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STATE OF NEW MEXICO

ENERGY, MINERALS AND NATURAL RESOURCES DEPARTMENT

OIL CONSERVATION DIVISION

DRUG FREE

BRUCE KING GOVERNOR

ANITA LOCKWOOD CABINET SECRETARY

> Yates Petroleum Corporation 105 South Fourth Street Artesia, NM 88210

Attention: Robert S. Fant

RE:

Injection Pressure Increase West Loco Hills Unit Tract 1, Well No. 9 Waterflood Project Eddy County, New Mexico

Dear Mr. Fant:

Reference is made to your request dated March 16, 1993 to increase the surface injection pressure on the above-referenced well. This request is based on a step rate tests conducted on this well on March 5, 1993. The results of the test have been reviewed by my staff and we feel an increase in injection pressure on this well is justified at this time.

You are therefore authorized to increase the surface injection pressure on the following well:

| Well and Location | Maximum Injection Surface Pressure |
|---|---------------------------------------|
| WLHU Tract 1 Well No. 9 1980' FNL - 40' FWL Unit E, Section 7, Township 18 South, Range 30 East | 1275 PSIG |
| The well is located in Eddy County, New | v Mexico. |

The Division Director may rescind this injection pressure increase if it becomes apparent that the injected water is not being confined to the injection zone or is endangering any fresh water aquifers.

Sincerely 00 William J. LeMay Director WJL/BES/amg CC: Oil Conservation Division - Artesia File: Case No. 2473 D. Catanach



April 5, 1993

POST OFFICE BOX 2088 STATE LAND OFFICE BUILDING SANTA FE, NEW MEXICO 87504 (505) 827-5800

| NO WAITING | PERIOD |
|-------------|-----------------------------------|
| COMPANY: | YATES PETROLEUM CORPORATION |
| ADDRESS: | 105 SOUTH FOURTH STREET |
| CITY, STATE | , ZIP: ARRESIA, Alew MEXICO 88210 |
| ATTENTION: | KOBERT S. FANT |

Re: Injection Pressure Increase <u>West loco Hills (INIT</u> <u>TRACT 1, WELL No. 9</u> <u>EDDY</u> County, New Mexico

Dear Sir:

Reference is made to your request dated $\underline{MARCH 16}$, 19<u>93</u>, to increase the surface injection pressure on <u>THE ABOVE REFERENCED</u> <u>wfree Hars</u>. This request is based on step rate tests conducted on these wells $\underline{NNMARCH 5}$, 19<u>73</u>. The results of the tests have been reviewed by my staff and we feel an increase in injection pressure on these wells is justified at this time.

You are therefore authorized to increase the surface injection pressure on the following wells:

Well & Location

Maximum Injection Surface Pressure

1275 PSIG

| WLHU TRACT I WELL NO. 9 |
|-------------------------|
| 1980'FNL + 40' FWL |
| "E" 7.185.30E |
| |

The Division Director may rescind this injection pressure increase if it becomes apparent that the injected water is not being confined to the injection zone or is endangering any fresh water aquifers.

| xc: | T. GALLEGOS | D. CATANA | CH FILE-CASE FILE | OCD-ARTESIA |
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MARTIN YATES, III 1912 - 1985 FRANK W. YATES 1936 - 1986

S. P. YATES AIRMAN OF THE BOARD JOHN A. YATES PRESIDENT PEYTON YATES ECUTIVE VICE PRESIDENT NDY G. PATTERSON SECRETARY DENNIS G. KINSEY ne TREASURER 844 ressure -1471 nue es Le STIONS 93 ert 10 HH à 0 18 A

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March 16

State of New Mexico Energy, Minerals and Natural Resources Department Oil Conservation Division Attention: David Catanach P.O. Box 2088 Santa Fe, New Mexico 87504

Request for Injection Pressure Increase, West Loco Hills Unit Tract 1 Well No. 9, Re: Eddy County, New Mexico

Dear Mr. Catanach:

By this letter, Yates Petroleum Corporation is requesting that, based upon the step rate test conducted on the WLHU Tract 1 Well No. 9, Unit E, Section 7, Township 18 South, Range 30 East, Eddy County, New Mexico and the addition information submitted herein, the maximum surface injection pressure for this well be increased to at least 1300 psig.

