MEMORANDUM

To: Mike Stogner

From: H. L. Babe Kendrick

Date: October 12, 1987

This copy of "Exhibit A" has been printed for your use in printing the manual for testing of Gas Wells in the San Juan Basin area of New Mexico. This is my understanding of what you, Jerry and I talked about in Santa Fe last week.

This copy was made from the same data that I had in the machine that was used to print the "Exhibit A" for the Order, with the only change being that necessary to cause the right and left margins to line up along a common edge. I also changed the top label of this print—out from "Exhibit A" to "RULES OF PROCEDURE FOR NORTHWEST NEW MEXICO". With these two changes, the remaining text should be identical to what is included in the order as "Exhibit A".

If you have any problems with this, please let me know so that I can make the necessary adjustments, and do it correctly.

Sincerely

H. L. Babe Kendrick

RULES OF PROCEDURE FOR NORTHWEST NEW MEXICO

CHAPTER I TYPE OF TESTS REQUIRED FOR WELLS COMPLETED IN PRORATED GAS

SECTION 1: Initial Deliverability and Shut-In Pressure Tests for Newly Completed Well

- A. Immediately upon completion of each gas well in northwest New Mexico, a shut-in pressure test of at least seven days duration shall be made. This initial shut-in pressure shall be filed with the Division's Aztec Office on either Form C-122 or C-104.
- B. Within 90 days after a well first delivers gas to a gas transportation facility, the well shall have been tested in accordance with Section 1 of Chapter II of these rules, "Initial Deliverability and Shut-In Pressure Test Procedures", and the results of the test filed in triplicate with the Division's Aztec office and one copy filed with the gas transportation facility to which the well is connected. This test is to be filed on Form C-122-A. Failure to file said test within the above-prescribed 90-day period will subject the well to the loss of one day's allowable for each day the test is late.
 - 1. If the newly first delivered well is an infill well on a proration unit, the old well on the unit is not required to be tested provided it has a valid test on file for the current proration year. Testing of the old well follows the regularly assigned test year for the pool in which the wells are located. The new well is required to be tested annually until at least three annual tests are on file and then the well is to be tested biennially with other wells in that pool.
 - 2. If the newly first delivered well is an infill well on a proration unit and the old well on the unit is "exempt", the old well is to be tested along with the new well for the Initial and Annual Deliverability and Shut-In Pressure Test. The old well will lose its "exempt" classification and must be tested biennially along with other wells in that pool. The new infill well is required to be tested annually until at least three annual tests are on file and then the well is to be tested biennially with other wells in that pool.

- C. The requirements for Initial Tests and Annual or Biennial Deliverability and Shut-In Pressure Tests and the notification requirements and scheduling of such tests which apply to newly completed wells shall also apply to recompleted wells.
- D. Any tests taken for informational purposes prior to pipeline connection shall not be recognized as official tests for the assignment of allowables.

SECTION 2. <u>Annual and Biennial Deliverability and Shut-In Pressure</u> <u>Tests</u>

- A. Annual or Biennial Deliverability and Shut-In Pressure Tests shall be made on all gas wells during the period from January 1 through December 31 of that year except as follows:
 - 1. A newly completed well or a recompleted well shall be tested on an annual basis until a minimum of three annual tests have been taken, after which the well shall be tested biennially as is required for other wells in the pool in which the well is located.
 - 2. Wells classified as "exempt" shall not be subject to the requirements of annual or biennial deliverability tests.

Classification of wells into or out of the "exempt" status shall be done once each year immediately following the reporting of June production and shall be effective for the succeeding annual test period.

Gas wells completed in the Pictured Cliffs or any shallower formation shall be classified "exempt" if at least three months of production history is available and the well failed to produce, and is incapable of producing, an average of 250 MCF or more per month during the months produced within the preceding 12-month period, and the well is classified as marginal in the August Gas Proration Schedule.

Gas wells completed in any formation deeper than the Pictured Cliffs formation shall be classified "exempt" if at least three months of production history is available and the well failed to produce, and is incapable of producing, an average of 2000 MCF or more per month during the months produced within the preceding 12-month period, and the well is classified as marginal in the August Gas Proration Schedule.

Gas wells on multiple well Gas Proration Units will not be classified "exempt" unless the Gas Proration Unit is classified as marginal. Any or all wells on a marginal multiple well Gas Proration Unit may be classified as "exempt" provided each Gas Proration Unit so classified meets the qualification for "exempt" status. Gas Proration Units for wells producing from formations deeper than the Pictured Cliffs formation shall be classified "exempt" if at least three months of production history is available and the Gas Proration Unit failed to produce, and is incapable of producing, an average of 2000 MCF or more per month during the months produced within the preceding 12-month period, and the Gas Proration Unit is classified as marginal in the August Gas Proration Schedule. Gas Proration Units are to be classified as "exempt" because of their low producing ability.

The District Supervisor of the Division's Aztec Office may classify a well or Gas Proration Unit as "exempt" at any time if the operator presents sufficient evidence to the District Supervisor indicating that the well or Gas Proration Unit is incapable of producing gas at a higher rate than that rate required for "exempt" classification for wells or Gas Proration Units in that pool.

Once a well or Gas Proration Unit has been declared "exempt" for the following test year, it shall remain classified "exempt" for that test year.

- 3. If a test is filed on any well on a gas proration unit, the test requirement for the gas proration unit has been met. The deliverability of the unit is taken only as the resulting sum of all wells tested.
- 4. A shut-in pressure must be filed on Form C-122-A even if no gas is measured during the production phase of the test. The filing of shut-in pressures for "exempt" wells is not required.
- B. All Annual and Biennial Deliverability and Shut-In Pressure Tests required by these rules must be filed with the Division's Aztec office and with the appropriate gas transportation facility within 90 days following the completion of each test. Provided however, that any test completed between October 31 of the test year and January 31 of the following year are due no later than January 31. No extension of time for filing tests beyond January 31 will be granted except after notice and hearing.

Failure to file any test within the above-prescribed times will subject the well to the loss of one day's allowable for each day the test is late. A well classified as marginal shall be shut-in one day for each day the test is late.

SECTION 3: <u>Scheduling of Tests</u>

A. Notification of Pools to be Tested

By September 1 of each year, the District Supervisor of the Aztec District Office of the Division shall by memorandum notify each gas transportation facility and each operator of the pools which are to be scheduled for biennial testing during the following testing period from January 1 through the last day of December of that test year. The District Supervisor will also provide a list of "exempt" wells and a list of wells that do not have a minimum of three Annual Deliverability and Shut-In Pressure Tests on file.

Any well scheduled for testing during its test year may have the conditioning period, test flow period, and some of the seven day shut-in period conducted in December of the previous year provided that if the 7 day shut-in period immediately follows the test flow period the 7 day shut-in pressure would be measured in January of the test year. The earliest date that a well could be scheduled for Annual or Biennial Deliverability and Shut-In Pressure Test would be such that the Test Flow Period would end on December 25 of the previous year.

Downhole commingled wells are to be scheduled for tests on dates for pool of the lowermost prorated completion of the well.

B. Annual and Biennial Deliverability Tests

By November 1 of each year, each gas transportation facility shall, in cooperation with the operators involved, prepare and submit a schedule of the wells to which it is connected which are to begin testing in December and January. Said schedule shall be entitled, "Annual and Biennial Deliverability and Shut-In Pressure Test Schedule", and one copy shall be submitted to the Division's Aztec office and to each operator concerned. The schedule shall indicate the date of tests, pool, operator, lease, well number, and location of each well.

At least 3D days prior to the beginning of each succeeding 2-month testing interval, a similar schedule shall be prepared and filed in accordance with the above.

The gas transportation facility and the Aztec District Office of the Division shall be notified immediately by any operator unable to conduct any test as scheduled.

In the event a well is not tested in accordance with the existing test schedule, the well shall be re-scheduled by the gas transportation facility, and the Division and the operator of the well so notified in writing. Every effort should be made to notify the Division of the new schedule prior to the conclusion of the newly assigned 14-day conditioning period.

Notice to the Division of Shut-In Pressure Tests which are scheduled at a time other than immediately following the flow test must be received prior to the time that the well is shut-in.

It shall be the responsibility of each operator to determine that all of its wells are properly scheduled for testing by the gas transportation facility to which they are connected, in order that all annual and biennial tests may be completed during the testing season.

In the event a well is shut-in by the state for over production, the operator may produce the well for a period of time to secure a test after notification to the Division. All gas produced during this testing period will be used in determining the over/under produced status of the well.

C. <u>Deliverability Re-Tests</u>

An operator may, in cooperation with the gas transportation facility, schedule a well for a deliverability re-test upon notification to the Division's Aztec office at least ten days before the test is to be commenced. Such re-test shall be for good and substantial reason and shall be subject to the approval of the Division. Re-tests shall in all ways be conducted in conformance with the Annual and Biennial Deliverability Test Procedures of these rules. The Division, at its discretion, may require the re-testing of any well by notification to the operator to schedule such re-test. These tests as filed on Form C-122-A should be identified as "RETEST" in the remarks column.

SECTION 4: Witnessing of Tests

Any Initial Annual or Biennial Deliverability and Shut-In Pressure Test may be witnessed by any or all of the following: an agent of the Division, an offset operator, a representative of the gas transportation facility connected to the well under test, or a representative of the gas transportation facility taking gas from an offset operator.

CHAPTER II PROCEDURE FOR TESTING

SECTION 1: Initial Deliverability and Shut-In Pressure Test Procedure

- A. Within 90 days after a newly completed well is first delivered to a gas transportation facility, the operator shall complete a deliverability and shut-in pressure test of the well in conformance with the "Annual and Biennial Deliverability and Shut-In Pressure Test Procedures", prescribed in Section 2 of this chapter. Results of the test shall be filed as required by Section 1 of Chapter I of these rules.
- B. In the event it is impractical to test a newly completed well in conformance with Paragraph A above, the operator may conduct the deliverability and shut-in pressure test in the following manner (provided, however, that any test so conducted will not be accepted as the first annual deliverability and shut-in pressure test as described in Paragraph A-1 of Section 2, Chapter I):
 - 1. A 7-day or 8-day production chart may be used as the basis for determining the well's deliverability, providing the chart so used is preceded by at least 14 days continuous production. The well shall produce through either the casing or tubing, but not both, into a pipeline during these periods. The production valve and the choke settings shall not be changed during either the conditioning or flow period with the exception of the first ten (10) days of the conditioning period when maximum production would over-range the meter chart or location production equipment.
 - 2. A shut-in pressure of at least seven days duration shall be taken. This shall be the shut-in test required in Paragraph A, Section 1 of Chapter I of these rules.
 - 3. The average daily static meter pressure shall be determined in accordance with Section 2 of Chapter II of these rules. This pressure shall be used as P_t in calculating P_w for the Deliverability Calculation.
 - 4. The daily average rate of flow shall be determined in accordance with Section 2 of Chapter II.
 - 5. The static wellhead working pressure (P_w) shall be determined in accordance with Section 2 of Chapter II.

- 6. The deliverability of the well shall be determined by using the data determined in Paragraphs 1 through 5 above in the deliverability formula in accordance with Section 2 of Chapter II.
- The data and calculations for Paragraphs 1 through 6 above shall be reported as required in Section 1 of Chapter I of these rules, upon the blue-colored Form C-122-A or on white Form C-122-A and identified as "INITIAL TEST ONLY" in remarks.

SECTION 2: <u>Annual and Biennial Deliverability and Shut-In Pressure</u> <u>Test Procedure</u>

This test shall begin by producing a well in the normal operating manner into the pipeline through either the casing or tubing, but not both, for a period of fourteen consecutive days. This shall be known as the conditioning period. The production valve and choke settings shall not be changed during either the conditioning or flow periods except during the first ten (10) days of the conditioning period when maximum production would over-range the meter chart or location production equipment. The first ten (10) days of said conditioning period shall not have more than forty eight (48) hours of cumulative interruptions of flow. The eleventh to fourteenth days, inclusive, of said conditioning period shall have no interruptions of flow whatsoever. Any interruption of flow that occurs as normal operation of the well as stop-cock flow, intermittent flow, or well blow down will not be counted as shut-in time in either the conditioning or flow period.

The daily flowing rate shall be determined from an average of seven or eight consecutive producing days, following a minimum conditioning period of 14 consecutive days of production. This shall be known as the flow period.

Instantaneous pressures shall be measured by deadweight gauge or other method approved by the Division during the 7-day or 8-day flow period at the casinghead, tubinghead, and orifice meter, and shall be recorded along with instantaneous meter-chart static pressure reading.

If a well is producing through a compressor that is located between the wellhead and the meter run, the meter run pressure and the wellhead casing pressure and the wellhead tubing pressure are to be reported on Form C-122-A. (Neither the suction pressure nor the discharge pressure of the compressor is considered <u>wellhead</u> pressure.) A note shall be entered in the remarks portion on Form C-122-A stating "This well produces through a compressor". When it is necessary to restrict the flow of gas between the wellhead and orifice meter, the ratio of the downstream pressure, psia, to the upstream pressure, psia shall be determined. When this ratio is 0.57, or less, critical flow conditions shall be considered to exist across the restriction.

When more than one restriction between the wellhead and orifice meter causes the pressures to reflect critical flow between the wellhead and orifice meter, the pressures across each of these restrictions shall be measured to determine whether critical flow exists at any restriction. When critical flow does not exist at any restriction, the pressures taken to disprove critical flow shall be reported to the Division on Form C-122-A in item (n) of the form. When critical flow conditions exist, the instantaneous flowing pressures required hereinabove shall be measured during the last 48 hours of the 7-day or 8-day flow period.

When critical flow exists between the wellhead and orifice meter, the measured wellhead flowing pressure of the string through which the well flowed during test shall be used as P_t when calculating the static wellhead working pressure (P_W) using the method established below.

When critical flow does not exist at any restriction, P_t shall be the corrected average static pressure from the meter chart plus friction loss from the wellhead to the orifice meter.

The static wellhead working pressure (P_w) of any well under test shall be the calculated 7-day or 8-day average static tubing pressure if the well is flowing through the casing; it shall be the calculated 7-day or 8-day average static casing pressure if the well is flowing through the tubing. The static wellhead working pressure (P_w) shall be calculated by applying the tables and procedures set out in this manual.

To obtain the shut-in pressure of a well under test, the well shall be shut in some time during the current testing season for a period of seven to fourteen consecutive days, which have been preceded by a minimum of seven days of uninterrupted production. Such shut-in pressure shall be measured with a deadweight gauge or other method approved by the Division on the seventh to fourteenth day of shut-in of the well. The 7-day shut-in pressure shall be measured on both the tubing and the casing when communication exists between the two The higher of such pressures shall be used as P_C in the strinas. deliverability calculation. When any such shut-in pressure is determined by the Division to be abnormally low or the well can not be shut-in due to "HARDSHIP" classification, the shut-in pressure to be used as P_c shall be determined by one of the following methods:

- 1. A Division-designated value.
- 2. An average shut-in pressure of all offset wells completed in the same zone. Offset wells include the four side and four corner wells, if available.
- 3. A calculated surface pressure based on a calculated bottom-hole pressure. Such calculation shall be made in accordance with the examples in this manual.

All Wellhead pressures as well as the flowing meter pressure tests which are to be taken during the 7-day or 8-day deliverability test period as required hereinabove shall be taken with a deadweight gauge or other method approved by the Division. The pressure readings and the date and time according to the chart shall be recorded and maintained in the operator's records with the test information.

Orifice meter charts shall be changed and so arranged as to reflect upon a single chart the flow data for the gas from each well for the full 7-day or 8-day deliverability test period; however, no tests shall be voided if satisfactory explanation is made as to the necessity for using test volumes through two chart periods. Corrections shall be made for pressure base, measured flowing temperature, specific gravity, and supercompressibility; provided however, if the specific gravity of the gas from any well under test is not available, an estimated specific gravity may be assumed therefor, based upon that of gas from near-by wells, the specific gravity of which has been actually determined by measurement.

The average flowing meter pressure for the 7-day or 8-day flow period and the corrected integrated volume shall be determined by the purchasing company that integrates the flow charts and furnished to the operator or testing agency.

The 7-day or 8-day flow period volume shall be calculated from the integrated readings as determined from the flow period orifice meter chart. The volume so calculated shall be divided by the number of testing days on the chart to determine the average daily rate of flow during said flow period. The flow period shall have a minimum of seven and a maximum of eight legibly recorded flowing days to be acceptable for test purposes. The volume used in this calculation shall be corrected to New Mexico Oil Conservation Division standard conditions of 15.025 psia pressure base, $60^{\circ}F$. temperature base and 0.60 specific gravity base.

The daily volume of flow as determined from the flow period chart readings shall be calculated by applying the Basic Orifice Meter Formula or other acceptable industry standard practices.

$$Q = C' (h_w P_f) \cdot 5$$

Where:

- Q = Metered volume of flow Mcf/d @ 15.025 psia, 60⁰ F., and 0.60 specific gravity.
- C' = The 24-hour basic orifice meter flow factor corrected for flowing temperature, gravity, and supercompressibility.
- h_w = Daily average differential meter pressure from flow period chart.
- Pf = Daily average flowing meter pressure from flow period chart.

The basic orifice meter flow factors, flowing temperature factor, and specific gravity factor shall be determined from the tables in this manual.

The daily flow period average corrected flowing meter pressure, psig, shall be used to determine the supercompressibility factor. Supercompressibility Tables may be obtained from the New Mexico Oil Conservation Division.

When supercompressibility correction is made for a gas containing either nitrogen or carbon dioxide in excess of two percent, the supercompressibility factors of such gas shall be determined by the use of Table V of the C.N.G.A. Bulletin TS-402 for pressures 100-500 psig, or Table II, TS-461 for pressures in excess of 500 psig.

The use of tables for calculating rates of flow from integrator readings which do not specifically conform to the New Mexico Oil Conservation Division "Back Pressure Test Manual", or this manual, may be approved for determining the daily flow period rates of flow upon a showing that such tables are appropriate and necessary.

The daily average integrated rate of flow for the 7-day or 8-day flow period shall be corrected for meter error by multiplication by a correction factor. Said correction factor shall be determined by dividing the square root of the deadweight flowing meter pressure, psia, by the square root of the chart flowing meter pressure, psia. Deliverability pressure. as used herein. is a defined pressure applied to each well and used in the process of comparing the abilities of wells in a pool to produce at static wellhead working pressures equal to a percentage of the 7-day shut-in pressure of the respective individual wells. Such percentage shall be determined and announced periodically by the Division based on the relationship of the average static wellhead working pressures (P_w) divided by the average 7-day shut-in pressure (P_c) of the pool.

The deliverability of gas at the "deliverability pressure" of any well under test shall be calculated from the test data derived from the tests hereinabove required by use of the following deliverability formula:

$$D = Q \left[\frac{(P_c^2 - P_d^2)}{(P_c^2 - P_w^2)} \right]^n$$

Where:

D = Deliverability Mcf/d at the deliverability pressure, (Pd), (at Standard Conditions of 15.025 psia, $60^{\circ}F$ and 0.60 sp. gr.).

Q = Daily flow rate in Mcf/d, at wellhead pressure (P_w) .

- P_c = 7-day shut-in Wellhead pressure, psia, determined in accordance with Section 2 of Chapter II.
- P_d = Deliverability pressure, psia, as defined above.

Pw = Average static wellhead working pressure, as determined from 7-day or 8-day flow period, psia, and calculated from tables in this manual entitled "Pressure Loss Due to Friction" Tables for northwest New Mexico.

n = Average pool slope of back pressure curves as
 follows:

For Pictured Cliffs and shallower formations 0.85

For formations deeper than Pictured Cliffs 0.75

(Note: Special rules for any specific pool or formation may supersede the above values. Check special rules if in doubt.) The value of the multiplier in the above formula (ratio factor after the application of the pool slope) by which Q is multiplied shall not exceed a limiting value to be determined and announced periodically by the Division. Such determination shall be made after a study of the test data of the pool obtained during the previous testing season.

Downhole commingled wells are to be tested in year for pool of lowermost prorated completion of well and shall use pool slope (n), and deliverability pressure of lowermost pool. The total flow rate from the downhole commingled well will be used to calculate a value of deliverability. For each prorated gas zone of a downhole commingled well, a Form C-122-A is required to be filed and in the Summary portion of that form, all zones will indicate the same data for line h, P_c , Q, P_w , and P_d . The value shown for Deliverability (D) will be that percentage of the total deliverability of the well that is applicable to this zone. A note shall be placed in the remarks column that indicates the percentage of deliverability to be allocated to this zone of the well.

Any test prescribed herein will be considered acceptable if the average flow rate for the final 7-day or 8-day deliverability test is not more than ten percent in excess of any consecutive 7-day or 8-day average of the preceding two weeks. A deliverability test not meeting this requirement may be declared invalid, requiring the well to be re-tested.

All charts relative to initial, annual, or biennial deliverability tests or copies thereof shall be made available to the Division upon its request.

All testing agencies, whether individuals, companies, pipeline companies, or operators, shall maintain a log of all tests accomplished by them, including all field test data. The operator shall maintain the above data for a period of not less than two (2) years plus the current test year.

All forms heretofore mentioned are hereby adopted for use in the northwest New Mexico Area in open form subject to such modification as experience may indicate desirable or necessary.

Initial and Annual or Biennial Deliverability and Shut-In Pressure Tests for gas wells in all formations shall be conducted and reported in accordance with these rules and procedures. Provided however, these rules shall be subject to any specific modification or change contained in Special Pool Rules adopted for any pool after notice and hearing.

CHAPTER III INFORMATIONAL TESTS

A. A one-point back pressure test may be taken on newly completed wells before their connection or reconnection to a gas transportation facility. This test shall not be a required official test but may be taken for informational purposes at the option of the operator. When taken, this test must be taken and reported as prescribed below:

ONE-POINT BACK PRESSURE POTENTIAL TEST PROCEDURE

- 1. This test shall be accomplished after a minimum shut-in of seven days. The shut-in pressure shall be measured with a deadweight gauge or other method approved by the Division.
- The flow rate shall be that rate in Mcf/d measured at the end of a three hour test flow period. The flow from the well shall be for three hours through a positive choke, which has a 3/4-inch orifice.
- 3. A 2-inch nipple which provides a mechanical means of accurately measuring the pressure and temperature of the flowing gas shall be installed immediately upstream from the positive choke.
- 4. The absolute open flow shall be calculated using the conventional back pressure formula as shown in this manual or the New Mexico Oil Conservation Division "Back Pressure Test Manual."
- 5. The observed data and flow calculations shall be reported in duplicate on Form C-122, "Multi-Point Back Pressure Test for Gas Wells."
- 6. Non-critical flow shall be considered to exist when the choke pressure is 13 psig or less. When this condition exists the flow rate shall be measured with a pitot tube and nipple as specified in this manual or in the Division's Manual of "Tables and Procedure for Pitot Tests." The pitot test nipple shall be installed immediately downstream from the 3/4-inch positive choke.
- 7. Any well completed with 2-inch nominal size tubing (1.995-inch ID) or larger shall be tested through the tubing.
- B. Other tests for informational purposes may be conducted prior to obtaining a pipeline connection for a newly completed well upon receiving specific approval therefor from the Division's Aztec

office. Approval of these tests shall be based primarily upon the volume of gas to be vented.

CHAPTER IV TYPE OF TESTS REQUIRED FOR WELLS COMPLETED IN NON-PRORATED POOLS

SECTION 1: Initial Shut-In Pressure Tests for Newly Completed Wells

A. (Same as Chapter I, Section 1, A)

SECTION 2: Biennial Shut-In Pressure Tests

- A. Non-prorated wells will be tested biennially as required by the District Office except as follows:
 - 1. Wells which meet the "exempt" qualification as shown in Chapter I, Section 2, paragraph A-2 of these rules shall also be exempt from shut-in test requirements.
 - 2. Wells classified as "hardship" wells during the test year shall also be exempt from shut-in test requirements.
- B. All shut-in tests required by these rules must be filed with the Division's Aztec office by January 31 of the following year. Failure to file the test will subject the well to being shut-in one day for each day the test is late.

SECTION 3: <u>Scheduling Tests</u>

A. By September 1 of each year, the District Supervisor of the Aztec District Office of the Division shall by memorandum notify each gas transportation facility and each operator of the pools which are to be scheduled for biennial shut-in pressure testing during the following testing period from January 1 through the last day of December of that test year. The District Supervisor will also provide a list of "exempt" wells.

Any well scheduled for testing during its test year may have the test flow period, and some of the seven day shut-in period conducted in December of the previous year. The earliest date that a well could be scheduled for Biennial Shut-In Pressure Test would be such that the Test Flow Period would end on December 25 of the previous year. Downhole commingled wells are to be scheduled for tests on dates for pool of lowermost completion of well.

SECTION 4: <u>Test Procedure</u>

A. To obtain the shut-in pressure of a well under test, the well shall be shut-in some time during the current testing season for a period of seven to fourteen consecutive days, which have been preceded by a minimum of seven days of uninterrupted production. Such shut-in pressure shall be measured by deadweight gauge or other method approved by the Division on the seventh to fourteenth day of shut-in of the well. The shut-in pressure shall be measured on both the tubing and the casing when communication exists between the two strings. The higher of such pressures shall be reported as the shut-in pressure of the well.

SECTION 5: Filing of Shut-In Pressure Data

The result of this test shall be reported in the last column of Division Form C-125 showing the pressure in psia and shall be filed in triplicate with the Aztec District Office of the Division.





September 24, 1987 Date:

Enclosed is a copy of Order R--333-I printed on "minute" paper for Florene. Also enclosed is a copy of R-333-1 printed on continuous form for Mike. These were all printed on the same printer so that each page should be exactly alike. The last time I printed this order, the printer left 2 lines out of the finished text. A copy on the continuous form is also being sent to Frank.

This has all of the corrections in it that I have discussed with Frank and Mike.

I was talking with Frank and we were trying to put a radical sign in the formula on page 11 and it looked good on the screen but when the printer put it on paper it looked like this " ¿ " .. Now, how do you like that?

This reminds me of the guy who was suffering with apathy and paranoia... - he knew someone was out to get him, but, he just didn't care. (This person may be me.)

I was running all this through the printer and keyboard when all of a sudden --- all went blank and now Frank will have some pages extra like 2 attempts to print page 14 before the real thing came along.

I also may not get the brackets put on the formula on page 13 like they should be. I sure need to get them on Florene's copy before it goes out. Will try.

Tell me if this copy is good or not.

See you later.

