PREPARED TESTIMONY OF DAVID T. BURLESON

- Question: Mr. Burleson, referring to El Paso's Exhibit No. 12, what does the red line show?
- Answer: The red line shows the pool boundaries of the Lusk-Strawn Oil Pool.
- Question: What does the yellow line show?
- Answer: The yellow line shows the boundaries of the Lusk Deep Unit.
- Question: Does this exhibit show the offset operators surrounding the Lusk-Strawn Oil Pool?
- Answer: Yes.
- Question: To your knowledge, has anyone opposed the granting of El Paso's application in this case.
- Answer: No.
- Question: Who are the committed working interest owners in the unit.
- Answer: El Paso Natural Gas Company, Phillips Petroleum Company, Kerr-McGee Oil Industries, Inc. and Gulf Oil Corporation. Question: Have they concurred in this application?
- Answer: Yes.
- <u>Question</u>: Please point out the presently approved participating area for the Strawn formation.
- <u>Answer</u>: The presently approved Strawn participating area consists of the NE/4 of Section 19, W/2 NW/4 of Section 20, SE/4 of Section 18, SW/4 SW/4 of Section 17, and the E/2 SW/4 of Section 18, all in Township 19 South, Range 32 East, N.M.P.M., Lea County, New Mexico, containing 520.00 acres, more or less.

PREPARED TESTIMONY OF RICHARD F. LEMON EL PASO NATURAL GAS COMPANY

Q. Have you prepared an exhibit which shows the outlines of the Lusk Deep Unit, the development of the Unit and the contours with respect to the Strawn formation?

A. Yes.

- Q. Please explain this exhibit to the Examiner.
- A. Exhibit 1 shows the outline of the Lusk Deep Unit, which is located in Sections
 7, 8, 17, 18, 19 and 20 in Township 19 South, Range 32 East, in west central
 Lea County and in the eastern one-half of Section 24, Township 19 South, Range
 31 East, in northeastern Eddy County, New Mexico.

The Lusk Deep Unit is located approximately 14 miles southwest of the town of Maljamar, New Mexico and underlies a portion of the producing area in the shallower Lusk-Yates oil field. The Lusk Deep Unit area includes 2,725 acres.

Exhibit 1 shows that three wells have been drilled in the Lusk Deep Unit to a depth sufficient to penetrate the Strawn limestone. These wells are the El Paso Natural Gas Company No. 1, No. 2 and No. 3 Lusk Deep Unit.

The El Paso Natural Gas Company No. 1 Lusk Deep Unit was completed as a dual Bone Springs oil-Strawn oil producing well. The Bone Springs potential test was taken on October 26, 1960. Official initial potential test was 141 barrels of oil per day calculated from an actual flow gauge of 47 barrels of oil in eight hours, through a 9/64" choke. Gas-oil ratio was 1342:1. Flowing tubing pressure ranged from 900 psig to 935 psig. Production was through casing perforations from 8759'-8777'. The formation was treated with 500 gallons of acid. The Strawn potential test on well No. 1 was taken on October 7, 1960. Official initial potential test was 732 barrels of oil per day, calculated from an actual flow of 122 barrels of oil in four hours, through a 16/64" choke. Gas-oil ratio was 2640:1. Flowing tubing pressure was 2345 psig. Production was through casing perforations from 11, 168'-11, 193'. Completion was natural.

The El Paso Natural Gas Company No. 2 Lusk Deep Unit was drilled to a total depth of 13,974' to test the Devonian and was subsequently plugged back and completed as a dual Strawn oil-Morrow gas well. The Strawn potential test was taken on April 1, 1961. Official initial potential test was 641 barrels of oil per day, calculated from an actual flow gauge of 53.4 barrels of oil in two hours, through a 16/64" choke. Gas-oil ratio was 3329:1. Flowing tubing pressure was 2400 psig. Production was through casing perforations from 11,220'-11,250'. Perforations were treated with 600 gallons of acid.

The Morrow potential test was taken on April 1, 1961. Calculated absolute open flowing potential was 31,500 Mcf of gas per day. Gas-condensate ratio was 24,790:1. Shut-in tubing pressure was 3618 psig. Production was through casing perforations from 12,380'-12,398'. Perforations were treated with 600 gallons of acid.

The El Paso Natural Gas Company No. 3 Lusk Deep Unit was completed as a dual Strawn oil-Morrow gas producing well. The Strawn potential test was taken on November 1, 1961. Official initial potential test was 285 barrels of oil, calculated from an actual flow gauge of 71.27 barrels of oil in six hours, through a 10/64" choke. Gas-oil ratio was 2397:1. Flowing tubing pressure was 2887 psig. Production was through casing perforations from 11,310'-11,340'. Completion was natural.

The Morrow potential test was taken on October 31, 1961. Calculated absolute open flowing potential was 30,000 Mcf of gas per day. Gas-condensate ratio was 12,559:1. Shut-in tubing pressure was 3845 psig after being shut in for 72 hours. Production was through easing perforations from 12,370'-12,390'. Completion was natural.

Shown on Exhibit 1 is an interpretation of the sub-surface configuration of the top of the Strawn limestone on the area covered by the plat. This plat is an excerpt taken from a larger structural map contoured on top of the Strawn limestone. This larger map was prepared from information obtained from correlation of electrical and radioactivity logs on a regional basis and incorporates a certain amount of siesmic data. The regional strike mapped on the top of the Strawn formation is approximately north-to-south in the immediate vicinity of the Lusk Deep Unit. A low structural area or trough on the eastern edge of the plat and a low area in the western one-half of Section 12, Township 19 South, Range 31 East are evident. The contours show that the regional dip of the geologic horizon created by the top of the Strawn formation is from west to east at approximately 450' per mile. This regional dip has a closure of a maximum of 200' in portions of Sections 17, 18, 19 and 20 with reference to the top of the Strawn formation. Additional drilling will be required to further detail the area and define the limits of production. The present and proposed revision to the unit participating area is indicated by the shaded areas.

- Q. Would you explain the cross-section of six wells on Exhibit No. 2 and what this exhibit shows, and other pertinent information concerning these wells which you have considered.
- A. Exhibit 2 is a geological cross-section relating the Strawn Limestone section in the Lusk Strawn Pool area. This cross-section trends in a northwest-southeasterly direction and contains the well logs on the three Lusk Unit Strawn completions, the Pan American Nos. 1 and 2 Greenwood Unit and the Shell No. 1 Perry-Federal. A sub-sea datum of 6000' was selected for purposes of correlating the logs. The sections in the wells over which drillstem tests were conducted and the perforated intervals are indicated in red and green. The trace of the cross-section appears in the inset map.

From an interpretation of this cross-section, the following inferences can be reasonably drawn:

- 1. The line of Section A-A' is almost parallel to regional strike.
- 2. The Strawn oil producing feature is not primarily related to any large deep regional structural feature or anticlinal trend, but is a local north-to-south trending anticlinal feature with an indicated structural closure of 200¹. The producing area is also controlled by porosity development, the thickness and quality of the producing horizon being dependent upon the degree of development of the porosity. An illustration

of this is the fact that no porosity is indicated in the Strawn formation from the electrical or radioactivity logs on the Pan American No. 2 Greenwood Unit, located 4 - 3/5 miles northest of the El Paso Natural Gas Company No. 2 Lusk Deep Unit. The porosity is also undeveloped in the equivalent Strawn section in the Shell Oil Company No. 1 Perry-Federal, located 4 - 1/3 miles southeast of the El Paso Natural Gas Company No. 3 Lusk Deep Unit.

- 3. The pool limits for the Lusk-Strawn Oil Pool are not as yet established by drilling.
- 4. The dip on the east flank of the producing structure is quite steep.The top of the Strawn in the No. 1 Lusk Unit is 148' higher structurally than in the No. 3 Lusk Unit.

There has been no evidence of formation water found in studies of test and production data for the Strawn formation in this immediate area. No formation water was found during testing or production of the three Lusk Deep Unit wells.

The nearest comparable oil production from the Strawn formation is in the Shell Oil Company No. 1 Querecho Plains Unit, located approximately six miles northeast of the El Paso Natural Gas Company No. 2 Lusk Deep Unit. This well was completed as a Strawn oil well on January 11, 1957, through casing perforations from 11,595'-11,625' in the Strawn limestone. Initial flowing potential was 221 barrels of oil per day with no water reported. The total cumulative production to November 1,1961 was 257,100 barrels of oil with no water being reported.

The Shell Oil Company No. 2 Querecho Plains Unit, located 1 - 1/3miles south of the No. 1 Querecho Plains Unit, drillstem tested the section equivalent to the producing zone in the No. 1 well. Recovery was 95' of drilling mud with no water.

It may be concluded from this exhibit that the lateral limits of the Lusk Strawn oil pool will be controlled principally by the development of porosity and permeability with no indication of the presence of a water drive. Furthermore, the Strawn reservoir will operate under a solution gas drive where the chief source of reservoir energy will be supplied by the expansion of the oil and gas.

- Q. Do you have an exhibit showing reservoir completion data on wells drilled in the Lusk-Strawn Oil Pool?
- A. Yes, that is El Paso's Exhibit No. 3.
- Q. Would you please explain this exhibit?
- A. The various reservoir and completion data available from the three wells completed to date are shown in summary form in Exhibit 3. The completion data such as top of pay, perforated interval, treatment and potential test information previously discussed are listed under item 2.

Item No. 3 of this exhibit sets forth the reservoir fluid characteristics. Analysis of a sub-surface oil sample taken on well No. 2 on August 20, 1961 indicated the following characteristics:

a. Saturation or bubble point pressure, psig......4150

- b. Reservoir volume factor @ orig. press......2.605
- d. Oil viscosity @ original press., cp.....0.146
- e. Oil gravity, ⁰API..... 47.5

The reservoir characteristics for the Strawn formation are shown under item 4. The Strawn formation in each of the three wells completed to date has been cored. The average formation factors based on averaging 86 feet of core considered to be the net pay interval are: porosity - 7.1%, water saturation - 30.9% and permeability of 17.7 millidarcys. The average net pay based on cores and well logs of the three wells is 38 feet.

