVD = 0.433 \times 1.093 \times 2405 = 1138.2 \text{ psi}$$

Where:

- SG – specific gravity
- TVD – true vertical depth (top of Bell Canyon) in feet

SEVERITAS 2 STATE SWD #001 Step Rate Test Report – Bell Canyon & Cherry Canyon

Surface injection pressure calculation:

$$P_{surface} = P_{BHP} - \Delta P_{hydrostatic} + \Delta P_{friction} = 1945.7 - 1138.2 + 0.181 = 807.7 \text{ psig}$$

Surface injection pressure gradient calculation – 0.9 safety factor

$$P_{max} = P_{surface} \times Safety \ Factor = 807.7 \times 0.9 = 727 \text{ psig}$$
$$Gradient_{SIP-top \ permit} = \frac{P_{max}}{Depth_{permit \ Top}} = \frac{727}{2377} = 0.306 \frac{psi}{ft}$$

Comparison to DFIT Results

Measurements of ISIP and Shmin from DFITs of the Cherry Canyon and Bell Canyon show similar values to the FPP measured from the SRTs. DFITs provide higher-confidence assessments of fracturing stress compared to step rate tests. Additionally, ISIP values determined via DFIT are closely correlated with FPP measurements from SRTs.

The Cherry Canyon FPP from the SRT was 0.651 psi/ft, measured from the BHP gauge depth. DFIT ISIP for the Cherry Canyon ranged from 0.71 – 0.73 psi/ft with the Shmin ranging from 0.61-0.67 psi/ft. Here the SRT measurement reflects the Shmin measured in the DFIT which is more conservative for FPP.

The Bell Canyon FPP from the SRT was 0.815 psi/ft, measured from the BHP gauge depth. DFIT ISIP for the Bell Canyon ranged from 0.75 – 0.87 psi/ft with the Shmin ranging from 0.64-0.72 psi/ft. The DFIT and the SRT both agree that the Bell Canyon in the Severitas has an elevated fracture pressure vs the Cherry Canyon.

The DFIT data and SRT data both show that the Cherry Canyon is the weaker of the two injection zones. The DFIT data also shows that the interpreted fracture gradient of 0.651 psi/ft from the SRT in the Cherry Canyon is a reasonable value which can be used to inform the maximum surface injection pressure in the Severitas well.

Test	Perf MD, ft	TVD, ft	Breakdown WHP, psi	ISIP, psi	Shmin, psi	ISIP Grad, psi/ft	Shmin Grad, psi/ft	Stress Confidence
Bell DFIT 3	2558.7 - 2561.7	2559.2	3579.0	2233.3	1841.0	0.87	0.72	High
Bell DFIT 2	2714.7 - 2717.7	2715.2	2674.2	2114.6	1882.6	0.78	0.69	High
Bell DFIT 1	3020.5 - 3023.5	3020.8	2880.7	2251.6	1930.9	0.75	0.64	High
Cherry DFIT 3	3487.0 - 3491.0	3488.0	1752.0	2534.2	2320.2	0.73	0.67	High
Cherry DFIT 2	3858.6 - 3861.6	3858.4	2537.0	2790.7	2337.7	0.72	0.61	Moderate
Cherry DFIT 1	4161.8 - 4164.8	4161.4	2929.0	2954.8	2624.8	0.71	0.63	High
Brushy DFIT 3	4911.0 - 4914.0	4909.7	3952.0	2919.2	2803.2	0.59	0.57	Moderate
Brushy DFIT 2	5077.0 - 5080.0	5076.1	2911.0	3281.8	2889.8	0.65	0.57	High

Table 6: Summarized Severitas DFIT Results

SEVERITAS 2 STATE SWD #001 Static BHP Measurement

Executive Summary

Memory gauges were run into the Severitas on 11/17/25-11/18/25 and 11/21/25 to measure BHP data during the Cherry and Bell step rate tests (SRT) respectively. The gauges were set in advance of and left in the well after each SRT with sufficient time to measure static bottom hole pressure (BHP). Both formations were isolated from each other during the memory gauge runs.

The Cherry Canyon memory gauge, set at 3227 ft. measured a static BHP of 1613 psia for a gradient of 0.50 psia/ft prior to the SRT. Following the SRT, the well's pressure was bled down. After bleeding down, the stabilized static BHP was 1547 psia for a gradient of 0.48 psia/ft.

The Bell Canyon memory gauge, set at 2405 ft. measured a static BHP of 1210 psia for a gradient of 0.50 psia/ft prior to the SRT. After the SRT, the well's pressure was bled down. After bleeding down, the stabilized static BHP was 1141 psia for a gradient of 0.47 psia/ft.