Exhibit A Case No. 8586 Order No. R-333-I

RULES OF PROCEDURE FOR NORTHWEST NEW MEXICO

CHAPTER I TYPE OF TESTS REQUIRED FOR WELLS COMPLETED IN PRORATED GAS POOLS

SECTION 1: Initial Deliverability and Shut-In Pressure Tests for Newly Completed Well

- A. Immediately upon completion of each gas well in northwest New Mexico, a shut-in pressure test of at least seven days duration shall be made. This initial shut-in pressure shall be filed with the Division's Aztec Office on either Form C-122 or C-104.
- B. Within 90 days after a well first delivers gas to a gas transportation facility, the well shall have been tested in accordance with Section 1 of Chapter II of these rules, "Initial Deliverability and Shut-In Pressure Test Procedures", and the results of the test filed in triplicate with the Division's Aztec office and one copy filed with the gas transportation facility to which the well is connected. This test is to be filed on Form C-122-A. Failure to file said test within the above-prescribed 90-day period will subject the well to the loss of one day's allowable for each day the test is late.
 - 1. If the newly first delivered well is an infill well on a proration unit, the old well on the unit is not required to be tested provided it has a valid test on file for the current proration year. Testing of the old well follows the regularly assigned test year for the pool in which the wells are located. The new well is required to be tested annually until at least three annual tests are on file and then the well is to be tested biennially with other wells in that pool.
 - 2. If the newly first delivered well is an infill well on a proration unit and the old well on the

unit is "exempt", the old well is to be tested along with the new well for the Initial and Annual Deliverability and Shut-In Pressure Test. The old well will lose its "exempt" classification and must be tested biennially along with other wells in that pool. The new infill well is required to be tested annually until at least three annual tests are on file and then the well is to be tested biennially with other wells in that pool.

- C. The requirements for Initial Tests and Annual or Biennial Deliverability and Shut-In Pressure Tests and the notification requirements and scheduling of such tests which apply to newly completed wells shall also apply to recompleted wells.
- D. Any tests taken for informational purposes prior to pipeline connection shall not be recognized as official tests for the assignment of allowables.

SECTION 2. <u>Annual and Biennial Deliverability and Shut-In</u> <u>Pressure Tests</u>

- A. Annual or Biennial Deliverability and Shut-In Pressure Tests shall be made on all gas wells during the period from January 1 through December 31 of that year except as follows:
 - 1. A newly completed well or a recompleted well shall be tested on an annual basis until a minimum of three annual tests have been taken, after which the well shall be tested biennially as is required for other wells in the pool in which the well is located.
 - 2. Wells classified as "exempt" shall not be subject to the requirements of annual or biennial deliverability tests.

Classification of wells into or out of the "exempt" status shall be done once each year immediately following the reporting of June production and shall be effective for the succeeding annual test period. Gas wells completed in the Pictured Cliffs or any shallower formation shall be classified "exempt" if at least three months of production history is available and the well failed to produce, and is incapable of producing, an average of 250 MCF or more per month during the months produced within the preceding 12-month period, and the well is classified as marginal in the August Gas Proration Schedule.

Gas wells completed in any formation deeper than the Pictured Cliffs formation shall be classified "exempt" if at least three months of production history is available and the well failed to produce, and is incapable of producing, an average of 2000 MCF or more per month during the months produced within the preceding 12-month period, and the well is classified as marginal in the August Gas Proration Schedule.

Gas wells on multiple well Gas Proration Units will not be classified "exempt" unless the Gas Proration Unit is classified as marginal. Any or all wells on a marginal multiple well Gas Proration Unit may be classified as "exempt" provided each Gas Proration Unit so classified meets the qualification for "exempt" status. Gas Proration Units for wells producing from formations deeper than the Pictured Cliffs formation shall be classified "exempt" if at least three months of production history is available and the Gas Proration Unit failed to produce, and is incapable of producing, an average of 2000 MCF or more per month during the months produced within the preceding 12-month period, and the Gas Proration Unit is classified as marginal in the August Gas Proration Schedule. Gas Proration Units are to be classified as "exempt" because of their low producing ability.

The District Supervisor of the Division's Aztec Office may classify a well or Gas Proration Unit as "exempt" at any time if the operator presents sufficient evidence to the District Supervisor indicating that the well or Gas Proration Unit is incapable of producing gas at a higher rate than that rate required for "exempt" classification for wells or Gas Proration Units in that pool.

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Once a well or Gas Proration Unit has been declared "exempt" for the following test year, it shall remain classified "exempt" for that test year.

- 3. If a test is filed on any well on a gas proration unit, the test requirement for the gas proration unit has been met. The deliverability of the unit is taken only as the resulting sum of all wells tested.
- 4. A shut-in pressure must be filed on Form C-122-A even if no gas is measured during the production phase of the test. The filing of shut-in pressures for "exempt" wells is not required.
- B. All Annual and Biennial Deliverability and Shut-In Pressure Tests required by these rules must be filed with the Division's Aztec office and with the appropriate gas transportation facility within 90 days following the completion of each test. Provided however, that any test completed between October 31 of the test year and January 31 of the following year are due no later than January 31. No extension of time for filing tests beyond January 31 will be granted except after notice and hearing.

Failure to file any test within the above-prescribed times will subject the well to the loss of one day's allowable for each day the test is late. A well classified as marginal shall be shut-in one day for each day the test is late.

SECTION 3: Scheduling of Tests

A. Notification of Pools to be Tested

By September 1 of each year, the District Supervisor of the Aztec District Office of the Division shall by memorandum notify each gas transportation facility and each operator of the pools which are to be scheduled for biennial testing during the following testing period from January 1 through the last day of December of that test year. The District Supervisor will also provide a list of "exempt" wells and a list of wells that do not have a minimum of three Annual Deliverability and Shut-In Pressure Tests on file.

Any well scheduled for testing during its test year may have the conditioning period, test flow period, and some of the seven day shut-in period conducted in December of the previous year provided that if the 7 day shut-in period immediately follows the test flow period the 7 day shut-in pressure would be measured in January of the test year. The earliest date that a well could be scheduled for Annual or Biennial Deliverability and Shut-In Pressure Test would be such that the Test Flow Period would end on December 25 of the previous year.

Downhole commingled wells are to be scheduled for tests on dates for pool of the lowermost prorated completion of the well.

B. Annual and Biennial Deliverability Tests

By November 1 of each year, each gas transportation facility shall, in cooperation with the operators involved, prepare and submit a schedule of the wells to which it is connected which are to begin testing in December and January. Said schedule shall be entitled, "Annual and Biennial Deliverability and Shut-In Pressure Test Schedule", and one copy shall be submitted to the Division's Aztec office and to each operator concerned. The schedule shall indicate the date of tests, pool, operator, lease, well number, and location of each well.

At least 30 days prior to the beginning of each succeeding 2-month testing interval, a similar schedule shall be prepared and filed in accordance with the above.

The gas transportation facility and the Aztec District Office of the Division shall be notified immediately by any operator unable to conduct any test as scheduled.

In the event a well is not tested in accordance with the existing test schedule, the well shall be re-scheduled by the gas transportation facility, and the Division and the operator of the well so notified in writing. Every effort should be made to notify the Division of the new schedule prior to the conclusion of the newly assigned 14-day conditioning period.

Notice to the Division of Shut-In Pressure Tests which are scheduled at a time other than immediately following the flow test must be received prior to the time that the well is shut-in.

It shall be the responsibility of each operator to determine that all of its wells are properly scheduled for testing by the gas transportation facility to which they are connected, in order that all annual and biennial tests may be completed during the testing season.

In the event a well is shut-in by the state for over production, the operator may produce the well for a period of time to secure a test after notification to the Division. All gas produced during this testing period will be used in determining the over/under produced status of the well.

C. Deliverability Re-Tests

An operator may, in cooperation with the gas transportation facility, schedule a well for a deliverability re-test upon notification to the Division's Aztec office at least ten days before the test is to be commenced. Such re-test shall be for good and substantial reason and shall be subject to the approval of the Division. Re-tests shall in all ways be conducted in conformance with the Annual and Biennial Deliverability Test Procedures of these rules. The Division, at its discretion, may require the re-testing of any well by notification to the operator to schedule such re-test. These tests as filed on Form C-122-A should be identified as "RETEST" in the remarks column.

SECTION 4: Witnessing of Tests

Any Initial Annual or Biennial Deliverability and Shut-In Pressure Test may be witnessed by any or all of the following: an agent of the Division, an offset operator, a representative of the gas transportation facility connected to the well under test, or a representative of the gas transportation facility taking gas from an offset operator.

CHAPTER II PROCEDURE FOR TESTING

SECTION 1: Initial Deliverability and Shut-In Pressure Test Procedure

- A. Within 90 days after a newly completed well is first delivered to a gas transportation facility, the operator shall complete a deliverability and shut-in pressure test of the well in conformance with the "Annual and Biennial Deliverability and Shut-In Pressure Test Procedures", prescribed in Section 2 of this chapter. Results of the test shall be filed as required by Section 1 of Chapter I of these rules.
- B. In the event it is impractical to test a newly completed well in conformance with Paragraph A above, the operator may conduct the deliverability and shut-in pressure test in the following manner (provided, howev≥r, that any test so conducted will not be accepted as the first annual deliverability and shut-in pressure test as described in Paragraph A-1 of Section 2, Chapter I):
 - 1. A 7-day or 8-day production chart may be used as the basis for determining the well's deliverability, providing the chart so used is preceded by at least 14 days continuous production. The well shall produce through either the casing or tubing, but not both, into a pipeline during these periods. The production valve and the choke settings shall not be changed during either the conditioning or flow period with the exception of the first ten (10) days of the conditioning period when maximum production would over-range the meter chart or location production equipment.
 - 2. A shut-in pressure of at least seven days duration shall be taken. This shall be the shut-in test required in Paragraph A, Section 1 of Chapter I of these rules.
 - 3. The average daily static meter pressure shall be determined in accordance with Section 2 of Chapter II of these rules. This pressure shall be used as P_t in calculating P_w for the Deliverability Calculation.

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- The daily average rate of flow shall be determined in accordance with Section 2 of Chapter II.
- 5. The static wellhead working pressure (P_w) shall be determined in accordance with Section 2 of Chapter II.
- 6. The deliverability of the well shall be determined by using the data determined in Paragraphs 1 through 5 above in the deliverability formula in accordance with Section 2 of Chapter II.
- 7. The data and calculations for Paragraphs 1 through 6 above shall be reported as required in Section 1 of Chapter I of these rules, upon the blue-colored Form C-122-A or on white Form C-122-A and identified as "INITIAL TEST ONLY" in remarks.

SECTION 2: Annual and Biennial Deliverability and Shut-In Pressure Test Procedure

This test shall begin by producing a well in the normal operating manner into the pipeline through either the casing or tubing, but not both, for a period of fourteen consecutive days. This shall be known as the conditioning period. The production valve and choke settings shall not be changed during either the conditioning or flow periods except during the first ten (10) days of the conditioning period when maximum production would over-range the meter chart or location production equipment. The first ten (10) days of said conditioning period shall not have more than forty eight (48) hours of cumulative interruptions of flow. The eleventh to fourteenth days, inclusive, of said conditioning period shall have no interruptions of flow whatsoever. Any interruption of flow that occurs as normal operation of the well as stop-cock flow, intermittent flow, or well blow down will not be counted as shut-in time in either the conditioning or flow period.

The daily flowing rate shall be determined from an average of seven or eight consecutive producing days,

following a minimum conditioning period of 14 consecutive days of production. This shall be known as the flow period.

Instantaneous pressures shall be measured by deadweight gauge or other method approved by the Division during the 7-day or 8-day flow period at the casinghead, tubinghead, and orifice meter, and shall be recorded along with instantaneous meter-chart static pressure reading.

If a well is producing through a compressor that is located between the wellhead and the meter run, the meter run pressure and the wellhead casing pressure and the wellhead tubing pressure are to be reported on Form C-122-A. (Neither the suction pressure nor the discharge pressure of the compressor is considered wellhead pressure.) A note shall be entered in the remarks portion on Form C-122-A stating "This well produces through a compressor".

When it is necessary to restrict the flow of gas between the wellhead and orifice meter, the ratio of the downstream pressure, psia, to the upstream pressure, psia shall be determined. When this ratio is 0.57, or less, critical flow conditions shall be considered to exist across the restriction.

When more than one restriction between the wellhead and orifice meter causes the pressures to reflect critical flow between the wellhead and orifice meter, the pressures across each of these restrictions shall be measured to determine whether critical flow exists at any restriction. When critical flow does not exist at any restriction, the pressures taken to disprove critical flow shall be reported to the Division on Form C-122-A in item (n) of the form. When critical flow conditions exist, the instantaneous flowing pressures required hereinabove shall be measured during the last 48 hours of the 7-day or 8-day flow period.

When critical flow exists between the wellhead and orifice meter, the measured wellhead flowing pressure of the string through which the well flowed during test shall be used as P_t when calculating the static wellhead working pressure (P_w) using the method established below. When critical flow does not exist at any restriction, P_t shall be the corrected average static pressure from the meter chart plus friction loss from the wellhead to the orifice meter.

The static wellhead working pressure (P_w) of any well under test shall be the calculated 7-day or 8-day average static tubing pressure if the well is flowing through the casing; it shall be the calculated 7-day or 8-day average static casing pressure if the well is flowing through the tubing. The static wellhead working pressure (P_w) shall be calculated by applying the tables and procedures set out in this manual.

To obtain the shut-in pressure of a well under test, the well shall be shut in some time during the current testing season for a period of seven to fourteen consecutive days, which have been preceded by a minimum of seven days of uninterrupted production. Such shut-in pressure shall be measured with a deadweight gauge or other method approved by the Division on the seventh to fourteenth day of shut-in of the well. The 7-day shut-in pressure shall be measured on both the tubing and the casing when communication exists between the two strings. The higher of such pressures shall be used as P_{C} in the deliverability calculation. When any such shut-in pressure is determined by the Division to be abnormally low or the well can not be shut-in due to "HARDSHIP" classification, the shut-in pressure to be used as Pc shall be determined by one of the following methods:

1. A Division-designated value.

- An average shut-in pressure of all offset wells completed in the same zone. Offset wells include the four side and four corner wells, if available.
- 3. A calculated surface pressure based on a calculated bottom-hole pressure. Such calculation shall be made in accordance with the examples in this manual.

All Wellhead pressures as well as the flowing meter pressure tests which are to be taken during the 7-day or 8-day deliverability test period as required hereinabove shall be taken with a deadweight gauge or other method approved by the Division. The pressure readings and the date and time according to the chart shall be recorded and maintained in the operator's records with the test information.

Orifice meter charts shall be changed and so arranged as to reflect upon a single chart the flow data for the gas from each well for the full 7-day or 8-day deliverability test period; however, no tests shall be voided if satisfactory explanation is made as to the necessity for using test volumes through two chart periods. Corrections shall be made for pressure base, measured flowing temperature, specific gravity, and supercompressibility; provided however, if the specific gravity of the gas from any well under test is not available, an estimated specific gravity may be assumed therefor, based upon that of gas from near-by wells, the specific gravity of which has been actually determined by measurement.

The average flowing meter pressure for the 7-day or 8-day flow period and the corrected integrated volume shall be determined by the purchasing company that integrates the flow charts and furnished to the operator or testing agency.

The 7-day or 8-day flow period volume shall be calculated from the integrated readings as determined from the flow period orifice meter chart. The volume so calculated shall be divided by the number of testing days on the chart to determine the average daily rate of flow during said flow period. The flow period shall have a minimum of seven and a maximum of eight legibly recorded flowing days to be acceptable for test purposes. The volume used in this calculation shall be corrected to New Mexico Oil Conservation Division standard conditions of 15.025 psia pressure base, 60°F. temperature base and 0.60 specific gravity base.

The daily volume of flow as determined from the flow period chart readings shall be calculated by applying the Basic Orifice Meter Formula or other acceptable industry standard practices.

 $Q = C' (h_w P_f)^{5}$

Where:

- Q = Metered volume of flow Mcf/d @ 15.025 psia, 60° F., and 0.60 specific gravity.
- C' = The 24-hour basic orifice meter flow factor corrected for flowing temperature, gravity, and supercompressibility.
- h_w = Daily average differential meter pressure
 from flow period chart.
- Pf = Daily average flowing meter pressure from flow period chart.

The basic orifice meter flow factors, flowing temperature factor, and specific gravity factor shall be determined from the tables in this manual.

The daily flow period average corrected flowing meter pressure, psig, shall be used to determine the supercompressibility factor. Supercompressibility Tables may be obtained from the New Mexico Oil Conservation Division.

When supercompressibility correction is made for a gas containing either nitrogen or carbon dioxide in excess of two percent, the supercompressibility factors of such gas shall be determined by the use of Table V of the C.N.G.A. Bulletin TS-402 for pressures 100-500 psig, or Table II, TS-461 for pressures in excess of 500 psig.

The use of tables for calculating rates of flow from integrator readings which do not specifically conform to the New Mexico Oil Conservation Division "Back Pressure Test Manual", or this manual, may be approved for determining the daily flow period rates of flow upon a showing that such tables are appropriate and necessary.

The daily average integrated rate of flow for the 7-day or 8-day flow period shall be corrected for meter error by multiplication by a correction factor. Said correction factor shall be determined by dividing the square root of the deadweight flowing meter pressure, psia, by the square root of the chart flowing meter pressure, psia. Deliverability pressure, as used herein, is a defined pressure applied to each well and used in the process of comparing the abilities of wells in a pool to produce at static wellhead working pressures equal to a percentage of the 7-day shut-in pressure of the respective individual wells. Such percentage shall be determined and announced periodically by the Division based on the relationship of the average static wellhead working pressures (P_w) divided by the average 7-day shut-in pressure (P_c) of the pool.

The deliverability of gas at the "deliverability pressure" of any well under test shall be calculated from the test data derived from the tests hereinabove required by use of the following deliverability formula:

$$D = Q \left[\frac{(P_{c}^{2} - P_{d}^{2})}{(P_{c}^{2} - P_{w}^{2})} \right]^{n}$$

Where:

- D = Deliverability Mcf/d at the deliverability pressure, (P_d), (at Standard Conditions of 15.025 psia, 60° F and 0.60 sp. gr.).
- Q = Daily flow rate in Mcf/d, at wellhead pressure (P_w).
- P_C = 7-day shut-in Wellhead pressure, psia, determined in accordance with Section 2 of Chapter II.
- P_d = Deliverability pressure, psia, as defined above.
- P_w = Average static wellhead working pressure, as determined from 7-day or 8-day flow period, psia, and calculated from tables in this manual entitled "Pressure Loss Due to Friction" Tables for northwest New Mexico.
- n = Average pool slope of back pressure curves
 as follows:

For Pictured Cliffs and shallower formations 0.85

For formations deeper than Pictured Cliffs 0.75

(Note: Special rules for any specific pool or formation may supersede the above values. Check special rules if in doubt.)

The value of the multiplier in the above formula (ratio factor after the application of the pool slope) by which Q is multiplied shall not exceed a limiting value to be determined and announced periodically by the Division. Such determination shall be made after a study of the test data of the pool obtained during the previous testing season.

Downhole commingled wells are to be tested in year for pool of lowermost prorated completion of well and shall use pool slope (n), and deliverability pressure of lowermost pool. The total flow rate from the downhole commingled well will be used to calculate a value of deliverability. For each prorated gas zone of a downhole commingled well, a Form C-122-A is required to be filed and in the Summary portion of that form, all zones will indicate the same data for line h, P_C , Q, P_W , and P_d . The value shown for Deliverability (D) will be that percentage of the total deliverability of the well that is applicable to this zone. A note shall be placed in the remarks column that indicates the percentage of deliverability to be allocated to this zone of the well.

Any test prescribed herein will be considered acceptable if the average flow rate for the final 7-day or 8-day deliverability test is not more than ten percent in excess of any consecutive 7-day or 8-day average of the preceding two weeks. A deliverability test not meeting this requirement may be declared invalid, requiring the well to be re-tested.

All charts relative to initial, annual, or biennial deliverability tests or copies thereof shall be made available to the Division upon its request.

All testing agencies, whether individuals, companies, pipeline companies, or operators, shall maintain a log of all tests accomplished by them, including all field test data. The operator shall maintain the above data for a period of not less than two (2) years plus the current test year.

All forms heretofore mentioned are hereby adopted for use in the northwest New Mexico Area in open form subject to such modification as experience may indicate desirable or necessary.

Initial and Annual or Biennial Deliverability and Shut-In Pressure Tests for gas wells in all formations shall be conducted and reported in accordance with these rules and procedures. Provided however, these rules shall be subject to any specific modification or change contained in Special Pool Rules adopted for any pool after notice and hearing.

CHAPTER III INFORMATIONAL TESTS

A. A one-point back pressure test may be taken on newly completed wells before their connection or reconnection to a gas transportation facility. This test shall not be a required official test but may be taken for informational purposes at the option of the operator. When taken, this test must be taken and reported as prescribed below:

ONE-POINT BACK PRESSURE POTENTIAL TEST PROCEDURE

- This test shall be accomplished after a minimum shut-in of seven days. The shut-in pressure shall be measured with a deadweight gauge or other method approved by the Division.
- 2. The flow rate shall be that rate in Mcf/d measured at the end of a three hour test flow period. The flow from the well shall be for three hours through a positive choke, which has a 3/4-inch orifice.
- 3. A 2-inch nipple which provides a mechanical means of accurately measuring the pressure and

temperature of the flowing gas shall be installed immediately upstream from the positive choke.

- 4. The absolute open flow shall be calculated using the conventional back pressure formula as shown in this manual or the New Mexico Oil Conservation Division "Back Pressure Test Manual."
- 5. The observed data and flow calculations shall be reported in duplicate on Form C-122, "Multi-Point Back Pressure Test for Gas Wells."
- 6. Non-critical flow shall be considered to exist when the choke pressure is 13 psig or less. When this condition exists the flow rate shall be measured with a pitot tube and nipple as specified in this manual or in the Division's Manual of "Tables and Procedure for Pitot Tests." The pitot test nipple shall be installed immediately downstream from the 3/4-inch positive choke.
- 7. Any well completed with 2-inch nominal size tubing (1.995-inch ID) or larger shall be tested through the tubing.
- B. Other tests for informational purposes may be conducted prior to obtaining a pipeline connection for a newly completed well upon receiving specific approval therefor from the Division's Aztec office. Approval of these tests shall be based primarily upon the volume of gas to be vented.
- CHAPTER IV TYPE OF TESTS REQUIRED FOR WELLS COMPLETED IN NON-PRORATED POOLS
- SECTION 1: Initial Shut-In Pressure Tests for Newly Completed Wells
- A. (Same as Chapter I, Section 1, A)
- SECTION 2: Biennial Shut-In Pressure Tests

- A. Non-prorated wells will be tested biennially as required by the District Office except as follows:
 - 1. Wells which meet the "exempt" qualification as shown in Chapter I, Section 2, paragraph A-2 of these rules shall also be exempt from shut-in test requirements.
 - Wells classified as "hardship" wells during the test year shall also be exempt from shut-in test requirements.
- B. All shut-in tests required by these rules must be filed with the Division's Aztec office by January 31 of the following year. Failure to file the test will subject the well to being shut-in one day for each day the test is late.

SECTION 3: Scheduling Tests

A. By September 1 of each year, the District Supervisor of the Aztec District Office of the Division shall by memorandum notify each gas transportation facility and each operator of the pools which are to be scheduled for biennial shut-in pressure testing during the following testing period from January 1 through the last day of December of that test year. The District Supervisor will also provide a list of "exempt" wells.

Any well scheduled for testing during its test year may have the test flow period, and some of the seven day shut-in period conducted in December of the previous year. The earliest date that a well could be scheduled for Biennial Shut-In Pressure Test would be such that the Test Flow Period would end on December 25 of the previous year.

Downhole commingled wells are to be scheduled for tests on dates for pool of lowermost completion of well.

SECTION 4: Test Procedure

A. To obtain the shut-in pressure of a well under test, the well shall be shut-in some time during the current testing season for a period of seven to fourteen consecutive days, which have been preceded by a minimum of seven days of uninterrupted production. Such shut-in pressure shall be measured by deadweight gauge or other method approved by the Division on the seventh to fourteenth day of shut-in of the well. The shut-in pressure shall be measured on both the tubing and the casing when communication exists between the two strings. The higher of such pressures shall be reported as the shut-in pressure of the well.

SECTION 5: Filing of Shut-In Pressure Data

The result of this test shall be reported in the last column of Division Form C-125 showing the pressure in psia and shall be filed in triplicate with the Aztec District Office of the Division.
MEMORANDUM

To: NMOCD

From: H. L. Babe

Date: August 14, 1987

Here is my attempt at putting this "Exhibit A" on minute paper. This is my first attempt at such an endeavor. I hope this works.

I arn enclosing 2 different prints of this exhibit. The first print that I ran was quite light from an old ribbon that was new when I put it on the machine. Today we searched the company and found some more ribbons and made another run of this paper and obtained some darker prints.

If for any reason this needs to be done over, or any part of it done over, let me know and I think it can be done easily without having to call the Governor's office.

Hopefully most of the words are spelled correctly. (I'm sure glad this was written many days ago because today the keys on the typewriter are in different places and some words look terrible this morning.)

I am sending the finished pages for Florene, the long page of report for Mike and I am also sending a like print of Mike's to Frank in Aztick.

I'll be waiting for your call for corrections.

P. S. Frank, for our test book, I think this 18 pages looks great when done in "justify" (with smooth margins on the left and right sides). I think I can do that in short order also. Any problems? STATE OF NEW MEXICO

ENERGY AND MINERALS DEPARTMENT

OIL CONSERVATION DIVISION



-

GARREY CARRUTHERS

POST OFFICE BOX 2088 STATE LAND OFFICE BUILDING SANTA FE, NEW MEXICO 87501 (505) 827-5800

MEMORANDUM

- TO: Frank Chaves, District Supervisor
 Vic Lyon, Engineering Bureau Chief
 William J. LeMay, Director
 Jeff Taylor, General Counsel
 H.L. (Babe) Kendrick, El Paso Natural Gas Co.
- FROM: Michael E. Stogner, Chief Hearing Officer
- SUBJECT: Gas Well Testing Procedures for Northwest New Mexico.
- DATE: August 11, 1987

pixe

Attached is a copy of the proposed order for Case No. 8586, heard on May 8, 1985 and December 1986. Please make any corrections and/or changes that you feel are necessary and return them to me so that an Order may then be issued. Once this Order is finalized the new testing manual will be ready for final review. Thank you for your assistance in this matter.

