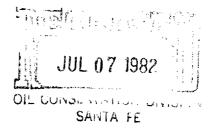
ARCO Oil and Gas Company

| 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 | 1964 |





July 1, 1982

Mr. M. Stogner Oil Conservation Division P. O. Box 2088 Santa Fe, New Mexico 87501

Dear Mr. Stogner:

ARCO Oil and Gas Company Case No. 5762; Order No. R-5295 State Vacuum Unit - Waterflood Project T17S, R34E, Lea County, New Mexico

Attached please find a copy of our proposal to increase the injection pressure on our State Vacuum Unit waterflood. Per your phone conversation with our secretary today, we understood that you never did receive the original sent May 4, 1982. Since production from the subject unit is decreasing more rapidly than anticipated, we would appreciate your most prompt consideration of this request.

Very truly yours,

Juan A. Fraga

Engineer

JAF/MJB:dmm Attachments

ARCO Oil and Gas Company

Perman, District Pest Prace Box 1616 Midland, Texas 79702 Felephane 915 684 0100 *****

May 4, 1982

Oil Conservation Division of the

New Mexico Dept. of Energy and Minerals
P. O. Box 2088
Santa Fe, New Mexico

Attention Mr. Ramey

Dear Mr. Ramey:

RE: Case No. 5762; Order No. R-5295
ARCO Oil and Gas Company
State Vacuum Unit - Waterflood Project
T17S, R34E, Lea County, New Mexico

Dear Mr. Ramey:

In the Order dated October 12, 1976, establishing the waterflood project, wellhead injection pressure was limited to 860 psi. Approval of a higher wellhead pressure could be obtained by showing that the increase in pressure would not fracture the confining strata. On April 14, 1980, evidence was offered to show that a wellhead injection pressure of 1422 psi would not fracture the formation. This proposal was approved administratively and the current limitation is 1422. As operator of the unit, ARCO Oil and Gas Company applies for administrative approval of a wellhead injection pressure of 1550 psi. The attached exhibits are offered as evidence that this pressure will not fracture the confining strata.

The exhibits are based on parting pressure tests run on April 19-26, 1982. Exhibit No. 1 is a map of the unit area showing the five injection wells which were tested. Four of the five wells were tested last time and provide reference for comparison purposes. The tests on these five wells indicate a range of surface parting pressures from 1600 to 2198 psi as shown in Exhibit No. 2. The necessary equipment and well data is included on Exhibit No. 3

The paper "Step-Rate Tests Determine Safe Injection Pressures in Floods" was used as a reference to help determine proper testing procedures and analysis methods. The tests were run by Atlantic Richfield Company using a downhole pressure recorder, surface pressure recorder and a Halliburton turbine flowmeter. Individual well data and results are shown in Exhibits 4 through 8.

Some injection wells exhibit non-D'Arcy flow characteristics which prevents determination of the parting pressure by the normal rate vs. pressure graphical technique. Two of the wells tested exhibited this behavior. By using the technique outlined in the reference paper

Catal + 1600ffice 6-2-62 Fracture presente result up become of flood, - Frotlems in area but not in tros do - thing this application is ok. NMOCD Case 5762; Order No. R-5295 May 4, 1982 Page 2

 $(q = D'q^2)$ parting pressures were determined for the two wells and are included as Exhibits 5A and 8A. Exhibits 9 and 10 are graphical solutions of the Williams and Hazen formula for determining the pressure drop due to friction in the injection tubing. Data for the individual wells is listed on Exhibit 2.

Some of the wells tested do not contain enough data points for a well-defined line after the formation parts. This is due to the limitation of the surface equipment during the tests. The wellheads have a 2000 psi working pressure limitation and this limited the injection rate during the test.

We feel that an increased wellhead injection pressure is necessary if we are to maintain adequate injection rates to promote the timely production of the secondary reserves in the unit. Our application for administrative approval of a wellhead injection pressure of 1550 psi should insure that we are not fracturing the formation strata but also allow us to increase our current injection rates. We will gladly forward any additional information which may be required and ask for your prompt consideration.