	Cherry Canyon	Bell Canyon
Gauge Depth, ft.	3227	2405
Top of Formation Depth, ft.	3196	2399
Top of Permit Depth, ft.	2377	2377
Pre-SRT BHP, psia	1613	1210
Pre-SRT BHP Gradient, psia/ft	0.50	0.50
Post-SRT BHP, psia	1547	1141
Post-SRT BHP Gradient, psia/ft	0.48	0.47

Table 1: BHP measurement summary

Cherry Canyon Memory Gauge – 3227 ft. 11/17/2025 – 11/18/2025

The Cherry Canyon was perforated, then the memory gauge was run on tubing to 3227 ft. Once tubing was set, the wellbore was circulated with 9.1 ppg fluid and the packer and casing were tested.

The circulation and testing operations ceased at approximately 7:00:00 PM on 11/17. The well sat idle while surface equipment was being tested and rigged up until 7:51:50 PM when the SRT commenced. The pre-SRT BHP measurement was the average BHP during this ~52 minutes of idle time and had a value of 1613 psia (0.50 psia/ft).

After the SRT the well was bled down. Bleeding down ceased at approximately 5:30:00 AM and the gauge stayed downhole until 9:30:00 AM on 11/18. The post-SRT BHP measurement was the average baseline BHP during these 4 hrs, ignoring several anomalous pressure reading spikes. It had a value of 1547 psia (0.48 psia/ft).

SEVERITAS 2 STATE SWD #001 Static BHP Measurement

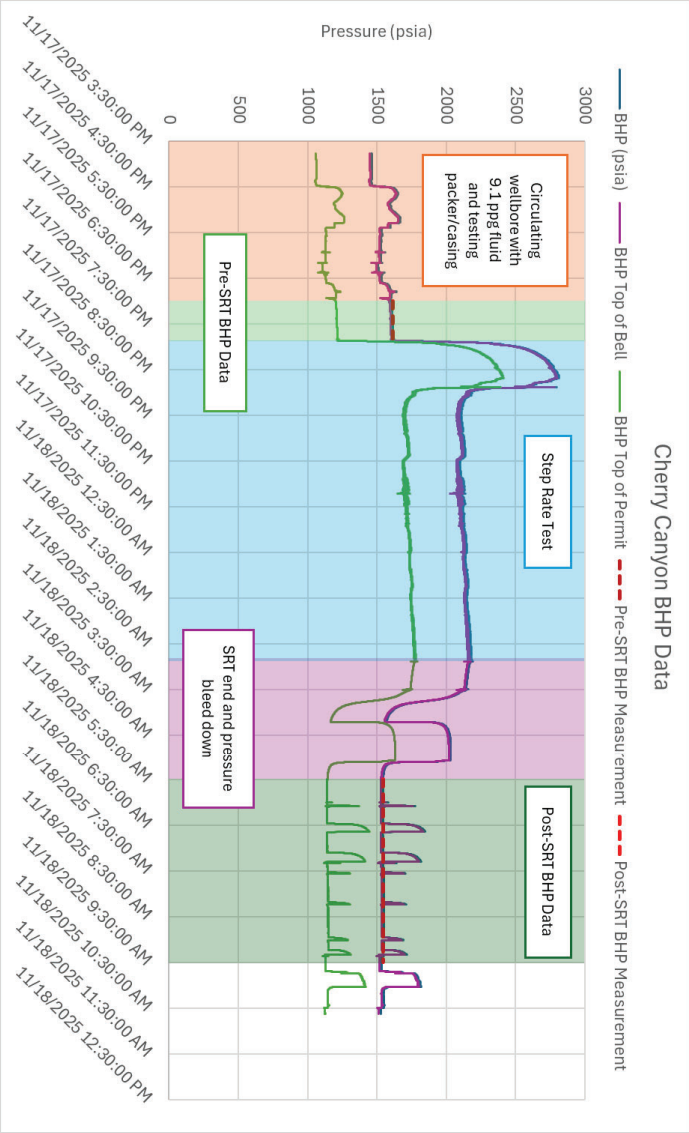


Figure 1: Cherry Canyon BHP gauge data 11/17/25-11/18/25, set at 3227 ft. BHP data collected both prior to and after the SRT was used for static BHP measurement. Pressure at top of formation and at the top of the permit calculated with 9.1 ppg fluid.