STATE OF NEW MEXICO

ENERGY, MINERALS AND NATURAL RESOURCES DEPARTMENT OIL CONSERVATION DIVISION

CASE NO: 8586

ORDER NO: R-333-I

IN THE MATTER OF THE HEARING CALLED BY THE OIL CONSERVATION DIVISION ON ITS OWN MOTION FOR RECISION OF DIVISION ORDER No. R-333, AS AMENDED, AND FOR RECODIFICATION AND REISSUANCE OF GAS WELL TESTING PROCEDURES FOR NORTHWEST NEW MEXICO. APPLICANT FURTHER SEEKS AN EXTENSION OF THE 1986 TESTING PERIOD AND SUSPENSION OF THE 1987 TESTING PERIOD. MCKINLEY, RIO ARRIBA, SANDOVAL, AND SAN JUAN COUNTIES, NEW MEXICO.

BY THE DIVISION:

This cause came on for hearing at 8:00 a.m. on May 8, 1985, and at 8:15 a.m. on December 3, 1986, in Santa Fe,

Page 2 Case No. 8586 Order No. R-333-I

New Mexico, before Examiners Gilbert P. Quintana and Michael E. Stogner, respectively.

NOW, on this _____ day of July, 1987, the Division Director, having considered the testimony, the record, and the recommendations of the Examiners, and being fully advised in the premises,

FINDS THAT:

(1) Due public notice having been given as required by law, the Division has jurisdiction of this cause and the subject matter thereof.

(2) The applicant in the instant case seeks to rescind Division Order No. R-333, as amended, and to recodify and amend the Special Rules and Regulations for the testing of gas wells in Northwest New Mexico contained therein.

(3) Special rules and regulations for the testing f gas wells in McKinley, Rio Arriba, Sandoval, and San Juan Counties, New Mexico, (Northwest New Mexico) have been adopted and amended by the Division and are embodied in Division Order R-333, as amended.

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(4) These existing rules and regulations relating to gas well testing procedures in Northwest New Mexico have been adopted over many years and are collected in numerous orders, therefore, making reference to them somewhat difficult.

(5) In addition some of the gas well testing procedures are out-dated and in need of revision.

(6) Because of the need to review these rules relating to gas well testing in Northwest New Mexico, the Division Director at that time appointed a committee to study the existing rules and to recommend changes.

(7) Harold L. Kendrick, Chairman of the Deliverability Test Committee, appeared on its behalf at the May 8, 1985 (at which time it was taken under advisement, however no order was issued) and December 3, 1987 examiner hearings and made the following recommendations regarding gas well testing procedures in Northwest New Mexico:

> (a) recodifying the rules and issuing them as the "Gas Well Testing Manual for Northwest New Mexico";

Page 4 Case No. 8586 Order No. R-333-I

- (b) to require deliverability testing in prorated gas pools on a biennial (every two years) basis;
- (c) to require biennial shut-in pressures in non-prorated gas pools with no deliverability testing;
- (d) the deliverability test year should be the same as the calendar year.
- (e) exemption from deliverability testing in the Blanco-Mesaverde Pool and Basin-Dakota Pool should be based upon the combined producibility of all wells on a gas proration unit;
- (f) wells shut-in for over production should be permitted to be produced for deliverability test purposes after the operator notifies the Division District office;
- (g) restriction on flow interruptions during the conditioning period should be eased slightly;

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Page 5 Case No. 8586 Order No. R-333-I

- (h) the 7-day shut in pressure should be permitted to be measured at a time during the current testing season other than immediately following the test flow period;
- (i) deliverability pressure (Pd) assigned as a percentage of the 7-day shut-in pressure should be adjusted in each pool to more nearly approximate the pool average operating conditions;
- (j) The 7-day shut-in pressure for wells in non-prorated gas pools should be filed with the Division on proposed Form C-125-A; and
- (j) All required tables should be included in the manual.

(8) All of the above proposals are embodied in Exhibit "A" attached hereto and made a part thereof.

(9) A manual for well testing as set out in said supplemental exhibit should be adopted.

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(10) Division Order No. R-333 as amended should be rescinded, in its entirety, and a new order designated R-333-I should be promulgated.

(11) It is further sought in this Case to extend the deadline for completing and filing 1986 deliverability tests to March 31, 1987, and for a one year suspension of biennial deliverability testing whereby the deliverability test cycle will begin again in 1988 with those pools which would have been tested in 1987.

(12) No testimony was received in opposition to this request.

(13) Approval of this application is in the best interest of conservation and will not cause waste nor impair correlative rights.

IT IS THEREFORE ORDERED THAT:

(1) Effective ______, the Special Rules and Regulations governing gas well testing in Northwest New Mexico, which includes McKinley, Rio Arriba, Sandoval and San Juan Counties, New Mexico, as described in Exhibit "A" attached hereto and made a part hereof, superseding the rules and regulations contained in its Page 7 Case No. 8586 Order No. R-333-I

entirety in Division Order No. R-333, as amended, are hereby promulgated and adopted as an exception to Rules 401 and 402 of the general statewide rules and regulations of this Division relating to gas well testing procedures.

(2) The deadline for completing and filing 1986 deliverability tests is hereby extended to March 31, 1987.

(3) A one year suspension of biennial deliverability testing whereby the deliverablity test cycle will begin again in 1988 with those pools which would have been tested in 1987.

(4) Jurisdiction of this cause is retained for the entry of such further orders as the Division may deem necessary.

DONE, at Santa Fe, New Mexico, on the day and year hereinabove designated.

STATE OF NEW MEXICO OIL CONSERVATION DIVISION Page 8 Case No. 8586 Order No. R-333-I

WILLIAM J. LEMAY

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Director

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EXF	IBII	r "A"	
CASE	NO.	8586	
ORDER	NO.	R-333-	I

RULES OF PROCEDURE FOR NORTHWEST NEW MEXICO

CHAPTER I <u>TYPE OF TESTS REQUIRED FOR WELLS COMPLETED IN PRORATED</u> GAS POOLS

SECTION 1: Initial Deliverability and Shut-In Pressure Tests for Newly Completed Well

- A. Immediately upon completion of each gas well in northwest New Mexico, a shut-in pressure test of at least seven days duration shall be made. This initial shut-in pressure shall be filed with the Division's Aztec Office on either Form C-122 or C-104.
- B. Within 90 days ater a well first delivers gas to a gas transportation facility, the well shall have been tested in accordance with Section 1 of Chapter II of these rules, "Initial Deliverability and Shut-In Pressure Test Procedures", and the results of the test filed in triplicate with the Division's Aztec office and one copy filed with the gas transportation facility to which the well is connected. This test is to be filed on Form C-122-A. Failure to file said test within the above-prescribed 90-day period will subject the well to the loss of one day's allowable for each day the test is late.
 - 1. If the newly first delivered well is an infill well on a proration unit, the old well on the unit is not required to be tested provided it has a valid test on file for the current proration year. Testing of the old well follows the regularly assigned test year for the pool in which the wells are located. The new well is required to be tested annually until at least three annual tests are on file and then the well is to be tested biennially with other wells in that pool.
 - 2. If the newly first delivered well is an infill well on a proration unit and the old well on the unit is "exempt", the old well is to be tested along with the new well for the Initial and Annual Deliverability and Shut-In Pressure Test. The old well will lose its "exempt" classification and must be tested biennially along with other wells in that pool. The new infill well is required to be tested annually until at least three annual tests are on file and then the well is to be tested biennially with other wells in that pool.

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C. The requirements for Initial Tests and Annual or Biennial Deliverability and Shut-In Pressure Tests and the notification requirements and scheduling of such tests which apply to newly completed wells shall also apply to recompleted wells. 1

D. Any tests taken for informational purposes prior to pipeline connection shall not be recognized as official tests for the assignment of allowables.

SECTION 2. <u>Annual and Biennial Deliverability and Shut-In Pressure</u> <u>Tests</u>

- A. Annual or Biennial Deliverability and Shut-In Pressure Tests shall be made on all gas wells during the period from January 1 through December 31 of that year except as follows:
 - 1. A newly completed well or a recompleted well shall be tested on an annual basis until a minimum of three annual tests have been taken, after which the well shall be tested biennially as is required for other wells in the pool in which the well is located.
 - 2. Wells classified as "exempt" shall not be subject to the requirements of annual or biennial deliverability tests.

Classification of wells into or out of the "exempt" status shall be done once each year immediately following the reporting of June production and shall be effective for the succeeding annual test period.

Gas wells completed in the Pictured Cliffs or any shallower formation shall be classified "exempt" if at least three months of production history is available and the well failed to produce, and is incapable of producing, an average of 250 MCF or more per month during the months produced within the preceding 12-month period, and the well is classified as marginal in the August Gas Proration Schedule.

Gas wells completed in any formation deeper than the Pictured Cliffs formation shall be classified "exempt" if at least three months of production history is available and the well failed to produce, and is incapable of producing, an average of 2000 MCF or more per month during the months produced within the preceding 12-month period, and the well is classified as marginal in the August Gas Proration Schedule.

Gas wells on multiple well Gas Proration Units will not be classified "exempt" unless the Gas Proration Unit is classified as marginal. Any or all wells on a marginal multiple well Gas Proration Unit may be classified as "exempt" provided each Gas Proration Unit so classified meets the qualification for "exempt" status. Gas Proration Units for wells producing from formations deeper than the Pictured Cliffs formation shall be classified "exempt" if at least three months of production history is available and the Gas Proration Unit failed to produce, and is incapable of producing, an average of 2000 MCF or more per month during the months produced within the preceding 12-month period, and the Gas Proration Unit is classified as marginal in the August Gas Proration Schedule. Gas Proration Units are to be classified as "exempt" because of their low producing ability.

The District Supervisor of the Division's Aztec Office may classify a well or Gas Proration Unit as "exempt" at any time if the operator presents sufficient evidence to the District Supervisor indicating that the well or Gas Proration Unit is incapable of producing gas at a higher rate than that rate required for "exempt" classification for wells or Gas Proration Units in that pool.

Once a well or Gas Proration Unit has been declared "exempt" for the following test year, it shall remain classified "exempt" for that test year.

- 3. If a test is filed on any well on a gas proration unit, the test requirement for the gas proration unit has been met. The deliverability of the unit is taken only as the resulting sum of all wells tested.
- 4. A shut-in pressure must be filed on Form C-122-A even if no gas is measured during the production phase of the test. "Exempt" wells do not require the filing of a shut-in pressure.
- B. All Annual and Biennial Deliverability and Shut-In Pressure Tests required by these rules must be filed with the Division's Aztec office and with the appropriate gas transportation facility within 90 days following the completion of each test. Provided however, that any test completed between October 31 of the test year and January 31 of the following year are due no later than January 31. No extension of time for filing tests beyond January 31 will be granted except after notice and hearing.

Failure to file any test within the above-prescribed times will subject the well to the loss of one day's allowable for each day the test is late. A well classified as marginal shall be shut-in one day for each day the test is late.

SECTION 3: <u>Scheduling of Tests</u>

A. Notification of Pools to be Tested

By September 1 of each year, the District Supervisor of the Aztec District Office of the Division shall by memorandum notify each gas transportation facility and each operator of the pools which are to be scheduled for biennial testing during the following testing period from January 1 through the last day of December of that test year. The District Supervisor will also provide a list of "exempt" wells and a list of wells that do not have a minimum of three Annual Deliverability and Shut-In Pressure Tests on file.

Any well scheduled for testing during its test year may have the conditioning period, test flow period, and some of the seven day shut-in period conducted in December of the previous year provided that if the 7 day shut-in period immediately follows the test flow period the 7 day shut-in pressure would be measured in January of the test year. The earliest date that a well could be scheduled for Annual or Biennial Deliverability and Shut-In Pressure Test would be such that the Test Flow Period would end on December 25 of the previous year.

Downhole commingled wells are to be scheduled for tests on dates for pool of lowermost prorated completion of well.

B. <u>Annual and Biennial Deliverability Tests</u>

By November 1 of each year, each gas transportation facility shall, in cooperation with the operators involved, prepare and submit a schedule of the wells to which it is connected which are to begin testing in December and January. Said schedule shall be entitled, "Annual and Biennial Deliverability and Shut-In Pressure Test Schedule", and one copy shall be submitted to the Division's Aztec office and to each operator concerned. The schedule shall indicate the date of tests, pool, operator, lease, well number, and location of each well.

At least 30 days prior to the beginning of each succeeding 2-month testing interval, a similar schedule shall be prepared and filed in accordance with the above.

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The gas transportation facility and the Aztec District Office of the Division shall be notified immediately by any operator unable to conduct any test as scheduled.

In the event a well is not tested in accordance with the existing test schedule, the well shall be re-scheduled by the gas transportation facility, and the Division and the operator of the well so notified in writing. Every effort should be made to notify the Division of the new schedule prior to the conclusion of the newly assigned 14-day conditioning period.

Notice to the Division of Shut-In Pressure Tests which are scheduled at a time other than immediately following the flow test must be received prior to the time that the well is shut-in.

It shall be the responsibility of each operator to determine that all of its wells are properly scheduled for testing by the gas transportation facility to which they are connected, in order that all annual and biennial tests may be completed during the testing season.

In the event a well is shut-in by the state for over production, the operator may produce the well for a period of time to secure a test after notification to the Division. All gas produced during this testing period will be used in determining the over/under produced status of the well.

C. <u>Deliverability Re-Tests</u>

An operator may, in cooperation with the gas transportation facility, schedule a well for a deliverability re-test upon notification to the Division's Aztec office at least ten days before the test is to be commenced. Such re-test shall be for good and substantial reason and shall be subject to the approval of the Division. Re-tests shall in all ways be conducted in conformance with the Annual and Biennial Deliverability Test Procedures of these rules. The Division, at its discretion, may require the re-testing of any well by notification to the operator to schedule such re-test. These tests as filed on Form C-122-A should be identified as "RETEST" in the remarks column.

SECTION 4: <u>Witnessing of Tests</u>

Any Initial Annual or Biennial Deliverability and Shut-In Pressure Test may be witnessed by any or all of the following: an agent of the Division, an offset operator, a representative of the gas transportation facility connected to the well under test, or a representative of the gas transportation facility taking gas from an offset operator.

CHAPTER II PROCEDURE FOR TESTING

SECTION 1: Initial Deliverability and Shut-In Pressure Test Procedure

- A. Within 90 days after a newly completed well is first delivered to a gas transportation facility, the operator shall complete a deliverability and shut-in pressure test of the well in conformance with the "Annual and Biennial Deliverability and Shut-In Pressure Test Procedures", prescribed in Section 2 of this chapter. Results of the test shall be filed as required by Section 1 of Chapter I of these rules.
- B. In the event it is impractical to test a newly completed well in conformance with Paragraph A above, the operator may conduct the deliverability and shut-in pressure test in the following manner (provided, however, that any test so conducted will not be accepted as the first annual deliverability and shut-in pressure test as described in Paragraph A-1 of Section 2, Chapter I):
 - 1. A 7-day or 8-day production chart may be used as the basis for determining the well's deliverability, providing the chart so used is preceded by at least 14 days continuous production. The well shall produce through either the casing or tubing, but not both, into a pipeline during these periods. The production valve and the choke settings shall not be changed during either the conditioning or flow period with the exception of the first ten (10) days of the conditioning period when maximum production would over-range the meter chart or location production equipment.
 - 2. A shut-in pressure of at least seven days duration shall be taken. This shall be the shut-in test required in Paragraph A, Section 1 of Chapter I of these rules.
 - 3. The average daily static meter pressure shall be determined in accordance with Section 2 of Chapter II of these rules. This pressure shall be used as P_t in calculating P_w for the Deliverability Calculation.
 - 4. The daily average rate of flow shall be determined in accordance with Section 2 of Chapter II.

- 5. The static wellhead working pressure (P_w) shall be determined in accordance with Section 2 of Chapter II.
- 6. The deliverability of the well shall be determined by using the data determined in Paragraphs 1 through 5 above in the deliverability formula in accordance with Section 2 of Chapter II.
- 7. The data and calculations for Paragraphs 1 through 6 above shall be reported as required in Section 1 of Chapter I of these rules, upon the blue-colored Form C-122-A or on white Form C-122-A and write "INITIAL TEST ONLY" in remarks.

SECTION 2: <u>Annual and Biennial Deliverability and Shut-In Pressure</u> <u>Test Procedure</u>

This test shall begin by producing a well in the normal operating manner into the pipeline through either the casing or tubing, but not both, for a period of fourteen consecutive days. This shall be known as the conditioning period. The production valve and choke settings shall not be changed during either the conditioning or flow periods except during the first ten (10) days of the conditioning period when maximum production would over-range the meter chart or location production equipment. The first ten (10) days of said conditioning period shall not have more than forty eight (48) hours of cumulative interruptions of flow. The eleventh to fourteenth days, inclusive, of said conditioning period shall have no interruptions of flow whatsoever. Any interruption of flow that occurs as normal operation of the well as stop-cock flow, intermittent flow, or well blow down will not be counted as shut-in time in either the conditioning or flow period.

The daily flowing rate shall be determined from an average of seven or eight consecutive producing days, following a minimum conditioning period of 14 consecutive days of production. This shall be known as the flow period.

Instantaneous pressures shall be measured by deadweight gauge or other method approved by the Division during the 7-day or 8-day flow period at the casinghead, tubinghead, and orifice meter, and shall be recorded along with instantaneous meter-chart static pressure reading.

If a well is producing through a compressor that is located between the wellhead and the meter run, the meter run pressure and the wellhead casing pressure and the wellhead tubing pressure are to be reported on Form C-122-A. (Neither the suction pressure nor

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the discharge pressure of the compressor is considered <u>wellhead</u> pressure.) A note shall be entered in the remarks portion on Form C-122-A stating "This well produces through a compressor".

When it is necessary to restrict the flow of gas between the wellhead and orifice meter, the ratio of the downstream pressure, psia, to the upstream pressure, psia shall be determined. When this ratio is 0.57, or less, critical flow conditions shall be considered to exist across the restriction.

When more than one restriction between the wellhead and orifice meter causes the pressures to reflect critical flow between the wellhead and orifice meter, the pressures across each of these restrictions shall be measured to determine whether critical flow exists at any restriction. When critical flow does not exist at any restriction, the pressures taken to disprove critical flow shall be reported to the Division on Form C-122-A in item (n) of the form. When critical flow conditions exist, the instantaneous flowing pressures required hereinabove shall be measured during the last 48 hours of the 7-day or 8-day flow period.

When critical flow exists between the wellhead and orifice meter, the measured wellhead flowing pressure of the string through which the well flowed during test shall be used as P_t when calculating the static wellhead working pressure (P_W) using the method established below.

When critical flow does not exist at any restriction, P_t shall be the corrected average static pressure from the meter chart plus friction loss from the wellhead to the orifice meter.

The static wellhead working pressure (P_W) of any well under test shall be the calculated 7-day or 8-day average static tubing pressure if the well is flowing through the casing; it shall be the calculated 7-day or 8-day average static casing pressure if the well is flowing through the tubing. The static wellhead working pressure (P_W) shall be calculated by applying the tables and procedures set out in this manual.

To obtain the shut-in pressure of a well under test, the well shall be shut in some time during the current testing season for a period of seven to fourteen consecutive days, which have been preceded by a minimum of seven days of uninterrupted production. Such shut-in pressure shall be measured with a deadweight gauge or other method approved by the Division on the seventh to fourteenth day of shut-in of the well. The 7-day shut-in pressure shall be measured on both the tubing and the casing when communication exists between the two strings. The higher of such pressures shall be used as P_C in the deliverability calculation. When any such shut-in pressure is determined by the Division to be abnormally low or the well can not be shut-in due to "HARDSHIP" classification, the shut-in pressure to be used as P_C shall be determined by one of the following methods:

- 1. A Division-designated value.
- 2. An average shut-in pressure of all offset wells completed in the same zone. Offset wells include the four side and four corner wells, if available.
- 3. A calculated surface pressure based on a calculated bottom-hole pressure. Such calculation shall be made in accordance with the examples in this manual.

All Wellhead pressures as well as the flowing meter pressure tests which are to be taken during the 7-day or 8-day deliverability test period as required hereinabove shall be taken with a deadweight gauge or other method approved by the Division. The pressure readings and the date and time according to the chart shall be recorded and maintained in the operator's records with the test information.

Orifice meter charts shall be changed and so arranged as to reflect upon a single chart the flow data for the gas from each well for the full 7-day or 8-day deliverability test period; however, no tests shall be voided if satisfactory explanation is made as to the necessity for using test volumes through two chart periods. Corrections shall be made for pressure base, measured flowing temperature, specific gravity, and supercompressibility; provided however, if the specific gravity of the gas from any well under test is not available, an estimated specific gravity may be assumed therefor, based upon that of gas from near-by wells, the specific gravity of which has been actually determined by measurement.

The average flowing meter pressure for the 7-day or 8-day flow period and the corrected integrated volume shall be determined by the purchasing company that integrates the flow charts and furnished to the operator or testing agency.

The 7-day or 8-day flow period volume shall be calculated from the integrated readings as determined from the flow period orifice meter chart. The volume so calculated shall be divided by the number of testing days on the chart to determine the average daily rate of flow during said flow period. The flow period shall have a minimum of seven and a maximum of eight legibly recorded flowing days to be acceptable for test purposes. The volume used in this calculation shall be corrected to New Mexico Oil Conservation

Division standard conditions of 15.025 psia pressure base, 60⁰F. temperature base and 0.60 specific gravity base.

The daily volume of flow as determined from the flow period chart readings shall be calculated by applying the Basic Orifice Meter Formula or other acceptable industry standard practices.

$$Q = C' \{h_{w}P_{f}\}^{1/2}$$

Where:

- Q = Metered volume of flow Mcf/d @ 15.025 psia, 60^o F., and 0.60 specific gravity.
- C' = The 24-hour basic orifice meter flow factor corrected for flowing temperature, gravity, and supercompressibility.
- Pf = Daily average flowing meter pressure from flow period chart.

The basic orifice meter flow factors, flowing temperature factor, and specific gravity factor shall be determined from the tables in this manual.

The daily flow period average corrected flowing meter pressure, psig, shall be used to determine the supercompressibility factor. Supercompressibility Tables may be obtained from the New Mexico Oil Conservation Division.

When supercompressibility correction is made for a gas containing either nitrogen or carbon dioxide in excess of two percent, the supercompressibility factors of such gas shall be determined by the use of Table V of the C.N.G.A. Bulletin TS-402 for pressures 100-500 psig, or Table II, TS-461 for pressures in excess of 500 psig.

The use of tables for calculating rates of flow from integrator readings which do not specifically conform to the New Mexico Oil Conservation Division "Back Pressure Test Manual", or this manual, may be approved for determining the daily flow period rates of flow upon a showing that such tables are appropriate and necessary. The daily average integrated rate of flow for the 7-day or 8-day flow period shall be corrected for meter error by multiplication by a correction factor. Said correction factor shall be determined by dividing the square root of the deadweight flowing meter pressure, psia, by the square root of the chart flowing meter pressure, psia.

Deliverability pressure, as used herein, is a defined pressure applied to each well and used in the process of comparing the abilities of wells in a pool to produce at static wellhead working pressures equal to a percentage of the 7-day shut-in pressure of the respective individual wells. Such percentage shall be determined and announced periodically by the Division based on the relationship of the average static wellhead working pressures (P_w) divided by the average 7-day shut-in pressure (P_c) of the pool.

The deliverability of gas at the "deliverability pressure" of any well under test shall be calculated from the test data derived from the tests hereinabove required by use of the following deliverability formula:

$$D = Q \left[\frac{(P_c^2 - P_d^2)}{(P_c^2 - P_w^2)} \right]^n$$

Where:

- D = Deliverability Mcf/d at the deliverability pressure, (P_d), (at Standard Conditions of 15.025 psia, 60⁰F and 0.60 sp. gr.).
- Q = Daily flow rate in Mcf/d, at wellhead pressure (P_W) .
- P_C = 7-day shut-in Wellhead pressure, psia, determined in accordance with Section 2 of Chapter II.
- P_d = Deliverability pressure, psia, as defined above.
- P_W = Average static wellhead working pressure, as determined from 7-day or 8-day flow period, psia, and calculated from tables in this manual entitled "Pressure Loss Due to Friction" Tables for northwest New Mexico.
- n = Average pool slope of back pressure curves as
 follows:

For Pictured Cliffs and shallower formations 0.85 For formations deeper than Pictured Cliffs 0.75

(Note: Special rules for any specific pool or formation may supersede the above values. Check special rules if in doubt.)

The value of the multiplier in the above formula (ratio factor after the application of the pool slope) by which Q is multiplied shall not exceed a limiting value to be determined and announced periodically by the Division. Such determination shall be made after a study of the test data of the pool obtained during the previous testing season.

Downhole commingled wells are to be tested in year for pool of lowermost prorated completion of well and shall use pool slope (n), and deliverability pressure of lowermost pool. The total flow rate from the downhole commingled well will be used to calculate a value of deliverability. For each prorated gas zone of a downhole commingled well, a Form C-122-A is required to be filed and in the Summary portion of that form, all zones will indicate the same data for line h, P_C , Q, P_W , and P_d . The value shown for Deliverability (D) will be that percentage of the total deliverability of the well that is applicable to this zone. A note shall be placed in the remarks column that indicates the percentage of deliverability to be allocated to this zone of the well.

Any test prescribed herein will be considered acceptable if the average flow rate for the final 7-day or 8-day deliverability test is not more than ten percent in excess of any consecutive 7-day or 8-day average of the preceding two weeks. A deliverability test not meeting this requirement may be declared invalid, requiring the well to be re-tested.

All charts relative to initial, annual, or biennial deliverability tests or copies thereof shall be made available to the Division upon its request.

All testing agencies, whether individuals, companies, pipeline companies, or operators, shall maintain a log of all tests accomplished by them, including all field test data. The operator shall maintain the above data for a period of not less than two (2) years plus the current test year.

All forms heretofore mentioned are hereby adopted for use in the northwest New Mexico Area in open form subject to such modification as experience may indicate desirable or necessary. Initial and Annual or Biennial Deliverability and Shut-In Pressure Tests for gas wells in all formations shall be conducted and reported in accordance with these rules and procedures. Provided however, these rules shall be subject to any specific modification or change contained in Special Pool Rules adopted for any pool after notice and hearing.

