George QJ #10 -- Drainage Area

1. Original Oil in Place (stock-tank barrels) is given by the equation

OOIP = 7758*A*h* phi*So/Boi

where h*phi*So is the hydrocarbon pore volume.

- 2. The log calculations for hydrocarbon pore volume yield h*phi*So = 0.769.
- 3. Boi = 1.28 from the Standing Correlations where the parameters are as follows:

| = | 600 |
|---|------------------|
| = | 110 degrees F |
| = | 0.7 |
| = | 42 degrees API |
| | = = = = |

4. Ultimate Primary Recovery (Np) = Recovery Factor*OOIP

where Recovery Factor (\mathbf{Rf}) = 0.25 from 1957 paper entitled

"Estimation of Ultimate Recovery from Solution Gas-Drive Reservoirs" by Wahl, Mullins and Elfrink of Magnolia Petroleum.

5. Then, Np = $Rf^{7758}A^{h*}phi^{SO}/Boi$

and, by rearranging, A = Np*Boi/(Rf*7758*h*phi*So) in acres

A = 223615*1.28/(0.25*7758*0.769) in acres

A = 192 acres is the Drainage Area

Yates Petroleum Corporation May 11, 2006 BEFORE THE OIL CONSERVATION DIVISION Santa Fe, New Mexico Case No. <u>13706</u> Exhibit No. 10 Submitted by: <u>YATES PETROLEUM CORPORATION</u> Hearing Date: <u>May 11, 2006</u>

George QJ #9 -- Drainage Area

1. Original Oil in Place (stock-tank barrels) is given by the equation

OOIP = 7758*A*h* phi*So/Boi

where h*phi*So is the hydrocarbon pore volume.

- 2. The log calculations for hydrocarbon pore volume yield h*phi*So = 1.047.
- 3. Boi = 1.28 from the Standing Correlations where the parameters are as follows:

| = | 600 |
|---|----------------|
| = | 110 degrees F |
| — | 0.7 |
| = | 42 degrees API |
| | = = = |

 4. Ultimate Primary Recovery (Np) = Recovery Factor*OOIP
 where Recovery Factor (Rf) = 0.25 from 1957 paper entitled
 "Estimation of Ultimate Recovery from Solution Gas-Drive Reservoirs" by Wahl, Mullins and Elfrink of Magnolia Petroleum.

5. Then, Np = Rf*7758*A*h*phi*So/Boi
 and, by rearranging, A = Np*Boi/(Rf*7758*h*phi*So) in acres
 A = 132384*1.28/(0.25*7758*1.047) in acres

A = 83 acres is the Drainage Area

George QJ #2Y -- Drainage Area

1. Original Oil in Place (stock-tank barrels) is given by the equation

OOIP = 7758*A*h* phi*So/Boi

where h*phi*So is the hydrocarbon pore volume.

2. The log calculations for hydrocarbon pore volume yield h*phi*So = 0.773.

3. Boi = 1.28 from the Standing Correlations where the parameters are as follows:

| Solution GOR | = | 600 |
|------------------|---|----------------|
| Temperature | = | 110 degrees F |
| Gas Gravity | | 0.7 |
| Tank Oil Gravity | = | 42 degrees API |
| | | |

 4. Ultimate Primary Recovery (Np) = Recovery Factor*OOIP
 where Recovery Factor (Rf) = 0.25 from 1957 paper entitled
 "Estimation of Ultimate Recovery from Solution Gas-Drive Reservoirs" by Wahl, Mullins and Elfrink of Magnolia Petroleum.

5. Then, Np = Rf*7758*A*h*phi*So/Boi
and, by rearranging, A = Np*Boi/(Rf*7758*h*phi*So) in acres
A = 33223*1.28/(0.25*7758*0.773) in acres
A = 28 acres is the Drainage Area (Oil Well)

George QJ #2Y -- Drainage Area

1. Original Gas in Place (Scf) is given by the equation

OGIP = 43560*A*h* phi*Sg*Bg

where h*phi*Sg is the hydrocarbon pore volume.

2. The log calculations for hydrocarbon pore volume yield h*phi*Sg = 0.773.

3. Bg = 35.35*p/(zT) in Scf per cubic foot where the parameters are as follows:

| | Pressu Tempo Gas G Tc Pc | ire erature ravity | | = = = | 2312 p 110 de 0.65 380 de 670 ps | osi egrees I egrees I i | F = R | 570 degrees R |
|---------------|--|--------------------------|------------|------------------|--|----------------------------------|----------|--------------------|
| | Then | Tr Pr | = | (460+1 2312/6 | 10)/38 570 | 0 | = | 1.50 3.45 |
| | And | Z | - | 0.77 | | | | |
| So | Bg | = | 35.35* | °2312/(0 |).77*57 | 0) | = | 186 Scf/cubic foot |
| 4. Ultimate I | Recover | y (Gp) | | Recov | ery Fac | tor*O(| SIP | |
| where | Recove | ery Fact | or (Rf) | = | 0.80 | for m | edium-j | porosity sands |
| 5. Then, Gp | = | Rf*43 | 560*A* | h*phi* | Sg*Bg | | | |
| and, b | A = Gp/(Rf*43560*h*phi*So*Bg) in acres | | | | | | | |
| | | | A = (|).313*1 | 0^9/(0.8 | 8*4356 | 0*0.77 | 3*186) in acres |
| | | | A = | 62 acre | s is th | e Drai | nage A | rea (Gas Well) |

Powers OL #6 -- Drainage Area

1. Original Gas in Place (Scf) is given by the equation

OGIP = 43560*A*h* phi*Sg*Bg

where h*phi*Sg is the hydrocarbon pore volume.

2. The log calculations for hydrocarbon pore volume yield h*phi*Sg = 0.344.

3. Bg = 35.35*p/(zT) in Scf per cubic foot where the parameters are as follows:

| | Pressu Tempe Gas Gr Tc Pc | re erature ravity | | = = = = | 2312 p 110 de 0.65 380 de 670 psi | si grees] grees] i | F = R | 570 degrees R |
|---------------|---|-------------------------|----------------|------------------|---|-------------------------------|----------|--------------------|
| | Then | Tr Pr | = | (460+1 2312/6 | .10)/380 70 |) | = | 1.50 3.45 |
| | And | Z | = | 0.77 | | | | |
| So | Bg | = | 35.35* | *2312/(0 |).77*57(| 0) | = | 186 Scf/cubic foot |
| 4. Ultimate R | lecovery | 7 (Gp) | = | Recove | ery Fact | or*O0 | GIP | |
| where | Recove | ery Fact | or (Rf) | = | 0.80 | for m | edium-j | porosity sands |
| 5. Then, Gp | = | Rf*43 | 560*A* | h*phi*S | Sg*Bg | | | |
| and, by | A = $Gp/(Rf^*43560^*h^*phi^*So^*Bg)$ in acres | | | | | | | |
| | | | A = (|).110*10 | 0^9/(0.8 | *4356 | 60*0.34 | 4*186) in acres |
| | | | A = | 49 acre | s is the | e Drai | nage Ai | rea (Gas Well) |