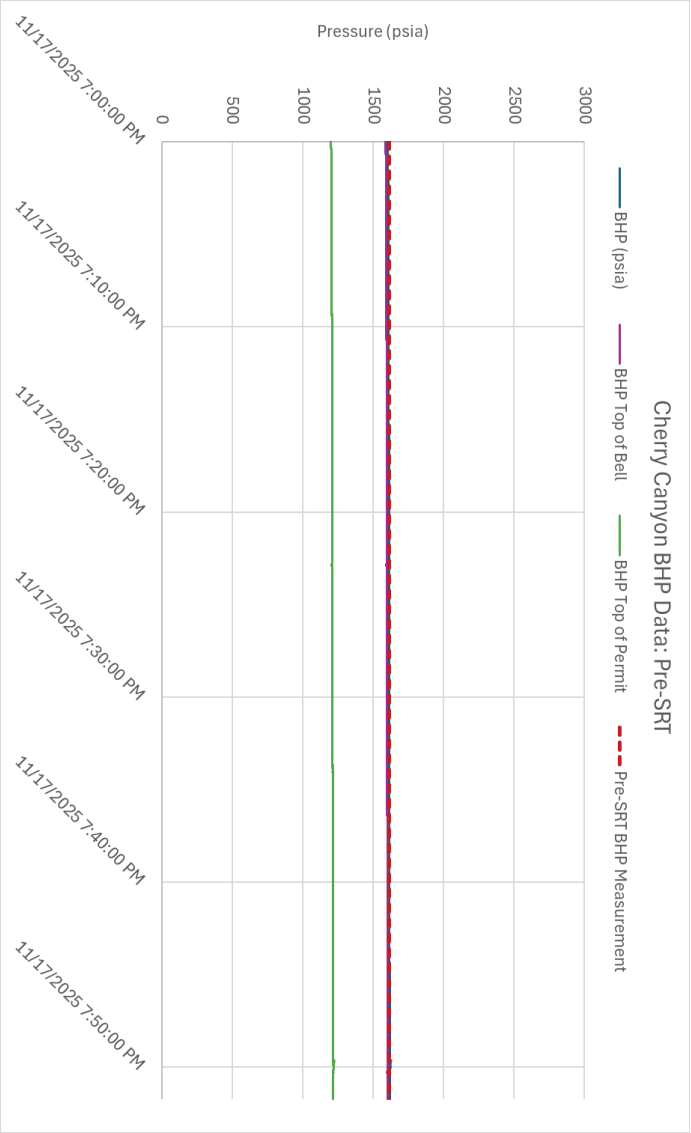


Figure 2: Portion of Cherry Canyon BHP gauge data used for pre-SRT static BHP measurement. Pressure at top of formation and at the top of the permit calculated with 9.1 ppg fluid.

SEVERITAS 2 STATE SWD #001 Static BHP Measurement

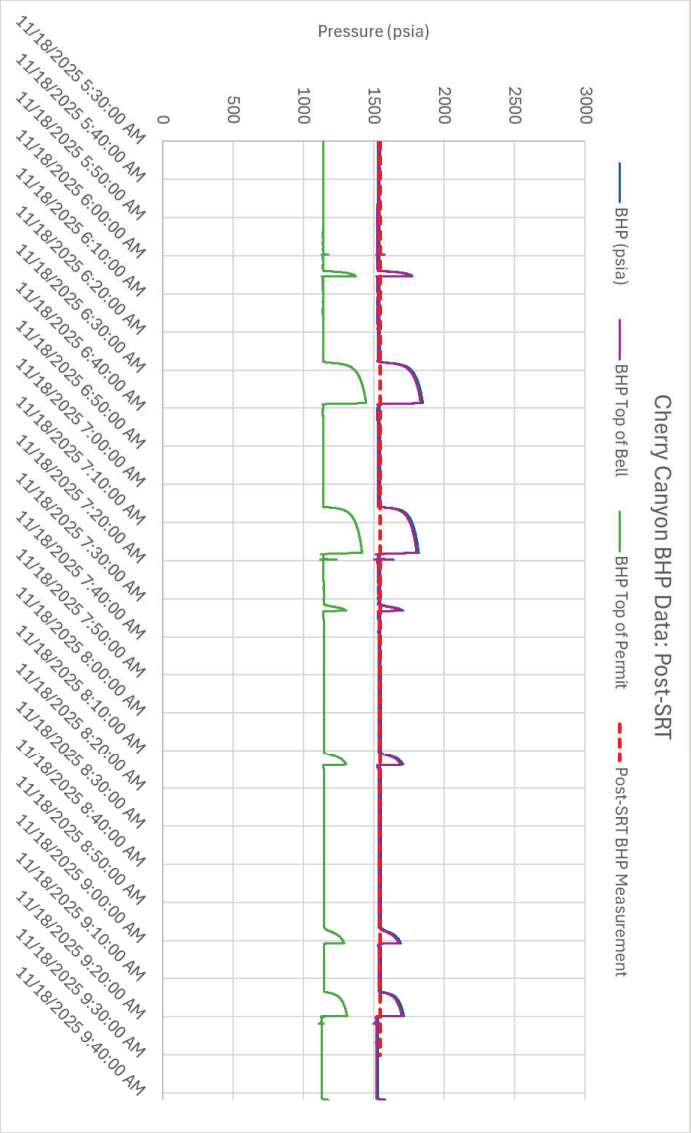


Figure 3: Portion of Cherry Canyon BHP gauge data used for post-SRT static BHP measurement. Pressure at top of formation and at the top of the permit calculated with 9.1 ppg fluid.