CHAPTER III INFORMATIONAL TESTS

A. A one-point back pressure test may be taken on newly completed wells before their connection or reconnection to a gas transportation facility. This test shall not be a required official test but may be taken for informational purposes at the option of the operator. When taken, this test must be taken and reported as prescribed below:

ONE-POINT BACK PRESSURE POTENTIAL TEST PROCEDURE

- 1. This test shall be accomplished after a minimum shut-in of seven days. The shut-in pressure shall be measured with a deadweight gauge or other method approved by the Division.
- The flow rate shall be that rate in Mcf/d measured at the end of a three hour test flow period. The flow from the well shall be for three hours through a positive choke, which has a 3/4-inch orifice.
- 3. A 2-inch nipple which provides a mechanical means of accurately measuring the pressure and temperature of the flowing gas shall be installed immediately upstream from the positive choke.
- 4. The absolute open flow shall be calculated using the conventional back pressure formula as shown in this manual or the New Mexico Oil Conservation Division "Back Pressure Test Manual."
- 5. The observed data and flow calculations shall be reported in duplicate on Form C-122, "Multi-Point Back Pressure Test for Gas Wells."
- 6. Non-critical flow shall be considered to exist when the choke pressure is 13 psig or less. When this condition exists the flow rate shall be measured with a pitot tube and nipple as specified in this manual or in the Division's Manual of "Tables and Procedure for Pitot

Tests." The pitot test nipple shall be installed immediately downstream from the 3/4-inch positive choke.

- 7. Any well completed with 2-inch nominal size tubing (1.995-inch ID) or larger shall be tested through the tubing.
- B. Other tests for informational purposes may be conducted prior to obtaining a pipeline connection for a newly completed well upon receiving specific approval therefor from the Division's Aztec office. Approval of these tests shall be based primarily upon the volume of gas to be vented.

CHAPTER IV <u>TYPE OF TESTS REQUIRED FOR WELLS COMPLETED IN</u> <u>NON-PRORATED POOLS</u>

SECTION 1: Initial Shut-In Pressure Tests for Newly Completed Wells

A. (Same as Chapter I, Section 1, A)

- SECTION 2: <u>Biennial Shut-In Pressure Tests</u>
- A. Non-prorated wells will be tested biennially as required by the District Office except as follows:
 - 1. Wells which meet the "exempt" qualification as shown in Chapter I, Section 2, paragraph A-2 of these rules shall also be exempt from shut-in test requirements.
 - 2. Wells classified as "hardship" wells during the test year shall also be exempt from shut-in test requirements.
- B. All shut-in tests required by these rules must be filed with the Division's Aztec office by January 31 of the following year. Failure to file the test will subject the well to being shut-in one day for each day the test is late.

SECTION 3: <u>Scheduling Tests</u>

A. By September 1 of each year, the District Supervisor of the Aztec District Office of the Division shall by memorandum notify each gas transportation facility and each operator of the pools which are to be scheduled for biennial shut-in pressure testing during the following testing period from January 1 through the last day of December of that test year. The District Supervisor will also provide a list of "exempt" wells.

Any well scheduled for testing during its test year may have the test flow period, and some of the seven day shut-in period conducted in December of the previous year. The earliest date that a well could be scheduled for Biennial Shut-In Pressure Test would be such that the Test Flow Period would end on December 25 of the previous year.

Downhole commingled wells are to be scheduled for tests on dates for pool of lowermost completion of well.

SECTION 4: Test Procedure

A. To obtain the shut-in pressure of a well under test, the well shall be shut-in some time during the current testing season for a period of seven to fourteen consecutive days, which have been preceded by a minimum of seven days of uninterrupted production. Such shut-in pressure shall be measured by deadweight gauge or other method approved by the Division on the seventh to fourteenth day of shut-in of the well. The shut-in pressure shall be measured on both the tubing and the casing when communication exists between the two strings. The higher of such pressures shall be reported as the shut-in pressure of the well

SECTION 5: Filing of Shut-In Pressure Data

The results of this test will be filed in triplicate on Form C-125-B showing the pressures in psia in column labeled "S. I. PRESSURE PSIA (DWT)" with the Aztec District Office.



STATE OF NEW MEXICO ENERGY AND MINERALS DEPARTMENT OIL CONSERVATION DIVISION AZTEC DISTRICT OFFICE

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GARREY CARRUTHERS GOVERNOR

1000 RIO BRAZOS ROAD AZTEC, NEW MEXICO 87410 (505) 334-6178

June 10, 1987

Mr. Victor T. Lyons Oil Conservation Div. P.O. Box 2088 Santa Fe, NM 87504

Re: Delinquent "D" Test Penalties

Dear Vic:

Before the new proration rules (Order R-8170) came out, we were penalizing a proration unit for its <u>full</u> allowable for delinquent tests. Under Rule 5(b)1 only the <u>deliverability</u> <u>portion</u> of the allowable is to be penalized by it not being assigned until a date later than first delivery. This was a significant change and is being reflected on all future supplements.

Sincerely,

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Frank T. Chavez District Supervisor

FTC/dj

xc: File Harold Garcia Alice Dugger



MEMORANDUM

TO: SAN JUAN DELIVERABILITY TEST COMMITTEE ·SAN JUAN BASIN OPERATORS AND PRODUCERS

FROM: H. L. BABE KENDRICK

DATE: JANUARY 23, 1987

This memorandum is your invitation to attend a meeting of San Juan Basin producers, operators and deliverability testers, to be held in <u>Farmington, New</u> <u>Mexico</u> at <u>THE INN</u>, at <u>9:00 am</u> on <u>Thursday</u>, <u>February 5</u>, 1987.

The Deliverability Test Committee has been working since January, 1984 trying to remake a test manual for all testing requirements for gas wells in the San Juan Basin. That work is near completion. At the latest meeting of the committee in late 1986, there was a lot of discussion about being able, and not being able, to test wells in the 1987 test year.

At the hearing before the New Mexico Oil Conservation Division in December, 1986, a Committee recommendation was made to the Division to forego deliverability flow testing in the 1987 test year. Since that time, there has been a lot more discussion concerning this problem.

At this meeting we want to:

- 1. hear from the producers and operators, and
- 2. hear from the testers, and
- 3. hear from the pipelines concerning availability of space necessary to permit test gas to flow during 1987.

This is your meeting, please be there. Please tell others.

Sincerely, ideil . Babe Kendrick

BLACKWOOD & NICHOLS CO., LTD.

P.O. BOX 1237 DURANGO, COLORADO 81302-1237

(303) 247-0728

December 22, 1986

Mr. Richard Stamets, DirectorOil Conservation DivisionP. O. Box 2208Santa Fe, New Mexico 87504-2208

Re: OCD Case Number 8586 (Reopened) Division Order R-333

Dear Mr. Stamets:

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At the December 3, 1986 Hearing, the referenced case was taken under advisement. Blackwood & Nichols Company, Ltd. wishes to make a statement in this matter.

We commend the members of the Testing Committee for their effort to update the testing rules and manual. All operators as well as the Division will benefit from this work. We support the extension of the 1986 deliverability test period as recommended.

However, suspension of the 1987 deliverability flow test requirement causes us to be concerned. Specifically, this suspension could have contractual ramifications, decrease the quality of a prorated pool's reservoir data, and possibly cause deliverability/allowable inequities. Following is a discussion of these points and then concluding remarks.

Blackwood & Nichols Company's Gas Sales Contract, which I believe is fairly typical in this nature to most of El Paso Natural Gas Company's contracts, makes specific reference to the deliverability tests. "... the daily stabilized producing capacity for each well shall be calculated for each year utilizing data obtained from the annual well deliverability test as prescribed by the New Mexico Oil Conservation Commission ..." Suspending all deliverability tests for one year increases the difficulty of determing a well's daily stabilized producing capacity

because the standardization factor is broken.

Obtaining only a shut-in pressure instead of a fully conditioned and controlled test will put an undesirable anomaly in the prorated pools reservoir data records.

It is possible inequities in assigned allowables could be caused under this proposed suspension. Suppose someone has a well which is four years old in 1986 and was last tested in 1985. Under the suspension Mr. Richard Stamets December 22, 1986 Page 2

proposal this well would be tested in 1988. The 1985 test would be used to calculate allowables for three years - 1986, 1987 and 1988. If this example well is spot market active for these three years, then it might be assigned an unreasonably high allowable as compared to an offset well which is older or less market active.

In summary, we believe there are several factors to be evaluated before a decision is made. During 1986, El Paso's well test gas displaced spot market production and was priced accordingly. If the pipeline companies feel it is too burdensome to flow a well for three weeks out of one hundred and four weeks, then, perhaps, a change is necessary.

Also the advertisement for the referenced case could have been more explicit. This is actually a suspension of the 1987 and 1988 tests, each for one year. The special procedures for new wells, less than three years old, required shut-in pressures and optional testing determined by the Commission, pipelines or operators? - needs to be clearly stated.

Sincerely,

BLACKWOOD & NICHOLS CO., LTD.

Villian F. C.

William F. Clark Operations Manager

WFC:ew

cc: J. Scott Hall Campbell & Black

ENERGY AND MINERALS DEPARTMENT

OIL CONSERVATION DIVISION



No. 8-86

TONEY ANAYA GOVERNOR

POST OFFICE BOX 2088 STATE LAND OFFICE BUILDING SANTA FE, NEW MEXICO 87501 (505) 827-5800

MEMORANDUM

TO:

SAN JUAN BASIN OPERATORS, PURCHASERS, AND TRANSPORTERS 1 -K

R. L. STAMETS, DIRECTOR FROM:

EXTENSION OF 1986 DELIVERABILITY TEST PERIOD, SUBJECT: SUSPENSION OF BIENNIAL TESTING

Case No. 8586 reopened December 3, 1986 was, in part, an application to extend the deadline for completing and filing 1986 deliverability tests to March 31, 1987, and for a one year suspension of biennial deliverability testing.

No testimony was received in opposition to this application and it will be granted. As completion of work necessary to prepare an order dealing with other matters in Case No. 8586 will take some time, this memorandum is being issued in order that all persons concerned with deliverability testing may be aware of our intentions and may take advantage of the relief to be granted.

The deliverability test cycle will begin again in 1988 with those pools which would have been tested in 1987. The three annual deliverability tests for new wells will continue to be required. Voluntary testing and retests after workover will be handled as at present.

December 15, 1986 /et

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MEMORANDUM

TO: TEST MANUAL PUTTER-TO-GETHERS

FROM: BABE

DATE: DECEMBER 12, 1986

Yesterday afternoon I mailed to some of you a couple of pages of TABLE OF CONTENTS for the booklet of testing for the northwest NM and then this morning I compared the looks of what I had sent and I thought that I ought to redo the VII table of c. Here it is. I took out the gaps between the VII — # and shrunk them up to VII—606 like TABLE of C. III—2. I also took out the extra spaces between the lines of the page so that it is not as long down the page.

I have seen that the dots following the printed letters across the page do not come out at the same position across the page and it in funny that it don't but these funny machines do funny things. I drew a line from the top of the page to the bottom and tried to get the dots to end at ABOUT the same place on the page.

I will be in Santa Fe on Tuesday and Wednesday and will be able to discuss this with anyone who wants to talk. I think that Mike is working hard on this now and will continue if he is unable to pawn it off on one of the others. (I would pawn it if I could.)

Also, you will note that I put the PITOT TABLES in SECTION VII but after TABLES VIII and IX. And, I will bet that I have not properly counted the pages and some of the page numbers are incorrect. I can fix these when I get back.

See you.

Babe

Dist: M. Stogner F. Chavez E. Marcum A. Kendrick M. Turnbaugh J. Levine J. Fox

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MEMORANDUM

TO: MEMBERS OF THE NMOCD DELIVERABILITY TEST COMMITTEE FROM: H. L. BABE KENDRICK

DATE: JUNE 14, 1985

Last week in Santa Fe, Dick Stamets asked how we are doing with the testing manual for the San Juan Basin. Of course I had to tell him that I had been very slow with everything but we are working to get things done. Since that time I have done a little more along the lines of getting everything in shape. Enclosed are some of the things that we have been dealing with that certainly need to be finalized so they can be published.

First, I have rewritten the rules and procedures with the following changes:

OLD COPY	NEW COPY	CHANGES
page 1	page 1	removed the heading about this should be the new Order R-333 and labeled the paper as a "MANUAL".
page 3	page 3	Item A-4. This paragraph was rewritten along with the ideas expressed at the hearing.
page 5	page 5	Chapter II, Section1, Paragraph B. The old reference was to paragraph A-3. I think this should now be to paragraph A-1. (Agree??)
page 8	page 7	top of old page, bottom of new page. The words "or the well can not be shut-in due to "HARDSHIP" classification" were added to take care of wells with "hardship" classification. NOTE: DO YOU THINK WE NEED TO ADD ANY OTHER DATA TO EXCLUDE THE TESTING OF "HARDSHIP" WELLS???
page 8	page 8	paragraph numbered 3. Words in this have been changed to update this to this manual

			and include the examples in this manual.
page	9	page 9	¶ that begins "The basic orifice meter" was changed to include reference to this manual.
page	9	page 9	¶ that begins "The use of tables for" was changed to include this manual.
page	10	page 10	¶ about P_w. Changed just to say tables "in this manual".
page	12	page 12	¶ #4. Words were added to say "in this manual".
page	12	page 12	% #6. Words were added to say "in this manual". NOTE: I MUST LOOK TO SEE IF I HAVE THE DATA NECESSARY TO ADD TO THIS MANUAL SO THIS WILL BE POSSIBLE.
page	13	page 13	¶ #1. This reference was changed to paragraph A-2 instead of part 2.
page	13	page 13	last ¶. The form number is referenced as C-125-B as was discussed in the hearing so that it is different from the form used in SE New Mexico. This leaves C-125 as the primary form. C-125-A could be the computer print-out for filing in SE New Mexico and then this C-125-B would be for San Juan Basin. Also, the remark is made here to insert the pressure in the column labeled "S. I. PRESSURE PSIA (DWT)" instead of by column number.

Now, I do not say that this finishes this program by any means. I am hopeful that it will be finished soon. Please read, and reread if necessary to see if you can find any boo-boos that have not been addressed to date. What else do we need and from where do we get it? I just happened to think about the reference that we have used on page 8, Item #3. The reference was made to example 7 in the B-P Manual. That was the one dated in 1956. There is a newer B-P Manual dated in 1966. This 1966 version is the one that I copied forms from to include in this manual.

What else do we need?

WELL, I JUST LOST THE FROSTING OFF THE CAKE.

I was running copies of data to send you to show you what other tables I have at hand. While running the stuff for PITOT TUBE TYPE TESTS, I found the data was fixed around sp. gr. = .65.. Now that is another reason why we should go all out to revise data in our manuals. Anyway; will someone please see it they can recalculate these values on a sp. gr. of 1.000 and make them into a table? The tables from the Back Pressure Manual are on 1.000.

The temperature correction table is based on 60° F. (Hurray, we won one).

Now, things that I do not have at hand:

1. An I. P. Test on C-122 form filled out.

2. Del. Test on C-122-A showing step by step progression through the calculation and the round-off and truncation points. Yes, I know that Frank Chavez supplied us with on in Farmington but I don't have it available and/or in printing form.

3. A Shut-in pressure measured on a non-prorated well and the data filled in on C-125-B.

4. There has to be more that I have forgotten. If you have it, please send it on in.

You have already received the Tables of F_C values and table of 1-e^{-S}. Those tables go into this manual also.

What else???

Thanks for your help!!!

Bobe BABE

SECTION III

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SECTION III

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MEMORANDUM



To: Deliverability Test Committee

From: H. L. Babe Kendrick

Date: December 5, 1986

Today I am printing the absolute latest edition of the test procedures for the area of northwest New Mexico. I have done a few things to this order to get it in what I hope is final form. Here are some of the things that I did to what you have read before:

1. Changed the name of this 15 pages to read "RULES OF PROCEDURE FOR NORTHWEST NEW MEXICO". This was done because as this is placed into a booklet, this booklet will look much like the BACK PRESSURE TEST MANUAL for New Mexico and will be placed in the book at page III-1 to 15.

2. Changed the name from <u>San Juan Basin</u> to <u>northwest New Mexico</u> because this will be a booklet that will pertain to all the wells of northwest New Mexico and not to just the San Juan Basin wells.

3. Tried to make sure that the word Commission was replaced with the word Division in all places possible.

4. Tried to clean up any references that were made to other booklets or publications that might be used when the data necessary for testing procedures or tables, etc are all enclosed in this booklet. Now there are words in this that say you can find the data in this booklet or you can find it in the other booklets.

NOW: If you will take your own copy of the "State of New Mexico Oil Conservation Division Manual For Back—Pressure Testing of Natural Gas Wells January 1, 1966 and follow the pages in it you can follow what we are trying to do in this case.

Page -i: OCD Title = OCD tell me what they want

Page i: Acknowledgment = OCD tell me what they want.

Page ii: New Table of Contents - This will be the last thing made.

Page iii: Preface - OCD tell me what they want.

Section I - Introduction:

Page I-1 to 6 - Introduction - OCD tell me what they want.

Section II - Nomenclature:

Page II-1 to 4 - See if Frank Chavez can find time to check to see if this has all the data necessary in it to be up to date with the terms that we have added in our description of the deliverability test.

Section III - Rules of Procedure

We need a First page which will serve as a table of contents for this section and I will try to do this today or next Wednesday.

Pages III-1 to 17 will be removed and replaced with the test I have enclosed to you now.

Section IV — Forms

We need to be sure that this section has a copy of a blank form of everything needed and this list would include the C-122, the C-122-A, and the C-125-B (the latest data page published in Santa Fe for the writing in of the shut-in pressures of wells.

Section V - Basic Calculations - Leave as is.

Section VI – Test Examples – Add into this section a Form C-122-A filled out properly and a description page about how the data is acquired and placed into the slots. Also add in a Form C-125-B filled in with the proper data and a description page of how this data was obtained and entered. I believe there is a Form C-122 page in this section, BUT, it may have some data that needs to be changed. For instance, any of the data shown in this section (or for that matter anywhere in the book) should have LOCATIONS, COUNTY NAMES, POOL NAMES (FAKE OR OTHERWISE) that are within the limits of the northwest New Mexico area. Again, I would like to call on Frank Chavez to supply the C-125-B and necessary descriptions and look for changes to be made to locations, counties, pools, etc. The Form C-122-A that Frank had earlier submitted to the committee was given to Mike Stogner to get this into this section. And, I see this will need a new Table of Contents page at the first of the section also.

Section VII – Tables Pages 2 to 5 – Leave as is. Pages 6, 7 and 8 – eliminate. Pages 9 to 86 – Leave as is. Pages 87 to 93 – These will be replaced with tables marked C-1 in the last hearing and add title to the pages. These are the $1-e^{-5}$ tables.

Pages 94, 95, 95A, and 96 – Replace these tables with tables marked D-1 in the last hearing and add title to the pages. These are the Friction Factor Tables. Page 97 is OK as is.

Page A-1 – Leave as is.

Page B-1 - Leave as is

Page C-1 to 5 - Eliminate. Here we need to add the description used by me in the calculation of the F_c values for Friction Calculations.

Page D-1 to 6 – Leave as is but Mike Stogner will get better copies.

AND - WE NEED TO INSERT SOME PAGES OF INITIAL POTENTIAL DATA SUCH AS THE PITOT TUBE IMPACT PRESSURE VS VOLUME TABLES AND THE SPECIFIC GRAVITY CORRECTION TABLES FOR THE PITOT CALCULATIONS. THIS COULD BE ADDED IN SECTION VII RIGHT AFTER PAGE VII-13 (SPECIFIC GRAVITY FACTORS) AND BEFORE PAGE VII-14 (PSEUDOCRITICAL PROPERTIES OF HYDROCARBON GASES). ******Now, Ladies and Gentlemen of the committee, here is your last chance to get this done correctly. Please read everything with the most critical eye looking at each word as if it is wrong and find all the corrections that need to be made. If you then have any extra time on your hands, please help Frank Chavez and Mike Stogner as they try to supply the missing details in making your book read the way that you want it to read. The NMOCD is placed with its back to the wall in trying to get this out by the first of the year (meaning 1987).. If you can help them, please do.*****

I want to express my thanks to each of you that have put up with my foolishness for the past 35 months in trying to make this publication one that will serve our needs for the next few years. THANK YOU!!!!

See you around.

BABE

RULES OF PROCEDURE FOR NORTHWEST NEW MEXICO

CHAPTER I TYPE OF TESTS REQUIRED FOR WELLS COMPLETED IN PRORATED GAS POOLS

SECTION 1: Initial Deliverability and Shut-In Pressure Tests for Newly Completed Well

- A. Immediately upon completion of each gas well in northwest New Mexico, a shut-in pressure test of at least seven days duration shall be made. This initial shut-in pressure shall be filed with the Division's Aztec Office on either Form C-122 or C-104.
- B. Within 90 days ater a well first delivers gas to a gas transportation facility, the well shall have been tested in accordance with Section 1 of Chapter II of these rules, "Initial Deliverability and Shut-In Pressure Test Procedures", and the results of the test filed in triplicate with the Division's Aztec office and one copy filed with the gas transportation facility to which the well is connected. This test is to be filed on Form C-122-A. Failure to file said test within the above-prescribed 90-day period will subject the well to the loss of one day's allowable for each day the test is late.
 - 1. If the newly first delivered well is an infill well on a proration unit, the old well on the unit is not required to be tested provided it has a valid test on file for the current proration year. Testing of the old well follows the regularly assigned test year for the pool in which the wells are located. The new well is required to be tested annually until at least three annual tests are on file and then the well is to be tested biennially with other wells in that pool.
 - 2. If the newly first delivered well is an infill well on a proration unit and the old well on the unit is "exempt", the old well is to be tested along with the new well for the Initial and Annual Deliverability and Shut-In Pressure Test. The old well will lose its "exempt" classification and must be tested biennially along with other wells in that pool. The new infill well is required to be tested annually until at least three annual tests are on file and then the well is to be tested biennially with other wells in that pool.

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- C. The requirements for Initial Tests and Annual or Biennial Deliverability and Shut-In Pressure Tests and the notification requirements and scheduling of such tests which apply to newly completed wells shall also apply to recompleted wells.
- D. Any tests taken for informational purposes prior to pipeline connection shall not be recognized as official tests for the assignment of allowables.

SECTION 2. <u>Annual and Biennial Deliverability and Shut-In Pressure</u> <u>Tests</u>

- A. Annual or Biennial Deliverability and Shut-In Pressure Tests shall be made on all gas wells during the period from January 1 through December 31 of that year except as follows:
 - A newly completed well or a recompleted well shall be tested on an annual basis until a minimum of three annual tests have been taken, after which the well shall be tested biennially as is required for other wells in the pool in which the well is located.
 - 2. Wells classified as "exempt" shall not be subject to the requirements of annual or biennial deliverability tests.

Classification of wells into or out of the "exempt" status shall be done once each year immediately following the reporting of June production and shall be effective for the succeeding annual test period.

Gas wells completed in the Pictured Cliffs or any shallower formation shall be classified "exempt" if at least three months of production history is available and the well failed to produce, and is incapable of producing, an average of 250 MCF or more per month during the months produced within the preceding 12-month period, and the well is classified as marginal in the August Gas Proration Schedule.

Gas wells completed in any formation deeper than the Pictured Cliffs formation shall be classified "exempt" if at least three months of production history is available and the well failed to produce, and is incapable of producing, an average of 2000 MCF or more per month during the months produced within the preceding 12-month period, and the well is classified as marginal in the August Gas Proration Schedule.

Gas wells on multiple well Gas Proration Units will not be classified "exempt" unless the Gas Proration Unit is classified as marginal. Any or all wells on a marginal multiple well Gas Proration Unit may be classified as "exempt" provided each Gas Proration Unit so classified meets the qualification for "exempt" status. Gas Proration Units for wells producing from formations deeper than the Pictured Cliffs formation shall be classified "exempt" if at least three months of production history is available and the Gas Proration Unit failed to produce, and is incapable of producing, an average of 2000 MCF or more per month during the months produced within the preceding 12-month period, and the Gas Proration Unit is classified as marginal in the August Gas Proration Schedule. Gas Provation Units are to be classified as "exempt" because of their low producing ability.

The District Supervisor of the Division's Aztec Office may classify a well or Gas Proration Unit as "exempt" at any time if the operator presents sufficient evidence to the District Supervisor indicating that the well or Gas Proration Unit is incapable of producing gas at a higher rate than that rate required for "exempt" classification for wells or Gas Proration Units in that pool.

Once a well or Gas Proration Unit has been declared "exempt" for the following test year, it shall remain classified "exempt" for that test year.

- If a test is filed on any well on a gas proration unit, the test requirement for the gas proration unit has been met. The deliverability of the unit is taken only as the resulting sum of all wells tested.
- 4. A shut-in pressure must be filed on Form C-122-A even if no gas is measured during the production phase of the test. "Exempt" wells do not require the filing of a shut-in pressure.
- B. All Annual and Biennial Deliverability and Shut-In Pressure Tests required by these rules must be filed with the Division's Aztec office and with the appropriate gas transportation facility within 90 days following the completion of each test. Provided however, that any test completed between October 31 of the test year and January 31 of the following year are due no later than January 31. No extension of time for filing tests beyond January 31 will be granted except after notice and hearing.

Failure to file any test within the above-prescribed times will subject the well to the loss of one day's allowable for each day the test is late. A well classified as marginal shall be shut-in one day for each day the test is late.

SECTION 3: Scheduling of Tests

A. Notification of Pools to be Tested

By September 1 of each year, the District Supervisor of the Aztec District Office of the Division shall by memorandum notify each gas transportation facility and each operator of the pools which are to be scheduled for biennial testing during the following testing period from January 1 through the last day of December of that test year. The District Supervisor will also provide a list of "exempt" wells and a list of wells that do not have a minimum of three Annual Deliverability and Shut-In Pressure Tests on file.

Any well scheduled for testing during its test year may have the conditioning period, test flow period, and some of the seven day shut-in period conducted in December of the previous year provided that if the 7 day shut-in period immediately follows the test flow period the 7 day shut-in pressure would be measured in January of the test year. The earliest date that a well could be scheduled for Annual or Biennial Deliverability and Shut-In Pressure Test would be such that the Test Flow Period would end on December 25 of the previous year.

Downhole commingled wells are to be scheduled for tests on dates for pool of lowermost prorated completion of well.

B. Annual and Biennial Deliverability Tests

By November 1 of each year, each gas transportation facility shall, in cooperation with the operators involved, prepare and submit a schedule of the wells to which it is connected which are to begin testing in December and January. Said schedule shall be entitled, "Annual and Biennial Deliverability and Shut-In Pressure Test Schedule", and one copy shall be submitted to the Division's Aztec office and to each operator concerned. The schedule shall indicate the date of tests, pool, operator, lease, well number, and location of each well.

At least 30 days prior to the beginning of each succeeding 2-month testing interval, a similar schedule shall be prepared and filed in accordance with the above. The gas transportation facility and the Aztec District Office of the Division shall be notified immediately by any operator unable to conduct any test as scheduled.