Very truly yours,

It Tweed

J. L. Tweed

District Engineer

JAF:JLT:cn

Attachments

AtlanticRichfieldCompany

Note: American Producing Division
The man District
Tool Office Box 1610
Formal d. Texas 79701
Turnshone 915 682 8631



May 19, 1978

Oil Conservation Division of the New Mexico Department of Energy and Minerals
P. O. Box 2088
Santa Fe, New Mexico

Attn: Mr. Ramey

Re: Case No. 5762; Order No. R-5295
Atlantic Richfield Company
State Vacuum Unit
Waterflood Project
T-17S, R-34E, Lea County, New Mexico

Dear Mr. Ramey:

In the Order establishing the waterflood project, wellhead injection pressure was limited to 860 psi. Approval of a higher wellhead pressure could be obtained by showing that the increase in pressure would not fracture the confining strata. As operator of the State Vacuum Unit, Atlantic Richfield Company applies for administrative approval of a wellhead injection pressure of 1134 psi. The attached exhibits are offered as evidence that this pressure will not fracture the confining strata.

The exhibits are based on pressure parting tests run on April 24-26, 1978. Exhibit 1 is a map of the unit area showing the seven injection wells which were tested. Insufficient pump capacity on Well No. 9 prevented the use of data from the test. The remaining six wells indicated a range of surface parting pressures from 1234 psi to 2101 psi as shown on Exhibit 2. Necessary equipment and well data is included on Exhibit 3.

The paper "Step-Rate Tests Determine Safe Injection Pressures in Floods" (Exhibit 10) was used as a reference to help determine proper testing procedures and analysis methods. The tests were run by Atlantic Richfield Company using a downhole pressure recorder and a Hallibruton turbine flowmeter. Individual well data and results are shown in Exhibits 4 through 9.

Some injection wells exhibit non-D'Arcy flow characteristics which prevents determination of the parting pressure by the normal rate vs. pressure graphical technique. Two of the wells

Oil Conservation Division of the New Mexico Department of Energy and Minerals May 19, 1978 Page 2

tested exhibited this behavior. By using the technique outlined in the reference paper $(q + Dq^2)$ parting pressures were determined for the two wells and are included as Exhibits 4A and 5A. Exhibit 11 is a graphical solution of the Williams and Hazen formula for determining the pressure drop due to friction in the injection tubing. Data for the individual wells is listed on Exhibit 2.

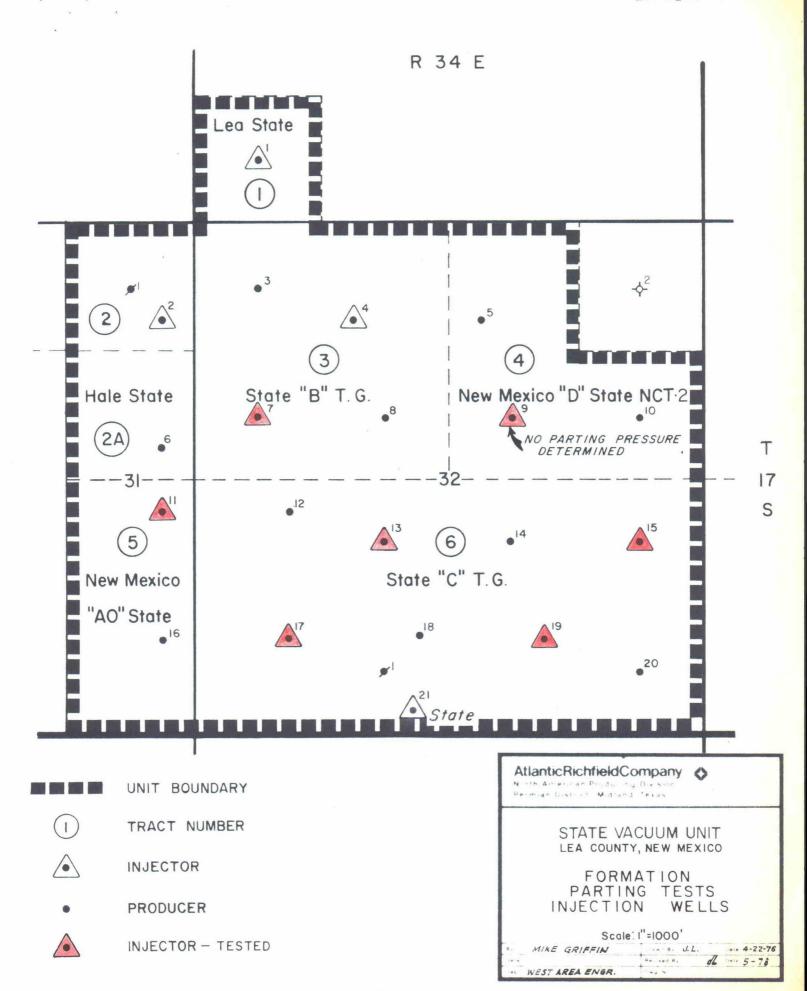
At the current limiting pressure of 860 psi, injection rates in the unit have begun to decline. We feel that an increased wellhead injection pressure is necessary if we are to maintain adequate injection rates to promote the timely production of the secondary reserves in the unit. Our application for administrative approval of a wellhead injection pressure of 1134 psi should insure that we are not fracturing the formation strata but also allow us to increase our current injection rates. We will gladly forward any additional information which may be required and ask for your prompt consideration.