Bell Canyon Memory Gauge – 2405 ft. 11/21/2025

The Bell Canyon was isolated from the Cherry Canyon with a plug then the Bell Canyon was perforated. The memory gauge was run on tubing to 2405 ft. Once tubing was set, the wellbore was circulated with 9.1 ppg fluid and the packer and casing were tested.

The circulation and testing operations ceased at approximately 11:30:00 AM on 11/21. The well sat idle while surface equipment was being tested and rigged up until 12:16:21 PM when the step rate test commenced. The pre-SRT BHP measurement was the average BHP during the idle time from 11:30:00 AM – 12:11:53 PM (~42 minutes) and had a value of 1210 psia (0.50 psia/ft).

After the SRT the well was bled down. Bleeding down ceased at approximately 8:00:00 PM and the gauge stayed downhole until 10:23:07 PM. The post-SRT BHP measurement was the average baseline BHP during these ~2.33 hrs, ignoring several anomalous pressure reading spikes. It had a value of 1141 psia (0.47 psia/ft).

SEVERITAS 2 STATE SWD #001 Static BHP Measurement

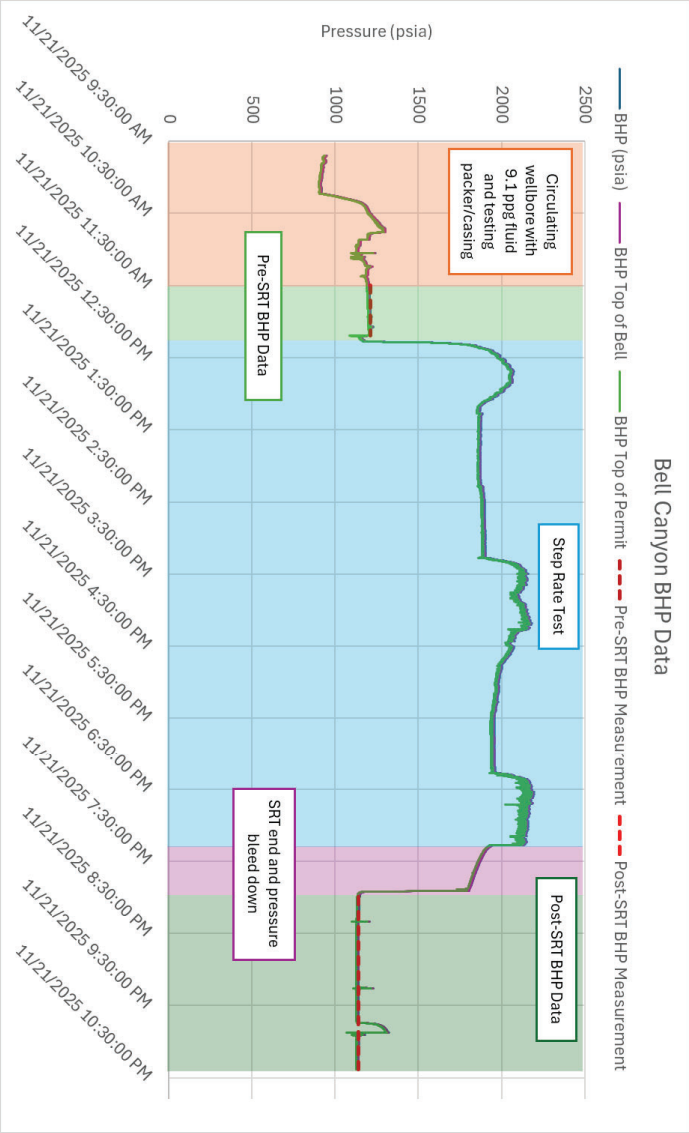


Figure 4: Bell Canyon BHP gauge data 11/21/25, set at 2405 ft. BHP data collected both prior to and after the SRT was used for static BHP measurement. Pressure at top of formation and at the top of the permit calculated with 9.1 ppg fluid.