In the event a well is not tested in accordance with the existing test schedule, the well shall be re-scheduled by the gas transportation facility, and the Division and the operator of the well so notified in writing. Every effort should be made to notify the Division of the new schedule prior to the conclusion of the newly assigned 14-day conditioning period.

Notice to the Division of Shut-In Pressure Tests which are scheduled at a time other than immediately following the flow test must be received prior to the time that the well is shut-in.

It shall be the responsibility of each operator to determine that all of its wells are properly scheduled for testing by the gas transportation facility to which they are connected, in order that all annual and biennial tests may be completed during the testing season.

In the event a well is shut-in by the state for over production, the operator may produce the well for a period of time to secure a test after notification to the Division. All gas produced during this testing period will be used in determining the over/under produced status of the well.

C. <u>Deliverability Re-Tests</u>

An operator may, in cooperation with the gas transportation facility, schedule a well for a deliverability re-test upon notification to the Division's Aztec office at least ten days before the test is to be commenced. Such re-test shall be for good and substantial reason and shall be subject to the approval of the Division. Re-tests shall in all ways be conducted in conformance with the Annual and Biennial Deliverability Test Procedures of these rules. The Division, at its discretion, may require the re-testing of any well by notification to the operator to schedule such re-test. These tests as filed on Form C-122-A should be identified as "RETEST" in the remarks column.

SECTION 4: <u>Witnessing of Tests</u>

Any Initial Annual or Biennial Deliverability and Shut-In Pressure Test may be witnessed by any or all of the following: an agent of the Division, an offset operator, a representative of the gas transportation facility connected to the well under test, or a representative of the gas transportation facility taking gas from an offset operator.

CHAPTER II PROCEDURE FOR TESTING

SECTION 1: Initial Deliverability and Shut-In Pressure Test Procedure

- A. Within 90 days after a newly completed well is first delivered to a gas transportation facility, the operator shall complete a deliverability and shut-in pressure test of the well in conformance with the "Annual and Biennial Deliverability and Shut-In Pressure Test Procedures", prescribed in Section 2 of this chapter. Results of the test shall be filed as required by Section 1 of Chapter I of these rules.
- B. In the event it is impractical to test a newly completed well in conformance with Paragraph A above, the operator may conduct the deliverability and shut-in pressure test in the following manner (provided, however, that any test so conducted will not be accepted as the first annual deliverability and shut-in pressure test as described in Paragraph A-1 of Section 2, Chapter I):
 - 1. A 7-day or 8-day production chart may be used as the basis for determining the well's deliverability, providing the chart so used is preceded by at least 14 days continuous production. The well shall produce through either the casing or tubing, but not both, into a pipeline during these periods. The production valve and the choke settings shall not be changed during either the conditioning or flow period with the exception of the first ten (10) days of the conditioning period when maximum production would over-range the meter chart or location production equipment.
 - 2. A shut-in pressure of at least seven days duration shall be taken. This shall be the shut-in test required in Paragraph A, Section 1 of Chapter I of these rules.
 - 3. The average daily static meter pressure shall be determined in accordance with Section 2 of Chapter II of these rules. This pressure shall be used as P_t in calculating P_w for the Deliverability Calculation.
 - 4. The daily average rate of flow shall be determined in accordance with Section 2 of Chapter II.

- 5. The static wellhead working pressure (P_w) shall be determined in accordance with Section 2 of Chapter II.
- The deliverability of the well shall be determined by using the data determined in Paragraphs 1 through 5 above in the deliverability formula in accordance with Section 2 of Chapter II.
- 7. The data and calculations for Paragraphs 1 through 6 above shall be reported as required in Section 1 of Chapter I of these rules, upon the blue-colored Form C-122-A or on white Form C-122-A and write "INITIAL TEST ONLY" in remarks.

SECTION 2: <u>Annual and Biennial Deliverability and Shut-In Pressure</u> <u>Test Procedure</u>

This test shall begin by producing a well in the normal operating manner into the pipeline through either the casing or tubing, but not both, for a period of fourteen consecutive days. This shall be known as the conditioning period. The production valve and choke settings shall not be changed during either the conditioning or flow periods except during the first ten (10) days of the conditioning period when maximum production would over-range the meter chart or location production equipment. The first ten (10) days of said conditioning period shall not have more than forty eight (48) hours of cumulative interruptions of flow. The eleventh to fourteenth days, inclusive, of said conditioning period shall have no interruptions of flow whatsoever. Any interruption of flow that occurs as normal operation of the well as stop-cock flow, intermittent flow, or well blow down will not be counted as shut-in time in either the conditioning or flow period.

The daily flowing rate shall be determined from an average of seven or eight consecutive producing days, following a minimum conditioning period of 14 consecutive days of production. This shall be known as the flow period.

Instantaneous pressures shall be measured by deadweight gauge or other method approved by the Division during the 7-day or 8-day flow period at the casinghead, tubinghead, and orifice meter, and shall be recorded along with instantaneous meter-chart static pressure reading.

If a well is producing through a compressor that is located between the wellhead and the meter run, the meter run pressure and the wellhead casing pressure and the wellhead tubing pressure are to be reported on Form C-122-A. (Neither the suction pressure nor

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the discharge pressure of the compressor is considered <u>wellhead</u> pressure.) A note shall be entered in the remarks portion on Form C-122-A stating "This well produces through a compressor".

When it is necessary to restrict the flow of gas between the wellhead and orifice meter, the ratio of the downstream pressure, psia, to the upstream pressure, psia shall be determined. When this ratio is 0.57, or less, critical flow conditions shall be considered to exist across the restriction.

When more than one restriction between the wellhead and orifice meter causes the pressures to reflect critical flow between the wellhead and orifice meter, the pressures across each of these restrictions shall be measured to determine whether critical flow exists at any restriction. When critical flow does not exist at any restriction, the pressures taken to disprove critical flow shall be reported to the Division on Form C-122-A in item (n) of the form. When critical flow conditions exist, the instantaneous flowing pressures required hereinabove shall be measured during the last 48 hours of the 7-day or 8-day flow period.

When critical flow exists between the wellhead and orifice meter, the measured wellhead flowing pressure of the string through which the well flowed during test shall be used as P_t when calculating the static wellhead working pressure (P_W) using the method established below.

When critical flow does not exist at any restriction, Pt shall be the corrected average static pressure from the meter chart plus friction loss from the wellhead to the orifice meter.

The static wellhead working pressure (P_W) of any well under test shall be the calculated 7-day or 8-day average static tubing pressure if the well is flowing through the casing; it shall be the calculated 7-day or 8-day average static casing pressure if the well is flowing through the tubing. The static wellhead working pressure (P_W) shall be calculated by applying the tables and procedures set out in this manual.

To obtain the shut-in pressure of a well under test, the well shall be shut in some time during the current testing season for a period of seven to fourteen consecutive days, which have been preceded by a minimum of seven days of uninterrupted production. Such shut-in pressure shall be measured with a deadweight gauge or other method approved by the Division on the seventh to fourteenth day of shut-in of the well. The 7-day shut-in pressure shall be measured on both the tubing and the casing when communication exists between the two strings. The higher of such pressures shall be used as P_C in the deliverability calculation. When any such shut-in pressure is determined by the Division to be abnormally low or the well can not be shut-in due to "HARDSHIP" classification, the shut-in pressure to be used as P_C shall be determined by one of the following methods:

- 1. A Division-designated value.
- 2. An average shut-in pressure of all offset wells completed in the same zone. Offset wells include the four side and four corner wells, if available.
- 3. A calculated surface pressure based on a calculated bottom-hole pressure. Such calculation shall be made in accordance with the examples in this manual.

All Wellhead pressures as well as the flowing meter pressure tests which are to be taken during the 7-day or 8-day deliverability test period as required hereinabove shall be taken with a deadweight gauge or other method approved by the Division. The pressure readings and the date and time according to the chart shall be recorded and maintained in the operator's records with the test information.

Orifice meter charts shall be changed and so arranged as to reflect upon a single chart the flow data for the gas from each well for the full 7-day or 8-day deliverability test period; however, no tests shall be voided if satisfactory explanation is made as to the necessity for using test volumes through two chart periods. Corrections shall be made for pressure base, measured flowing temperature, specific gravity, and supercompressibility; provided however, if the specific gravity of the gas from any well under test is not available, an estimated specific gravity may be assumed therefor, based upon that of gas from near-by wells, the specific gravity of which has been actually determined by measurement.

The average flowing meter pressure for the 7-day or 8-day flow period and the corrected integrated volume shall be determined by the purchasing company that integrates the flow charts and furnished to the operator or testing agency.

The 7-day or 8-day flow period volume shall be calculated from the integrated readings as determined from the flow period orifice meter chart. The volume so calculated shall be divided by the number of testing days on the chart to determine the average daily rate of flow during said flow period. The flow period shall have a minimum of seven and a maximum of eight legibly recorded flowing days to be acceptable for test purposes. The volume used in this calculation shall be corrected to New Mexico Oil Conservation

Division standard conditions of 15.025 psia pressure base, 60⁰F. temperature base and 0.60 specific gravity base.

The daily volume of flow as determined from the flow period chart readings shall be calculated by applying the Basic Orifice Meter Formula or other acceptable industry standard practices.

$$Q = C' \{h_w P_f\}^{1/2}$$

Where:

- Q = Metered volume of flow Mcf/d @ 15.025 psia, 60^o F., and 0.60 specific gravity.
- C' = The 24-hour basic orifice meter flow factor corrected for flowing temperature, gravity, and supercompressibility.
- hw = Daily average differential meter pressure from flow period chart.
- Pf = Daily average flowing meter pressure from flow
 period chart.

The basic orifice meter flow factors, flowing temperature factor, and specific gravity factor shall be determined from the tables in this manual.

The daily flow period average corrected flowing meter pressure, psig, shall be used to determine the supercompressibility factor. Supercompressibility Tables may be obtained from the New Mexico Oil Conservation Division.

When supercompressibility correction is made for a gas containing either nitrogen or carbon dioxide in excess of two percent, the supercompressibility factors of such gas shall be determined by the use of Table V of the C.N.G.A. Bulletin TS-402 for pressures 100-500 psig, or Table II, TS-461 for pressures in excess of 500 psig.

The use of tables for calculating rates of flow from integrator readings which do not specifically conform to the New Mexico Oil Conservation Division "Back Pressure Test Manual", or this manual, may be approved for determining the daily flow period rates of flow upon a showing that such tables are appropriate and necessary. The daily average integrated rate of flow for the 7-day or 8-day flow period shall be corrected for meter error by multiplication by a correction factor. Said correction factor shall be determined by dividing the square root of the deadweight flowing meter pressure, psia, by the square root of the chart flowing meter pressure, psia.

Deliverability pressure, as used herein, is a defined pressure applied to each well and used in the process of comparing the abilities of wells in a pool to produce at static wellhead working pressures equal to a percentage of the 7-day shut-in pressure of the respective individual wells. Such percentage shall be determined and announced periodically by the Division based on the relationship of the average static wellhead working pressures (P_w) divided by the average 7-day shut-in pressure (P_c) of the pool.

The deliverability of gas at the "deliverability pressure" of any well under test shall be calculated from the test data derived from the tests hereinabove required by use of the following deliverability formula:

$$D = Q \left[\frac{(P_c^2 - P_d^2)}{(P_c^2 - P_w^2)} \right]^n$$

Where:

- D = Deliverability Mcf/d at the deliverability pressure, (Pd), (at Standard Conditions of 15.025 psia, $60^{\circ}F$ and 0.60 sp. gr.).
- Q = Daily flow rate in Mcf/d, at wellhead pressure (P_w) .
- P_C = 7-day shut-in Wellhead pressure, psia, determined in accordance with Section 2 of Chapter II.
- P_d = Deliverability pressure, psia, as defined above.
- Pw = Average static wellhead working pressure, as determined from 7-day or 8-day flow period, psia, and calculated from tables in this manual entitled "Pressure Loss Due to Friction" Tables for northwest New Mexico.
- n = Average pool slope of back pressure curves as
 follows:

For Pictured Cliffs and shallower formations 0.85 For formations deeper than Pictured Cliffs 0.75

(Note: Special rules for any specific pool or formation may supersede the above values. Check special rules if in doubt.)

The value of the multiplier in the above formula (ratio factor after the application of the pool slope) by which Q is multiplied shall not exceed a limiting value to be determined and announced periodically by the Division. Such determination shall be made after a study of the test data of the pool obtained during the previous testing season.

Downhole commingled wells are to be tested in year for pool of lowermost prorated completion of well and shall use pool slope (n), and deliverability pressure of lowermost pool. The total flow rate from the downhole commingled well will be used to calculate a value of deliverability. For each prorated gas zone of a downhole commingled well, a Form C-122-A is required to be filed and in the Summary portion of that form, all zones will indicate the same data for line h, P_C , Q, P_W , and P_d . The value shown for Deliverability (D) will be that percentage of the total deliverability of the well that is applicable to this zone. A note shall be placed in the remarks column that indicates the percentage of deliverability to be allocated to this zone of the well.

Any test prescribed herein will be considered acceptable if the average flow rate for the final 7-day or 8-day deliverability test is not more than ten percent in excess of any consecutive 7-day or 8-day average of the preceding two weeks. A deliverability test not meeting this requirement may be declared invalid, requiring the well to be re-tested.

All charts relative to initial, annual, or biennial deliverability tests or copies thereof shall be made available to the Division upon its request.

All testing agencies, whether individuals, companies, pipeline companies, or operators, shall maintain a log of all tests accomplished by them, including all field test data. The operator shall maintain the above data for a period of not less than two (2) years plus the current test year.

All forms heretofore mentioned are hereby adopted for use in the northwest New Mexico Area in open form subject to such modification as experience may indicate desirable or necessary. Initial and Annual or Biennial Deliverability and Shut-In Pressure Tests for gas wells in all formations shall be conducted and reported in accordance with these rules and procedures. Provided however, these rules shall be subject to any specific modification or change contained in Special Pool Rules adopted for any pool after notice and hearing.

CHAPTER III INFORMATIONAL TESTS

A. A one-point back pressure test may be taken on newly completed wells before their connection or reconnection to a gas transportation facility. This test shall not be a required official test but may be taken for informational purposes at the option of the operator. When taken, this test must be taken and reported as prescribed below:

ONE-POINT BACK PRESSURE POTENTIAL TEST PROCEDURE

- This test shall be accomplished after a minimum shut-in of seven days. The shut-in pressure shall be measured with a deadweight gauge or other method approved by the Division.
- 2. The flow rate shall be that rate in Mcf/d measured at the end of a three hour test flow period. The flow from the well shall be for three hours through a positive choke, which has a 3/4-inch orifice.
- 3. A 2-inch nipple which provides a mechanical means of accurately measuring the pressure and temperature of the flowing gas shall be installed immediately upstream from the positive choke.
- 4. The absolute open flow shall be calculated using the conventional back pressure formula as shown in this manual or the New Mexico Oil Conservation Division "Back Pressure Test Manual."
- 5. The observed data and flow calculations shall be reported in duplicate on Form C-122, "Multi-Point Back Pressure Test for Gas Wells."
- 6. Non-critical flow shall be considered to exist when the choke pressure is 13 psig or less. When this condition exists the flow rate shall be measured with a pitot tube and nipple as specified in this manual or in the Division's Manual of "Tables and Procedure for Pitot

Tests." The pitot test nipple shall be installed immediately downstream from the 3/4-inch positive choke.

- 7. Any well completed with 2-inch nominal size tubing (1.995-inch ID) or larger shall be tested through the tubing.
- B. Other tests for informational purposes may be conducted prior to obtaining a pipeline connection for a newly completed well upon receiving specific approval therefor from the Division's Aztec office. Approval of these tests shall be based primarily upon the volume of gas to be vented.

CHAPTER IV <u>TYPE OF TESTS REQUIRED FOR WELLS COMPLETED IN</u> NON-PROBATED POOLS

- SECTION 1: Initial Shut-In Pressure Tests for Newly Completed Wells
- A. (Same as Chapter I, Section 1, A)
- SECTION 2: Biennial Shut-In Pressure Tests
- A. Non-prorated wells will be tested biennially as required by the District Office except as follows:
 - Wells which meet the "exempt" qualification as shown in Chapter I, Section 2, paragraph A-2 of these rules shall also be exempt from shut-in test requirements.
 - 2. Wells classified as "hardship" wells during the test year shall also be exempt from shut-in test requirements.
- B. All shut-in tests required by these rules must be filed with the Division's Aztec office by January 31 of the following year. Failure to file the test will subject the well to being shut-in one day for each day the test is late.

SECTION 3: <u>Scheduling Tests</u>

A. By September 1 of each year, the District Supervisor of the Aztec District Office of the Division shall by memorandum notify each gas transportation facility and each operator of the pools which are to be scheduled for biennial shut-in pressure testing during the following testing period from January 1 through the last day of December of that test year. The District Supervisor will also provide a list of "exempt" wells.

Any well scheduled for testing during its test year may have the test flow period, and some of the seven day shut-in period conducted in December of the previous year. The earliest date that a well could be scheduled for Biennial Shut-In Pressure Test would be such that the Test Flow Period would end on December 25 of the previous year.

Downhole commingled wells are to be scheduled for tests on dates for pool of lowermost completion of well.

SECTION 4: <u>Test Procedure</u>

A. To obtain the shut-in pressure of a well under test, the well shall be shut-in some time during the current testing season for a period of seven to fourteen consecutive days, which have been preceded by a minimum of seven days of uninterrupted production. Such shut-in pressure shall be measured by deadweight gauge or other method approved by the Division on the seventh to fourteenth day of shut-in of the well. The shut-in pressure shall be measured on both the tubing and the casing when communication exists between the two strings. The higher of such pressures shall be reported as the shut-in pressure of the well

SECTION 5: Filing of Shut-In Pressure Data

The results of this test will be filed in triplicate on Form C-125-B showing the pressures in psia in column labeled "S. I. PRESSURE PSIA (DWT)" with the Aztec District Office.

NOTES FOR TESTIMONY DECEMBER 3, 1986

FIRST, I NEED TO MAKE SOME COMMENTS ABOUT THE PREVIOUS TESTIMONY GIVEN IN THIS CASE ON _______. AT THAT HEARING I WAS SUPPOSEDLY READING INTO THE RECORD SOME OF THE MATERIAL CONTAINED IN THE TEST PROCEDURE THAT WE IN THE COMMITTEE HAVE FORMULATED AND DOING SO, I PARAPHRASED SOME OF THE WORDS FROM THE DOCUMENT. REGARDLESS OF WHAT I READ THAT DAY, OR MAY SAY TODAY, THE WRITTEN TEXT AS WE HAVE IT IS THE TEXT THAT WE WOULD LIKE TO SUBMIT TO THE DIVISION TO BE ENACTED AS THE RULES OF PROCEDURE FOR TESTING IN THE SAN JUAN BASIN, UNLESS IT IS DECIDED AT THIS HEARING TO SPECIFICALLY CHANGE CERTAIN WORDS IN THE WRITTEN TEST.

NOW, WITH THAT OUT OF THE WAY, LET US SEE WHAT WE HAVE TODAY THAT IS DIFFERENT TO WHAT WAS PRESENTED AT THE LAST HEARING.

I BELIEVE THAT THE TEST AS I HAVE IT HERE TODAY IS THE RESULT OF CHANGES SUGGESTED AT THE LAST HEARING PLUS CHANGES THAT WERE MADE BY THE COMMITTEE AT ITS MORE RECENT MEETINGS.

ONE OF THOSE CHANGES IS THE ADDITION OF A PARAGRAPH ON PAGE SEVEN. THIS IS THE SECOND PARAGRAPH ON THE PAGE. I WILL READ THIS PARAGRAPH IN ITS ENTIRETY AS IT IS A SHORT PARAGRAPH. QUOTE:

"IF A WELL IS PRODUCING THROUGH A COMPRESSOR THAT IS LOCATED BETWEEN THE WELLHEAD AND THE METER RUN, THE METER RUN PRESSURE AND THE WELLHEAD CASING PRESSURE AND THE WELLHEAD TUBING PRESSURE ARE TO BE REPORTED ON FORM C-122-A. (NEITHER THE SUCTION PRESSURE NOR THE DISCHARGE PRESSURE OF THE COMPRESSOR IS CONSIDERED WELLHEAD PRESSURE.) A NOTE SHALL BE ENTERED IN THE REMARKS PORTION ON FORM C-122-A STATING 'THIS WELL PRODUCES THROUGH A COMPRESSOR'."

THIS PARAGRAPH HAS BEEN PLACED INTO THE PROCEDURE BECAUSE WE BELIEVE THAT THERE ARE (OR HAVE BEEN) TESTERS IN THE AREA THAT HAVE NOT FULLY UNDERSTOOD WHAT THE CORRECT PROCEDURE SHOULD BE WHEN A COMPRESSOR IS IN USE ON AN INDIVIDUAL WELL.

THE COMMITTEE BELIEVES THAT THIS TESTING PROCEDURE WILL DEFINE THE TYPES OF TESTS THAT ARE REQUIRED IN THE SAN JUAN BASIN, AND THAT EVERYONE TESTING WELLS IN THE AREA WILL DO IT IN THE SAME MANNER. AT LEAST, THIS IS OUR INTENTION.

ALONG WITH THIS TEXT, WE ARE SUBMITTING A GROUP OF TABLES TO BE INCORPORATED INTO THE TEST MANUAL. THESE TABLES INCLUDE:

- 1. A TABLE OF VALUES OF 1-e^{^s} CALCULATED FOR VARIOUS VALUES OF GRAVITY TIMES LENGTH.
- 2. A SET OF TABLES FOR FRICTION FACTORS (F_c) FOR SMALL AND LARGE SIZE TUBING AND FOR ANNULAR FLOW WITH VARIOUS COMBINATIONS OF CASING AND TUBING SIZES.
- 3. A TABLE OF FLOW RATES DETERMINED FROM PITOT TUBE IMPACT PRESSURE READINGS FOR WELL TESTS TO DETERMINE THE OPEN FLOW POTENTIAL OF THE WELL. THESE TABLES HAVE IMPACT PRESSURES MEASURED IN INCHES OF WATER, OUNCES PER SQUARE INCH, INCHES OF MERCURY, AND POUNDS PER SQUARE INCH.
- 4. THE PITOT TABLES JUST MENTIONED WERE CALCULATED FOR AN ELEVATION OF 6,000 FEET. ALSO THEY WERE CALCULATED USING A GRAVITY OF THE GAS AS 0.600. THEREFORE, TO MAKE CORRECTIONS TO THE FLOW RATE IN THE PITOT TABLES FOR GAS AT OTHER THAN 0.600 A TABLE OF SPECIFIC GRAVITY CORRECTIONS IS SUBMITTED.
- 5. OTHER TABLES AND EXAMPLES OF CALCULATIONS FOR VARIOUS PROCEDURES ARE TO BE TAKEN FROM THE BACK PRESSURE MANUAL AS PUBLISHED BY THE NMOCC. THE COPY THAT I HAVE IS DATED AS JANUARY 1, 1966. THE PAGES OF MATERIAL THAT SHOULD BE DUPLICATED FROM THIS MANUAL AND PLACED IN THE MANUAL FOR TESTING GAS WELLS IN THE SAN JUAN BASIN ARE LISTED AS FOLLOWS: (see attached list of pages).
- 6. THERE ARE OTHER PAGES THAT ARE BEING SUBMITTED. ONE IS A COPY OF A FORM C-122-A THAT HAS VALUES WRITTEN IN THE VARIOUS BLANK SPACES INDICATING HOW THE VALUES ARE ENTERED AND A PAGE OF TEXT INDICATING HOW THE VALUES ARE DETERMINED.
- 7. A FORM C-122 IS INCLUDED WITH A PAGE OF DESCRIPTION INDICATING HOW EACH BLANK IS FILLED IN ON THAT FORM.
- 8. OTHER DATA?

CASE NO. 9050 AS ADVERTISED ON THE DOCKET FOR DECEMBER 3, 1986 INCLUDES LANGUAGE THAT ASKS TO DEFINE "RETESTS" IN ORDER NO. R-8170. WE FEEL THIS IS NECESSARY TO COVER THE PROCESS APPLIED TO DELIVERABILITY RETESTS AS THEY OCCUR IN THE SAN JUAN BASIN. WE ARE LOOKING FOR A PROCEDURE TO BE APPLIED TO ALL WELLS SO THAT THEY CAN BE TREATED AUTOMATICALLY, AND, ALL IN THE SAME MANNER WHEN SO NEEDED. THE DEFINITION OF DELIVERABILITY RETEST AS WE HAVE IT DEFINED AND AS WE PROPOSE THAT IT REPLACE THE RULE 9(b) THAT IS PRESENTLY IN ORDER NO. R-8170 IS:

"RULE 9(b) DELIVERABILITY RETESTS: A change in a well's deliverability due to retest after any activity, other than routine

maintenance, which changes the deliverability of the well shall become effective the later of:

(1) the date of redelivery after such activity, such date to be indicated on the sundry notice (if a sundry notice is required) and on the remarks portion of the Form C-122-A; or

(2) 90 days prior to the date of receipt of the appropriate deliverability test report form at the appropriate Division district office.

A change in a well's deliverability due to any other reason shall become effective on the first day of the month following the month during which the retest is approved in the appropriate Division district office."

IN READING THE RULES AS WRITTEN IN ORDER NO. R- 8170, FOR THE FOUR PRORATED GAS POOLS OF NORTHWEST NEW MEXICO, I NOTICE THAT RULE 9(a) IN INCLUDED IN EACH OF THE SPECIAL POOL RULES. I FEEL THAT IT IS NOT NECESSARY TO INCLUDE RULE 9(b) IN EACH OF THE SPECIAL POOL RULES AS IT IS A COMMON RULE TO ALL OF THOSE POOLS.

THERE HAS BEEN A LITTLE BIT OF A PROBLEM IN BEING ABLE TO PLEASE COMPLETE THE TESTING OF ALL THE WELLS DURING THE 1986 TEST YEAR THAT ARE REQUIRED TO BE TESTED. THE COMMITTEE AT ITS LAST MEETING THOUGHT THAT IT WOULD BE POSSIBLE TO COMPLETE THE 1986 TESTS BY MARCH 31, 1987. WITH THIS LATE COMPLETION DATE, WE THOUGHT IT MIGHT BE NECESSARY TO SUSPEND THE TESTING REQUIREMENTS FOR THOSE WELLS IN THE POOLS THAT WOULD NORMALLY BE REQUIRED TO BE TESTED IN 1987 AND THEN THOSE WELLS IN THOSE POOLS WOULD BE TESTED IN 1988. AFTER MUCH DISCUSSION IT WAS DECIDED TO MAKE THIS RECOMMENDATION TO THE N DIVISION. AFTER THIS MEETING, SOME OPERATORS AND PIPELINE 0 COMPANIES HAVE MADE INDICATIONS THAT THEY WOULD PREFER TO GO TE AHEAD AND TEST IN THE NORMAL MANNER IN 1987. FOR ADDITIONAL DATA CONCERNING THIS POINT I BEG THE EXAMINERS INDULGENCE TO HEAR REPORTS FROM THOSE OPERATORS AND PIPELINES THAT ARE 11 PRESENT AND TAKE ACTION AS FURTHER RECOMMENDED.