Very truly yours,

J & Tweed

J. L. Tweed

MG/agp



17	15	13	7	4	NO. L
32.6	643.0	99.3	385.9	8.4	CUM.INJ. 3/1/80 (MB)
4741	1661	4685	4574	4609	PRESS.BOMB SETTING DEPTH (FT)
2052.8	2018.2	2028.5	1980.5	1995.7	HYDRO- STATIC HEAD' (PSI)
1145	3800	1900	2800	1000	INJ.RATE@ PTG.PRES. (BPD)
1.15	10.5	2.95	6.0	1.63	PRESS.DROP FRICTION ² ΔP_{ξ} (PSI/100 FT)
54.5	489.4	138.2	274.4	75.1	A & TOTAL @ SETTING DEPTH(psi)
3580	Mn 3770	Mn 3975	Mn 3278	Mn 3865	BTM HOLE PTG.PRES. (psi)
1581.7	2241.2	2084.7	1571.9	1944.4	SURF.PTG. PRESSURE (psi)
.755	.809	.848	.717	.838	PTG.GRAD- IENT (psi/ft)

Injection water has specific gravity equal to 1.001; pressure gradient = .433 psi/ft.

^{2.} Taken from Exhibit 10 (Williams and Hazen formula).

Surface parting pressure = bottom hole parting pressure - hydrostatic head + Δ P_f

