

DEC 291938

December 22, 1998

New Mexico Oil Conservation Division 2040 S. Pacheco Street Santa Fe, New Mexico 87505 Attention: Mr. David Catanach

Re: Case No. 12098 Unorthodox Location and Simultaneous Well Dedication Ute Mountain Tribal J # 6 SW/4 Section 1-31N-14W San Juan County, New Mexico

Gentlemen:

Pursuant to our hearing last Thursday, please find enclosed volumetric calculations for the Dakota formation under the captioned land.

Should you have any questions or need additional information please call me at (817)877-2336.

Yours very truly,

Win Than

Edwin S. Ryan, Jr.

Cc: Bureau of Land Management San Juan Resource Area 701 Camino Del Rio Durango, Colorado 81301 Attn: Mr. Dan Rabinowitz

> Data Consultants Inc. P.O. Box 14749 Albuquerque, New Mexico 87191 Attn: G.D. Simon

Mr. Jim Bruce P.O. Box 1056 Santa Fe, New Mexico 87505

Ute Mountain Ute Tribe P.O. Box 248 Towaoc, Colorado 81334 Attn: Mr. Gordon Hammond

#### Volumetrics - SW/4 Sec 1 T31N R14W

Sand	OGIP (MMCF)	Rec Gas (85% RF) (MMCF)	
First Dakota	338	287	
Second Dakota	606	514	
Third Dakota	120	101	
Total	1064	902	

The following pages contain the calculation sheets for the Upper Dakota Sands in the SW/4 of Section 1 T31N R14W. The following table summarizes the results.

Currently there are two wells producing in the SW/4 of Section 1: Ute Mountain Tribal J 1 and Ute Mountain Tribal J 4. The wells were drilled by Amoco to test fault separation. The Ute Mountain Tribal J 1 was completed in July of 1973. The well was completed in the upper 3 sands of the Dakota and the 6<sup>th</sup> sand. In June of 1984, the Dakota zones were reperforated and restimulated. The well showed no significant response to this action. In September of 1993, production fell from 1624 mcf/mo to 138 mcf/mo and continued to fall below 100 mcf/mo. In July of 1994, fill was cleaned out, and the Dakota was acidized. The well did not respond to this.

The Ute Mountain Tribal J 4 was completed in February of 1974. The well was completed in the Morrison and the 6<sup>th</sup> sand. It was produced from these zones until March of 1984 (cumulative production at this time: 586 MMCF). At this time, the 2<sup>nd</sup>, 3<sup>rd</sup>, and 5<sup>th</sup> sands were added, and the new and old zones were stimulated together. In July of 1988, fill was checked but none was found. In June of 1991, 17 feet of fill was cleaned out. In March of 1993 fill was checked but none was found. In July of 1994, the Morrison was abandoned with a CIBP, and the remaining zones were acidized. The well responded at about 500 mcfd. Currently the well is making approximately 60 mcfd.

The following table summarizes the production estimated from the two wells (J 4 production is less the cumulative production prior to the 1984 workover).

Well	Cumulative Production (MMCF)	Decline Curve EUR (MMCF)	
Ute Mountain Tribal J 1	460	460	
Ute Mountain Tribal J 4	309	506	
Total	769	966	

The J 1 well production also includes Lower Dakota sand production. If porosity thickness were used to determine the percentage of reserves attributable to the different productive zones, the Lower Dakota would account for approximately 26% of the production from the J 1. In addition, the J 1 is located 220 feet from the east-west center section line; therefore, some of its drainage is occurring in the north half of the section.

When the J 4 was completed to the upper Dakota in 1984, the J 1 had produced approximately 333 MMCF. The J 1 had a reported shut-in surface pressure of 458 psi in December of 1972 on a Multipoint and Back Pressure Test form submitted to the NMOCC. The J 4 had a reported shut-in surface pressure of 317 psi on the same type form after the workover in 1984. If the J 1 had depleted close to a third of the reserves in place in the upper Dakota, the surface pressure on the J 4 would have been expected to be lower than what was observed. Although, these pressures are suspect due to the fact that fluid level is unknown and insufficient build-up time.

One factor that points to the J 4 recovering unique reserves and pressure not attributable to the J 1 is the production curves. In 1994, a CIBP was set over the lower perfs in the J 4 and it was producing from the upper sands. The initial rate was over 500 mcfd as compared to the late production of approximately 50 mcfd on the J 1. Four years later in 1998, the J 4 is still producing at a rate of approximately 83 mcfd.

The Ute Mountain Tribal J 6 will be a Morrison and Dakota drill well located in the SW/4 of Section 1. The well is intended to test a fault block that has not been tested to date. To test for fault separation from the rest of the quarter section, RFT's are planned to test the pressure in the individual Dakota sands.