HOWEVER, IN THE EVENT THE DIVISION DOES CHOOSE TO SUSPEND THE TESTING FOR 1987, IT IS OUR FIRM RECOMMENDATION THAT SHUT IN PRESSURE TESTS BE SCHEDULED FOR MEASUREMENT WITH A MINIMUM OF SEVEN DAYS PRE-FLOW PRIOR TO BEING SHUTIN; AND, THAT FULL DELIVERABILITY TESTS BE CONDUCTED ON WELLS THAT HAVE NOT MET THE REQUIREMENT OF HAVING FILED AT LEAST THREE ANNUAL DELIVERABILITY TESTS BEFORE BEING PLACED ON THE BIENNIAL TESTING SCHEDULE OR THE SUSPENSION LIST FOR 1987. WELL TESTING IN NON-PRORATED POOLS WOULD NOT BE SUSPENDED FOR 1987 AND THE TESTS WOULD BE SCHEDULED AND TESTED ACCORDING TO THE NORMAL PROCEDURE.

I SUBMIT TO THE EXAMINER A LIST OF NAME AND ADDRESSES THAT I HAVE COMBINED AS MEMBERS OF THE NMOCD DELIVERABILITY TEST COMMITTEE AS IT HAS PROGRESSED THROUGH THESE NEARLY 3 YEARS, AND I EXPRESS MY THANKS TO EACH AND ALL OF THEM FOR THEIR PATIENCE AND THOUGHTFUL WORK IN MAKING THIS MANUAL POSSIBLE. EI00-55-W-1



MICHAEL E. STOGNER NMOCD P.O. BOX 2088 SANTA FE, NM 87501

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P. O. BOX 1492 EL PASO, TEXAS 79978

MEMORANDUM

To: Deliverability Test Committee

From: H. L. Babe Kendrick

Date: November 18, 1986

This morning I found the opportunity to write up a couple of tables to be included in the Manual for the San Juan Basin. These tables are for the temperature corrections and for the specific gravity corrections for gas flow through flow nipples measured with a pitot tube or with the pressure on the choke. You will note that the temperature chart has 60°F as the base temperature with a correction of 1.000 and the specific gravity table has a gravity of 0.600 as the base and is <u>not</u> with a 1.000 specific gravity base. In making the tables for Pitot Tube Flow and for Friction Factors for various sizes of flow strings, I tried to make the coefficients using a temperature and specific gravity base of 60°F and 0.600 respectively. I hope that I have done the jobs correctly.

Again I plead with you to look these over very, very carefully to see if they are prepared correctly **and** are they done in the manner that you want them.

For the supercompressibility tables, how about using the first page out of the old publication that was reprinted by the NMOCD that originally came from the California Gas Association (or where—ever they came from). I do not have a copy of it here in El Paso, but as I remember the listing on the first page, it would cover most of the gas tested provided the pressure was above 50 psi or maybe it was 500 psi. What I am getting at is to print the least amount of tables that are necessary to get the job done. If this table is not adequate, then we might have to duplicate the tables that are in the Back Pressure Test Manual for New Mexico. (I think they are only 67 pages.)

So far I have not made the tables for choke coefficients. Do you have one made that can be used??

After today, I will be in the office in El Paso 4 days before the hearing on the 3rd of December. Those dates are November 21, 25, 26, and December 1. If you have things to help us, let me know and send it in. Thank you.

Please look this over good and let me know what changes need to be made.

I have noticed that December 3rd is racing along at an unprecedented speed. I hope that I can get through before it gets me.

Ele Q

Babe

Observed										
Temp.	. 0	1	2 .	3	4	5	6	7	8	9
۴										
0	1.063	1.062	1.061	1.060	1.059	1.057	1.056	1.055	1.054	1.053
10	1.052	1.051	1.050	1.049	1.047	1.046	1.045	1.044	1.043	1.042
20	1.041	1.040	1.039	1.038	1.037	1.035	1.034	1.033	1.032	1.031
30	1.030	1.029	1.028	1.027	1.026	1.025	1.024	1.023	1.022	1.021
40	1.020	1.019	1.018	1.017	1.016	1.015	1.014	1.013	1.012	1.011
50	1.010	1.009	1.008	1.007	1.006	1.005	1.004	1.003	1.002	1.001
60	1.000	. 9990	.9981	. 9971	. 9962	. 9952	. 9943	. 9933	.9924	.9915
70	. 9905	. 9896	.9887	.9877	. 9868	. 9859	. 9850	.9840	. 9831	. 9822
80	. 9813	. 9804	. 9795	.9786	.9777	.9768	.9759	.9750	.9741	.9732
90	.9723	.9715	.9706	. 9697	. 9688	. 9680	.9671	.9662	. 9653	.9645
100	. 9636	. 9628	.9619	.9611	.9602	. 9594	. 9585	. 9577	. 9568	.9560
110	. 9551	.9543	. 9535	. 9526	.9518	.9510	.9501	. 9493	. 9485	.9477
120	. 9469	. 9460	. 9452	. 9444	. 9436	. 9428	.9420	. 9412	.9404	. 9396
130	. 9388	. 9380	.9372	. 9364	. 9356	. 9349	. 9341	. 9333	. 9325	. 9317
140	. 9309	. 9302	. 9294	. 9286	.9279	. 9271	. 9263	. 9256	. 9248	.9240
150	. 9233	. 9225	. 9218	.9210	. 9203	. 9195	. 9188	.9180	.9173	. 9166
160	. 9158	. 9151	.9143	. 9136	. 9129	.9121	.9114	.9107	.9100	. 9092
170	. 9085	. 9078	.9071	. 9064	.9056	. 9049	. 9042	. 9035	. 9028	.9021
180	. 9014	. 9007	. 9000	. 8993	. 8986	. 8979	. 8972	. 8965	. 8958	. 8951
190	. 8944	. 8937	. 8931	. 8924	.8917	. 8910	. 8903	. 8896	. 8890	. 8883
200	.8876	. 8870	. 8863	. 8856	. 8849	. 8843	. 8836	. 8830	. 8823	. 8816
210	.8810	. 8803	.8797	. 8790	.8784	.8777	.8771	. 8764	. 8758	.8751
220	.8745	. 8738	. 8732	. 8726	.8719	. 8713	.8706	.8700	. 8694	. 8687
230	. 8681	. 8675	. 8669	. 8662	. 8656	.8650	. 8644	.8637	.8631	. 8625
240	.8619	. 8613	. 8607	.8601	. 8594	. 8588	. 8582	.8576	.8570	. 8564
250	.8558	. 8552	. 8546	. 8540	. 8534	. 8528	.8522	.8516	.8510	. 8504

Specific	I	r	r	Г						·
Gravity		001	.002	. 003	. 004	.005	. 006	. 007	. 008	. 009
.510	1.085	1.084	1.083	1.081	1.080	1.079	1.078	1.077	1.076	1.075
. 520	1.074	1.073	1.072	1.071	1.070	1.069	1.068	1.067	1.066	1.065
. 530	1.064	1.063	1,062	1.061	1.060	1.059	1.058	1,057	1.056	1.055
. 540	1.054	1.053	1.052	1.051	1.050	1,049	1.048	1.047	1.046	1.045
.550	1.044	1.044	1.043	1.042	1.041	1.040	1.039	1.038	1.037	1.036
. 560	1.035	1.034	1.033	1.032	1.031	1.031	1.030	1.029	1.028	1.027
.570	1.026	1.025	1.024	1.023	1.022	1.022	1.021	1.020	1.019	1.018
. 580	1.017	1.016	1.015	1.014	1.014	1.013	1.012	1.011	1.010	1.009
. 590	1.008	1.008	1.007	1.006	1.005	1.004	1.003	1.003	1.002	1.001
. 600	1.000	. 9992	. 9983	.9975	. 9967	. 9959	. 9950	. 9942	. 9934	. 9926
. 610	. 9918	.9910	. 9901	. 9893	. 9885	.9877	. 9869	. 9861	. 9853	. 9845
. 620	. 9837	. 9829	. 9822	. 9814	.9806	.9798	.9790	.9782	.9775	. 9767
. 630	. 9759	.9751	.9744	.9736	.9728	.9721	. 9713	.9705	. 9698	. 9690
. 640	. 9682	. 9675	. 9667	.9660	. 9652	. 9645	. 9637	. 9630	. 9623	. 9615
. 650	.9608	.9600	. 9593	. 9586	.9578	.9571	. 9564	. 9556	. 9549	. 9542
. 660	. 9535	. 9527	.9520	. 9513	.9506	. 9499	. 9492	. 9484	.9477	.9470
. 670	. 9463	. 9456	. 9449	.9442	. 9435	. 9428	.9421	. 9414	. 9407	. 9400
. 680	. 9393	. 9386	. 9380	. 9373	. 9366	. 9359	. 9352	. 9345	. 9339	. 9332
. 690	. 9325	. 9318	. 9312	.9305	. 9298	. 9291	. 9285	. 9278	. 9271	. 9265
.700	. 9258	. 9252	. 9245	. 9238	. 9232	. 9225	. 9219	. 9212	. 9206	. 9199
.710	.9193	. 9186	.9180	.9173	.9167	. 9161	. 9154	. 9148	. 9141	. 9135
. 720	.9129	.9122	. 9116	.9110	. 9103	. 9097	. 9091	. 9085	. 9078	. 9072
_ 730	. 9066	.9060	. 9054	. 9047	. 9041	. 9035	. 9029	. 9023	. 9017	. 9011
. 740	.9005	. 8998	<u> </u>	. 8986	. 8980	. 8974	. 8968	. 8962	. 8956	. 8950
. 750	. 8944	. 8938	. 8932	. 8926	. 8921	. 8915	. 8909	. 8903	. 8897	. 8891
. 760	. 8885	. 8879	. 8874	. 8868	. 8862	. 8856	. 8850	. 8845	. 8839	. 8833
. 770	. 8827	·. 8822	.8816	. 8810	. 8805	. 8799	. 8793	.8787	. 8782	.8776
. 780	.8771	.8765	. 8759	. 8754	. 8748	.8743	.8737	.8731	.8726	.8720
. 790	.8715	.8709	.8704	. 8698	. 8693	. 8687	. 8682	.8677	.8671	. 8666
. 800	.8660	. 8655	. 8649	.8644	. 8639	. 8633	. 8628	. 8623	.8617	.8612
.810	.8607	.8601	. 8596	.8591	. 8585	. 8580	.8575	.8570	.8564	.8559
.820	. 8554	.8549	.8544	.8538	.8533	. 8528	.8523	.8518	.8513	.8507
. 830	. 8502	.8497	.8492	. 848/	. 8482	.84//	.84/2	.8467	. 8462	. 8457
.840	.8452	.8447	. 844)	. 8430	.8431	.8427	. 8422	.8417		. 8407
. 050	. 8402	. 6397	. 8392	. 8387	. 8382	.83//	.0372	.8307	. 8302	. 8358
.000	.0303	. 0340	.0343	.0330	.0333	.0329	. 0324	.0319	.0314	.0309
. 070	0303	.0300	. 0293	. 0290	. 0200	. 0201	. 02 /0	.0211	. 0207	. 0202
.000	.0237	. 0233	.0240	0243	0102	.0234	.0229	.0223	.0220	9170
. 090	9165	9160	9166	0151	0192	0100	0100	0122	01/4	8124
. 900	.0105	.0100	.0130	9107	.0147	.0142	.0130	<u>.0133</u>	0129 0005	8024
.910	9076	.0110	.0111	2010.	0050	. 0090	.0093	.0009	.0003	9027
. 920	.0070	2071	8024	8010	801E	8011	0000	0040	7000	7004
040	7020	70020	7024	7077	- 0013	7060	7064	7050	7055	7051
050	70/7	. 1903	7020	7025	7021	702	7022	7010	7014	7010
060	7006	7002	7807	7902	7880	7895	7921	7910	7914	7860
<u> </u>	7865	7861	7957	7952	7840	7845	78/1	- 10/1	7922	7820
	7825	7821	7817	7812	7800	7805	7801	7707	2000	7780
	7785	7781	7777	- 1013	7760	7765	7762	7759	7754	7750
. 330					1.1109			. //30	1.1134	1.110

PITOT TUBE TABLES FOR SAN JUAN BASIN

The Pitot Tube Tables on the accompanying pages were calculated using the equations found in <u>Handbook of Natural Gas Engineering</u> by Katz, Cornell, Kobayashi, Poettmann, Vary, Elenbaas, and Weinaug as published by McGraw—Hill Book Company. The atmospheric pressure at an elevation of 6,000 feet, which was selected as an average elevation for wells in the San Juan Basin area of northwest New Mexico, was calculated using the following equation:

Using this pressure in the formula

 $Q = C D^2 (h_V P / G)^{0.5}$ Mcf/day at a pressure base of 14.7 and a gas gravity of 0.600.

where:

$$C = 31.14371055$$

Correcting to a pressure base of 15.025 then

 $Q = 30.47005292 D^2 (h_v)^{0.5} Mcf/day$

where:

D = pipe diameter in inches $h_V = impact-velocity head in inches of water$

Note: The values in the accompanying tables were calculated by use of an Apple Lisa computer and the values shown for C were not individually calculated.

El Paso Natural Gas Company P. O. Box 1492 El Paso, Texas 79978

April 2, 1986

Mr. Al Greer, P. E. 211 Petroleum Center Building Farmington, New Mexico 87401

Dear AI:

Thank you for your letter of September 5, 1985 enlightening me about calculations necessary for Pitot Tube Tables for the San Juan Basin.

I have used your data and followed through with the calculations for a set of tables to be used and in this data I arbitrarily used the atmospheric pressure at an elevation of 6,000 feet which calculates to be 11.88.....thinking that a 6,000 foot elevation should be about the average for wells in the San Juan Basin.

Al, if you have an opportunity to look at some of this data, one more time, I would certainly appreciate it.

The pages I have enclosed with this letter are numbered 1, 2, 23, 24, 46, 47, and 58 which are laid out in rectangles with a formula written in to tell what was done to get the answer that is in each block. Each block is identified by a letter and number as: Q1 and Q11. The value in each block can be used to multiply (or + - /) with other values from other blocks. Page 1 would represent the upper left corner of a large page. Page 2 fits immediately below page 1. Page 23 fits immediately to the right of page 1 and page 24 fits to the right of page 2. Then page 45 fits to the right of page 23 and page 46 fits to the right of page 24.

The calculation for atmospheric pressure at 6,000 feet was done in block S7 on page 45. (Data in blocks S5 and S6 was used in block S7.)

Various portions of the flow formulas from Katz appear in blocks Q1, Q3, Q7, Q9, Q10, all on page 45 and in block Q11 on page 46. Block Q12 was used merely to show a value of C = 30.47005292 at a pressure base of 15.025. Block Q12 was not used in the calculations of the tables elsewhere as I had put the pressure base correction to 15.025 into each separate block as you con see in block D7 on page 1.

Page 58 has a value shown in block Q112 which is the conversion factor I used to convert pressure in inches of water to pressure in pounds per square inch. Multiply inches of water times Q112 equals psi.

To convert from pressure in inches of water to pressure in inches of mercury, I divided the reading in inches of water by 13.59.

To convert from pressure in inches of mercury to pressure in psi, I multiplied the reading in inches of mercury by 14.676 divided by 29.92.

When impact pressures exceeded what might be measured in inches of water, the table was made to progress in inches of mercury. To change the formula to calculate these flow rates I multiplied the reading in inches of mercury by 13.59 to convert that reading into inches of water. (From 3" Hg to 30" Hg.)

When impact pressures exceeded what might be measured in inches of mercury, the table was made to progress in pounds per square inch. To change the formula to calculate these flow rates I multiplied the reading in psi by 144 times 12 divided by 62.428 to convert that reading inches of water. (From 15 psi to end of table.)

All calculated values were made to fourteen significant figures and only the final values in Mcf/day were rounded to the nearest integer.

I have also enclosed 6 pages which will be the table printed in the test manual if these values are correct.

AI, I certainly do appreciate all you have done to help in making these tables as correct as possible and someday soon, I hope to see them in print by the NMOCD.

Sincerely,

H. L. Kendrick
FRICTION	FACTORS	(Fc)	For	LARGE	DIAMETER	FLO₩	STRINGS
CASING	CASING	CASING	FRICTION	CASING	CASING	CASING	FRICTION
NOMINAL	WEIGHT	INSIDE	FACTOR	NOMINAL	WEIGHT	INSIDE	FACTOR
SIZE	POUNDS	DIAMETER		SIZE	POUNDS	DIAMETER	
INCHES	PER FT.	INCHES	Fc	INCHES	PER FT.	INCHES	Fc
	·						
5.000	15.00	4.408	1.187	7.625	47.10	6.375	. 4577
5.000	13.00	4.494	1.129	7.625	45.00	6.445	. 4450
5.000	11.50	4.560	1.087	7.625	42.80	6.501	. 4352
				7.625	39.00	6.625	. 4144
		•		7.625	33.70	6.765	. 3927
5.500	25.00	4.580	1.075	7.625	29.70	6.875	. 3766
5.500	23.00	4.670	1.022	7.625	26.40	6.969	. 3637
5.500	20.00	4.778	. 9637	7.625	24.00	7.025	. 3562
5.500	17.00	4.892	.9068				
5.500	15.50	4.950	. 8796				
5.500	15.00	4.976	. 8 678	8.625	49.00	7.511	. 2997
5.500	14.00	5.012	. 8518	8.625	44.00	7.651	. 2858
5.500	13.00	5.044	. 8379	8.625	43.00	7.625	. 2883
				8.625	40.00	7.725	. 2787
				8.625	38.00	7.775	. 2741
6.000	26.00	5.140	. 7981	8.625	36.00	7.825	. 2696
6.000	23.00	5.240	. 7594	8.625	32.00	7.907	. 2625
6.000	20.00	5.352	.7190	8.625	32.00	7.921	. 2613
6.000	18.00	5.424	. 6 946	8.625	28.00	8.003	. 2544
6.000	17.00	5.450	. 6861	8.625	28.00	8.017	. 2533
6.000	15.00	5.524	. 6626	8.625	24.00	8.097	. 2469
				8.625	20.00	8.191	. 2396
				8.625	17.50	8.249	. 2353
6.625	34.00	5.595	.6411				
6.625	32.00	5.675	.6181		•		
6.625	28.00	5.791	. 5866	9.625	58.00	8.435	. 2221
6 .625	26.00	5.855	. 5702	9.625	53.50	8.535	. 2155
6.625	24.00	5.921	. 5539	9.625	47.00	8.681	. 2062
6.625	22.00	5.989	. 5378	9.625	43.50	8.755	. 2018
6.625	20.00	6.049	. 5242	 9.625	40.00	8.835	. 1971
				9.625	36.00	8.921	. 1922
	10.00			9.625	32.30	9.001	. 1878
7.000	40.00	5.836	. 5750				··· <u>·</u> ·····
7.000	38.00	5.920	. 5542		ļ		
7.000	35.00	5.004	. 5344		ļ	····	
7.000	32.00	6.094	.5142				
1.000	30.00	<u>b. 154</u>	.5014		Į		
7.000	29.00	D. 184	.4951				
7.000	28.00	0.214	. 4890				
7.000	20.00	0.270	.4/00		 		
1.000	24.00	0.330	. 4050				
1.000	23.00		. 4594	·			
	22.00	0.398	. 4535				
1.000	20.00	0.450	. 4430		ļ		
1.000	17.00	0.536	. 4200		l		

FRICTION	FACTORS	(Fc)	FOR	ANNUL	AR FLO	₩ IN	GAS	WELL	FLOW	STRINGS
									·	
CASING	CASING	CASING				TUBING		SIZES		
OUTSIDE	WEIGHT	INSIDE			OUTSIDE		DIAMETE	R	INCHES	
DIAMETER	POUNDS	DIAMETER								
INCHES	PER FT.	INCHES		1.050	1.315	1.660	1.900	2.0625	2.375	2.875
2.375	5.95	1.867		27.12	46.77	205.1				
2.375	4.70	1.995		20.54	32.13	91.08	. 651.7			
2.375	4.00	2.041		18.75	28.51	73.10	340.8			
		•								
2.875	8.70	2.259-	·	12.71	17.53	33.29	71.59	182.0		
2.875	6.50	2.441		9.609	12.56	20.74	35.41	60.71	948.2	
								0.1 7.1		
3.500	12.95	2.750 .	 	6.389	7.848	11.27	15.96	21.71	54.16	
3.500	9.30	2.992		4.846	5.762	1.133	10.13	12.71	23.17	309.3
3.500	7.70	3.068		4.472	5.271	6.957	8.949	11.03	18.95	136.3
			╞╼╼╼┥					·		
				0.450	0.005	A 470	E 444	0.005	0.055	00.54
4.000	11.60	3.428		3.156	3.605	4.4/9	5.411	6.295	9.055	23.54
4.000	11.00	3.4/6		3.024	3.442	4.250	5.102	5.902	8.358	20.43
4.000	10.40	3.500		2.960	3.364	4.141	4.957	5.719	8.039	19.11
4.000	*9.50	3.548		2.839	3.216	3.935	4.685	5.378	1.455	16.83
	- <u>-</u>									
	15 10	0.000		0.050	0 510	0.005	0.407	0.000	5 054	
4.500	15.10	3.826		2.259	2.518	2.995	3.46/	3.885	5.054	9.241
4.500	13.50	3.920		2.100	2.331	2. 149	3. 159	3.518	4.499	7.020
4.500	12.75	3.958		2.040	2.200	2.000	3.045	3.303	4.300	1.349
4.500	10.50	4.000		1.9//	2,100	2.303	2.921	3.243	4.095	6.070
4.500		4.052		1.903	2.099	2.431	2.709	3.001	3.001	0.339
4.300	9.00	4.090	┝──┥	1.031	2.039	2.314	2.094	2.970	3.702	5.990
5 000	24 10	1 000		1 077	2 196	2 562	2 027	2 242	1 005	6 870
5.000	24.10	4.000		1 902	1 084	2.303	2.927	2 870	9.093	5 695
5.000	21.40	4. 120		1.003	1.904	2.304	2.003	2.070	2 456	5 464
5 000	18 00	4 276	┝──┤	1 622	1 775	2.23	2.040	2.750	2 049	A 627
5,000	15.00	4.270		1 485	1 616	1 845	2.291	2.000	2 682	3 038
5.000	13.00	A AQA		1 403	1 524	1 731	1 021	2.200	2 478	3 564
5 000	11.50	4.560	-	1 345	1 457	1 650	1 826	1 972	2 336	3 312
0.000		1.000							2.000	0.012
			<u>├</u>						{	
5,500	25,00	4,580		1,328	1,438	1.627	1,799	1,941	2,295	3,241
5,500	23.00	4.670	<u>├</u> ──┤	1.249	1.356	1.527	1.682	1.809	2.124	2.948
5,500	20.00	4.778		1, 170	1.258	1.418	1.556	1.668	1.943	2.645
5,500	17.00	4,892	†	1.094	1, 173	1.315	1.437	1.536	1.775	2.373
5.500	15.50	4.950		1.058	1.133	1.257	1.381	1.474	1.697	2.250
5.500	15.00	4.976	t	1.043	1,115	1.237	1.357	1.447	1.664	2, 198
5,500	14.00	5.012		1.022	1.092	1.209	1.325	1.412	1.619	2.129
5,500	13,00	5.044	<u> </u>	1,003	1,072	1, 185	1,298	1,381	1,581	2.070
			ا				1			

FRICTION	FACTORS	(Fo)	FOR	ANNUL	AR FLU	w IN	GAS	WELL	FLOW	SIKINGS
040700	OAOTHO	OAOTHO	· · · · ·			TUDTUO		07750		
CASING	CASING	UASING			OUTOTOE	IUBING	DTANETE	SIZES	THOUSO	
DUISIDE		INSIDE			UNISTRE		DIAMETE	R	INCHES	
DIAREIER		DINNETER		1 050	1 015	1 600	1 000	0.0000	0.075	0.075
INCHES	PEK FI.	INCHES		1.050	1.315	1.000	1.900	2.0025	2.3/5	2.8/5
6.000	26.00	5.140		. 9513	1.014	1.118	1.209	1.295	1.475	1.907
6.000	23.00	5.240		.9011	. 9588	1.054	1.136	1.202	1.374	1.757
6.000	20.00	5.352		. 8492	. 9017	. 9875	1.062	1.121	1.260	1.609
6.000	18.00	5.424		.8179	. 8674	. 9480	1.018	1.073	1.202	1.523
6.000	17.00	5.450		.8071	. 8555	. 9343	1.002	1.056	1.182	1.493
6.000	15.00	5.524		.7772	. 8229	. 8968	. 9605	1.011	1.127	1.414
6 625	24 00			7500	7021	0620	0226	0607	1 070	1 244
6.625	34.00	5 675		7200	7614	8267	. 9220	. 9097	1.079	1.344
6 625	28 00	5 701		6814	7185	7780	8285	8680	0588	1 161
6.625	26.00	5.855		6609	6963	7528	8008	8381	9238	1 113
6 625	24,00	5,921		. 6407	.6744	7280	7735	8088	8896	1,067
6.625	22.00	5.989		. 6208	.6528	. 7037	.7467	. 7801	. 8563	1.023
6.625	20.00	6.049		. 6039	. 6345	. 6832	.7242	.7560	. 8283	. 9855
7.000	40.0 0	5.836		. 6669	. 7028	. 7601	.8089	. 8469	. 9340	1.127
7.000	38.00	5.920		.6410	.6747	. 7284	.7739	. 8093	. 8901	1.068
7.000	35.00	6.004	ļ	.0105	. 6481	. 6985	. /410	. / /40	. 8492	1.013
7.000	32.00	D. U94		. 3910	.0213	. 0004	. 7060	. /300	. 0002	. 9590
7.000	30.00	6 194		. 5750	5060	.0493	.00/1	7055	7700	. 9252
7.000	29.00	6 214		5606	5870	6310	6670	. 7033	7570	8021
7,000	26.00	6 276		5455	5716	6128	6472	6737	7336	8616
7 000	24 00	6.336		5313	5564	5050	6288	6541	7112	8326
7,000	23,00	6,366		. 5245	.5490	.5877	6199	. 6446	7003	8187
7.000	22.00	6.398		.5173	.5413	.5791	.6105	.6347	. 6890	.8041
7.000	20.00	6.456		. 5046	. 5277	. 5640	. 5941	.6173	. 6692	. 7788
7.000	17.00	6.538		. 4874	. 5093	. 5436	. 5720	. 5938	. 6425	.7448
7.005	47 10	<u> </u>		E004	F 460	5050	6470	6410	6071	
7.625	47.10	0.3/5		. 5224	. 5409	. 5852	.01/2	. 64 18	. 69/1	. 8145
7.625	43.00	0.443 6 501		. 3070	. 3303 5175	. 3000	. 3972	.0203	.0729	. 7500
7 625	30 00	6 625	 	4931	<u>, 3173</u> <u>1007</u>	5220	5/08	5702	6159	7111
7.625	33.00	6 765		4430	4628	4022	5165	5340	5760	6613
7 625	29.70	6.875	┼──┤	. 4247	. 4424	4698	4923	5094	5473	6256
7.625	26.40	6.969		.4092	. 4259	. 4517	. 4728	. 4889	5244	. 5973
7.625	24.00	7.025		. 4004	. 4165	. 4414	. 4618	. 4772	.5114	. 5813