In connection with reservoir characteristics, production tests have indicated the wells to have high producing capacities. Productivity indexes of 2.0 and 2.6 have been calculated from production tests on wells Nos. 1 and 2. It is significant to note from these tests that producing rates of 300 BOPD and 390 BOPD from wells Nos. 1 and 2 can be obtained with a drawdown in bottom-hole pressure of only 150 psi. Although a PI test has not been conducted on well No. 3, it is anticipated that this well will have similar producing characteristics. Q.

Do you have performance history data for the Lusk-Strawn Oil Pool?

A. Yes, that is El Paso's Exhibit No. 4.

Q. Would you please explain what this exhibit shows?

A. The performance history of the Lusk-Strawn Oil Pool is depicted graphically in Exhibit 4. This exhibit shows the number of producing wells, oil production and pressure data related to time. The total cumulative oil production for the three producing wells to December 1, 1961 is 122,537 barrels. The wells produced 14,134 barrels during the month of November. The pressure information shown on this graph will be discussed in detail in a later exhibit.

Recent gas-oil ratio tests, although not represented in Exhibit 4, indicate a producing ratio of approximately 2400 cubic feet per barrel. In view of the high initial producing gas-oil ratio of the undersaturated Strawn oil, the limiting ratio of 4000 cubic feet per barrel being requested in this case is, in my opinion, a reasonable limit.

The gas production from the pool is presently being flared; however, a processing agreement is being worked out with Phillips to provide for gathering the produced gas. It is anticipated that this agreement will be consummated in the very near future.

Q. El Paso's Exhibit No. 5 is a composite electrical log of Well No. 1 in the LuskDeep Unit. Is that correct?

A. That is correct.

- Q. Please explain the pertinent facts that this log shows.
- A. Exhibit 5 shows the correlation of the electric log with the micro log on Lusk
 Deep Unit Well No. 1 with reference to the perforated interval. The micro log,
 which indicates formation porosity, reveals the Strawn limestone interval to be
 a continuous section with no important barriers which would block the flow of
 reservoir fluids.
- Q. What is El Paso's Exhibit No. 6?
- A. It is a core analysis summary of Well No. 1 in the Lusk Deep Unit.
- Q. Please explain this exhibit to the Examiner.
- A. The Core Analysis Summary for the Lusk Deep Unit Well No. 1 is shown in Exhibit 6. It is indicated in this exhibit that 33 of the 41 net feet assigned this well was actually cored. The net interval of 41 feet is based on cores available and well logs. The average characteristics of the 33 feet of the net pay interval which was cored are: Porosity 8.3%, water saturation 28.5% and permeability 24.6 millidarcys. It is important to note that fractures were noted over much of the cored interval which would enhance the ability for free fluid movement. Therefore, considering the characteristics of the Strawn reservoir complete drainage both vertically and horizontally should occur.
- Q. Do you have information and data to show that one well will effectively and efficiently drain an area in excess of 160 acres in the Lusk-Strawn Oil Pool?
- A. Yes, I have a pressure interference graph which is El Paso's Exhibit No. 7.
- Q. Please explain this exhibit to the Examiner?

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Α. Exhibit 7 presents the pressure interference observed from data on the three Strawn completions in the Lusk Deep Unit. This graph relates the bottom-hole pressure at a subsea datum of 7585' against time for each well. It is apparent from this exhibit that production from the producing wells has caused a reduction in reservoir pressure which becomes evident when pressures are taken on newly completed wells prior to production. The first such indication was observed upon completion of Well No. 2 in April, 1961. The bottom-hole pressure in Well No. 2 after five days shut-in time was 5799 psig, 11 pounds below the original reservoir pressure of 5810 psig. A pressure taken in No. 1 seven days later after the well had been shut-in for 73 hours was 5802 psig. The approximate oil production corresponding with these pressures was 35,000 barrels. Although in this instance the pressure reduction from the original pressure is slight the pressures on the two wells are in very close agreement. Wells Nos. 1 and 2 are located 1866 feet apart. A circle having a radius of 1866 feet indicates a drainage area of 251 acres.

Bottom-hole pressures taken on August 5, 1961 on Wells Nos. 1 and 2 after approximately 80,000 barrels of oil had been produced were 5766 psig and 5765 psig, respectively. These pressures were recorded the same day after the wells had been shut-in for 72 hours and were recorded by the same bottom-hole pressure bomb. The close agreement of pressures in these two wells indicates excellent communication within the Strawn reservoir.

A bottom-hole pressure survey conducted the 6th and 7th of November, 1961 on Wells Nos. 1 and 2 and a new completion, No. 3, indicated the following pressure data: Well No. 1 - 5704 psig, Well No. 2 - 5706 psig and No. 3 -5710 psig. On this survey the wells were shut-in 100 hours, 98 hours and 136 hours, respectively. The significant fact apparent from these data is the pressure recorded on Well No. 3. The pressure of 5710 psig, 100 psi below the original, was very nearly the same as those recorded on Wells Nos. 1 and 2, even though Well No. 3 had not previously produced. Thus the oil production from Wells Nos. 1 and 2, which totaled 110,000 barrels, caused a reduction in reservoir pressure in Well No. 3. The distance between Wells Nos. 1 and 3 is 1650 feet. The drainage area indicated by this distance is 196 acres.

It is therefore obvious that drainage has occurred over areas in excess of 160 acres within a period of several months.

- Q. What is your conclusion from this exhibit with reference to the extent that one well is able to effectively and efficiently drain an area in the Lusk-Strawn Oil Pool?
- A. In my opinion, from the data shown on this exhibit and other data and information I have studied, one well in the Lusk-Strawn Oil Pool will effectively and efficiently drain an area in excess of 160 acres.
- Q. Have you calculated recoverable oil reserves in the Lusk-Strawn Oil Pool?
- A. Yes, and I have shown these reserves on El Paso's Exhibit No. 8.
- Q. Please explain this exhibit to the Examiner.
- A. Exhibit 8 shows the volumetric or pore volume reserve calculation using data derived from averaging reservoir data of the three completed Strawn wells.
 Utilizing an average porosity of 7.1%, water saturation of 30.9%, net pay of 38

feet, an original reservoir volume factor of 2.605 and an estimated recovery factor of 15%, original recoverable oil reserve of 833 barrels per acre is calculated. The estimated barrels of oil recovery for 40, 80 and 160 acre spacing patterns are 33, 320, 66, 640 and 133, 280, respectively. The corresponding recoverable gas reserves for these spacing patterns computed on the basis of 14,920 Mcf/acre are 597,000 Mcf, 1, 194,000 Mcf and 2, 387,000 Mcf, respectively.

- Q. Have you compared the calculated performance of wells if they were drilled on
 40, 80 and 160 acre spacing with the actual performance of Well No. 1 in the
 Lusk-Strawn Oil Pool?
- A. Yes, and I have shown this comparison on El Paso's Exhibit No. 9.
- Q. Please explain this exhibit to the Examiner.
- A. Exhibit 9 shows the pressure history of the Lusk Deep Well No. 1 plotted against cumulative oil production. Superimposed upon this graph are the calculated pressure-production trends assuming production is derived solely from 40, 80 and 160 acre spacing units. The calculated performance curves are shown for the pressure range above the saturation or bubble point pressure where the reservoir energy is supplied principally by the expansion of reservoir oil. In this instance, however, the expansion of the rock and connate water were considered in the material balance calculation in calculating the individual pressure trends.

Reservoir characteristics such as net feet of pay, porosity and connate water saturation pertaining to Well No. 1 were employed in computing the calculated pressure trends. These factors combine to present what is considered to be a maximum relation between pressure and cumulative oil production for the various spacing patterns. It is noted from studying this graph that the actual pressure performance observed in Well No. 1 is almost flat compared with the predicted performance curves for 40, 80 and 160 acre drainage areas.

The maintenance of the actual pressure is, in my opinion, caused by the influx of fluid into the vicinity of Well No. 1. In the absence of evidence supporting a water drive it may be concluded that the influxing fluid is oil. It is, therefore, quite apparent from this exhibit, which presents an independent approach from that previously discussed in Exhibit 7, that the drainage area of Well No. 1 is considerably in excess of 160 acres.

- Q. Have you made a study of the profit or loss to be derived from drilling wells on 40, 80 and 160 acre spacing in the Lusk-Strawn Oil Pool?
- A. Yes, and I have compared the economics for each of these spacing patterns on El Paso's Exhibit No. 10.
- Q. Please explain this exhibit to the Examiner.
- A. Exhibit 10 has been prepared to show the economics assuming the Lusk-Strawn Pool is completely developed on a spacing pattern of 40, 80 and 160 acres per well. This exhibit shows that a net loss of \$187,000 per well would result if the pool was developed entirely on 40 acre spacing. On 80 acre spacing a net loss of \$75,000 per well would result. For 160 acre spacing a net profit of \$147,000 per well would be realized. The 160 acre spacing pattern is the smallest regular spacing pattern which results in a profitable well. The net profit to investment ratio for this spacing is 0.50 to 1.

The foregoing economics are based on an estimated well cost of \$298,000 for a single completion well in the Strawn formation. Although the three wells completed to date have been duals, in the Strawn and Bone Springs or Morrow, complete development of the pool, however, would require the drilling and completion of a number of singly completed wells. I have, therefore, used the single completion well cost in presenting my economics for the various spacing patterns. The net profit for each of the well spacing patterns are computed before income tax or deduction of overriding royalties or base royalties in excess of the usual 1/8.

Q. Mr. Lemon, from all of your studies, these exhibits and the data and information you have obtained pertaining to the Lusk-Strawn Oil Pool, are you of the opinion that in this pool one well will effectively and efficiently drain an area in excess of 160 acres?

A. Iam.

Q. Then, is it your recommendation that this Commission promulgate rules which will provide for 160 acre spacing for oil wells in this pool?

A. That is my recommendation.

Q. If the Commission sees fit to grant applicant's application in this case, is it your opinion that that would prevent waste and protect correlative rights?