## UTE DOME DAKOTA SW/4 SECTION 1-T31N-R14W 1<sup>ST</sup> SAND

### Fluid Properties

=	0.616	Gas Analysis
=	355 °R	Standing's correlation
=	671 psi	Standing's correlation
=	90 °F	Log Measurement
=	732 psi	Calculated (0.32 psi/ft.)
=	120 psi	Estimate
=	0.01926 ft <sup>3</sup> /SCF	Standing & Katz's correlation
=	0.12752 ft <sup>3</sup> /SCF	Standing & Katz's correlation
		= 0.616 = $355 ^{\circ}R$ = $671  \text{psi}$ = $90 ^{\circ}F$ = $732  \text{psi}$ = $120  \text{psi}$ = $0.01926  \text{ft}^3/\text{SCF}$ = $0.12752  \text{ft}^3/\text{SCF}$

Calculate Theoretical Recovery Factor

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$$RF_t = 1 - \frac{B_{gi}}{B_{ga}}$$

 $RF_{t} = 1 - \frac{0.01926}{0.12752}$ 

$$RF_t = 0.8489$$
 (fraction)

Rock Properties

Acre - Feet	=	2,091	Planimetered from net pay thickness maps
Average Porosity	=	0.14	(fraction)ød Avg. (Ute Mountain Tribal J4 Log)
Water Saturation	=	0.49	(fraction) Avg.

Ute Dome Dakota 1<sup>st</sup> Sand Page 2

Calculate GIP, Theoretical and Actual EUR

$$GIP = \frac{.04356Ah_{\emptyset}(1-S_{w})}{B_{gi}} MMCF$$

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$$GIP = \frac{.04356(2,091)(0.14)(1-0.49)}{0.01926} MMCF$$

=	338 MMCF
=	RF <sub>t</sub> x GIP
=	(0.8489)(338)
	=

 $EUR_t = 287 \text{ MMCF}$ 

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#### UTE DOME DAKOTA SW/4 SECTION 1-T31N-R14W 2<sup>nd</sup> SAND

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### Fluid Properties

Gas Gravity	=	0.616	Gas Analysis
T <sub>c</sub>	=	355 °R	Standing's correlation
Pc	=	671 psi	Standing's correlation
T <sub>r</sub>	=	90 °F	Log Measurement
P <sub>ri</sub>	=	732 psi	Calculated (0.32 psi/ft.)
P <sub>ra</sub>	=	120 psi	Estimate
$\mathbf{B}_{gi}$	=	0.01926 ft <sup>3</sup> /SCF	Standing & Katz's correlation
$B_{ga}$	=	0.12752 ft <sup>3</sup> /SCF	Standing & Katz's correlation

#### Calculate Theoretical Recovery Factor

$$RF_{i} = 1 - \frac{B_{gi}}{B_{ga}}$$

$$RF_t = 1 - \frac{0.01926}{0.12752}$$

$$RF_t = 0.8489$$
 (fraction)

**Rock Properties** 

Acre - Feet	=	2,424	Planimetered from net pay thickness maps
Average Porosity	==	0.17	(fraction)ø <sub>d</sub> Avg. (Ute Mountain Tribal J4 Log)
Water Saturation	=	0.35	(fraction) Avg.

Ute Dome Dakota 2<sup>nd</sup> Sand Page 2

Calculate GIP, Theoretical and Actual EUR

$$GIP = \frac{.04356Ah \otimes (1 - S_w)}{B_{gi}} MMCF$$

$$GIP = \frac{.04356(2,424)(0.17)(1-0.35)}{0.01926} MMCF$$

GIP	=	606 MMCF
EUR	=	RF <sub>t</sub> x GIP
EUR	=	(0.8489)(606)

 $EUR_t = 514 \text{ MMCF}$ 

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### UTE DOME DAKOTA SW/4 SECTION 1-T31N-R14W 3<sup>rd</sup> Sand

# Fluid Properties

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Gas Gravity	=	0.616	Gas Analysis
T <sub>c</sub>	=	355 °R	Standing's correlation
Pc	=	671 psi	Standing's correlation
T <sub>r</sub>	=	90 °F	Log Measurement
P <sub>ri</sub>	=	732 psi	Calculated (0.32 psi/ft.)
P <sub>ra</sub>	=	120 psi	Estimate
$\mathbf{B}_{\mathbf{gi}}$	=	0.01926 ft <sup>3</sup> /SCF	Standing & Katz's correlation
$B_{ga}$	=	0.12752 ft <sup>3</sup> /SCF	Standing & Katz's correlation

#### Calculate Theoretical Recovery Factor

$$RF_t = 1 - \frac{B_{gi}}{B_{ga}}$$

$$RF_i = 1 - \frac{0.01926}{0.12752}$$

$$RF_1 = 0.8489$$
 (fraction)

**Rock Properties** 

Acre - Feet	=	782	Planimetered from net pay thickness maps
Average Porosity	=	0.13	(fraction)ø <sub>d</sub> Avg. (Ute Mountain Tribal J4 Log)
Water Saturation	=	0.48	(fraction) Avg.

Ute Dome Dakota 3<sup>rd</sup> Sand Page 2

Calculate GIP, Theoretical and Actual EUR

$$GIP = \frac{.04356Ah \otimes (1 - S_w)}{B_{gi}} MMCF$$

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$$GIP = \frac{.04356(782)(0.13)(1-0.48)}{0.01926} MMCF$$

GIP	=	120 MMCF
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$EUR_{t} = Rr_{t} \times GIR$	EUR,	=	RF <sub>t</sub>	x	GIP
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- $EUR_t = (0.8489)(120)$
- $EUR_t = 101 \text{ MMCF}$

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