The test was run by John West Engineering on March 5, 1993, and witnessed by Mr. John Robinson of the Artesia NMOCD Office. Mr. Robinson indicated the day of the test that at least one point on the step rate test needed to be below the current 560 psig surface pressure limitation. However, due to CO₂ gas in the tubing, the shut-in pressure on the well was 601 psig on the morning of the test after the well had been shut-in for 4 days. Analysis of the fall-off test conducted on the well during these 4 days indicates a static reservoir pressure of 368 psig at the surface. After filling the tubing, the test was begun.

The test was begun at an initial rate of 298 bwipd (as limited by the equipment on location). Flow rates below this range are not possible with the equipment of John West Engineering. The pressure at 15 minutes was 566.68 psig (corrected for friction). The next three points on the test show a gentle curve until a constant slope is obtained through points 5 through 8. Another constant slope is obtained through points 10 through 13, indicating a fracture pressure of 1325 psig. Although the pressure for the first rate is slightly above the desired limit of 560 psig and the first 4 points do not show a straight line, I believe the data presented below will clearly demonstrate that the fracture pressure for this well is 1325 psig.

The high pressure during the initial rate is simply due to the inability of the equipment to inject at lower rates and to the presence of CO_2 in the wellbore. CO_2 injection had been ceased only 5 days prior to the shut-in period preceding the step rate test. As a result, some CO_2 (+/- 800 feet of gaseous CO_2) entered the wellbore during the shut-in period. This volume of CO_2 was not displaced from the wellbore until the end of the second rate period. This clearly indicates that there was some CO_2 in the reservoir near the wellbore. As the test proceeded, the CO_2 in and near the wellbore was displaced further into the reservoir. Since CO_2 reduces the relative permeability to water, as the CO_2 was displaced further into the reservoir, the injectivity to water increased. As the CO_2 was displaced further into the reservoir, the incremental injectivity increases became insignificant after the fourth point. This accounts for the increase in injectivity in the first four points of the test. Analysis of the remaining portion of the step rate test clearly shows a fracture pressure of 1325 psig.

Due to a miscommunication, there was a time period in late 1992 when the pressure limit was mistakenly believed to be 1140 psig. When the error was discovered, the situation was immediately corrected. However, important data was gathered during this time. Water injection was almost constant for the first 75 days of injection. Cold weather caused erratic injection for the next 2-3 weeks after which, CO₂ injection was commenced. I have constructed a "Hall Plot" for the first 75 days of injection. The "Hall Plot" is a plot of cumulative injection (on the x-axis) versus the summation of (delta p)*(delta t). Where delta p is the injection pressure above static pressure and delta t is the specific time interval for which delta p is applicable. Mathematically, the slope of this line is inversely proportional to the injectivity of the well. Consequently, if the injectivity is constant, the plot should exhibit a straight line. Early time data (days 1-7) do not exhibit a straight line due to transient effects. There is a hump in the data at a cumulative injection of about 8500 bbl's due to a pressure fall-off test being run. The rest of the data indicates that there is little variance in the slope of the plot indicating that injectivity is not increasing and consequently, the well is not being fractured. This indicates that no fracturing was occurring during the time when a maximum pressure of 1140 psig was utilized.

A "Hall Plot" can also be constructed for a theoretical low compressibility system injecting water. Exhibit 3 shows two curves. The solid curve is the "Hall Plot" for this theoretical system (the parameters used for the theoretical model were taken from the October fall-off test analysis) while the dashed curve is for the WLHU 1-9 during the first 75 days of injection. There is a discrepancy in some of the early data, but the late time data is almost a perfect match. A theoretical model can also be constructed to examine the effect of continuously increasing the fracture length in a well. Exhibit 4 shows two curves. The solid curve is for a well injecting above fracture pressure and extending the fracture length at a rate of 1 foot per day. The dashed curve is again the "Hall Plot" for the WLHU 1-9. Review of these curves clearly indicates that no fracturing occurred in the WLHU 1-9.