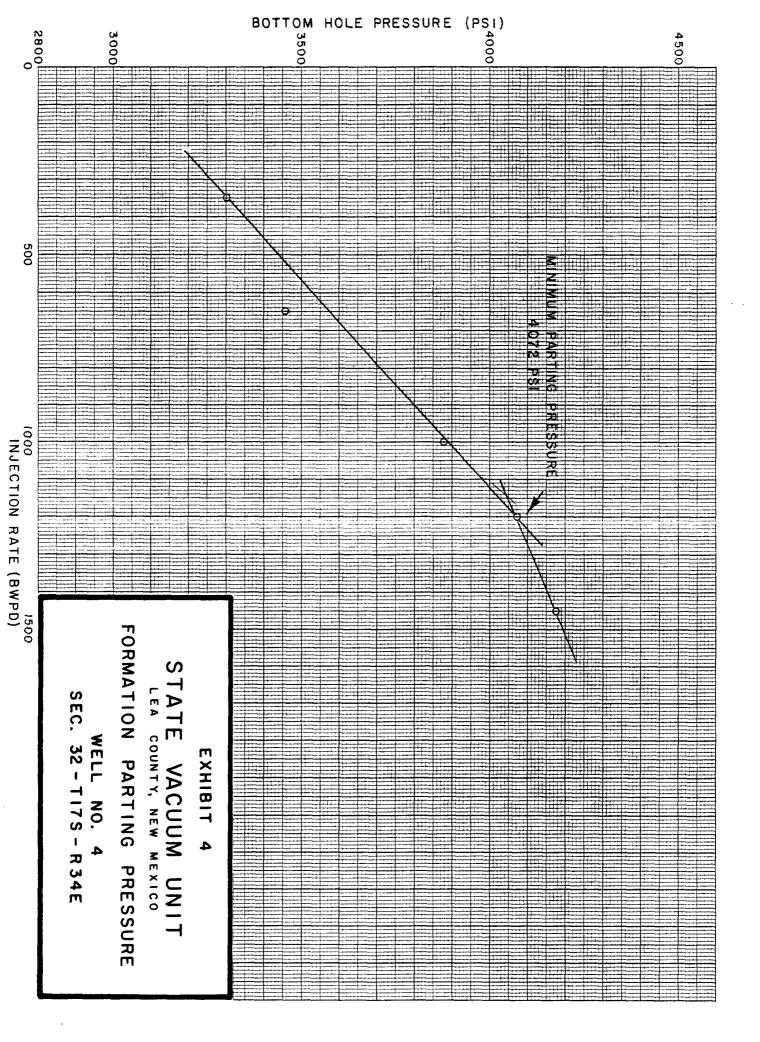
STATE VACUUM UNIT PRESSURE PARTING TESTS INJECTION WELL DATA

WELL NO.	COMPLETION CASING SIZE (DEPTH)	TUBING SIZE*	DEPTH SET	PERFORATIONS
4	3½" liner (3440-4700)	2-3/8" 2-1/16"	1153' 4550'	4594-4624'
7	3½" liner (4426-4728)	2-3/8"	44261	4671-47181
13	3½" liner (4241-4717)	2-3/8"	4241 *	4660-4710'
15	3½" liner (4249-4708)	2-3/8"	4249 '	4636-4686'
17	3½" liner (4416-4750)	2-3/8"	4416'	4692-4742'

^{*} All tubing is internally plastic coated.

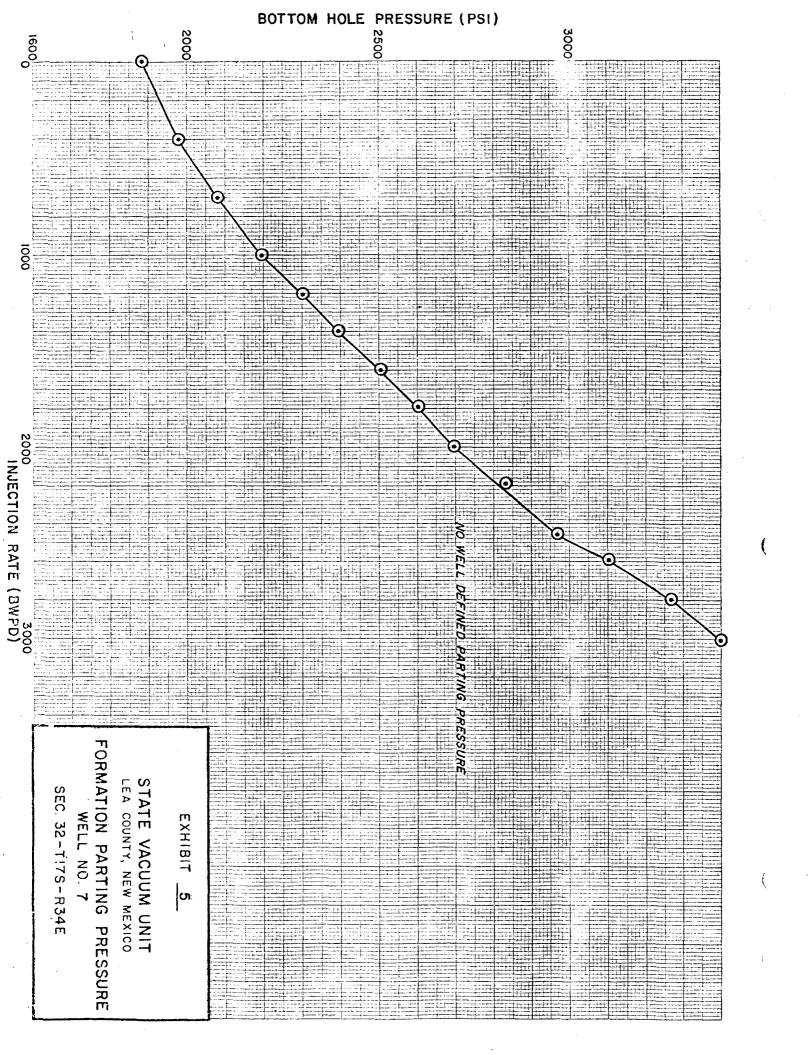
LEASE: State Vacuum Unit	DATE OF TEST 4-26-82
WELL NUMBER: 4	ELEMENT: 36391
COUNTY: Lea	TEST DEPTH: 4609