A. That is my opinion.

Q. Were exhibits 1 through 10 prepared by you or under your supervision?

A. They were.

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PREPARED TESTIMONY

DAVID H. RAINEY FOR EL PASO NATURAL GAS COMPANY

IN CASE NO. 2469

- Question: Will you please state the purpose of the rules which you intend to propose?
- Answer: I believe that the evidence has clearly shown that 160 acre spacing is not only justified but necessary for the development of the Lusk Strawn Pool. We, therefore, intend to propose field rules which will provide for 160 acre spacing. Because of the high solution gasoil ratio and the high producing gas-oil ratio in this under-saturated reservoir, which, according to the evidence, is still producing at pressures substantially in excess of the bubble point, we believe that the evidence shows that a gas-oil ratio limit of 4,000 cubic feet of gas per barrel of oil is reasonable and equitable.
- Question: Do you have proposed special rules and regulations for the Lusk Strawn Pool?
- Answer: Yes. I have seven Special Rules which I would recommend that the Commission adopt for this Pool. They are contained as follows in El Paso's Exhibit No. 11.

-1-

- Rule 1. Each well completed or recompleted in the Lusk-Strawn Pool or in the Strawn Formation within one mile of said Pool, and not nearer to nor within the limits of another designated Strawn Pool, shall be spaced, drilled, operated, and prorated in accordance with the Special Rules and Regulations hereafter set forth.
- Rule 2. Each well completed or recompleted in the Lusk-Strawn Pool or in the Strawn Formation within one mile of said Pool, shall be located on a designated drilling tract consisting of 160 contiguous acres, more or less, substantially in the form of a square, which is a quarter section being a legal subdivision of the United States Public Lands Survey.
- Rule 3. Each well completed or recompleted in the Lusk Strawn Pool or in the Strawn Formation within one mile of said pool shall not be drilled closer than 660 feet to any quarter section line of the tract or closer than 330 feet to any quarter quarter section line, or subdivision inner-boundary, nor closer than 1,320 feet to a well drilled to or capable of producing from the same pool.
- Rule 4a. For good cause shown, the Secretary-Director of the Commission may grant an exception to the requirement of Special Rule 2. without notice and hearing where an application has been filed in due form and where the unorthodox size or shape of the tract is due to a variation in the legal subdivision of the United States Pu = 2 Lands Survey <u>or</u> where the following facts exist and the following provisions are complied with:

Case 2469 EPNG Exhibit No. 11.

-2-

- The non-standard unit consists of less than a standard unit and lies wholly within a single governmental quarter section.
- (2) The entire non-standard unit may reasonably be presumed to be productive of oil from said pool.
- (3) The applicant presents written consent in the form of waivers from all offset operators.
- (4) In lieu of Paragraph 3 of this Rule, the applicant may furnish proof of the fact that said offset operators were notified by registered mail of his intent to form such nonstandard unit. The Secretary-Director may approve the application if, after a period of 30 days, no operator has entered an objection to the formation of the non-standard unit.
- Rule 4b. The allowable assigned to such non-standard unit shall bear the same ratio to a standard allowable in the Lusk Strawn Pool as the acreage in such non-standard unit bears to 160 acres.
- Rule 5. A 160 acre proration unit in the Lusk Strawn Oil Pool shall be assigned a 160 acre proportional factor of 8,67 for allowable purposes. For purposes of computing allowables a unit of not less than 158 acres nor more than 162 acres shall be considered to contain the number of acres in a standard unit. In the event there is more than one well on a 160 acre proration unit, the operator may produce the allowable assigned to the unit from the wells on that unit in any proportion.

-3-

- Rule 6. The gas-oil ratio limitation for all wells in the Lusk Strawn Pool shall be four thousand (4,000) cubic feet of gas per barrel for oil produced. Any oil well in the Lusk Strawn Oil Pool producing with a gas-oil ratio in excess of four thousand (4,000) cubic feet per barrel of oil shall be allowed to produce daily only that volume of gas obtained by multiplying the top unit allowable for the pool as determined by the applicable rules of the Commission and, as proposed herein, times the limiting gas-oil ratio (four thousand (4,000) cubic feet). The gas volume thus obtained shall be known as the daily gas limit of such well. The daily oil allowable therefore shall then be determined and assigned by dividing the daily gas limit by its producing gas oil ratio.
- Rule 7. The vertical limits of the Lusk-Strawn Oil Pool shall be the Strawn Formation.

- Question: How did you arrive at the figure of 8.67 as the proportional factor for a 160 acre oil well in Rule 5?
- Answer: The proportional factor of 8.67 is arrived at by using the proportional factor for a 40 acre unit with a depth range of 11,000 feet to 12,000 feet and adding three normal unit allowables for the three additional 40 acre units. That is, we have followed the procedure which the Commission used in going from a 40 acre unit to an 80 acre unit.

PREPARED TESTIMONY OF DAVID T. BURLESON

- Question: Mr. Burleson, referring to El Paso's Exhibit No. 12, what does the red line show?
- Answer: The red line shows the pool boundaries of the Lusk-Strawn Oil Pool.

Question: What does the yellow line show?

- Answer: The yellow line shows the boundaries of the Lusk Deep Unit.
- Question: Does this exhibit show the offset operators surrounding the Lusk-Strawn Oil Pool?
- Answer: Yes.
- Question: To your knowledge, has anyone opposed the granting of El Paso's

application in this case.

Answer: No.

- Question: Who are the committed working interest owners in the unit.
- Answer: El Paso Natural Gas Company, Phillips Petroleum Company, Kerr-McGee Oil Industries, Inc. and Gulf Oil Corporation. Question: Have they concurred in this application?
- Answer: Yes.
- <u>Question</u>: Please point out the presently approved participating area for the Strawn formation.
- <u>Answer:</u> The presently approved Strawn participating area consists of the NE/4 of Section 19, W/2 NW/4 of Section 20, SE/4 of Section 18, SW/4 SW/4 of Section 17, and the E/2 SW/4 of Section 18, all in Township 19 South, Range 32 East, N.M.P.M., Lea County, New Mexico, containing 520.00 acres, more or less.

RESERVOIR AND COMPLETION DATA

LUSK STRAWN POOL

1. Location of Pool

Approximately 14 miles southwest of Maljamar, New Mexico, Sections 18, 19, and 20, T-19S, R-32E, Lea County, New Mexico.

2. Completion Data-Lusk Deep Unit Wells:

a.	Formation		Pennsylvanian Strawn	Limestone			
b.	Well Number	1	2	3			
c.	Total Depth	11,232'	13,974'	12,623'			
d.	Top of Strawn Limestone	11,017' (-7416')	11,070' (-7465')	11, 156' (-7563')			
e,	Top of Strawn Pay	11, 149' (-7548')	11,216' (-7611')	11,291' (-7698')			
f.	Completion Date	10-7-60	4-1-61	11-1-61			
g.	Perforated Interval	11, 168' - 11, 193'	11,220' - 11,250'	11,310' - 11,340'			
h.	Treatment	Natural	600 gals. acid	Natural			
i.	Initial Potential Test						
	(1) Potential (BOPD)	732	641	285			
	(2) Choke size (in.)	16/64	16/64	10/64			
	(3) GOR (cu. ft. /bbl.)	2640	3329	2397			
	(4) Casing Pressure (psig)	Packer	Packer	Packer			
	(5) Tubing Pressure (psig)	2345	2400	2887			
3.	Reservoir Fluid Characte	eristics:					
a.	Saturation Pressure (bubb	ole point) (psig)	4150				
b.	Formation Volume Factor	r @ Original Pressure	2.605				
c.	Solution Gas-Oil Ratio (cu	1. ft./bbl.)	3084 V				
d.	Oil Viscosity @ Original 1	Pressure (cp)	0.146				
e.	Oil Gravity (°API @ 60°F)) 4	17.5				
4.	Reservoir Characteristic	<u>8:</u>					
a.	Porosity		7.1				
b.	Permeability (md.)		17.7				
c.	Water Saturation (%)	÷	30.9				
d.	Net Pay (ft.)		38 (average 3 wells)				
e.	Reservoir Temperature (oF)	161				
f.	Original Reservoir Press	ure (psig)	5810				
g.	Probable Reservoir Mech	anism	Solution gas drive				
37							
N	M.U.U.U. Case No. 240) y					

EPNG Exhibit No. 3 Date January 4, 1962

RESERVOIR AND COMPLETION DATA

LUSK STRAWN POOL

1. Location of Pool

EPNG Exhibit No. 3 Date January 4, 1962

Approximately 14 miles southwest of Maljamar, New Mexico, Sections 18, 19, and 20, T-19S, R-32E, Lea County, New Mexico.

2. Completion Data-Lusk Deep Unit Wells:

a.	Formation		Pennsylvanian Strawn	Limestone
b.	Well Number	1	2	3
c.	Total Depth	11,232'	13,974'	12,623'
d.	Top of Strawn Limestone	11,017' (-7416')	11,070' (-7465')	11,156' (-7563')
e.	Top of Strawn Pay	11, 149' (-7548')	11,216' (-7611')	11,291' (-7698')
f.	Completion Date	10-7-60	4-1-61	11-1-61
g.	Perforated Interval	11, 168' - 11, 193'	11,220' - 11,250'	11,310' - 11,340'
h.	Treatment	Natural	600 gals. acid	Natural
i.	Initial Potential Test			
	(1) Potential (BOPD)	732	641	285
	(2) Choke size (in.)	16/64	16/64	10/64
	(3) GOR (cu.ft./bbl.)	2640	3329	2397
	(4) Casing Pressure (psig)	Packer	Packer	Packer
	(5) Tubing Pressure (psig)	2345	2400	2887
a. b. c.	Saturation Pressure (bubb Formation Volume Factor Solution Gas-Oil Ratio (cu	ble point) (psig) c @ Original Pressure 1. ft./bbl.)	4150 2.605 3084	
α.	Oil Crowity (OA DI @ 600F)	Pressure (cp)	0.146	
е.	Oli Gravity (CAPI @ 60°F))	£7.0	
4.	Reservoir Characteristic	<u>s:</u>		
a.	Porosity		7.1	
b.	Permeability (md.)		17.7	
c.	Water Saturation (%)	:	30.9	
d.	Net Pay (ft.)		38 (average 3 wells)	
e.	Reservoir Temperature (^o F)	161	
f.	Original Reservoir Press	ure (psig)	5810	
g.	Probable Reservoir Mech	anism	Solution gas drive	
			а. С. С. С	
N.	M.O.C.C. Case No. 246	39		

EL PASO NATURAL GAS COMPANY

LUSK DEEP UNIT WELL NO. I

ELEV. 3600 D.F.