Pressure fall-off tests were run in mid October 1992 and early March 1993. The October test was run after injecting at 1140 psig while the March test was run after injecting at 560 psig. Analysis results of both tests are shown below:

| | October 1992 | March 1993 |
|---------------------------------|--------------|------------|
| Max Wellhead Injection Pressure | 1140 psig | 560 psig |
| Permeability to Water | 14.6 md | 14.4 md |
| Skin Factor | -1.78 | -1.60 |

Calculated permeability is virtually identical and in both cased the skin is slightly negative. This negative skin is due to the hydraulic fracture treatment performed during completion of the well. Linear flow would be attributable to large fractures and neither test exhibited significant linear flow. These test results indicate that no fracturing occurs at 560 or 1140 psig.

The final evidence submitted is well logs on the WLHU 1-9. Exhibits 5 through 7 are portions of the resistivity, porosity, and cement bond logs respectively. The resistivity and porosity logs indicate that there are no porous or permeable zones within 150' of the top of the pay interval (2784'-2824'). The cement bond log indicates excellent bond across the pay zone and up the hole.

Exhibits 8 through 10 are injection profile/channel check logs run after completion (September 1992), the first water cycle (December 1992), and the first CO_2 cycle (February 1993). These logs indicate that fluid is entering the formation through the perf's and dispersing from a top of 2776' to a bottom of 2831'. Surface injection pressures were as high as 1240 psig. These measurements are within 8 feet of the pay interval and the porosity logs show that this portion is essentially zero porosity. This extra interval is most likely due to some small fracture height growth during the fracture stimulation treatment performed during completion. It should be noted that the final survey shows neither an upward nor downward channelling of fluid.

In summary, the following points have been demonstrated:

- 1. Static surface pressure at the end of shut-in period was 370 psig from the fall-off test.
- 2. The step rate test is slightly curved in the initial points due to changing permeability to water as a result of decreasing CO_2 saturations near the wellbore.
- 3. Analysis of the higher pressure region of the step rate indicates fracturing occurs 1325 psig surface injection pressure.
- 4. Analysis of the "Hall Plot" for the WLHU 1-9 while injection at a maximum surface injection pressure of 1140 indicates no fracturing.
- 5. Analyses of pressure transient tests performed after injecting at 560 and 1140 psig yield almost identical results and show no evidence of large fractures.
- 6. Profile logs show no channeling up or down with surface injection pressures as high as 1240 psig.

Consequently, fracturing is not occurring at surface injection pressures below at least 1240 psig and based upon the March 5, 1993, step rate test, fracturing occurs at a surface pressure of 1325 psig.

On the basis of this, Yates Petroleum Corporation requests that the maximum surface injection pressure for the West Loco Hills Unit Tract 1 Well No. 9 be increased to at least 1300 psig.

If you have any question regarding my analysis or data, please contact me at (505) 748-1471 extension 185.