COUNTY: Lea		TEST DEPTH: 4609		
TIME/ AM PM	APPROXIMATE RATE (BPD)	BHP @ TEST DEPTH (PSI)	SURFACE PRESSURE (PSI)	
12:12	0	2823	833	
12:32	350	3300	1050	
12:49	650	3458	1458	
1:04	1000	3878	1820	
1:19	1200	4072	2030	
1:34	1450	4174	2270	



EASE: State Vacuum	DATE OF TEST 3-17-80
ELL NUMBER: 7	ELEMENT: 5505
OUNTY: Lea	TEST DEPTH: 4574

AM TIME/PM	APPROX. RATE (BPD)	BHP @ TEST DEPTH (PSI)	SURFACE PRESSURE (PSI)
10:42	0	1839	Vacuum
12:16	400	1978	Vacuum
12:33	700	2079	130
12:48	1000	2191	280
1:03	1200	2299	390
1:20	1400	2392	500
1:34	1600	2507	620
1:49	1800	2600	730
2:05	2000	2692	850
2:20	2175	. 2836	1015
2:36	2450	2790	1240
2:51	2600	3107	1390
3:05	2800	3277	1650
3:20	3000	3397	1830
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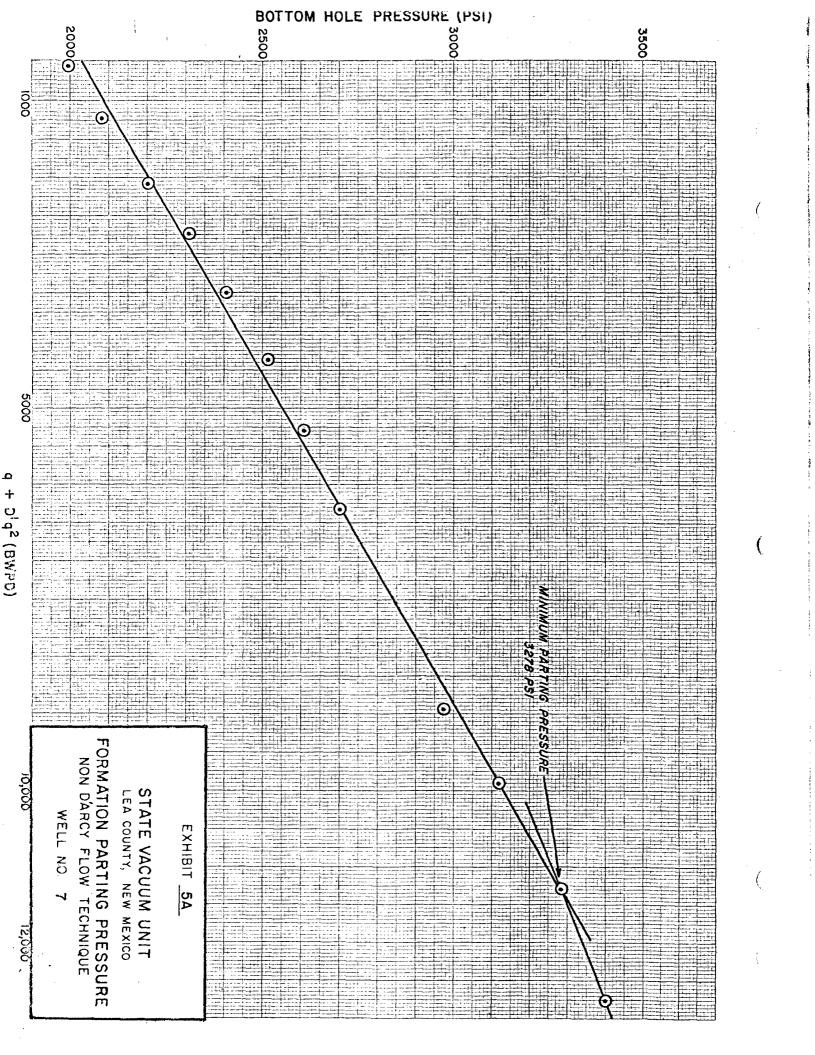
STATE VACUUM UNIT FORMANTION PARTING PRESSURE NON D'ARFY FLOW TECHNIQUE WELL NO. 7