NE/4 NE/4 SEC. 19, T-19-S, R-32-E ELECTRIC LOG OF STRAWN PAY SECTION

COMPOSITE ELECTRIC LOG

MICRO LOG



CORE ANALYSIS

LUSK DEEP UNIT WELL #1

STRAWN PAY

Porous Interval (Micro Log) 11, 149'-11, 196'. Net Pay (Micro Log) 41'.

Cored Interval 11, 148'-11, 198'

Perforated Interval 11, 168'-11, 193'

Depth Correlation 11, 148' Core-Gamma = 11, 161' Micro Log

		Permeability	Porosity	Water Saturation
epth Interval	Footage	(md.)	(%)	(% Pore Space)
1,148.0-49.6	1.6	16.5	11.5	28.3
49.6-51.1	1.5	22.0	11.8	22.9
51,1-52,1	1.0	21.0	10.9	24.4
52.1-53.5	1.4	9.8	9.9	24.8
53.5-55.0	1.5	15.0	11.0	25.0
55.0-56.4	1.4	6.2	9.6	26.2
56.4-58.0	1.6	20.0	8.9	21.6
58.0-59.5	1.5	49.0	8.2	30.3
59,5-61.0	1.5	11.1	9.6	32.2
61.0-62.3	1.3	11.0	9.5	25.0
62.3-63.9	1.6	37.9	7.6	21.7
63.9-65.0	1.1	14.0	9.6	26.6
65,0-66,5	1.5	19.5	9.2	27.6
66.5-68.0	1.5	13.0	9.8	22.3
68.0-69.4	1.4	1.9	7.4	20.3
69.4-71.0	1.6	6.1	5.9	27.5
71.0-72.1	1,1	23,0	7.7	28.7
72.1-73.0	0.9	36.0	10.6	27.4
73.0-74.5	1.5	39.0	6.3	37.6
74.5-76.2	1.7	5.1	6.3	30.6
77.4-79.0	1.6	1.8	2.7	33.5
79.0-80.0	1.8	18.5	6.1	39.5
80.8-82.5		152.0	4.8	45.1
Net Pay (Cored	Int.) 33 3			
Weighted Avera	ge	24.6	8.3	28.5

Note: (1) Only Porosity values over 4% and Permeability values over 0.1 millidarcy are included.

(2) Total Strawn Porosity Interval was not cored in this well.

N.M.O.C.C. Case No. 2469 EPNG Exhibit No. 6 Date January 4, 1962





RECOVERABLE OIL RESERVES

LUSK STRAWN POOL

STRAWN LIMESTONE PRODUCING INTERVAL

Basic Data

Porosity 7.1% (avg. from core analyses #1, #2, and #3 wells) Permeability 17.7 md. (avg. from core analyses #1, #2, and #3 wells) Net Pay 38 ft. (avg. from micro log and core analyses #1, #2, and #3 wells) Water Saturation 30.9% (avg. from core analyses #1, #2, and #3 wells) Recovery Factor 15% (estimated)

Formation Volume Factor 2.605 @ original pressure.

Volumetric Calculation

Original Recoverable Oil Reserve = $\frac{7758 \ \text{\emptyset} (1-\text{Sw}) \ \text{Ah}}{\text{Bo}}$ X Oil Recovery Factor Original Recoverable Oil Reserve = (7758) (0, 071) (0, 691) (38)

Original Recoverable Oil Reserve = $(7758)(0.071)(0.691)(38) \times 0.15 = 8$

Original Recoverable Oil Reserve = 833 Bbls./Acre

In which: 7758 bbls. = equivalent volume in 1 acre foot
Ø (phi) = porosity as a decimal fraction of bulk volume
Sw = interstitial water as a decimal fraction of the pore volume
Ah = volume of 1 acre of reservoir, in acre feet
Bo = formation volume factor

N. M. O. C. C. Case No. 2469 EPNG Exhibit No. 8 Date January 4, 1962



N. M. O. C. C. Case No. 2469 EPNG Exhibit No. 10 Date January 4, 1962

- Rule 1. Each well completed or recompleted in the Lusk-Strawn Pool or in the Strawn Formation within one mile of said Pool, and not nearer to nor within the limits of another designated Strawn Pool, shall be spaced, drilled, operated, and prorated in accordance with the Special Rules and Regulations hereafter set forth.
- Rule 2. Each well completed or recompleted in the Lusk-Strawn Pool or in the Strawn Formation within one mile of said Pool, shall be located on a designated drilling tract consisting of 160 contiguous acres, more or less, substantially in the form of a square, which is a quarter section being a legal subdivision of the United States Public Lands Survey.
- Rule 3. Each well completed or recompleted in the Lusk Strawn Pool or in the Strawn Formation within one mile of said pool shall not be drilled closer than 660 feet to any quarter section line of the tract or closer than 330 feet to any quarter quarter section line, or subdivision inner-boundary, nor closer than 1,320 feet to a well drilled to or capable of producing from the same pool.
- Rule 4a. For good cause shown, the Secretary-Director of the Commission may grant an exception to the requirement of Special Rule 2. without notice and hearing where an application has been filed in due form and where the unorthodox size or shape of the tract is due to a variation in the legal subdivision of the United States Public Lands Survey <u>or</u> where the following facts exist and the following provisions are complied with:

Case 2469 EPNG Exhibit No. 11.

-2-

- The non-standard unit consists of less than a standard unit and lies wholly within a single governmental quarter section.
- (2) The entire non-standard unit may reasonably be presumed to be productive of oil from said pool.
- (3) The applicant presents written consent in the form of waivers from all offset operators.
- (4) In lieu of Paragraph 3 of this Rule, the applicant may furnish proof of the fact that said offset operators were notified by registered mail of his intent to form such nonstandard unit. The Secretary-Director may approve the application if, after a period of 30 days, no operator has entered an objection to the formation of the non-standard unit.
- Rule 4b. The allowable assigned to such non-standard unit shall bear the same ratio to a standard allowable in the Lusk Strawn Pool as the acreage in such non-standard unit bears to 160 acres.
- Rule 5. A 160 acre proration unit in the Lusk Strawn Oil Pool shall be assigned a 160 acre proportional factor of 8.67 for allowable purposes. For purposes of computing allowables a unit of not less than 158 acres nor more than 162 acres shall be considered to contain the number of acres in a standard unit. In the event there is more than one well on a 160 acre proration unit, the operator may produce the allowable assigned to the unit from the wells on that unit in any proportion.

-3-

- Rule 6. The gas-oil ratio limitation for all wells in the Lusk Strawn Pool shall be four thousand (4,000) cubic feet of gas per barrel for oil produced. Any oil well in the Lusk Strawn Oil Pool producing with a gas-oil ratio in excess of four thousand (4,000) cubic feet per barrel of oil shall be allowed to produce daily only that volume of gas obtained by multiplying the top unit allowable for the pool as determined by the applicable rules of the Commission and, as proposed herein, times the limiting gas-oil ratio (four thousand (4,000) cubic feet). The gas volume thus obtained shall be known as the daily gas limit of such well. The daily oil allowable therefore shall then be determined and assigned by dividing the daily gas limit by its producing gas oil ratio.
- Rule 7. The vertical limits of the Lusk-Strawn Oil Pool shall be the Strawn Formation.

Distribution of Final Reports

20 Copies	Mr. L. C. Zinc El Paso Natural Gas Company 19th Floor, Wilco Building Midland, Texas
2 Copies	Mr. John J. Gill Pan American Petroleum Corporation Box 268 Lubbock, Texas
2 Copies	Phillips Petroleum Company Box 791 Midland, Texas
2 Copies	Delhi-Taylor Oil Corporation Box 67 Farmington, New Mexico
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2 Copies	Southern California Petroleum Corporation Petroleum Life Building Midland, Texas
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2 Copies	Delhi-Taylor Oil Corporation 1700 Corrigan Tower Building Dallas, Texas



THE COMPANY WILL APPRECIATE SUGGESTIONS FROM ITS PATRONS CONCERNING ITS SERVICE



GOVERNOR EDWIN L. MECHEM CHAIRMAN

State of New Mexico O il Conservation Commission

LAND COMMISSIONER E. S. JOHNNY WALKER MEMBER



STATE GEOLOGIST A. L. PORTER, JR. SECRETARY - DIRECTOR

P. O. BOX 871 SANTA FE

January 30, 1962

Re: CASE NO. 2469 ORDER NO. R-2175 APPLICANT:

Mr. Garrett Whitworth Mr. Ben Howell El Paso Natural Gas Company Box 1492 El Paso, Texas

El Paso Natural Gas Company

Dear Sir:

Enclosed herewith are two copies of the above-referenced Commission order recently entered in the subject case.

Very truly yours,

A. L. PORTER, Jr.' Secretary-Director

ir/

Carbon copy of order also sent to:

Hobbs OCC X Artesia OCC Aztec OCC OTHER Mr. Bill Kastler (Gulf Oil Corporation) Mr. Oliver Seth GOVERNOR EDWIN L. MECHEM CHAIRMAN

State of New Mexico O il Conservation Commission

LAND COMMISSIONER E. S. JOHNNY WALKER MEMBER



P. O. BOX 871 Santa Fe

April 4, 1962

Mr. Ben Howell El Paso Natural Gas Company P. O. Box 1492 El Paso, Texas

	El Paso	Natural	Gas Compa	iny
	APPLICA	NT:		
	ORDER N	0. <u>R-2</u>	175-B	
Re:	CASE NO	2	469	

STATE GEOLOGIST

A. L. PORTER, JR.

SECRETARY - DIRECTOR

Dear Sir:

Enclosed herewith are two copies of the above-referenced Commission order recently entered in the subject case.