Robert S. Fant Engineer

RSF/rsf

JOHN WEST ENGINEERING COMPANY

Hobbs, New Mexico

STEP RATE INJECTION TEST

DATE: March 5, 1993

CLIENT: Yates Petroleum Corporation

WO#: 93-14-0349

WELL NAME: West Loco Hills Unit Well No. 1-9 Eddy County, New Mexico

MID-PERFS. =

PACKER DEPTH =

| внр | GAUGE DI | EPTH = 28 | 000 | | | | (6) | (6) | (7) |
|-----|--------------|-----------|--------------------------|-------------|---------------------------------|--------------------------------|---|--|--------------------------|
| | | | (1) | (2) | (8) | (e) | | | |
| 8 | TEP NO. A | | BURFACE TURING PRESS. | CUMMULATIVE | INJECTION RATE (bbls/day) | FRICTION HEAD LOSS (pol) | CORHECTED TUBING PRESS. (pst) (1)-(4) | INJECTION BATE (gpm) (0)/34.2857 | MEASURED BHP (psi) |
| R | EMARKS | TIME | (paig) | COUD | 8888 Salada Anno 2 Solo | | | | |
| | | | 500 6 | | 316.8 | 2.880 | 525.7 | 9.24 | |
| | | 9:55 | 520.0 | 1.0 | 288.0 | 2.415 | 549.0 | 8.40 | |
| | | 10:00 | 550.0 | 2.1 | 316.8 | 2.880 | 556.1 | 9.24 | |
| | | 10:05 | 569.2 | 3.1 | 288.0 | 2.415 | 566.8 | 8.40 | |
| | 1 | 10:10 | 508.2 | | 297.6 | | | 44.70 | |
| | | 40.45 | 655.2 | 4.5 | 403.2 | 4.500 | 650.7 | 11.70 | |
| | | 10:15 | 670.4 | 6.0 | 432.0 | 5.113 | 665.3 | 12.00 | |
| | 0 | 10.20 | 689.4 | 7.4 | 403.2 | 4.500 | 684.9 | 11.70 | |
| | 2 | 10.20 | | | 412.8 | | 707 5 | 15.06 | 3 |
| | | 10:30 | 775.4 | 9.3 | 547.2 | 7.917 | 767.5 | 15.90 | s |
| | | 10:35 | 802.0 | 11.2 | 547.2 | 7.917 | 794.1 | 15.9 | 8 |
| | 3 | 10:40 | 803.3 | 3 13.1 | 547.2 | 2 7.917 | 795.4 | 10.0 | |
| | 5 | 10.11 | | | 547.2 | 2 | | 21 0 | 0 |
| | | 10:45 | 5 895.0 | 3 15.6 | 5 720.0 | 0 13.154 | 002. | 21.0 | 0 |
| | | 10:50 | 917. | 2 18.1 | 720. | 0 13.15 | 906 | 3 21.0 | 0 |
| | 4 | 10:5 | 5 919. | B 20.6 | 3 720. | 0 13.15 | 4 000. | | |
| | | | | | /20. | 0 20 76 | 983. | 7 26.8 | 8 |
| | | 11:0 | 0 1004. | 5 23. | 8 921. | e 20.70 | 9 1012. | 9 26.8 | 8 |
| | | 11:0 | 5 1033. | 7 27. | 0 921. | 6 20.76 | 9 1018. | 0 26.8 | 38 |
| | 5 | 11:1 | 0 1038. | 8 30. | 2 921 | 6 20.10 | | | |
| | | | | | 921 | 8 32.85 | 1095. | 9 34.4 | 14 |
| | | 11:1 | 5 1128 | .7 34. | 0 1123 | 2 29.94 | 1115 | .3 32.7 | 76 |
| | | 11:2 | 0 1145 | .2 38. | 2 1123 | 0 31.38 | 1123 | .9 33.0 | 60 |
| | 6 | 11:2 | 1155 | .3 42 | 1152 | 0 | | | |
| | | | | 48 | 9 1324 | 8 40.64 | 1170 | .4 38. | 64 |
| | | 11:3 | 30 1211 | .0 40 | 4 1324 | 8 40.6 | 1184 | .3 38. | 64 |
| | | 11: | 35 1224 | .9 51 | 0 1324 | .8 40.6 | 43 1202 | .0 38. | 64 |
| | 7 | 11:4 | 1242 | .0 50 | 1324 | .8 | | | |
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Exhibit 1