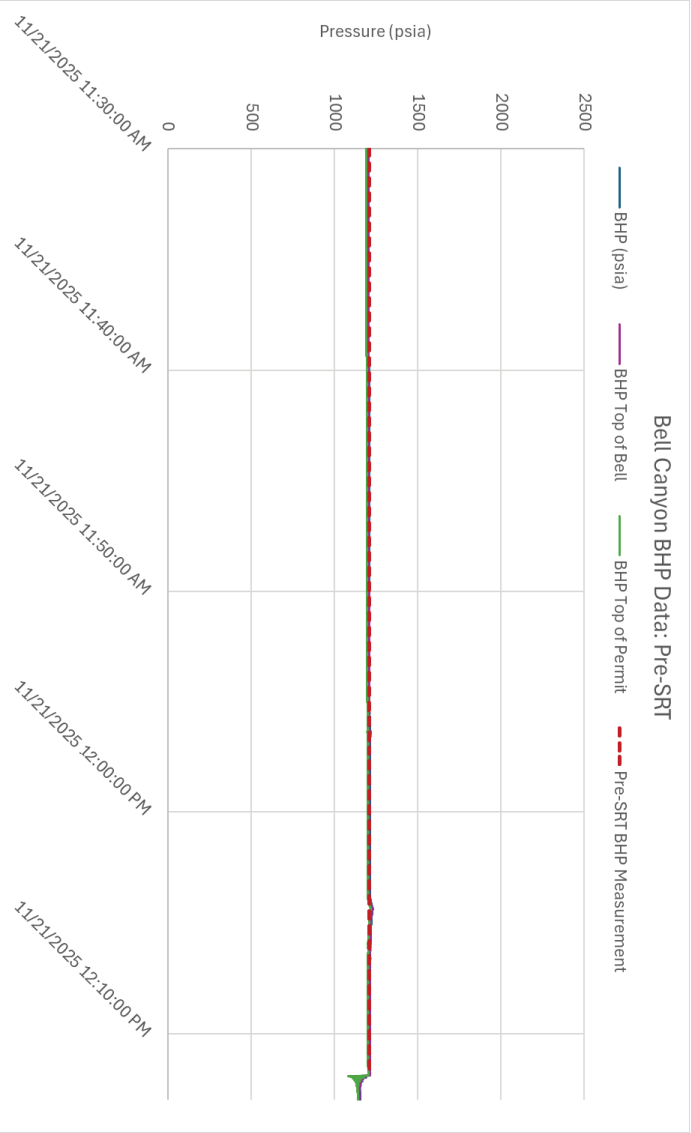


Figure 5: Portion of Bell Canyon BHP gauge data used for pre-SRT static BHP measurement. Pressure at top of formation and at the top of the permit calculated with 9.1 ppg fluid.

SEVERITAS 2 STATE SWD #001 Static BHP Measurement

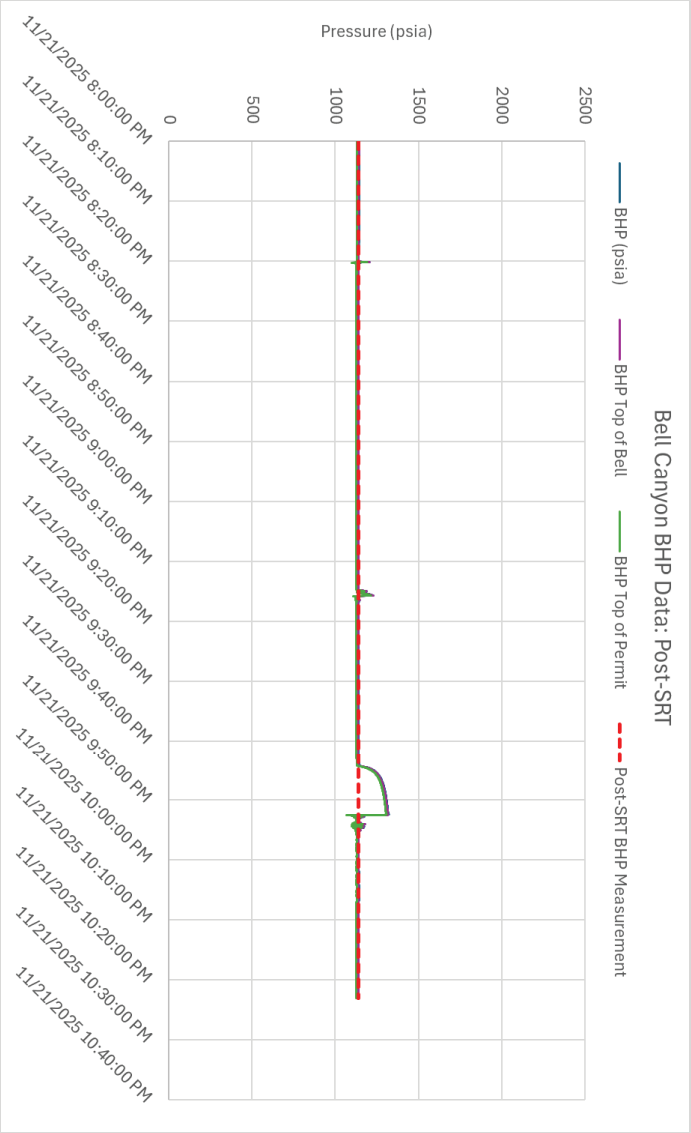


Figure 6: Portion of Cherry Canyon BHP gauge data used for post-SRT static BHP measurement. Pressure at top of formation and at the top of the permit calculated with 9.1 ppg fluid.