Very truly yours,

A. L. PORTER, Jr.

Secretary-Director

ir/

Carbon copy of order also sent to:

Hobbs OCC X Artesia OCC Aztec OCC OTHER Mr. Garrett Whitworth Mr. Oliver Seth Mr. O. P. Nicola



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	Jon Lags/Strawn		11,232'			
			PRODUCIN	G WELL	TRY HOLE	
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int. Casing	5, Ft. <u>9-5/8</u> Inch.	\$/Ft.	29,800			
Prod. Casing	_1, Ft. / Inch.	\$/Ft.	54,000			
	Ft Inch	\$/Ft.				
Tubing	11, 25 Ft. $2-3/8$ Inch.	\$/Ft.	7,800			
	8,710 Ft. 2-1/16 Inch.	\$⁄Ft.	9,600	<u>\$ 107,100</u>		
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					-	
OTHER EQUIPMEN	<u>6</u>		4 100	4 100		
Liner Hangers an	d Production Packers		4,100	4,100		
CONTRACT COSTS						
Footage	Ft.	\$/Ft.	158,500			
Daywork	Day	\$/Day				
Daywork	Day	\$/Day		158,500		
Daywork	Day					
CEMENTING: (Cema	nt and Fump Trucks)					
Surface			1,200			
Intermediate			3,300			
Liner						
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Sq. Job.			2,400	12,000		
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Acidizing			2,800			
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Sand				n 000		
Tank Rental				2,000		
SPECIAL SERVICES	: Surveys and Tests)					
Perforating			3,000			
Mud Logging			6,500			
Electric and Radi	loactiveogging		11,000			
Cores			1,300	21,800		
MATERIALS:			42,000			
Drilling Mud and	C.emic⊂ 3					
Water		,	2,000			
Bits			35,000			
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Miscellaneous (w	elding, making, rental of tongs, etc.)		17,900	117,000		
ACCESS AND LOCA	<u>N:</u>		8,500	8,500		
	Total Dire	ct Cost	439,000	439,000	·····	
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El Paso Natu	ral Di	٦.	ъœ
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Bits 53,500 Fuel 2,600 Cement Equator (modes, collars, etc.) 2,600 Bits Programs Repained 60,000 Cetters AND LOCATION: 6,300 Cetters AND LOCATION: 6,300 Cetters Programs Repained 65,400 Bits Programs Repained 65,400 Bits Programs Repained 65,400 Store Programs Repained 53,000 Cetters Programs Repained 65,400 Bits Programs Repained 531,000 Store Programs Repained 531,000 Bits Programs Repained 531,000 Store Programs Repained 531,000 Bits Programs Repained 531,000 Bits Programs Repained 531,000 Bits Programs Repained 531,000 Bits Programs Repained 531,000	Drilling Gas or A Water					4,100		
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Intocellaneous (welaing, hilding, rental of tongs, etc.) Intocellaneous (welaing, hilding,	Cement Equipue Barrise Passione	(oes,	pollars, etc.)			<u> </u>	-	
CCESS AND LOCATION: 5,300 6,300 Total Direct Cost 665,600 665,600 Legal, Stor, Supervision, etc. XXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXX	.mocellaneous (w	velaing, h	uling, rental of tongs, etc.)			60,000	207,700	
Total Direct Cost 665,600 Legal, Stor, Supervision, etc. XXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXX	CESS AND LOCA	<u>T10N:</u>				ó,300	6,300	
Legal, Stort Supervision, etc. XXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXX	.	~		Potal Direct (Cost	665,600	665,600	
ESTIMATED TOTAL COST \$ /51,000 \$ /51,000 \$ Sting INTEREST: ESTIMATED COST ONLY – Each participation owner to proportionate share of actual well cost subject to operating agreement.	Legal, Stor.	., Suj.	ervision, etc. XXXX	XXXXXXXXXXXX	XXXXXXX		731 000	
	- ,. ,		- ESTIM	ATED TOTA	L COST	\$ 731,000	\$ 101,000	<u> \$</u>
	Cthers	I Gas Cor	: pany			proportionate share	on <u>t</u> - Each par e of actual well cost	subject to pay
		. <u></u>				F	ARTNER'S APPR	CVAL:

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-cue Name AS		Well 1	ic. 3		<u>.</u>
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inila (194		Est.	Total Depth:		
ι . Γ ά	A CONTROL STATE	. <u></u>	12,021		
		-	PRODUCIN	G WELL	Y HOLE
TUBULAR GOODS			Sub.	Total	
Surface Casing		2/Ft.	s 346		\$
Int. Casing	13-3/8 Inch.	S/Ft.	5,606		
And Creins	9-5/8 Inch	S/Et.	26.635		
	-5-1/2 Inch	S/E+	32,331		
	it inch	S/Ft			and the second
	-2-1/16	5/Ft	8 608		
Tubing	$r_{\rm t} = \frac{21/10}{0.1/16}$ linch,	\$7Ft	0,000	. 05 010	
-4, č	F:Z-1/10 Inch	\$/Ft.		\$ 85,819	
			± / 0 رئي		
SELLHEAD EQUIPMENT:					
	·····	i F	7,714	7,714	
THER EQUIPMENT:					
Liner Hangers and Producted	on Packers		2,726	2,726	
indicate and i to ducite					-
CONTRACT COSTS					
Footage	F't.	\$/Ft-	116,438		
Davwork	Dav	\$/Dav			
Daywork	Dav	\$/Dov			
Daywork	547	\$/Day		116,438	
	Ddy	(Cuy	· · · · · · · · · · · · · · · · · · ·		
	T ()				
CEMENTING: (CEMENT and PUM	<u>p Irucks)</u>		2 300		
Surface		-	5,000		
Intermediate		r dan	0,900		
Production		+	2,2/3		
Liner		1			
Liner		L. L			
<u></u>		ŀ			
Se, Job.		-	2,900	<u> 13,373 </u>	
		-			
FUL ATION TREAT STR		1			
		:			
Stacturing Emiltra					
		-			
etuid Go		-			
C	water	ŀ			
Sand L: -					
Tank Rental					
SPECIAL SERVICES: (Survey	and Tests)		2 700		
Perforating		ŀ	2,700		
Mud Logging		Ē	7.000		
Electric and Radioactive 😂	gging		7,000		
Drill Stem Tests			4,900		
Cores			1,436	16,036	
ATERIALS					
Dutting Mud and Constant		ĺ	33,671		
Drilling Muu and Chemicals		F			
Dritting Gas or Air		ŀ	7 206		
Water		F	0 4°70		
Bits		F	7,470 2 070		
Fuel		-	3,972		
Cement	ollars, etc.)	1	3,200		
Bridge Light and Retainer		}-	0/ 001	00 010	
Mit relianceous (welding, he.	ing, rental of tongs, etc.)	1 	20,291	<u>کا</u> م, کاک	
Surface Installation	(Tanks, etc.)		15,843		
CESS AND LOCATION:			10 007		
			12,907	28,/50	
	Total Direct	Cost	354,674	354,674	
Legal Stores Sp	rvision.etc. maxxxxxxx	WAREK	20 , 222	20,222	
Topari Marco, Da	· · · · · · · · · · · · · · · · · · ·				
	complete ESTIMATED TOTA	AL COST	s 374,895	\$ 374.896	s
				NILV Each	icingting owner to -
NTEREST			ESTIMATED COST (UNLI - Each part	icipating owner to pay
5 Natural Gub Ce	:cny		proportionate share	or actual well cost	subject to operating
			corcement.		
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		4 6	PA	ARTNER'S APPRO	OVAL:
		Date			· · · · · · · · · · · · · · · · · · ·
		Ву			

Approve- .

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El Paso Natural Cas Company WELL COST ESTIMAT

Lease Name	Lusl: Deep Unit Area	Single Completion	Development	Lusit Deep Unit
Location	T-11-S, R-32-E	County Lea		State New Mexico
Formation	Straw - Single	Est. Total Depth: 11,500'		
· · · · · · · · · · · · · · · · · · ·		PRODUCIN	IG WELL	JRY HOLE
TUBULAR GOODS	600 12 27 0	Sub.	Total	
Surface Casing	$-\frac{6.00}{4.500}$ Ft. $\frac{13-3/8}{0.5/9}$ Inch. $3/1$	Ft. \$ 3,488	4	\$
Int. Casing	$\frac{4,7}{11,500}$ Ft. $\frac{9-5/8}{5-1/2}$ Inch \$/I	Ft. 27,000		
Prod. Casing	FtInch\$/F	Ft. 27,420		
	Ft. Inch. S/I	Ft.		
Tubing	<u>1,150 Ft. 2-3/8 Inch.</u> \$/1	Ft. 10,350	4	
Csg. Inspect	tion & Trucking Inch s/1	Ft. 2,000	<u>\$</u> 74,270	
WELLHEAD EQUIP	MENT:	5,800	5,800	
OTHER FOUIPMEN	Τ.		•	
Liner Hongers of	 nd Production Packers	1,200	1,200	
CONTRACT COSTS	<u>.</u>			
Footage	Ft\$/Ft.	80,535		
Daywork	Day \$/Day		-	
Daywork	Dαy\$/Dαγ		86,535	
Daywork	Day \$7 Day			
CEMENTING: (Ceme	ent and Pump Trucks)			
Surface		1,200	-	
Intermediate		3,000		
Production			-	
Liner				
	_			
Sq. Job.			10,100	
FORMATION TREA Acidizing 50	IMENI: 0 gallens MCA plus trucking	650		
Fluid	Gai. Oil			
	Gal, Water]	
Sand	Lbs.		(
Tank Rental			650	
Perforating	5: (Surveys and Lests)	1,500		
Mud Logging				
Ele and Rad	hoactive Logging	9,500	-	
Drill Stem Tests		1,500	14 100	
Cores	- Tank Bantal	1 000	14,100	
Deperator C		1,000		
MATERIALS: Drilling Mid and	Chemicals	28,000	ļ	
Drilling Gas or A	Air			
Water		6,000		
Bits		5,460	1	
Fuel		3,250	1	
Cement Equipment	nt (ences, collars, etc.)	2,800	-	·
Bridge Plugs and	d H. tainers	12.500	72.010	
Miscellaneous (v Tank Batter	werding, naturna, rental or longs, etc.) V	14,000		
ACCESS AND LOCA	ATION:	-		
<u></u>		8,500	8,500	
	Total Direct Cost F	273,165	273,165	
	Plus <u>3</u> % Contingency	15,038	13,038	
	ESTIMATED TOTAL COST	s 286,8 23	\$ 286,823	\$
WORKING INTER.	<u>2</u>	ESTIMATED COST	ONLY - Each part	icipating owner to pay
El Paso Natura	l Gas Company	proportionate share	of actual well cost	subject to operating
Others		_ cgreement.		
rn				
Date		P/ Date	ARTNER'S APPR	UVAL:
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improved By		Ву		

RECOVERABLE OIL RESERVES

LUSK STRAWN POOL

STRAWN LIMESTONE PRODUCING INTERVAL

Basic Data

Porosity 7.1% (avg. from core analyses #1, #2, and #3 wells) Permeability 17.7 md. (avg. from core analyses #1, #2, and #3 wells) Net Pay 38 ft. (avg. from micro log and core analyses #1, #2, and #3 wells) Water Saturation 30.9% (avg. from core analyses #1, #2, and #3 wells) Recovery Factor 15.6% (calculated) Formation Volume Factor 2.605 @ original pressure.