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[HALL.XLW]Chart1





Page 1

[HALIDEAL.XLW]Chart1

Ideal Transient System vs Actual Field Data



[HALIDEAL.XLW]Chart3





Exhibit 4

Page 1

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| Bottom Log Interval | th I | 2904 F | | | | - | | | | | | | | | | 000 | | | | | | | | | | | | | | 1 | | | |
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| Casing Driller Size | @ Depth | 8.625 IN | @ 385 F | | @ | 1 | | | | | | | | | | | | _ | | | | | | | | | | | | | | | _ |
| Casing Schlumberg | ger | 390 F | | | | | | | | | | | | TTT | | 11 | | | | | | | | | | | | | | | | | |
| Bit Size | | 7.875 IN | | | | -"+++ | | | | | | | | | | | | | | | | | | | | | | 11 | | | | 11 | |
| Type Fluid In Hole | Vicencity | BRINE | 00.0 | | | -1 | | | | | | | | | +++ | | | | | | | +++ | | +++ | | | +++ | | +++ | | +++ | ++-' | + |
| | | IU LB/G | 20.5 | | | - | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Source Of Sample | | PIT | 0 | | | - 11 | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| BM @ Measured Te | emperature | 0.051 OHMM | @ 76 DEGE | : | 0 | | | +++ | | +++ | | +++ | +++ | +++ | +++ | + | ++- | $\left \right $ | | +++ | +++ | +++ | + | | | A | | \mathbf{H} | +++ | +++ | +++ | ++- | + |
| RMF @ Measured 1 | Temperature | 0.038 OHMM | @ 75 DEGF | | @ | | | | | | | | | | hII | | ٨ | | M | h | | | | | | | h | | | | | | \perp |
| RMC @ Measured | Temperature | | @ | | @ | | | | | Th | IN | | | | Λ | | Π | | 7 | | | | | | 1 | | | | | | | | |
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| FINAL PRI Schlumbe | I NT rger | CEMENT I DEM | BOND VA NSITY LO | RIABLE G | | | | | | | | _ | | S | | | | | | | | | | | | تين تين أفري | | 200 بہتی پہنی | | |
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| vpe Fluid in Hole | 2% KCL WATER | | | | reh | -i | 1 | | 111 | Y | 1 | 1 | | 1 | | | 11 | | | | 1 | | | 4+ | 14 | -11 | | 11/1 | - | |
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FAST FM



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| ECARDINA SURVEYS | (0. | EJECTO LOG Tempera Micro-Cal | ture : | es 950ps | - · · · · · · · · · · · · · · · · · · · | | |
|---|---|---|--|--|---|--|--|
| HLE NO. FAK COPY Rush Info | COMPANY late WELLWest have FIELD West COUNTY Edge LOCATION: SEC 7_TWP_ | 8-5 RGE 30-E | Corp #-1-9 N 443 Other Services | Shut w Temperature 12 hn SI @ 11:152 | Servorak. | | Exhibit 10 |
| Permanent Datum Log Measured from Drilling Measured from Date Run No. Type Log Depth-Driller Depth-Driller Depth-Logger Bottom Logged Interval | 2-19-93 | Elev. 3529 Ft. Above Permanent Datu | KB <u>353</u> DF GL <u>352</u> 5 | ν υ υ υ υ υ υ υ υ υ υ υ υ υ υ υ υ υ υ υ | Frijech F. | | |
| Top Logged Interval Type Fluid in Hole Salinity Ppm Cl. Density Lb./Gal. Level Max. Rec. Temp. Deg. F Opr. Rig Time Recorded By Witnessed By | 2600 COZ 75° Scott FANT | | | CARDINAL SURVEYS | | | CER VELOCITIES 60 80 100 61 2700 |
| Run Bore Hol | le Record To Si S S 2.3 | Casing Record ze Wgt. From 5/5 0 12 1.5.5 0 8 0 | d To 385 2900 2768 | P. 02 | | | ERCENT BASED ON THAT |



2794-2821- 100% FLUID LOSS

1031 SLIRFREE PRESSLIRE LNJECTING



ATES POTROLEZEM (ORD) SUMMARC TUBING VEROCITY RATE INDICATED 400 BPD TD-2830 PERFS 28-2784-86 -7 No iNDICATION OF FLUID LOSS 2794-2821- 100% FLUID LOSS

1031 SLURFREE PRESSLIRE LNJECTING 950 SHUT AFE-IN RESSLIRE 1/2 HEUR & 1 HEUR NO CAANINER DOWNI INDICATED