From Exhibit 9:

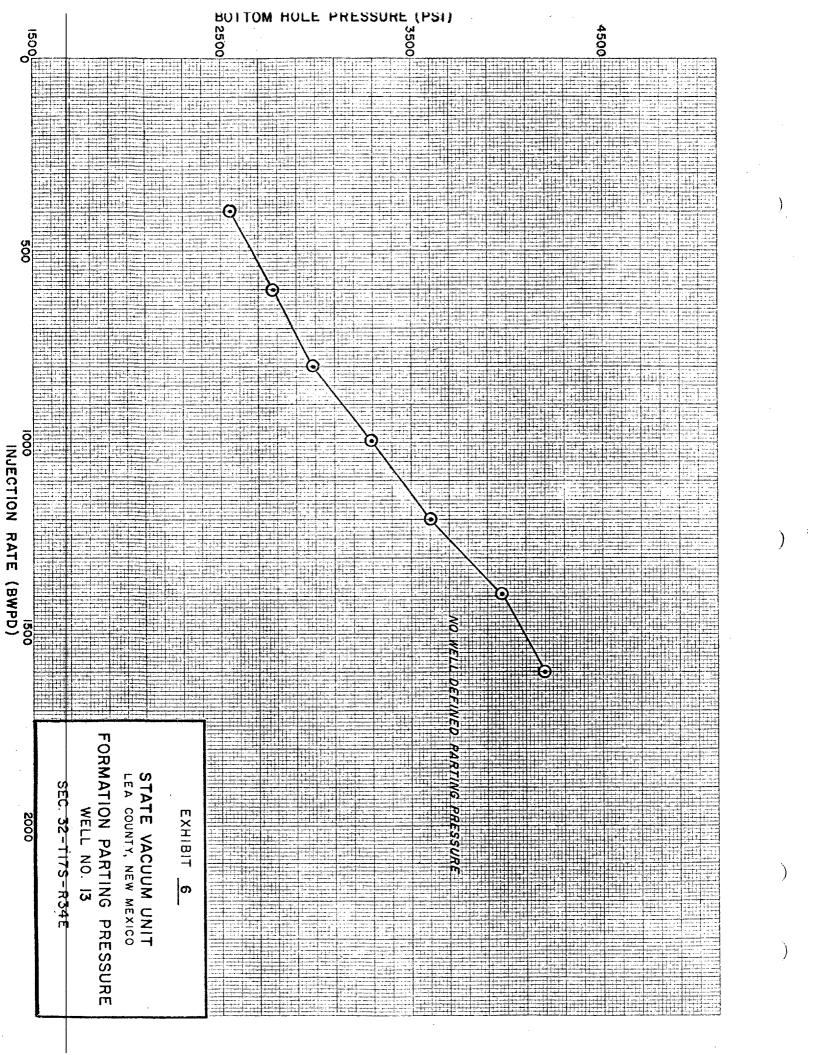
$$D' = (q_2 \triangle P_1 - q_1 \triangle P_2) / (q_1^2 \triangle P_2 - q_2^2 \triangle P_1)$$

Substituting: $q_1 = 400 \text{ BPD}$ $P_1 = 1978$ $\Delta P_1 = 88$ $q_2 = 700 \text{ BPD}$ $P_2 = 2079$ $\Delta P_2 = 189$

Injection Rate BPD	D'=.00109 B/D ⁻¹ BHP @ TEST DEPTH (psi)	q + D'q ² (BPD)
0	1839	
400	1978	573
700	2079	1233
1000	2191	2087
1200	2299	2765
1400	2392	3530
1600	2507	4383
1800	2600	5322
2000	2692	6348
2175	2836	7331
2450	2790	8974
2600	3107	9948
2800	3277	11321
3000	3397	12783