Volumetric Calculation

Original Recoverable Oil Reserve = (7758) (0.071) (0.691) (38)(2.605) X 0.156

Original Recoverable Oil Reserve = 866 Bbls./Acre

In which: 7758 bbls. = equivalent volume in 1 acre foot Ø (phi) = porosity as a decimal fraction of bulk volume Sw = interstitial water as a decimal fraction of the pore volume Ah = volume of 1 acre of reservoir, in acre feet Bo = formation volume factor

N. M. O. C. C. Case No. 2469 Rehearing EPNG Exhibit No. 8 Revised Date March 14, 1962

ECONOMICS FOR VARIOUS WELL SPACING PATTERNS LUSK STRAWN POOL

1.	Basic Data	
	Oil Value (After transportation expense), \$/Bbl.	2.76
	Estimated Value of Produced Gas, \$/M ² cf	90
	Net Lease Interest, %	87.5
	State Production Taxes, %	6.15
	Lifting Costs, \$/Bbl.	0.25
	Well Investment, \$	287,000
	W.I. Net Income = [Oil Recovery X Oil Price + Gas R	ecovery X Gas Price]
	X Net Interest X (1 - Taxes) - Lif	ting Cost
2.	40 Acre Spacing Units	
	Estimated Reserves:	
	Oil - 34,640 Bbls.	
	$Gas - 600 M^2 cf$	
	W.I. Net Income = [34, 640 X 2.76 + 600 X 90] X 0.87	5 (1-0.0615) -
	34,640 X 0.25 = \$114,166	
	Loss per Well = \$287,000 - \$114,166 = \$172,834 (\$173	3,000)
3.	80 Acre Spacing Units	
	Estimated Reserves:	
	Oil - 69,280 Bbls.	
	Gas - 1, 200 M^2 cf	
	W.I. Net Income = [69, 280 X 2.76 + 1200 X 90] X 0.8	75 (1 - 0.0615) -
	69, 280 X 0.25 = \$228, 334	
	Loss per Well = \$287,000 - \$228,334 = \$58,666 (\$59,	000)

4. 160 Acre Spacing Units

Estimated Reserves: Oil - 138,560 Bbls. Gas - 2,400 M^2cf W.I. Net Income = [138,560 X 2.76 + 2400 X 90] X 0.875 (1 - 0.0615) -138,560 X 0.25 = \$456,668 Net Profit = \$456,668 - \$287,000 = \$169,668 (\$170,000) Profit to Investment Ratio = 0.59 to 1

N. M. O. C. C. Case No. 2469 Rehearing EPNG Exhibit No. 10 Revised Date March 14, 1962 CORE LABORATORIES, INC. Petroleum Reservoir Engineering DALLAS. TEXAS October 12, 1960

REPLY TO P. O. BOX 4337 MIDLAND, TEXAS - ----

El Paso Natural Gas Company 19th Floor, Wilco Building Midland, Texas

Attention: Mr. L. C. Zinc

Subject: Core Analysis Lusk Deep Unit No. 1 Well Wildcat Lea County, New Mexico Location: Sec. 19-T19S-R32E

Gentlemen:

Strawn formation analyzed from 11, 148 to 11, 198 feet is interpreted to be oil productive where permeable. The measured productive capacity of 838 millidarcy-feet is believed adequate for natural flow rates. Average core analysis values and calculated original stock-tank oil in place are given on page one of the report.

Formation analyzed from 11, 198 to 11, 221 feet was found to be impermeable and nonproductive

We sincerely appreciate this opportunity to be of service to you.

Very truly yours,

Core Laboratories, Inc.

R& Bynum J

R. S. Bynum, Jr., District Manager

RSB:PE:sp

CORE LABORATORIES, INC.

Petroleum Reservoir Engineering DALLAS, TEXAS

> Page 1 of 1 File WP-3-1546 Well Lusk Deep Unit No. 1

CORE SUMMARY AND CALCULATED RECOVERABLE OIL

FORMATION NAME AND DEPTH INTERVAL: Strawn 11, 148. 0-11, 198. 0

FEET OF CORE RECOVERED FROM Above Interval		50.0	AVERAGE TOTAL WATER SATURATION: Per cent of pore space		31.5
FEET OF CORE Included in Averages		44.1	AVERAGE CONNATE WATER SATURATION: Per cent of pore space	(e)	27
AVERAGE PERMEABILITY: Millidargys	Max. 90 ⁰	19 7.2	DIL GRAVITY: [•] Api	(e)	48
PRODUCTIVE CAPACITY: MILLIDARCY-FEET	Max. 90 ⁰	838 318	ORIGINAL SOLUTION GAB-OIL RATIO: Cubic feet per barrel	(e)	1000
AVERAGE POROSITY: PER CENT		7.1	DRIGINAL FORMATION VOLUME FACTOR: BARRELE(e) saturated oil per barrel stock-tank oil		1.60
AVERAGE RESIDUAL DIL SATURATION: PER CENT OF PORE SPACE		7.6	CALCULATED ORIGINAL BTOCK-TANK DIL IN PLACE: Barrels per Acre-Fdot		251
		1	1		

Calculated maximum solution gas drive recovery is barrels per acre-foot, assuming production could be continued until reservoir pressure declined to zero psig. Calculated maximum water drive recovery is barrels per acre-foot, assuming full maintenance of original reservoir pressure, 100% areal and vertical coverage, and continuation of production to 100% water cut. (*Please refer to footnotes for further discussion of recovery estimates.*)

FORMATION NAME AND DEPTH INTERVAL:

FEET OF CORE RECOVERED FROM Above Interval	AVERAGE TOTAL WATER SATURATION: Per cent of pore space	
FEET DF CORE Included in Averages	AVERAGE CONNATE WATER SATURATION: PER CENT OF PORE SPACE	
AVERAGE PERMEABILITY: MILLIDARCYS	DIL GRAVITY: [•] API	
PRODUCTIVE CAPACITY: Millidarcy-feet	ORIGINAL SOLUTION GAS-DIL RATID: Cubic feet per barrel	
AVERAGE POROSITY: PER CENT	DRIGINAL FORMATION VOLUME FACTOR: BARRELS Saturated Oil per Barrel Stock-Tank Oil	
AVERAGE RESIDUAL DIL SATURATION: PER CENT OF PORE SPACE	CALCULATED ORIGINAL STOCK-TANK DIL IN PLACE: Barrels per acre-foot	

Calculated maximum solution gas drive recovery is barrels per acre-foot, assuming production could be continued until reservoir pressure declined to zero psig. Calculated maximum water drive recovery is barrels per acre-foot, assuming full maintenance of original reservoir pressure, 100% areal and vertical coverage, and continuation of production to 100% water cut. (*Please refer to footnotes for further discussion of recovery estimates.*)

(c) Calculated (e) Estimated (m) Measured (*) Refer to attached letter.

These recovery estimates represent theoretical maximum values for solution gas and water drive. They assume that production is started at original reservoir pressure; i.e., no account is taken of production to date or of prior drainage to other areas. The effects of factors tending to reduce actual ultimate recovery, such as economic limits on oil production rates, gas-oil ratios, or water-oil ratios, have not been taken into account. Neither have factors been considered which may result in actual recovery intermediate between solution gas and complete water drive recoveries, such as gas cap expansion, gravity drainage, or partial water drive. Detailed predictions of ultimate oil recovery to specific abandonment conditions may be made in an engineering study in which consideration is given to overall reservoir characteristics and economic factors.

These analyses, opinions or interpretations are based on observations and materials supplied by the client to whom, and for whose exclusive and confidential use, this report is made. The interpretations or opinions expressed represent the best judgment of Core Laboratories, Inc. (all errors and omissions excepted); but Core Laboratories, Inc., and its officers and employees assume no responsibility and make no warranty or representation as to the productivity, proper operation, or provide the productivity of the producti

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20 Copies	Mr. L. C. Zinc El Paso Natural Gas Company 19th Floor, Wilco Building Midland, Texas
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2 Copies	Three States Natural Gas Company 1700 Corrigan Tower Building Dallas, Texas

CORE LABORATORIES, INC. Petroleum Reservoir Engineering DALLAS. TEXAS September 29, 1961

RESERVOIR FLUID DIVISION

El Paso Natural Gas Company 19th Floor, Wilco Building Midland, Texas

Attention: Mr. Dale Lockett

Subject: Reservoir Fluid Study E. P. Lusk No. 2 Well Lea County, New Mexico Our File Number: RFL 1974

Gentlemen:

Subsurface fluid samples were collected from the E. P. Lusk No. 2 well by a representative of Core Laboratories, Inc. The results of fluid studies performed using these samples are transmitted to you in the following report.

The saturation pressure of the fluid was determined to be-4450 psig at the reservoir temperature of 161° F. This value is significantly lower than the reservoir pressure measured prior to sampling and is indication that the reservoir presently exists in an undersaturated condition. At the time of sampling, the oil level in the tubing was at the surface. This condition is often found in undersaturated reservoirs and tends to confirm the conclusion.

Under differential pressure depletion conditions at the reservoir temperature of 161° F., the fluid evolved 3084 cubic feet of gas at 14.696 psia and 60° F. per barrel of residual oil at 60° F. The associated formation volume factor was measured to be 2.722 barrels of saturated fluid per barrel of residual oil. The specific gravity and compressibility of the gas evolved during this depletion are presented on page five of the report with the density of the liquid phase at the various depletion pressures. The viscosity of the liquid phase under similar depletion conditions varied from a minimum of 0.134 centipoise at saturation pressure to 1.352 centipoises at atmospheric pressure. El Paso Natural Gas Company E. P. Lusk No. 2 Well Page Two

A stage separation test was performed on the fluid at pressures approximating field conditions. The primary separator gas tank liquid ratio was measured to be 1916 standard cubic feet of gas per barrel of stock tank oil. The formation volume factor was measured to be 2.181 barrels of saturated fluid per barrel of stock tank oil.

