SE/4 Section 2 T31N R14W

Current Producing Morrison Wells

	10/00 CUM	Decline EUR
Well	(mmcf)	(mmcf)
Ute Indians A #27-Case #1	680	1,230
Ute Indians A #27-Case #2	680	810

Recoverable Gas in Place (RGIP)

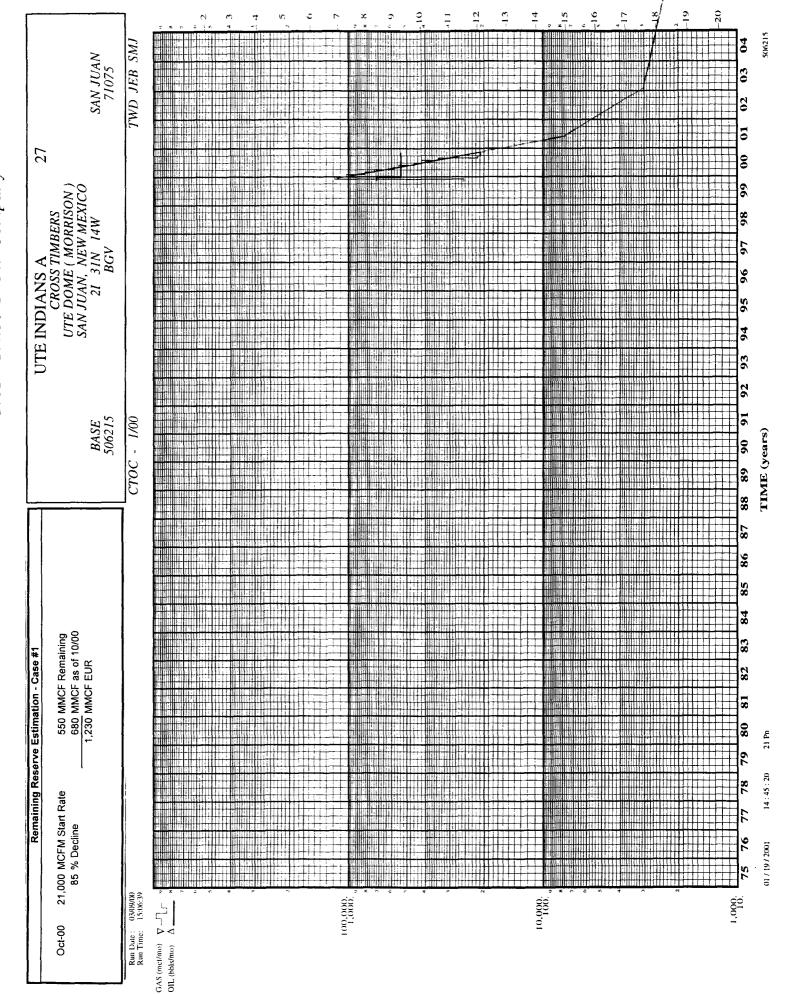
	GIP	RGIP
Sand	(mmcf)	(mmcf)
3rd Morrison	1,675	1,472