WELLD OG.
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Client: Chevron

Well Name: Serveritas State 2 SWD 1

Formation Name: Bell Canyon

Test Date: 21/11/2025 - 22/11/2025



Client: Chevron
Test Date: 21/11/2025 - 22/11/2025
Tool Serial: DC3757

Well Name: Serveritas State 2 SWD 1
Location: Field / Pool:

Summary

Well Information

Client Name:	Chevron	
Well Name:	Serveritas State 2 SWD 1	Tubing in Well: Yes
Formation Name:	Bell Canyon	Flow Path: Tubing
Packer:	Yes	

Test Information

Test Name:	Bell Cayon SRT	
Test Purpose:	Initial Test	Gauge Run Depth [ft KB (TVD)]: 2,405'

Gauge 1 Information

Gauge Serial Number:	DC3757	
Date/Time Gauge On Bottom:	11/21/2025 6:45:00 AM	Date/Time Gauge Off Bottom: 11/22/2025 12:08:00 AM
Date Of Last Calibration:	2/3/2025	



Client: Chevron
Test Date: 21/11/2025 - 22/11/2025
Tool Serial: DC3757

Well Name: Serveritas State 2 SWD 1
Location:
Field / Pool:

Events

	Date	Real Time	Pressure	Temp.	Events
	(dd/MM/yyyy)	(HH:mm:ss)	(psia)	(degF)	
1	21/11/2025	08:02:15	14.223	47.100	Start RIH
2	21/11/2025	09:42:15	948.487	83.123	Finish RIH
3	21/11/2025	12:16:21	1180.803	80.962	Start injection test 0.5 BPM
4	21/11/2025	13:15:58	1867.084	79.914	Increase to 0.6 BPM
5	21/11/2025	14:16:26	1876.252	78.569	Increase to 0.7 BPM
6	21/11/2025	15:16:12	1902.581	77.034	Increase to 0.9 BPM
7	21/11/2025	16:16:05	2150.090	76.013	Increase to 1.1 BPM
8	21/11/2025	17:16:20	1970.336	75.146	Increase to 1.4 BPM
9	21/11/2025	18:16:11	1954.540	74.808	Increase to 1.7 BPM
10	21/11/2025	19:16:27	2125.329	74.381	Finish injection test
11	21/11/2025	22:23:08	1141.356	78.128	Start POOH
12	21/11/2025	23:48:31	13.220	72.021	Finish POOH



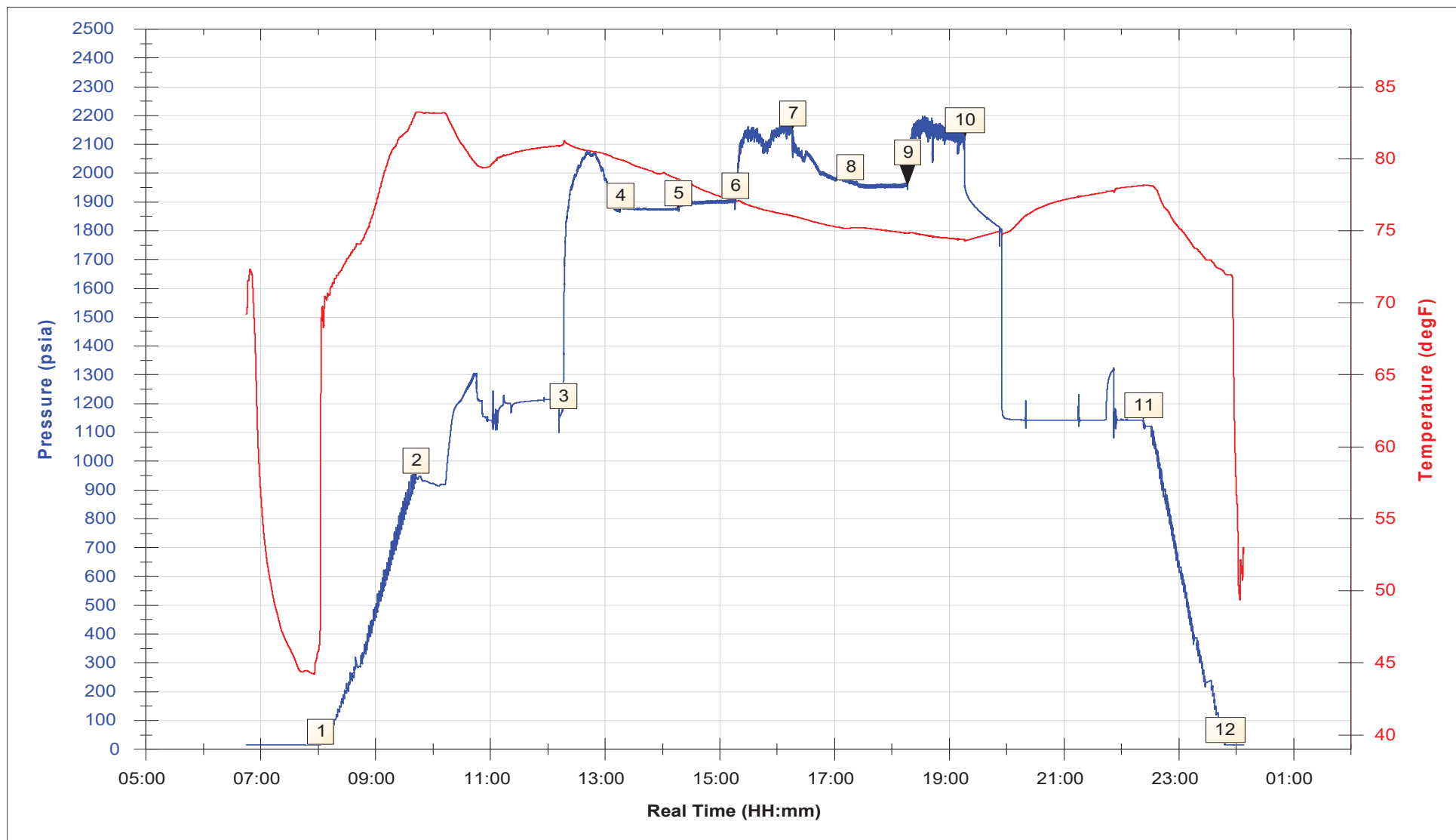
Client:
Test Date:
Tool Serial:
Max Press 1:

Chevron
21/11/2025 - 22/11/2025
DC3757
2196.717

Well Name:
Location:
Field / Pool:
Max Temp 1:

Serveritas State 2 SWD 1

83.237





WELLD OG.
TRULY UNCONVENTIONAL™

Client: Chevron

Well Name: Serveritas State 2 SWD 1

Formation Name: Cherry Canyon

Test Date: 11/17/2025 - 11/18/2025



Client: Chevron
Test Date: 11/17/2025 - 11/18/2025
Tool Serial: DC3757

Well Name: Serveritas State 2 SWD 1
Location: Field / Pool:

Summary

Well Information

Client Name:	Chevron	
Well Name:	Serveritas State 2 SWD 1	Tubing in Well: Yes
Formation Name:	Cherry Canyon	Flow Path: Tubing
Packer:	Yes	

Test Information

Test Name:	Cherry Canyon SRT	
Test Purpose:	Initial Test	Gauge Run Depth [ft KB (TVD)]: 3,227'

Gauge 1 Information

Gauge Serial Number:	DC3757	
Date/Time Gauge On Bottom:	11/17/2025 7:52:00 AM	Date/Time Gauge Off Bottom: 11/18/2025 12:41:00 PM
Date Of Last Calibration:	2/3/2025	



Client: Chevron
Test Date: 11/17/2025 - 11/18/2025
Tool Serial: DC3757

Well Name: Serveritas State 2 SWD 1
Location:
Field / Pool:

Events

	Date (MM/dd/yyyy)	Real Time (HH:mm:ss)	Pressure (psia)	Temp. (degF)	Events
1	11/17/2025	13:06:15	13.300	83.200	Start RIH
2	11/17/2025	15:45:40	1460.600	90.600	Finish RIH
3	11/17/2025	19:51:50	1618.000	88.500	Start Injection Test @ 0.5BPM Increase to 0.9 BPM
4	11/17/2025	20:52:26	2544.700	85.500	
5	11/17/2025	21:53:34	2103.200	82.400	
6	11/17/2025	22:52:24	2112.000	80.300	
7	11/17/2025	23:54:27	2112.700	80.600	Increase to 2.6 BPM
8	11/18/2025	00:52:05	2142.500	80.800	Increase to 3.4 BPM
9	11/18/2025	01:51:54	2154.800	81.300	Increase to 4.3 BPM
10	11/18/2025	02:53:02	2184.900	81.800	Finish testing, bleed off pressure Start POOH
11	11/18/2025	10:37:24	1529.000	87.500	
12	11/18/2025	12:30:59	16.100	74.800	Finish POOH