It was a pleasure to cooperate with you in performing this study. Should you have any questions or if we may assist you further, please do not hesitate to contact us.

Very truly yours,

Core Laboratories, Inc. Reservoir Fluid Division

P. J. Moses

P. L. Moses, Operations Supervisor

PLM:pb 7 cc. - Addressee Form 69385

CORE LABORATORIES, INC.

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Petroleum Reservoir Engineering DALLAS, TEXAS

		Pagelo	f11
		File RFL	1974
Company El Paso Natural Gas Company	Date Sam	pled August 20, 196	61
Well E. P. Lusk No. 2	County	Lea	
Field Undesignated	Ounty	New Mexico	
EORMATION (HARACTERIS	TTCS	
Formation Name	IIANACI EM	Strawn	
Date First Well Completed			, 19
Original Reservoir Pressure		PSIG @	Ft.
Original Produced Gas-Oil Ratio			SCF/Bbl
Production Rate			Bbl/Day
Separator Pressure and Temperature		PSIG,	°F.
Oil Gravity at 60° F.			°API
Datum		7585	Ft. Subsea
Original Gas Cap		<u></u>	
WELL CHA	RACTERISTIC	CS	
Elevation		3605 KB	Ft.
Total Depth			Ft.
Producing Interval		11,220-11,250	Ft.
Tubing Size and Depth		In. to	Ft.
Productivity Index		Bbl/D/PSI @	Bbl/Day
Last Reservoir Pressure		<u> </u>	<u>11,100</u> Ft.
Date		August 20	, 19_61_
Reservoir Temperature		<u> 160 * </u>	<u>11,100</u> Ft.
Status of Well		Shut in	
Pressure Gauge		<u> </u>	
Normal Production Rate			Bbl/Day
Gas-Oil Ratio			SCF/Bbl
Separator Pressure and Temperature		PSIG,	°F.
Base Pressure			PSIA
Well Making Water		None	% Cut
SAMPLING	CONDITIONS	8	
Sampled at		_ 11.100	Ft.
Status of Well		Shut in	
Gas-Oil Ratio			SCF/Bbl
Separator Pressure and Temperature		PSIG,	° F .
Tubing Pressure		2964	PSIG
Casing Pressure		_Dual	PSIG
Core Laboratories Engineer		SR	
Type Sampler		Perco	

REMARKS: * Temperature extrapolated to mid-point of producing interval = 161° F.

CORE LABORATORIES, INC. Petroleum Reservoir Engineering DALLAS, TEXAS

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Well_	<u>E.P.</u>	Lus	<u>sk No.</u>	2

VOLUMETRIC DATA OF Reservoir Fluid SAMPLE

1.	Saturation pressure (bubble-point pressur	re)		4	150	_PSIG @	<u>161</u> ° F .
2.	Thermal expansion of saturated oil $@60$	000_ PS	$\mathbf{I} = \frac{\mathbf{V} @ 1}{\mathbf{V} @ 7}$	$\frac{61 ^{\circ}\mathbf{F}}{4.5 ^{\circ}\mathbf{F}} =$	=1.	07755	
3.	Compressibility of saturated oil @ reserv	voir tem	perature: Vo	ol/Vol/PS	SI:		
		From _	<u>6000</u> PSI t	o5500	PSI == .	21.62	x 10 ⁻⁶
		From	<u>5500</u> PSI t	0 <u>4800</u>	PSI = .	24.47	x 10 ⁻⁶
		From	4800 PSI t	0 <u>4150</u>	PSI — _	31.64	x 10 ⁻⁶
4.	Specific volume at saturation pressure: ft	³/lb			0.0	<u>3001</u> @	<u>161</u> °F.

CORE LABORATORIES, INC.

Petroleum Reservoir Engineering

DALLAS, TEXAS

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Reservoir Fluid SAMPLE TABULAR DATA

	PRESSURE-VOLUME	VISCOSITY	DIFFERENTI	AL LIBERATION @	161 °F.
PRESSURE PSI GAUGE	@ 161 °F., RELATIVE VOLUME OF OIL AND GAS, V/VSAT.	OF OIL @ 161°F., CENTIPOISES	GAS/OIL RATIO LIBERATED PER BARREL OF RESIDUAL OIL	GAS/OIL RATIO IN SOLUTION PER BARREL OF RESIDUAL OIL	RELATIVE OIL VOLUME, V/VR
6000	0.9523				2.592
5500	0.9627				2.620
5420		0.146			
5200		0.144			
5000	0.9742	0.141			2.652
4800	0.9794	0.139			2.666
4600	0.9849	0.137			2.681
4500	0.9882				2.690
4400	0.9913	0.135			2.698
4300	0.9946				2.707
4200	0.9981	0.135			2.717
4150	1.0000	0.134	0	3084	2.722
4125	1.0015				
4106	1.0027				
4101			179	2905	2.612
4078	1.0045				
4051			337	2747	2.520
4050		0.139			
4004	1.0094				
4000		0.143			
3977			522	2562	2.412
3950		0.146			
3902			680	2404	2,321
3891	1.0172				
3850		0.152			
3800			852	2232	2.225
3771	1.0274				
3700		0.160			
3674			1025	2059	2.129
3558	1.0478				
3527			1187	1897	2.041
3500		0.172			
3352			1349	1735	1.954

v = Volume at given pressure

 $v_{sat.}$ = Volume at saturation pressure and the specified temperature.

 v_R = Residual oil volume at 14.7 PSI absolute and 60° F.

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CORE LABORATORIES, INC. Petroleum Reservoir Engineering DALLAS, TEXAS

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File	RFL 1974	
Well_	E. P. Lusk No. 2	

Reservoir Fluid SAMPLE TABULAR DATA

	PRESSURE-VOLUME	VISCOSITY	DIFFERENT	AL LIBERATION @	161 °F.
PRESSURE PSI GAUGE	@ 161 °F., RELATIVE VOLUME OF OIL AND GAS, V/VSAT.	OF OIL @ 161°F., CENTIPOISES	GAS/OIL RATIO LIBERATED PER BARREL OF RESIDUAL OIL	GAS/OIL RATIO IN SOLUTION PER BARREL OF RESIDUAL OIL	RELATIVE OIL VOLUME, V/VR
3302	1.0786				
3300		0.184			
3100			1543	1541	1.853
3042	1.1201				
3000		0.202			
2756	1.1809				
2752			1762	1322	1.743
2600		0.228			
2436	1.2753				
2351			1970	1114	1.642
2200		0.258			
2144	1.4024				
1950			2152	932	1.555
1888	1.5495				
1800		0.302			
1649	1.7494				
1550			2319	765	1.477
1463	1.9630				
1400		0.356			
1252	2.2793				
1150			2472	612	1.406
1030	2.7986				
1000		0.430			
772	3.7963				
748			2626	458	1.336
600		0.530			
347			2783	301	1.259
130			2907	177	1.187
0		1.352	3084	0	1.052
				@ 60 ⁰ F	`. = 1.000 '

Gravity of residual oil = 42.9 ^OAPI @ 60^O F.

 $\mathbf{v} = \mathbf{Volume} \ \mathbf{at} \ \mathbf{given} \ \mathbf{pressure}$

 $v_{\text{SAT.}}$ = Volume at saturation pressure and the specified temperature.

 v_R = Residual oil volume at 14.7 PSI absolute and 60° F.

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Petroleum Reservoir Engineering

DALLAS, TEXAS

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Differential Pressure Depletion at 161°F.

Pressure PSIG	Oil Density Gms/Cc	Gas Gravity	Deviation Factor Z
4150	0.5342		
4101	0.5409	1.050	0.865
4051	0.5459	1.040	0.849
3977	0.5531	1.031	0.825
3902	0.5597	1.015	0.823
3800	0.5668	0.994	0.811
3674	0.5754	0.964	0.799
3527	0.5840	0.934	0.784
3352	0.5937	0.901	0.774
3100	0.6063	0.864	0.766
2752	0.6221	0.823	0.765
2351	0.6383	0.794	0.772
1950	0.6540	0.777	0.787
1 5 5 0	0.6697	0.766	0.813
1150	0.6848	0.781	0.843
748	0.7010	0.810	0.886
347	0.7189	0.904	0.933
130	0.7369	1.135	0.967
0	0.7704	1.666	

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Petroleum Reservoir Engineering DALLAS, TEXAS

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Well E. P. Lusk No. 2

SEPARATOR TESTS OF Reservoir Fluid SAMPLE

SEPARATOR PRESSURE, PSI GAUGE	SEPARATOR TEMPERATURE, °F.	SEPARATOR GAS/OIL RATIO See Foot Note (1)	STOCK TANK GAS/OIL RATIO See Foot Note (1)	STOCK TANK GRAVITY, • API @ 60° F.	SHRINKAGE FACTOR, VR/VSAT. See Foot Note (2)	FORMATION VOLUME FACTOR, VSAT./VR See Foot Nate (3)	SPECIFIC GRAVITY OF FLASHED GAS
390	72	1916					
to 32	72	306	6	47.9	0.4586	2.181	0.777 *

* Specific gravity of composite gases.

- (1) Separator and Stock Tank Gas/Oil Ratio in cubic feet of gas @ 60° F. and 14.7 PSI absolute per barrel of stock tank oil @ 60° F.
- (2) Shrinkage Factor: VR/VSAT. is barrels of stock tank oil @ 60° F. per barrel of saturated oil @ 4150 PSI gauge and 161 ° F.
- (3) Formation Volume Factor: VSAT./VR is barrels of saturated oil @_4150PSI gauge and 161_° F. per barrel of stock tank oil @ 60° F.