Estimation of Remaining Recoverable Gas

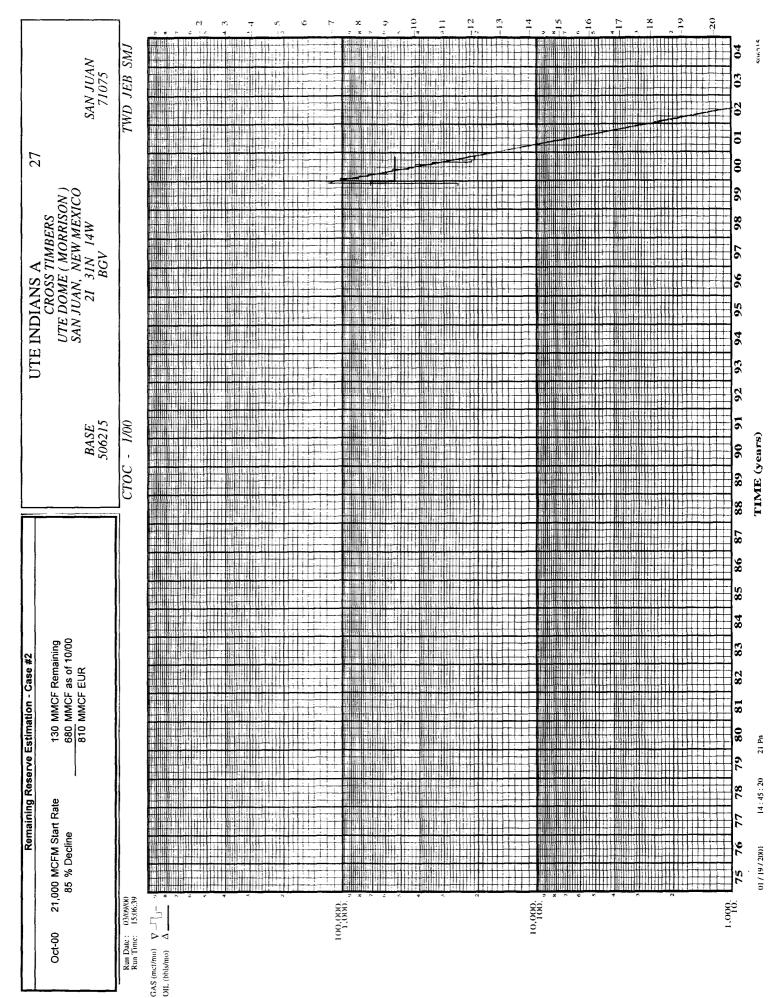
Case #1	(mmcf)
Calculated RGIP from Net Sand Isopach	1,472
Less Decline EUR Current Producers	1,230
Estimated Remaining Recoverable Gas	242

Case #2	(mmcf)	
Calculated RGIP from Net Sand Isopach	1,472	
Less Decline EUR Current Producers	810	
Estimated Remaining Recoverable Gas	662	

OIL CONS	SERVATION	DIVISION
CASE NUM	BER	
	EXHIBIT	8.



Cross Timbers Oil Company



UTE DOME SE/4 SECTION 2-T31N-R14W 3rd MORRISON

Fluid Properties

Gas Gravity	=	0.630	Gas Analysis
T_c	=	363°R	Standing's Correlation
P_c	==	667 psi	Standing's Correlation
T_r	=	113 °F	Log Measurement
$\mathbf{P_{ri}}$	=	1,000 psi	Calculated from Surface Pressure
$\mathbf{P}_{\mathbf{ra}}$	=	135 psi	Estimate
$\mathrm{B_{gi}}$	=	$0.01433 \text{ ft}^3/\text{SCF}$	Standing & Katz's Correlation
$egin{aligned} \mathbf{B_{gi}} \\ \mathbf{B_{ga}} \end{aligned}$	=	0.11797 ft ³ /SCF	Standing & Katz's Correlation

Calculate Theoretical Recovery Factor:

$$RF_{t}=1-\frac{B_{gi}}{B_{ga}}$$

$$RF_i = 1 - \frac{0.01433}{0.11797}$$

$$RF_t = 0.8785$$
 (fraction)

Rock Properties

Acre - Feet	=	3,868	Planimetered from net sand thickness maps
Average Porosity	=	0.19	(Fraction) \mathcal{O}_{dn} Ute Indians A #27
Water Saturation	=	0.25	(Fraction) Ute Indians A #27

Ute Dome 3rd Morrison Page 2 of 2

Calculate GIP, Theoretical and Actual EUR:

$$GIP = \frac{.04356Ah_{\varnothing}(1-S_{w})}{B_{gi}}MMCF$$

$$GIP = \frac{.04356(3,868)(0.19)(1-0.25)}{0.01433} MMCF$$

GIP = 1,675 MMCF

 $EUR_t = RF_t \times GIP$

 $EUR_t = (0.8785)(1,675)$

 $EUR_t = 1,472 \text{ MMCF}$