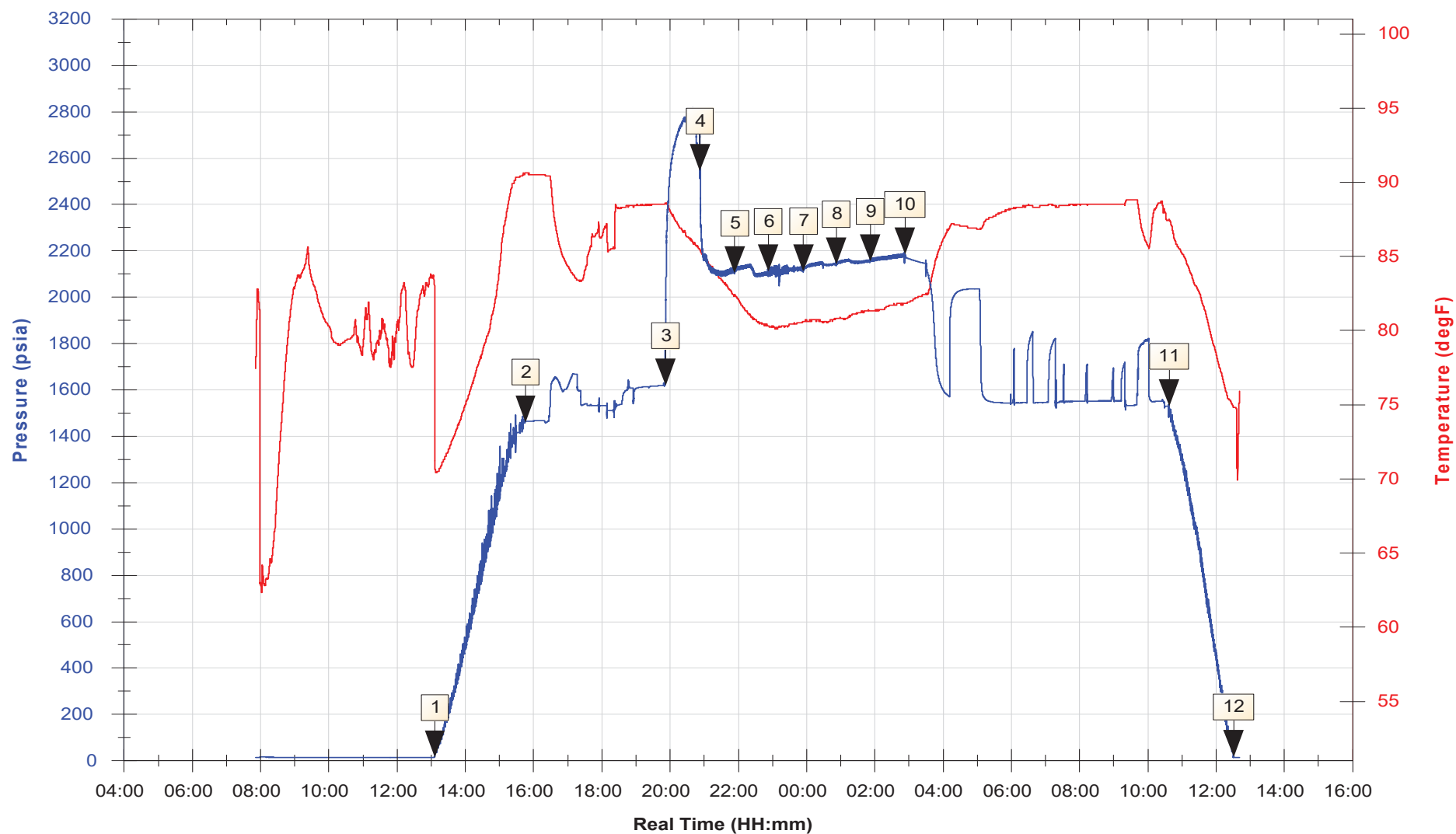
Client:
Test Date:
Tool Serial:
Max Press 1:

Chevron
11/17/2025 - 11/18/2025
DC3757
2816.7

Well Name:
Location:
Field / Pool:
Max Temp 1:

Serveritas State 2 SWD 1

90.6



Sante Fe Main Office
Phone: (505) 476-3441

General Information
Phone: (505) 629-6116

Online Phone Directory
<https://www.emnrd.nm.gov/ocd/contact-us>

State of New Mexico
Energy, Minerals and Natural Resources
Oil Conservation Division
1220 S. St Francis Dr.
Santa Fe, NM 87505

CONDITIONS

Action 539866

CONDITIONS

Operator: CHEVRON U S A INC 6301 Deauville Blvd Midland, TX 79706	OGRID: 4323
	Action Number: 539866
	Action Type: [C-103] Sub. General Sundry (C-103Z)

CONDITIONS

Created By	Condition	Condition Date
anthony.harris	Approved with Maximum Surface Injection Pressure = 503 psi for injection operations	2/3/2026