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FRICTION	FACTORS	(Fc)	FOR	ANNUL	AR FLO	W IN	GAS	WELL	FLOW	STRINGS
CASING	CASING	CASING				TUBING		SIZES		
OUTSIDE	WEIGHT	INSIDE			OUTSIDE		DIAMETE	R	INCHES	[
DIAMETER	POUNDS	DIAMETER								
INCHES	PER FT.	INCHES		1.050	1.315	1.660	1.900	2.0625	2.375	2.875
	•									
0.625	40.00	7 511	 	7007	0450	0644	0704	2000	4100	4650
0.023	49.00	7.511	┨╌╌┨	. 3337	. 3430	. 3044	. 3/94	. 3900	. 4155	. 4050
0.025	44.00	7.051	┨───┤	. 3174	. 3260	. 3458	. 3590	0707	. 3920	.4311
8.625	43.00	1.625	┟───┤	. 3203	. 3317	. 3491	. 3032	.3/3/	. 3967	. 4426
8.625	40.00	1.125		. 3092	. 3200	. 3354	. 3497	. 3595	. 3812	. 4242
8.625	38.00	1.775	 	. 3038	. 3144	. 3303	. 3432	. 3528	.3738	. 4155
8.625	36.00	7.825		. 2986	. 3088	. 3244	. 3369	. 3463	. 3666	. 4069
8.625	32.0 0	7.907		. 2903	. 3001	.3149	. 3269	. 3358	. 3552	. 3935
8.625	32.00	7.921		. 2889	. 2965	. 3134	. 3252	. 3341	. 3533	. 3912
8.625	28.00	8.003		. 2810	. 2903	. 3044	.3157	. 3241	. 3424	. 3785
8.625	28.00	8.017		. 2796	. 2889	. 3029	. 3141	. 3225	. 3406	. 3764
8.625	24.00	8.097		.2722	. 2811	. 2945	. 3053	. 3133	. 3306	. 3646
8.625	20.00	8. 191		. 2639	. 2723	. 2851	. 2953	. 3029	. 3193	. 3515
8.625	17.50	8.249		. 2589	. 2671	. 2795	. 2894	. 2967	. 3126	. 3437
			 							
9 625	58 00	8 435		2438	2513	2625	2715	2781	2925	3203
9,625	53.50	8.535		. 2362	. 2433	.2540	. 2625	. 2688	. 2824	.3087
9,625	47.00	8,681		. 2255	. 2323	.2422	.2501	. 2550	. 2685	. 2928
9,625	43.50	8,755		. 2205	. 2269	. 2365	.2441	.2498	.2618	. 2851
9,625	40,00	8,835		. 2152	. 2214	. 2306	.2379	.2433	.2549	.2772
9,625	36.00	8.921	<u> </u>	. 2097	. 2156	. 2245	.2315	.2367	.2477	. 2690
9.625	32.30	9.001		. 2047	.2104	. 2190	. 2257	. 2307	.2413	.2617
			• #		· · · · · · · · · · · · · · · · · · ·				• · · · · · · · · · · · · · · · · · · ·	· · · · · · · · · · · · · · · · · · ·

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Con File Dee 3

To: Deliverability Test Committee

From: H. L. Babe Kendrick

Case 9050

Date: November 17, 1986

Attached is a table for Pitot Tube Test Values for your edification. This thing was done quite rapidly from the latest table you have, and I have not had an opportunity to even scan the pages to see just how many things are wrong.

Please look this over good and let me know what changes need to be made.

I have noticed that December 3rd is coming around the corner fast. I hope that i can out run it.....

Babe

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PITOT	TUBE	IMPACT	PRESSURE	FLOW	NIPPLE	INSIDE	DIAMETER
INCHES	OUNCES/	INCHES	LBS. PER	1" nominal	2" nominal	3" nominal	4" nominal
WATER	SQ. IN.	MERCURY	50. IN.	actual dia.	actual dia.	actual dia.	actual dia.
L	ļ	<u> </u>	ļ	1.049	2.067	3.068	4.026
ļ	 	 	ļ				
<u> </u>	ļ	•		11	41	91	156
.2	ļ			15	58	128	221
.3	<u> </u>			18	71	157	271
.4	ļ		[21	82	181	312
.5	<u> </u>	1	<u> </u>	24	92	203	349
<u>-</u>	 			20		222	303
<u> </u>				20	109	240	413
	52	<u> </u>		30	124	23/	442
	. 52				124	212	409
1 1	┼────	<u>+</u>	 	25	127	201	519
+ <u>12</u>	<u> </u>		<u> </u>	27	142	214	510 641
13		<u> </u>		28	143	227	562
1.0	<u> </u>	<u> </u>	<u> </u>	40	154	320	584
15	<u> </u>		+	<u> </u>	150	251	605
1.0		+	1	47	165	363	625
17	98			44	170	374	644
1.8				45	175	385	663
1.9		+	1	46	179	395	681
2.0	<u> </u>	1	1	47	184	406	698
2.1		1		49	189	416	716
2.2			1	50	193	425	733
2.3				51	197	435	749
2.4				52	202	444	765
2.5				53	206	453	781
2.6	1.50			54	210	462	796
2.7		. 20		55	214	471	812
2.8				56	218	480	826
2.9				57	222	488	841
3.0			L	58	225	497	855
3.1	ļ	· · · · ·	<u> </u>	59	229	505	870
3.2	1		l	60	233	513	883
3.3	<u> </u>			61	236	521	897
3.4		_	ļ	02	240	529	<u> </u>
3.5	2.02		<u> </u>	03			924
3.0	<u> </u>	+	<u> </u>	04 EA	24/	1 244	93/
3.1	<u> </u>		<u> </u>	0 9	230		
3.0	<u> </u>	+	<u> </u>		234	209	903
3. ¥	+	+	<u> </u>	67	201	574	099
A 1		20	······································	89	264	591	1 000
A 2			<u> </u>	00	267	599	1 012
A 2	2 40	+	<u> </u>	70	270	505	1 024
	2.43	+	 	70	272	602	1 026
45	<u> </u>	+	+	71	276	602	1 048
4.5	+	+	<u> </u>	72	270	615	1 050
L		4	L	<u> </u>			

8.2 8.3 8.4 8.5 8.6 8.6 8.7

8.8 8.9 9.0 9.1

9.2

5.03

							-
PTTOT	TURF	TMPACT	PRESSURE	FLOW	NTPPI E	TNSIDE	DIAMETER
INCHES	OUNCES/	INCHES	LBS. PER	1" nominal	2" nominal	3" nominal	4" nominal
IATER	SQ. IN.	MERCURY	SQ. IN.	actual dia.	actual dia.	actual dia.	actual dia.
				1.049	2.067	3.068	4.026
4.7				73	282	622	1.071
4.8	1			73	285	628	1.082
4.9	1	<u>+</u>	1	74	288	635	1,093
5.0	†	· · · ·	-	75	291	641	1, 104
5.1	1	1		76	294	648	1, 115
5.2	3.01	1	1	76	297	654	1, 126
5.3	1		1	77	300	660	1, 137
5.4		. 40		78	303	.566	1, 148
5.5		1	1	79	305	673	1, 158
5.6	1	1		79	308	679	1, 169
5.7	1	1	1	80	311	685	1, 179
5.8	1	1	1	81	314	691	1, 189
5.9			1	81	316	697	1,200
6.0	1			82	319	703	1,210
6.1	3.53	1		83	322	708	1,220
6.2	1	1		83	324	714	1,230
6.3				84	327	720	1, 240
6.4				85	329	726	1, 249
6.5				85	332	731	1, 259
6.6				86	334	737	1, 269
6.7				87	337	742	1, 278
6.8		. 50		87	339	748	1, 288
6.9	3.99		. 25	88	342	753	1, 297
7.0				69	344	759	1,307
7.1				89	347	764	1, 316
7.2				90	349	770	1, 325
7.3				91	352	775	1, 334
7.4				91	354	780	1, 343
7.5				92	357	785	1, 353
7.6				92	359	791	1, 362
7.7			1	93	361	796	1,370
7.8	4.51	L		94	364	801	1,379
7.9		<u> </u>	<u> </u>	94	366	806	1,388
8.0	I			95	368	811	1,397

	94	366	806	1,388
	95	368	811	1, 397
	95	371	816	1,406
. 60	96	373	821	1, 414
	97	375	826	1, 423
	97	377	831	1, 431
	96	380	836	1, 440
	96	382	841	1, 448
	99	384	846	1,457
	99	386	851	1, 465
	100	366	856	1, 473
	101	391	860	1, 482
	101	393	865	1, 490
	102	395	870	1, 498

PITOT	TUBE	IMPACT	PRESSURE	FLOW	NIPPLE	INSIDE	DIAMETER
INCHES	OUNCES/	INCHES	LBS. PER	1" nominal	2" nominal	3" nominal	4" nominal
WATER	SQ. IN.	MERCURY	SQ. IN.	actual dia.	actual dia.	actual dia.	actual dia.
				1.049	2.067	3.068	4.026
9.3		•		102	397	e 7 5	1, 506
9.4				103	399	879	1, 514
9.5	5.49	.70		103	401	884	1, 522
9.6				104	403	⊈ara 889	1, 530
9.7				104	405	893	1, 536
9.8				105	406	898	1, 546
9.9				105	410	902	1, 554
10.0				106	412	907	1, 562
10.1				107	414	911	1,570
10.2		. 75		107	416	916	1, 577
10.3				106	418	920	1, 585
10.4	6.01			108	420	9 25	1, 593
10.5				109	422	929	1,600
10.6				109	424	934	1,608
10.7				110	426	938	1,616
10.8		. 79		110	428	94 3	1,623
10.9		. 80		111	430	947	1,631
11.0				111	432	9 51	1,638
11.1				112	434	956	1,645
11.2				112	436	9 60	1,653
11.3	6.53			113	438	964	1,660
11.4				113	440	968	1,668
11.5				114	441	973	1,675
11.6				114	443	977	1, 682
11.7				115	445	981	1,689
11.8				115	447	98 5	1,697
11.9				116	449	989	1, 704
12.0				116	451	994	1,711
12.1	6 <i>.</i> 99			117	453	99 8	1, 718
12.2				117	455	1,002	1, 725
12.3				118	457	1,006	1,732
12.4				118	458	1,010	1,739
12.5				119	460	1,014	1,746
* 13.0	7.50	L		121	469	1,033	1,779
	7.75	. 99		123	477	1,050	1,808
	8.00		. 50	125	484	1,067	1,837
	8.25	ļ		127	492	1,064	1,866
	8,50	ļ	ļ	129	499	1, 100	1,894
	8.75	ļ	ļ	130	507	1, 116	1,922
	9.00	 	ļ	132	514	1, 132	1,949
	9.25	ļ	L	134	521	1, 147	1,976
	9.50		Į	136	528	1, 163	2,002
L	9,75	1.24	ļ	138	535	1, 178	2,028
		 		139	541	1, 193	2,054
	10.25			14]	548	1,208	2,080
18.2	10.50	1.34	. 66	143	555	1,722	2,105

the second s		والمسادر القرني فتقاد المستحد المستح	ويستعد الشريب والمستات والمسترية				
PITOT	TUBE	IMPACT	PRESSURE	FLOW	NIPPLE	INSIDE	DIAMETER
INCHES	DUNCES/	INCHES	LBS. PER	<u>1" nominal</u>	2" nominal	3" nominal	4" nominal
WATER	SQ. IN.	MERCURY	SQ. IN.	actual dia.	actual dia.	actual dia.	actual dia.
	_			1.049	2.067	3.068	4.020
10.0	11.00	1.40			- Foo		
19.0	11.00	1.40	.709	140	568	1,251	2,154
19.9	11.50	1 50		150	581	1,2/9	2, 203
		1.53	/3	153	593	1, 30/	2,230
1	12.50			150		1, 334	2,291
	13.00			159	61/	1,300	2.342
à.	13.50			102	029	1,300	2,381
	14.00			165	<u>D41</u>	1,411	2,431
25.1	14.50	ļ		108	152	1,430	2,474
	15.00			171	663	1,461	2,516
	15.50	1.97		174	674	1, 485	2,557
	16.00		1.00	176	685	1, 509	2, 598
	16.50		ļ	179	696	1, 532	2,639
	17.00		ļ	182	706	1,555	2,678
30.3	17.50			184	716	1, 578	2,717
	18.00			187	726	1,600	2,756
	18.50			190	736	1,623	2, 794
	19.00		ļ	192	746	1,644	2,832
	19.50	2.48		195	756	1,666	2,869
	20.00		1.25	197	766	1,687	2,905
35.5	20.50			200	775	1,708	2,941
	21.00			202	785	1.729	2.977
	21.50			204	794	1, 749	3,012
	22.00			207	803	1, 769	3, 047
	22.50			209	812	1,789	3, 081
39.8	23.00			211	821	1,809	3, 115
	23.50	2.99		214	830	1,829	3, 149
	24.00		1.50	216	839	1,848	3, 182
	24.50			218	848	1,86/	3,215
	25.00			221	850	1,000	3.248
AE O	23.50			223	070	1,905	3,280
45.0	20.00		 	223	0/3	1, 924	3, 312
	20.30	ļ	 	221	900	1,942	3, 344
	27.00	2 50		229	6090	1,900	3,375
	27.50	3.30	1 95	231	090	1, 9/0	3,407
	20.00	<u> </u>	1.73	233	900	1,990	3,431
50.0	20.00	<u> </u>		235	914	2,014	3, 400
<u> </u>	29.00		!	231	922		3, 490
	29.30	ļ		240	930	2,049	3, 520
Ļ	30.00		<u> </u>	242	046	2,000	3, 330
<u> </u>	21 00		<u> </u>	244	940	2 100	3, 300
EA E	31.00 #01 E0	4 00	1 100	240		2,100	3,011
34.3	-31.30	4.00	1.30	24/	<u> </u>	2 167	3,041
	 	4.20	<u> </u>	233	304	2 210	3, 131
			<u> </u>	209	1 020	2 260	3,019
65 2	27 71		2 25	200	1 029	2 216	3, 903
	1 37.71	1 7.00	1 2.33			6,310	1 3,303

PITOT	TUBE	IMPACT	PRESSURE	FLOW	NIPPLE	INSIDE	DIAMETER
INCHES	OUNCES/	INCHES	LBS. PER	1" nominal	2" nominal	3" nominal	4" nominal
WATER	SQ. IN.	MERCURY	SQ. IN.	actual dia.	actual dia.	actual dia.	actual dia.
	L			1.049	2.067	3.068	4.026
68.0	1 39.28	5.00	2.45	276	1,0/3	2,854	4,0/1
	40.85	5.20	2.55	262	1,094	2,411	4, 152
		5.40		28/	1, 115	2,457	4,231
		5.60	-	293	1, 136	2, 502	4, 308
		5.80		298	1, 156	. 2, 546	4, 385
		6.00		303	1, 176	2,590	4,460
		6.20	3.04	306	1, 195	2,633	4, 533
	50.28	5.40	1	313	1,214	2,675	4,606
		6.60		318	1,233	2,716	4,677
	<u> </u>	<u> </u>	ļ	322	1,251	2,757	4,748
L	Į	7,00		327	1,270	2,797	4,817
	ļ	7,20	3.53	332	1,288	2,837	4,885
		7.40	<u> </u>	330	1,306	2,876	4,953
ļ	59.70	7.60		341	1, 323	2,915	5,019
		1.80		345	1, 340	2,953	5,085
ļ	ļ	8.00		350	1,357	2,990	5, 150
<u> </u>	<u></u>	8.20	4.02	354	1,374	3,028	5,214
		8,40	 	358	1, 391	3,064	5,277
	· · · · · · · · · · · · · · · · · · ·	8,60		362	1,407	3, 101	5, 339
		8.80	L	367	1, 424	3, 136	5,401
ļ	10.70	9.00		3/1	1, 440	3, 172	5,462
		9.20	4.51	375	1,456	3,207	5,522
<u> </u>		9.40		3/9	1,4/1	3,242	5, 582
	15.41	9.60	l	383	1,487	3,276	5,641
L		9.80		387	1,502	3,310	5,700
<u> </u>	80 12	10.00	5 00	391	1,518	3, 343	5,151
<u> </u>	00.13	10.20	5.00	395	1,000	3,311	5,013
 	+	10.40		402	1,540	3,410	5,071
<u> </u>	- 04 04	10.00	+	406	1, 502	3,442	5,920
<u> </u>	1 07.07			<u>410</u>	1 502	2 507	<u> </u>
	<u> </u>	11 20	5 40		1 606	3 528	6 102
	80 55	11 40	<u> </u>	<u><u>417</u></u>	1 620	3 570	6 147
	103.00	11 60	<u> </u>	A21	1 625	103.570	6 201
J	+	11 80	<u> </u>	425	1 640	3 622	6 254
	04 27	12 00		A28	1 662	3 662	6 207
	05 R4	12 20	5 09	122	1 676	<u> </u>	6 250
	1	12 40	<u> </u>	435	1 690	3 723	<u>6 411</u>
	+	12.60	1	430	1.704	3,753	6.463
	100.55	12.80	<u> </u>	442	1.717	3,783	6.514
	1.00.00	13.00	<u> </u>	446	1,730	3, 812	6,565
}	+	13.20	6,47	449	1.744	3.841	6.615
	105.26	13,40	†	452	1,757	3,870	6,665
 	+	13.60	1	456	1,770	3,899	6,714
	1	13.80	1	459	1,783	3, 928	6,763
190.3	109.98	14.00	6.87	462	1, 796	3,956	6, 812
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PITOT	TUBE	IMPACT	PRESSURE	FLOW	NIPPLE	INSIDE	DIAMETER
			~				
INCHES	OUNCES/	INCHES	LBS. PER	1" nominal	2" nominal	3" nominal	4" nominal
WATER	ISQ. IN.	HERCURY	SQ. IN.	actual dia.	actual dia.	actual dia.	actual dia.
	ļ			1.049	2.067	3.068	4.026
	110 01						
197.1	113.91	14.50	7.11	471	1,627	4,026	6, 933
		15.00		479	1,859	4,095	7,051
	105 00	15.50	-	487	1,889	4, 163	7, 168
<u> </u>	125.69	16.00	- A AA	494	1,920	4,229	7,283
		10.50	8.09	502	1,949	4, 240	7, 390
	ļ	17.00	 	510	1,9/9	4,339	7.507
		18 00		317 2.35 24	2,000	4,423	7 724
		10.00	0.07	532	2,000		7 921
	140 25	10.00	9.07	530	2 007	4,540	7 036
		19.50	<u> </u>	546	2 110	4, 669	8,040
	<u> </u>	20.00	<u> </u>	553	2,146	4, 728	8, 142
	<u> </u>	20.50	10.06	560	2,173	4, 787	8,243
	<u> </u>	21.00		566	2.199	4, 845	8, 343
	t	21.50	T	573	2,225	4,902	8, 442
	<u>†</u>	22.00	<u> </u>	580	2,251	4,959	8,540
	176.75	22.50	11.04	586	2,276	5,015	8,636
		23.00		593	2,302	5,071	8,732
		23.50		599	2, 326	5, 125	8,826
	1	24.00		606	2,351	5, 180	8,919
		24.50	12.02	612	2,375	5, 233	9,012
		25.00		618	2,400	5, 286	9, 103
	200.32	25.50		624	2, 423	5, 339	9, 194
		26.00		630	2, 447	5, 391	9, 284
		26.50	13.00	636	2,471	5, 443	9,372
		27.00		642	2,494	5, 494	9,460
ļ	ļ	27.50	ļ	648	2,517	5, 544	9, 548
ļ		28.00		654	2, 539	5, 595	9,634
· · · · · · · · · · · · · · · · · · ·	223.88	28.50	13.98	000	2,562	5, 644	9,720
	 	29.00	ļ	000	2,504	5,094	9,805
	_	29.50	<u> </u>	0/1	2.00/	5, 143	9,009
	240.00	JU. UU	15 00		2,029	3, /91	9,912
	240.22	20.00		706	2,003	5,044	10,003
	250.24	24 66		100	2 924	6 221	10, 394
ļ	 	26 70		749	2,024	6 402	11 004
	304 20	38 74		760	2, 900	6 577	11 226
}	007.23	40.77	20 00	780	3 063	6 74A	11 620
}	<u> </u>	42, 81	21.00	808	3,130	6 015	11 007
 	t	44.85	22.00	827	3,213	7.077	12 187
	<u> </u>	46.89	23.00	846	3,285	7.237	12,461
}	1	48.93	24.00	864	3,355	7.392	12,720
692.6	400.38	50.97	25.00	882	3.425	7.545	12.992
	1	53.01	26.00	899	3, 492	7,694	13,249
 	1	55.04	27.00	917	3, 559	7,841	13, 502
775.8	448.42	57.08	28.00	933	3, 624	7,984	13, 749
	and the second	and the second se	And the second se	· · · · · · · · · · · · · · · · · · ·		the second se	

MEMORANDUM



To: NMOCD Deliverability Test Committee

From: H. L. Babe Kendrick

Date: November 11, 1986

At the Farmington meeting on November 6, 1986, it was decided to be ready to submit this testing procedure to the NMOCD for hearing on December 3, 1986. For this to happen, I must get in gear and stay in gear until the job is completed. Your help is very much needed to be a proof—reader and to furnish technical data to make some of the calculations necessary for the data book and to place the tables and other pages in proper sequence.

Today, all that I have ready for you is the documentation for the rules procedure with the paragraph added into it on page 7 as you authorized. Please read the enclosed pages and read carefully to find all the errors that may be contained therein. Please let me know of anything that is incorrect in this portion of this booklet.

Additional data will be submitted to you as I get it in what should be a "final form".

Your comments are solicited.

Babe

GAS WELL TESTING MANUAL FOR SAN JUAN BASIN, NEW MEXICO

CHAPTER I TYPE OF TESTS REQUIRED FOR WELLS COMPLETED IN PRORATED GAS

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SECTION 1: <u>Initial Deliverability and Shut-In Pressure Tests for Newly</u> <u>Completed Well</u> =

A. Immediately upon completion of each gas well in the San Juan Basin, a shut-in pressure test of at least seven days duration shall be made. This initial shut-in pressure shall be filed with the Division's Aztec Office on either Form C-122 or C-104.

B. Within 90 days after a well first delivers gas to a gas transportation facility, the well shall have been tested in accordance with Section 1 of Chapter II of these rules, "Initial Deliverability and Shut-In Pressure Test Procedures", and the results of the test filed in triplicate with the Division's Aztec office and one copy filed with the gas transportation facility to which the well is connected. This test is to be filed on Form C-122-A. Failure to file said test within the above-prescribed 90-day period will subject the well to the loss of one day's allowable for each day the test is late.

- 1. If the newly first delivered well is an infill well on a proration unit, the old well on the unit is not required to be tested provided it has a valid test on file for the current proration year. Testing of the old well follows the regularly assigned test year for the pool in which the wells are located. The new well is required to be tested annually until at least three annual tests are on file and then the well is to be tested biennially with other wells in that pool.
- 2. If the newly first delivered well is an infill well on a proration unit and the old well on the unit is "exempt", the old well is to be tested along with the new well for the Initial and Annual Deliverability and Shut-In Pressure Test. The old well will lose its "exempt" classification and must be tested biennially along with other wells in that pool. The new infill well is required to be tested annually until at least three annual tests are on file and then the well is to be tested biennially with other wells in that pool.

C. The requirements for Initial Tests and Annual or Biennial Deliverability and Shut-In Pressure Tests and the notification requirements and scheduling of such tests which apply to newly completed wells shall also apply to recompleted wells. D. Any tests taken for informational purposes prior to pipeline connection shall not be recognized as official tests for the assignment of allowables.

SECTION 2. <u>Annual and Biennial Deliverability and Shut-In Pressure</u> <u>Tests</u>

A. Annual or Biennial Deliverability and Shut-In Pressure Tests shall be made on all gas wells during the period from January 1 through December 31 of that year except as follows:

- 1. A newly completed well or a recompleted well shall be tested on an annual basis until a minimum of three annual tests have been taken, after which the well shall be tested biennially as is required for other wells in the pool in which the well is located.
- 2. Wells classified as "exempt" shall not be subject to the requirements of annual or biennial deliverability tests.

Classification of wells into or out of the "exempt" status shall be done once each year immediately following the reporting of June production and shall be effective for the succeeding annual test period.

Gas wells completed in the Pictured Cliffs or any shallower formation shall be classified "exempt" if at least three months of production history is available and the well failed to produce, and is incapable of producing, an average of 250 MCF or more per month during the months produced within the preceding 12-month period, and the well is classified as marginal in the August Gas Proration Schedule.

Gas wells completed in any formation deeper than the Pictured Cliffs formation shall be classified "exempt" if at least three months of production history is available and the well failed to produce, and is incapable of producing, an average of 2000 MCF or more per month during the months produced within the preceding 12-month period, and the well is classified as marginal in the August Gas Proration Schedule.

Gas wells on multiple well Gas Proration Units will not be classified "exempt" unless the Gas Proration Unit is classified as marginal. Any or all wells on a marginal multiple well Gas Proration Unit may be classified as "exempt" provided each Gas Proration Unit so classified meets the qualification for "exempt" status. Gas Proration Units for wells producing from formations deeper than the Pictured Cliffs formation shall be classified "exempt" if at least three months of production history is available and the Gas Proration Unit failed to produce, and is incapable of producing, an average of 2000 MCF or more per month during the months produced within the preceding 12-month period, and the Gas Proration Unit is classified as marginal in the August Gas Proration Schedule. Gas Proration Units are to be classified as "exempt" because of their low producing ability.