LEASE:State Vacuum		DATE OF	TEST <u>3-11-80</u>
WELL NUMBER:	13	ELEMENT:	7287
COUNTY:	Lea	TEST DEP	TH: 4685
AM TIME/RM	APPROX. RATE (BPD)	BHP @ TEST DEPTH (PSI)	SURFACE PRESSURE (PSI)
10:56	0	1844	Vacuum
11:22	400	2555	280
11:42	600	2788	640
1	800	2995	960
12:03PM	1000	3305	1300
12:23		3618	1650
,_,,	1200		2160
1:05	1400 1700	3971 4198	2280



STATE VACUUM UNIT FORMATION PARTING PRESSURE NON D'ARCY FLOW TECHNIQUE WELL NO. 13

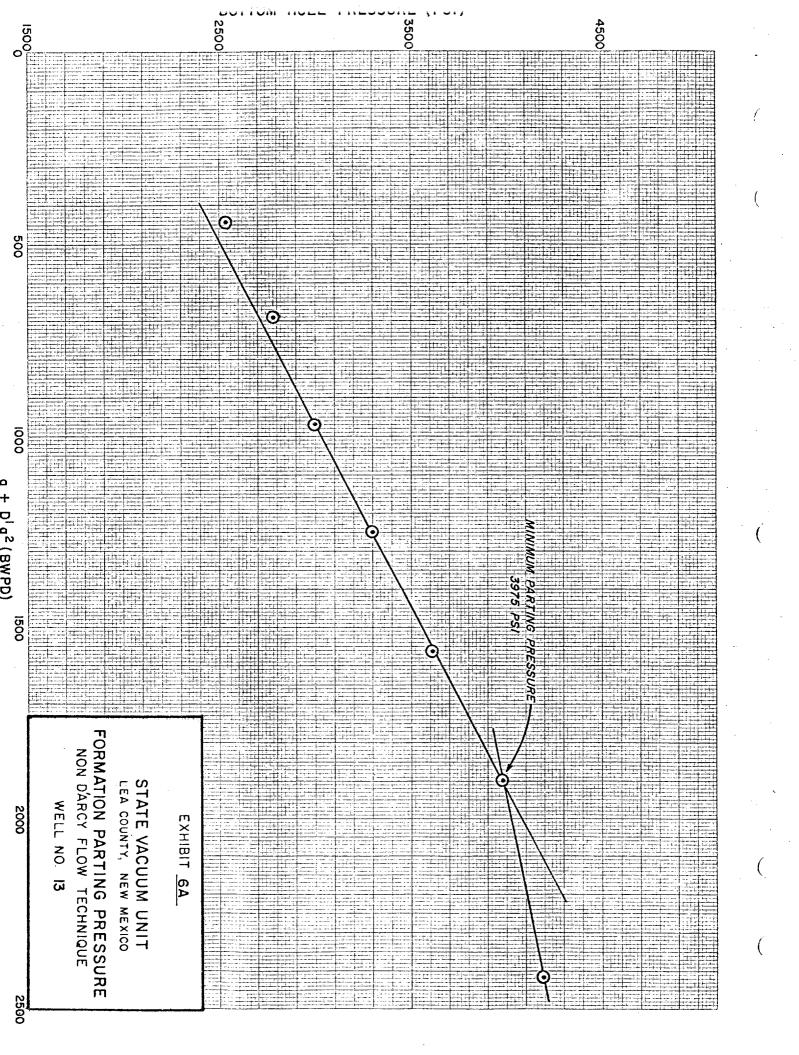
From Exhibit 9:

$$D' = (q_2 \Delta P_1 - q_1 \Delta P_2) / (q_1^2 \Delta P_2 - q_2^2 \Delta P_1)$$

Substituting: $q_1 = 600$ $P_1 = 2788$ $\Delta P_1 = 528$ $q_2 = 800$ $P_2 = 2995$ $\Delta P_2 = 735$