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CORE LABORATORIES, INC. Petroleum Reservoir Engineering DALLAS, TEXAS

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			File_RFL_1974
Company_	El Paso Natural Gas Company	Formation	Strawn
Well	E. P. Lusk No. 2	County	Lea
Field	Undesignated	State	New Mexico

HYDROCARBON ANALYSIS OF Reservoir Fluid SAMPLE

COMPONENT	WEIGHT PER CENT	MOL PER CENT	DENSITY @ 60 ⁹ F. GRAMS PER CUBIC CENTIMETER	° API @ 60° F.	MOLECULAR WEIGHT
Hydrogen Sulfide					
Carbon Dioxide	0.21	0.24			
Nitrogen	0.83	1.58			
Methane	16.39	53.85			
Ethane	7.21	12.65			
Propane	6.73	8.06			
iso-Butane	1.18	1.07			
n-Butane	2.86	2.60			
iso-Pentane	1.54	1.12			
n-Pentane	1.99	1.46			
Hexanes	3.43	2.10			
Heptanes plus	57.63	15.27	0.8209	40.7	199
	100.00	100 00			

Core Laboratories, Inc. Reservoir Fluid Division

P. J. Moses (FV)

P. L. Moses, Operations Supervisor

CURE LABORATORIES, INC. Fetroleum Reservoir Engineering

DALLAS, TEXAS

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FRESSURE VOLUMY RELATIONS OF RESERVOIR FLUID



PRESSURE: POUNDS PER SQUARE INCH GAUGE

CORE LABORATORIES, INC. Petroleum Reservoir Engineering DALLAS, TEXAS

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RELATIVE LIQUID VOLUME: V/VR

DIFFERENTIAL VAPORIZATION OF RESERVOIR FLUID



PRESSURE: POUNDS PER SQUARE INCH GAUGE

GAS LIBERATED: STANDARD CUBIC FEET PER BARREL OF RESIDUAL OIL

CORE LABORATORIES, INC. Petroleum Reservoir Engineering DALLAS, TEXAS

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VISCOSITY OF RESERVOIR FLUID



CORE LABORATORIES, INC. Petroleum Reservois Engineering DALLAS TEXAS

Page <u>11</u> of <u>11</u> File <u>RFL 1974</u>









LARGE FORMAT EXHIBIT HAS BEEN REMOVED AND IS LOCATED IN THE NEXT FILE CORE LABORATORIES. INC. Petroleum Reservoir Engineering DALLAS, TEXAS April 3, 1961

REPLY TO P. O. BOX 4337 MIDLAND, TEXAS

El Paso Natural Gas Company 19th Floor, Wilco Building Midland, Texas

Attn: Mr. L. C. Zinc

Subject: Core Analysis Lusk Deep Unit No. 2 Well Lea County, New Mexico Location: Sec. 18-T19S-R32E

Gentlemen:

Strawn formation analyzed between 11, 221 and 11, 276 feet is interpreted to be oil productive where permeable. A formation treatment may possibly be necessary to increase flow rates. Average core analysis values and calculated original stock-tank oil in place have been prepared for the permeable feet analyzed in the interval and are given on page one of the report.

Formation analyzed between 8762 and 8795 feet is interpreted to be essentially nonproductive due to very low permeability. Formation analyzed from 13,640 to 13,691 feet is virtually impermeable; however, any fluid produced from the zone is expected to be water due to the unfavorable residual fluid saturations.

Thank you for the opportunity to be of service to you.

Very truly yours,

Core Laboratories, Inc.

\$ 13ynum #

R. S. Bynum, Jr., District Manager

RSB:LW:bd

CORE LABORATORIES, INC. Petroleum Reservoir Engineering DALLAS. TEXAS

Page 1 of 1 File WP-3-1593 Well Lusk Deep Unit No. 2

CORE SUMMARY AND CALCULATED RECOVERABLE OIL

FORMATION NAME AND DEPTH INTERVAL: Strawn 11,221.0 - 11,276.0						
FEET OF CORE RECOVERED FROM Above Interval		54.0	AVERAGE TOTAL WATER BATURATION: Per cent of pore space		36.7	
FEET OF CORE Included in Averages		33. 3~	AVERAGE CONNATE WA ter Batur ation: Per cent of pore space	(c)	36.7	
AVERAGE PERMEABILITY: Millidarcys	Max. 900	12 3.0	OIL GRAVITY: ⁹ api	(e)	48	
PRODUCTIVE CAPACITY: MILLIDARCY-FEET	Max. 90 ⁰	400 100	DRIGINAL SOLUTION GAS-OIL RATIO: Cubic feet per Barrel	(e)	1130	
AVERAGE POROBITY: PER CENT		4.1	ORIGINAL FORMATION VOLUME FACTOR: BARRELS Saturated dil per barrel Stock-tank dil	(e)	1.69	
AVERAGE RESIDUAL OIL SATURATION: PER CENT OF FORE SPACE		5.8	CALCULATED ORIGINAL STOCK-TANK OIL IN PLACE: Barrels Per Acre-Foot		119	

Calculated maximum solution gas drive recovery is barrels per acre-foot, assuming production could be continued until reservoir pressure declined to zero psig. Calculated maximum water drive recovery is barrels per acre-foot, assuming full maintenance of original reservoir pressure, 100% areal and vertical coverage, and continuation of production to 100% water cut. (*Please refer to footnotes for further discussion of recovery estimates.*)

FORMATION NAME AND DEPTH INTERVAL:

FEET OF CORE RECOVERED FROM	AVERAGE TOTAL WATER SATURATION:
Above Interval	Per cent of pore space
FEET OF CORE	AVERAGE CONNATE WATER SATURATION:
Included in averages	Per cent of pore space
AVERAGE PERMEABILITY: MILLIDARCYS	DIL GRAVITY: *API
PRODUCTIVE CAPACITY:	ORIGINAL BOLUTION GAB-OIL RATIO:
Millidarcy-feet	Cubic feet per Barrel
AVERAGE POROBITY: PER CENT	ORIGINAL FORMATION VOLUME FACTOR: BARRELS Saturated Oil per Barrel Stock-Tank Oil
AVERAGE REBIDUAL OIL BATURATION:	CALCULATED ORIGINAL STOCK-TANK OIL IN PLACE:
PER CENT OF PORE SPACE	Barrels per acre-foot

Calculated maximum solution gas drive recovery is barrels per acre-foot, assuming production could be continued until reservoir pressure declined to zero psig. Calculated maximum water drive recovery is barrels per acre-foot, assuming full maintenance of original reservoir pressure, 100% areal and vertical coverage, and continuation of production to 100% water cut. (*Please refer to footnotes for further discussion of recovery estimates.*)

(c) Calculated (e) Estimated (m) Measured (*) Refer to attached letter.

These recovery estimates represent theoretical maximum values for solution gas and water drive. They assume that production is started at original reservoir pressure; i.e., no account is taken of production to date or of prior drainage to other areas. The effects of factors tending to reduce actual ultimate recovery, such as economic limits on oil production rates, gas-oil ratios, or water-oil ratios, have not been taken into account. Neither have factors been considered which may result in actual recovery intermediate between solution gas and complete water drive recoveries, such as gas cap expansion, gravity drainage, or partial water drive. Detailed predictions of ultimate oil recovery to specific abandonment conditions may be made in an engineering study in which consideration is given to overall reservoir characteristics and economic factors.

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CORE LABORATORIES, INC. VVIUI Petroleum Reservoir Engineering

- COMPANY EL PASO NATURAL GAS COMPANY FIELD WILDCAT FILE WP-3-1593
- WELL LUSK DEEP UNIT NO. 2 COUNTY LEA DATE 12-14-60
- LOCATION 660 FS & 1980 FS SEC 18-T198- STATE NEW MEXICO ELEV. 3605' DF

CORE-GAMMA CORRELATION

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VERTICAL SCALE: 5" = 100'

CORE-GAMMA SURFACE LOG

COREGRAPH

GAMMA RAY



PERCENT TOTAL WATER

TOTAL WATER -



CORE LABORATORIES, INC. VVIUL Petroleum Reservoir Engineering

COMPANY EL PASO NATURAL GAS COMPANY FIELD WILDCAT FILE WP-3-1546

WELL LUSK DEEP UNIT NO. 1 COUNTY LEA DATE 9-22-60

LOCATION 660 FN & EL SEC 19-T195-R32E STATE NEW MEXICO ELEV.

CORE-GAMMA CORRELATION

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VERTICAL SCALE: 5" = 100'

CORE-GAMMA SURFACE LOG

<u>....</u>

(PATENT APPLIED FOR)

GAMMA RAY



COREGRAPH

TOTAL WATER -

PERCENT TOTAL WATER

SAMPLE NUMBER NUMBER FERTH FERTH FERTH	SAND	COMPANY EL PASO WELL LUSK DEI FIELD UNDESIGI COUNTY LEA LOCATION 1980 FE	CORE
FE: MG: CG = Type Grain Size S:Style HORIZONTAL MAX, 900 WHOLE CORE ANALYSIS	These analyses, opinions or interpretations and use this report is made. The interpretations of operation, or profilebleness of any oil gos o LIMESTONE	NATURAL GAS COMPANY P UNIT NO. 2 NATED STATE NE & 660 FSL SEC 18-T19 COMPI	ABORATORIES, II
DIITIC V-VURRY D-OIL W-WA	 based an observation, and material (upplied by the (term of principler) and index no entropy other mineral well or and in connection with which such soften mineral well or and in connection with which such to be a soften defined by a soften definition defined by a soften d	DATE 1 FORMATION A M MEXICO DRLG. FLD D S-R32E REMARKS S *	
The production of the production of the second seco	it to whem, and for where exclusive and carlidential aborations Inc. "oll errors and ominians, escepted any of orgenerations as to the productivity, proper report is used or relied upon CHERT	EGRAPH	Petroleum Reservo
IOTAL WATER O-O PERCENT PORE SPACE 75 50 25 OIL SATURATION XX PERCENT PORE SPACE 25 50 75 25 50 75	ANHYDRITE	O WP-3-1593 BOONE 3605' DF DIAMOND 14 3/8" CLIENT	ir Engineering

R-31-E





LUSK DEEP UNIT LEA & EDDY COUNTIES, NEW MEXICO EL PASO NAT. GAS COMPANY - OPERATOR UNIT AREA BOUNDARY LUSK STRAWN POOL

SLANTED LETTERING-LESSEE OF RECORD VERTICAL LETTERING-WORKING INTEREST OWNER

ACREAGE SURROUNDING UNIT VERTICAL LETTERING-WORKING INTEREST OWNER & LESSEE OF RECORD OTHER INTEREST-AS INDICATED

SCALE - 2"= I MILE

NMOCC CASE NO. 2469 EPNG EXHIBIT NO. 12 JAN. 4, 1962