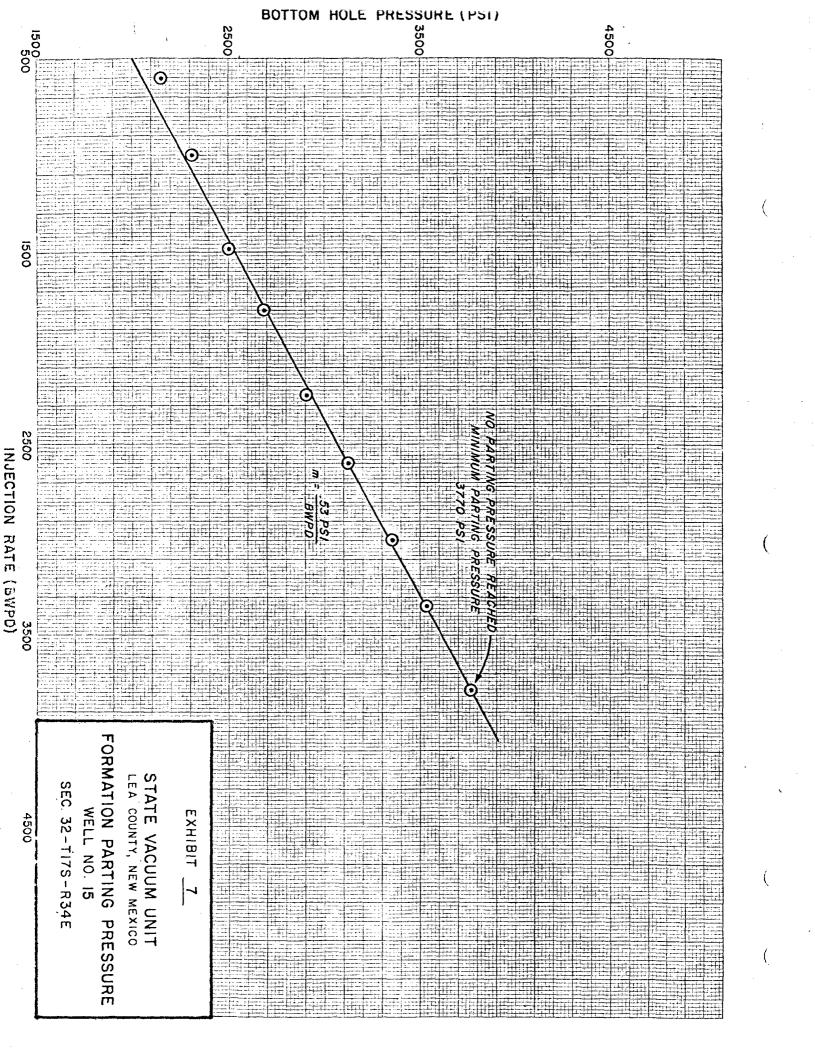
 $D^{1} = .00254$

Injection Rate (BPD)	BHP @ TEST DEPTH (PSI)	q+D'q ² (BPD)
0	1844	
400	2555	441
600	2788	691
800	2995	962
1000	3305	1254
1200	3618	1566
1400	3971	1898
1700	4198	2434



EASE:	State Vacuum	DATE OF TEST	3-10-80
VELL NUMBER:	15	ELEMENT:	5505
COUNTY:	Lea	TEST DEPTH:	4661

COUNTY: 252		TEST DEPTH: 4001		
AM TIME/PM	APPROX. RATE (BPD)	BHP @ TEST DEPTH (PSI)	SURFACE PRESSURE (PSI)	
10:55	0	1727	Vacuum	
1:25 PM	600	2155	150	
1:41	1000	2312	340	
2:02	1475	2508	560	
2:23	1800	2687	775	
2:42	2250	2919	1080	
3:02	2600	3129	1340	
3:22	3000	3359	1650	
3:42	3350	3540	1900	
4:01	3600	3645	2010	
4:15	3800	3776	2225	
		·		
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	te Vacuum		TEST 3-4-80
ELL NUMBER:	17	ELEMENT:	5505
OUNTY:	Lea	TEST DEPTH: 4741	
AM IME/PM	APPROX. RATE (BPD)	BHP 🍖 TEST DEPTH (PSI)	SURFACE PRESSURE (PSI)
10:51	0	2335	220
11:08	260	2539	360
11:24	425	2713	537
11:39	590	2918	750
11:56	850	3221	1090
12:11 PM	1015	3427	1300
12:26	1275	3635	1540
12:42	1500	3796	1750
12:57	1700	3913	1900
1:12	2000	4039	2075
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