The District Supervisor of the Division's Aztec Office may classify a well or Gas Proration Unit as "exempt" at any time if the operator presents sufficient evidence to the District Supervisor indicating that the well or Gas Proration Unit is incapable of producing gas at a higher rate than that rate required for "exempt" classification for wells or Gas Proration Units in that pool.

Once a well or Gas Proration Unit has been declared "exempt" for the following test year, it shall remain classified "exempt" for that test year.

- 3. If a test is filed on any well on a gas proration unit, the test requirement for the gas proration unit has been met. The deliverability of the unit is taken only as the resulting sum of all wells tested.
- 4. A shut-in pressure must be filed on Form C-122-A even if no gas is measured during the production phase of the test. "Exempt" wells do not require the filing of a shut-in pressure.

B. All Annual and Biennial Deliverability and Shut-In Pressure Tests required by these rules must be filed with the Division's Aztec office and with the appropriate gas transportation facility within 90 days following the completion of each test. Provided however, that any test completed between October 31 of the test year and January 31 of the following year are due no later than January 31. No extension of time for filing tests beyond January 31 will be granted except after notice and hearing.

Failure to file any test within the above-prescribed times will subject the well to the loss of one day's allowable for each day the test is late. A well classified as marginal shall be shut-in one day for each day the test is late.

SECTION 3: <u>Scheduling of Tests</u>

A. Notification of Pools to be Tested

By September 1 of each year, the District Supervisor of the Aztec District Office of the Division shall by memorandum notify each gas transportation facility and each operator of the pools which are to be scheduled for biennial testing during the following testing period from January 1 through the last day of December of that test year. The District Supervisor will also provide a list of "exempt" wells and a list of wells that do not have a minimum of three Annual Deliverability and Shut-In Pressure Tests on file. Any well scheduled for testing during its test year may have the conditioning period, test flow period, and some of the seven day shut-in period conducted in December of the previous year provided that if the 7 day shut-in period immediately follows the test flow period the 7 day shut-in pressure would be measured in January of the test year. The earliest date that a well could be scheduled for Annual or Biennial Deliverability and Shut-In Pressure Test would be such that the Test Flow Period would end on December 25 of the previous year.

Downhole commingled wells are to be scheduled for tests on dates for pool of lowermost prorated completion of well.

B. Annual and Biennial Deliverability Tests

By November 1 of each year, each gas transportation facility shall, in cooperation with the operators involved, prepare and submit a schedule of the wells to which it is connected which are to begin testing in December and January. Said schedule shall be entitled, "Annual and Biennial Deliverability and Shut-In Pressure Test Schedule", and one copy shall be submitted to the Division's Aztec office and to each operator concerned. The schedule shall indicate the date of tests, pool, operator, lease, well number, and location of each well.

At least 30 days prior to the beginning of each succeeding 2-month testing interval, a similar schedule shall be prepared and filed in accordance with the above.

The gas transportation facility and the Aztec District Office of the Division shall be notified immediately by any operator unable to conduct any test as scheduled.

In the event a well is not tested in accordance with the existing test schedule, the well shall be re-scheduled by the gas transportation facility, and the Division and the operator of the well so notified in writing. Every effort should be made to notify the Division of the new schedule prior to the conclusion of the newly assigned 14-day conditioning period.

Notice to the Division of Shut-In Pressure Tests which are scheduled at a time other than immediately following the flow test must be received prior to the time that the well is shut-in.

It shall be the responsibility of each operator to determine that all of its wells are properly scheduled for testing by the gas transportation facility to which they are connected, in order that all annual and biennial tests may be completed during the testing season.

In the event a well is shut-in by the state for over production, the operator may produce the well for a period of time to secure a test after notification to the Division. All gas produced during this testing period will be used in determining the over/under produced status of the well.

C. <u>Deliverability Re-Tests</u>

An operator may, in cooperation with the gas transportation facility, schedule a well for a deliverability re-test upon notification to the Division's Aztec office at least ten days before the test is to be commenced. Such re-test shall be for good and substantial reason and shall be subject to the approval of the Division. Re-tests shall in all ways be conducted in conformance with the Annual and Biennial Deliverability Test Procedures of these rules. The Division, at its discretion, may require the re-testing of any well by notification to the operator to schedule such re-test. These tests as filed on Form C-122-A should be identified as "RETEST" in the remarks column.

SECTION 4: Witnessing of Tests

Any Initial Annual or Biennial Deliverability and Shut-In Pressure Test may be witnessed by any or all of the following: an agent of the Division, an offset operator, a representative of the gas transportation facility connected to the well under test, or a representative of the gas transportation facility taking gas from an offset operator.

CHAPTER II PROCEDURE FOR TESTING

SECTION 1: Initial Deliverability and Shut-In Pressure Test Procedure

A. Within 90 days after a newly completed well is first delivered to a gas transportation facility, the operator shall complete a deliverability and shut-in pressure test of the well in conformance with the "Annual and Biennial Deliverability and Shut-In Pressure Test Procedures", prescribed in Section 2 of this chapter. Results of the test shall be filed as required by Section 1 of Chapter I of these rules.

B. In the event it is impractical to test a newly completed well in conformance with Paragraph A above, the operator may conduct the deliverability and shut-in pressure test in the following manner (provided, however, that any test so conducted will not be accepted as the first annual deliverability and shut-in pressure test as described in Paragraph A-1 of Section 2, Chapter I):

1. A 7-day or 8-day production chart may be used as the basis for determining the well's deliverability, providing the chart so used is preceded by at least 14 days continuous production. The well shall produce through either the casing or tubing, but not both, into a pipeline during these periods. The production valve and the choke settings shall not be changed during either the conditioning or flow period with the exception of the first ten (10) days of the conditioning period when maximum production would over-range the meter chart or location production equipment.

- 2. A shut-in pressure of at least seven days duration shall be taken. This shall be the shut-in test required in Paragraph A, Section 1 of Chapter I of these rules.
- 3. The average daily static meter pressure shall be determined in accordance with Section 2 of Chapter II of these rules. This pressure shall be used as Pt in calculating Pw for the Deliverability Calculation.
- 4. The daily average rate of flow shall be determined in accordance with Section 2 of Chapter II.
- 5. The static wellhead working pressure (P_W) shall be determined in accordance with Section 2 of Chapter II.
- 6. The deliverability of the well shall be determined by using the data determined in Paragraphs 1 through 5 above in the deliverability formula in accordance with Section 2 of Chapter II.
- 7. The data and calculations for Paragraphs 1 through 6 above shall be reported as required in Section 1 of Chapter I of these rules, upon the blue-colored Form C-122-A or on white Form C-122-A and write "INITIAL TEST ONLY" in remarks.

SECTION 2: <u>Annual and Biennial Deliverability and Shut-In Pressure Test</u> <u>Procedure</u>

This test shall begin by producing a well in the normal operating manner into the pipeline through either the casing or tubing, but not both, for a period of fourteen consecutive days. This shall be known as the conditioning period. The production valve and choke settings shall not be changed during either the conditioning or flow periods except during the first ten (10) days of the conditioning period when maximum production would over-range the meter chart or location production equipment. The first ten (10) days of said conditioning period shall not have more than forty eight (48) hours of cumulative interruptions of flow. The eleventh to fourteenth days, inclusive, of said conditioning period shall have no interruptions of flow whatsoever. Any interruption of flow that occurs as normal operation of the well as stop-cock flow, intermittent flow, or well blow down will not be counted as shut-in time in either the conditioning or flow period.

The daily flowing rate shall be determined from an average of seven or eight consecutive producing days, following a minimum conditioning period of 14 consecutive days of production. This shall be known as the flow period. Instantaneous pressures shall be measured by deadweight gauge or other method approved by the Division during the 7-day or 8-day flow period at the casinghead, tubinghead, and orifice meter, and shall be recorded along with instantaneous meter-chart static pressure reading.

If a well is producing through a compressor that is located between the wellhead and the meter run, the meter run pressure and the wellhead casing pressure and the wellhead tubing pressure are to be reported on Form C-122-A. (Neither the suction pressure nor the discharge pressure of the compressor is considered wellhead pressure.) A note shall be entered in the remarks portion on Form C-122-A stating "This well produces through a compressor".

When it is necessary to restrict the flow of gas between the wellhead and orifice meter, the ratio of the downstream pressure, psia, to the upstream pressure, psia shall be determined. When this ratio is 0.57, or less, critical flow conditions shall be considered to exist across the restriction.

When more than one restriction between the wellhead and orifice meter causes the pressures to reflect critical flow between the wellhead and orifice meter, the pressures across each of these restrictions shall be measured to determine whether critical flow exists at any restriction. When critical flow does not exist at any restriction, the pressures taken to disprove critical flow shall be reported to the Division on Form C-122-A in item (n) of the form. When critical flow conditions exist, the instantaneous flowing pressures required hereinabove shall be measured during the last 48 hours of the 7-day or 8-day flow period.

When critical flow exists between the wellhead and orifice meter, the measured wellhead flowing pressure of the string through which the well flowed during test shall be used as P_t when calculating the static wellhead working pressure (P_w) using the method established below.

When critical flow does not exist at any restriction, P_t shall be the corrected average static pressure from the meter chart plus friction loss from the wellhead to the orifice meter.

The static wellhead working pressure (P_w) of any well under test shall be the calculated 7-day or 8-day average static tubing pressure if the well is flowing through the casing; it shall be the calculated 7-day or 8-day average static casing pressure if the well is flowing through the tubing. The static wellhead working pressure (P_w) shall be calculated by applying the tables and procedures set out in this manual.

To obtain the shut-in pressure of a well under test, the well shall be shut in some time during the current testing season for a period of seven to fourteen consecutive days, which have been preceded by a minimum of seven days of uninterrupted production. Such shut-in pressure shall be measured with a deadweight gauge or other method approved by the Division on the seventh to fourteenth day of shut-in of the well. The 7-day shut-in pressure shall be measured on both the tubing and the casing when communication exists between the two strings. The higher of such pressures shall be used as P_C in the deliverability calculation. When any such shut-in pressure is determined by the Division to be abnormally low or the well can not be shut-in due to "HARDSHIP" classification, the shut-in pressure to be used as P_C shall be determined by one of the following methods:

- 1. A Division-designated value:
- An average shut-in pressure of all offset wells completed in the same zone. Offset wells include the four side and four corner wells, if available.
- 3. A calculated surface pressure based on a calculated bottom-hole pressure. Such calculation shall be made in accordance with the examples in this manual.

All Wellhead pressures as well as the flowing meter pressure tests which are to be taken during the 7-day or 8-day deliverability test period as required hereinabove shall be taken with a deadweight gauge or other method approved by the Division. The pressure readings and the date and time according to the chart shall be recorded and maintained in the operator's records with the test information.

Orifice meter charts shall be changed and so arranged as to reflect upon a single chart the flow data for the gas from each well for the full 7-day or 8-day deliverability test period; however, no tests shall be voided if satisfactory explanation is made as to the necessity for using test volumes through two chart periods. Corrections shall be made for pressure base, measured flowing temperature, specific gravity, and supercompressibility; provided however, if the specific gravity of the gas from any well under test is not available, an estimated specific gravity may be assumed therefor, based upon that of gas from near-by wells, the specific gravity of which has been actually determined by measurement.

The average flowing meter pressure for the 7-day or 8-day flow period and the corrected integrated volume shall be determined by the purchasing company that integrates the flow charts and furnished to the operator or testing agency.

The 7-day or 8-day flow period volume shall be calculated from the integrated readings as determined from the flow period orifice meter chart. The volume so calculated shall be divided by the number of testing days on the chart to determine the average daily rate of flow during said flow period. The flow period shall have a minimum of seven

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and a maximum of eight legibly recorded flowing days to be acceptable for test purposes. The volume used in this calculation shall be corrected to New Mexico Oil Conservation Division standard conditions of 15.025 psia pressure base, 60°F. temperature base and 0.60 specific gravity base.

The daily volume of flow as determined from the flow period chart readings shall be calculated by applying the Basic Orifice Meter Formula or other acceptable industry standard practices.

 $Q = C' \{h_{\omega}P_{f}\}^{1/2}$

Where:

Q = Metered volume of flow Mcf/d @ 15.025 psia, 60⁰ F., and 0.60 specific gravity.

C' = The 24-hour basic orifice meter flow factor corrected for flowing temperature, gravity, and supercompressibility.

 h_{W} = Daily average differential meter pressure from flow period chart.

P_f = Daily average flowing meter pressure from flow period chart.

The basic orifice meter flow factors, flowing temperature factor, and specific gravity factor shall be determined from the tables in this manual.

The daily flow period average corrected flowing meter pressure, psig, shall be used to determine the supercompressibility factor. Supercompressibility Tables may be obtained from the New Mexico Oil Conservation Division.

When supercompressibility correction is made for a gas containing either nitrogen or carbon dioxide in excess of two percent, the supercompressibility factors of such gas shall be determined by the use of Table V of the C.N.G.A. Bulletin TS-402 for pressures 100-500 psig, or Table II, TS-461 for pressures in excess of 500 psig.

The use of tables for calculating rates of flow from integrator readings which do not specifically conform to the New Mexico Oil Conservation Division "Back Pressure Test Manual", or this manual, may be approved for determining the daily flow period rates of flow upon a showing that such tables are appropriate and necessary.

The daily average integrated rate of flow for the 7-day or 8-day flow period shall be corrected for meter error by multiplication by a

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correction factor. Said correction factor shall be determined by dividing the square root of the deadweight flowing meter pressure, psia, by the square root of the chart flowing meter pressure, psia.

Deliverability pressure, as used herein, is a defined pressure applied to each well and used in the process of comparing the abilities of wells in a pool to produce at static wellhead working pressures equal to a percentage of the 7-day shut-in pressure of the respective individual wells. Such percentage shall be determined and announced periodically by the Division based on the relationship of the average static wellhead working pressures (P_W) divided by the average 7-day shut-in pressure (P_C) of the pool.

The deliverability of gas at the "deliverability pressure" of any well under test shall be calculated from the test data derived from the tests hereinabove required by use of the following deliverability formula:

 $D = Q \qquad \frac{(P_c^2 - P_d^2)^n}{(P_c^2 - P_w^2)}$

Where:

D = Deliverability Mcf/d at the deliverability pressure, (P_d), (at Standard Conditions of 15.025 psia, 60° F and 0.60 sp. gr.).

Q = Daily flow rate in Mcf/d, at wellhead pressure (P_w) .

 P_{C} = 7-day shut-in Wellhead pressure, psia, determined in accordance with Section 2 of Chapter II.

 P_d = Deliverability pressure, psia, as defined above.

 P_w = Average static wellhead working pressure, as determined from 7-day or 8-day flow period, psia, and calculated from tables in this manual entitled "Pressure Loss Due to Friction" Tables for San Juan Basin.

n = Average pool slope of back pressure curves as follows:

For	Pictured C	liffs and	shallower	formations	0.8 5
For	formations	deeper t	han Picture	ed Cliffs	0.75

(Note: Special Rules for Any Specific Pool or Formation May Supersede The Above Values. Check Special Rules If In Doubt.)

The value of the multiplier in the above formula (ratio factor after the application of the pool slope) by which Q is multiplied shall not exceed

a limiting value to be determined and announced periodically by the Division. Such determination shall be made after a study of the test data of the pool obtained during the previous testing season.

Downhole commingled wells are to be tested in year for pool of lowermost prorated completion of well and shall use pool slope (n), and deliverability pressure of lowermost pool. The total flow rate from the downhole commingled well will be used to calculate a value of deliverability. For each prorated gas zone of a downhole commingled well, a Form C-122-A is required to be filed and in the Summary portion of that form, all zones will indicate the same data for line h, P_C , Q, P_W , and P_d . The value shown for Deliverability (D) will be that percentage of the total deliverability of the well that is applicable to this zone. A note shall be placed in the remarks column that indicates the percentage of deliverability to be allocated to this zone of the well.

Any test prescribed herein will be considered acceptable if the average flow rate for the final 7-day or 8-day deliverability test is not more than ten percent in excess of any consecutive 7-day or 8-day average of the preceding two weeks. A deliverability test not meeting this requirement may be declared invalid, requiring the well to be re-tested.

All charts relative to initial, annual, or biennial deliverability tests or copies thereof shall be made available to the Division upon its request.

All testing agencies, whether individuals, companies, pipeline companies, or operators, shall maintain a log of all tests accomplished by them, including all field test data. The operator shall maintain the above data for a period of not less than two (2) years plus the current test year.

All forms heretofore mentioned are hereby adopted for use in the San Juan Basin Area in open form subject to such modification as experience may indicate desirable or necessary.

Initial and Annual or Biennial Deliverability and Shut-In Pressure Tests for gas wells in all formations shall be conducted and reported in accordance with these rules and procedures. Provided however, these rules shall be subject to any specific modification or change contained in Special Pool Rules adopted for any pool after notice and hearing.

CHAPTER III INFORMATIONAL TESTS

A. A one-point back pressure test may be taken on newly completed wells before their connection or reconnection to a gas transportation facility. This test shall not be a required official test but may be taken for informational purposes at the option of the operator. When taken, this test must be taken and reported as prescribed below:

ONE-POINT BACK PRESSURE POTENTIAL TEST PROCEDURE

- 1. This test shall be accomplished after a minimum shut-in of seven days. The shut-in pressure shall be measured with a deadweight gauge or other method approved by the Division.
- 2. The flow rate shall be that rate in Mcf/d measured at the end of a three hour test flow period. The flow from the well shall be for three hours through a positive choke, which has a 3/4-inch orifice.
- 3. A 2-inch nipple which provides a mechanical means of accurately measuring the pressure and temperature of the flowing gas shall be installed immediately upstream from the positive choke.
- 4. The absolute open flow shall be calculated using the conventional back pressure formula as shown in this manual or the New Mexico Oil Conservation Division "Back Pressure Test Manual."
- 5. The observed data and flow calculations shall be reported in duplicate on Form C-122, "Multi-Point Back Pressure Test for Gas Wells."
- 6. Non-critical flow shall be considered to exist when the choke pressure is 13 psig or less. When this condition exists the flow rate shall be measured with a pitot tube and nipple as specified in this manual or in the Division's Manual of "Tables and Procedure for Pitot Tests." The pitot test nipple shall be installed immediately downstream from the 3/4-inch positive choke.
- 7. Any well completed with 2-inch nominal size tubing (1.995-inch ID) or larger shall be tested through the tubing.

B. Other tests for informational purposes may be conducted prior to obtaining a pipeline connection for a newly completed well upon receiving specific approval therefor from the Division's Aztec office. Approval of these tests shall be based primarily upon the volume of gas to be vented.

CHAPTER IV Type of Tests Required for Wells Completed in Non-Prorated Pools

SECTION 1: Initial Shut-in Pressure Tests for newly Completed Wells.

A. (Same as Chapter I, Section 1, A)

SECTION 2: <u>Biennial Shut-in Pressure Tests</u>

A. Non-prorated wells will be tested biennially as required by the District Office except as follows:

- 1. Wells which meet the "exempt" qualification as shown in Chapter I, Section 2, paragraph A-2 of these rules shall also be exempt from shut-in.test requirements.
- 2. Wells classified as "hardship" wells during the test year shall also be exempt from shut-in test requirements.

B. All shut-in tests required by these rules must be filed with the Division's Aztec office by January 31 of the following year. Failure to file the test will subject the well to being shut-in one day for each day the test is late.

SECTION 3: <u>Scheduling Tests</u>

A. By September 1 of each year, the District Supervisor of the Aztec District Office of the Division shall by memorandum notify each gas transportation facility and each operator of the pools which are to be scheduled for biennial shut-in pressure testing during the following testing period from January 1 through the last day of December of that test year. The District Supervisor will also provide a list of "exempt" wells.

Any well scheduled for testing during its test year may have the test flow period, and some of the seven day shut-in period conducted in December of the previous year. The earliest date that a well could be scheduled for Biennial Shut-In Pressure Test would be such that the Test Flow Period would end on December 25 of the previous year.

Downhole commingled wells are to be scheduled for tests on dates for pool of lowermost completion of well.

SECTION 4: <u>Test Procedure</u>

A. To obtain the shut-in pressure of a well under test, the well shall be shut-in some time during the current testing season for a period of seven to fourteen consecutive days, which have been preceded by a minimum of seven days of uninterrupted production. Such shut-in pressure shall be measured by deadweight gauge or other method approved by the Division on the seventh to fourteenth day of shut-in of the well. The shut-in pressure shall be measured on both the tubing and the casing when communication exists between the two strings. The higher of such pressures shall be reported as the shut-in pressure of the well.

SECTION 5: Filing of shut-in Pressure Data

The results of this test will be filed in triplicate on Form C-125-B showing the pressures in psia in column labeled "S. I. PRESSURE PSIA (DWT)" with the Aztec District Office.

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END OF THIS PROPOSED MANUAL FOR TESTING IN SJB 11/10/86

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MEMORANDUM

To: NMOCD Deliverability Test Committee

From: H. L. Babe Kendrick

Date: November 11, 1986

At the Farmington meeting on November 6, 1986, it was decided to be ready to submit this testing procedure to the NMOCD for hearing on December 3, 1986. For this to happen, I must get in gear and stay in gear until the job is completed. Your help is very much needed to be a proof—reader and to furnish technical data to make some of the calculations necessary for the data book and to place the tables and other pages in proper sequence.

Today, all that I have ready for you is the documentation for the rules procedure with the paragraph added into it on page 7 as you authorized. Please read the enclosed pages and read carefully to find all the errors that may be contained therein. Please let me know of anything that is incorrect in this portion of this booklet.

Additional data will be submitted to you as I get it in what should be a "final form".

Your comments are solicited.

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Babe



TO: NMOCD DELIVERABILITY TEST COMMITTEE

FROM: H. L. BABE KENDRICK

DATE: OCTOBER 15,1986

At the Santa Fe meeting on September 30, 1986, it was decided to have the next meeting in Farmington, NM in late October. In arranging a meeting place, and looking further at work schedules, the October meeting must be pushed back to Thursday, November 6, 1986, 8:00 AM, in the El Paso Natural Gas Company building located in Reilly Heights.

As a result of the discussion on producing and testing a well through a compressor, what do you think of adding the following paragraph into the testing instructions as the second paragraph on Page 7?

If a well is producing through a compressor that is located between the wellhead and the meter run, the meter run pressure and the wellhead casing pressure and the wellhead tubing pressure are to be reported on the C-122-A Form. (Neither the suction pressure nor the discharge pressure of the compressor is considered <u>wellhead</u> pressure.) A note shall be entered in the remarks portion of the C-122-A Form stating "This well produces through a compressor."

At this point we might try to add two definitions into this test procedure which are for workovers and retest. These might include:

WORKOVER: Anything done to a well to change its productivity.

RESTEST: A test conducted on a well that has a current test on record with the Division that does not reflect the current producing ability of the well.

Your choice of words is important in each of the above descriptions so get out the "correcting pen" and go to work.

See you later.

Babe

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9/30/86

505-598-9464 Oco Hazter 6 Finie Busch 227-5809 " Sonta Fe 6 Vic Lyon 327 - 0251 Meridian Oil Co. Farmington P Douglas & Harris Gas Company of New Maxico (AIB, NM) 888-8378 7 Joel Levine R.E. MATHIS MESA OPERATING LIMITED PARTNERSHIP (606) 378-1000 505-327-5351 7 Mike Turnbaugh NWP 505-329.4631 Sothern Union Exp Co. T Martin Boggs T Stille Whiteher I burly Liese Das Company of Mus Marico 505-632-3311 nulP 545-327-5351 325-5870 EPNG TEd Marcun FKF- 641-6133 EPNG BOXINGY ELPHSOTY H.L. BABE KELDRICK 1 Louis JONES TENNECO Oil P.O. Box 3249 303-740.4845 Englewood, 6 30155 P Joel Joy 303-7402550 TENNECO OIL P.O. Box 3249 Englewood, CO 80155 1 Jack Erane Schalk Development Co. 505-325-5018 P A.R. Hendrick 4 Corners Gastroducers 505.334-2355 Box 516 Aztac NM Columbus Energy Corp. PO. Ecx 2038 Farminhan 63=- 8056 P. Wayne Converse Oil Conservation - Santa Fe 6 Michael E. Stogner 505-927-5811



MEMORANDUM

TO: NMOCD Deliverability Test Committee

DATE: September 19, 1986

FROM: H. L. "Babe" Kendrick

PLACE: Production Control Department

A meeting has been set for 8:30 and Toester Amptemperion, 1986 in Morgan Hall in the basement of the State Land Stripe Building in Santa Fe, New Mexico.

This meeting is needed to complete the workings of the prior committee activities and to arrange our data to publish a test manual for the San Juan Basin.

Also, certain topics need to be discussed such as:

individual wells producing through compressors; where to enter data on Cl22A; workovers; what is a workover; what is not a workover; scheduling requirements for tests; possibility of late tests; possibility of no test.

The above list is not intended to limit the discussion in any manner. This list may only cover a few of the many items that need discussing.

If you have all of the latest documents we have prepared and the testing order and/or procedure, please bring them along. If anyone can start arranging those in a presentable manner, please do so and help speed the process.

If we have items that you feel need to be discussed with your management prior to further committee action we can recess and meet again to finalize a committee presentation.

See you in Santa Fe.

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CAPS HUBSER, AMOCO PRODUCTION COMPANY 501 AIRPORT DRIVE FARMINGTON, NM 87401

H. L. BABE KENDRICK EL PASO NATURAL GAS CO F.O. BOX 1492 EL PASO, TX 79978

HAROLD GARCIA NEW MEXICO OIL CONSERVATION DIV P.O. BOX 2088 SANTA FE, NM 87501

HUGH INGRAM CONOCO P.O. BOX 460 HOBBS, NM 88240

JACK EVANS SCHALK DEVELOPMENT COMPANY P.O. BCX 2078 FARMINGTON, NM 87401

JOHN COOK TENNECO P.O. BOX 3249 ENGLEWOOD, CO 80155

KEN RODDY UNION TEXAS PETROLEUM P.O. BOX 1290 FARMINGTON, NM 87499

DON READ MERIDIAN OIL CO.

WLAR BUHLING GULF P.O. BOX 1150) MIDLAND, TX 79702) BARBARA REX U-TEX 6331 BOXWOOD ROAD SALT LAKE CITY, UT 84121 1 . BARBARA WILLIAMS INDEPENDENT P.O. BOX 2038 FARMINGTON, NM 87401 BOB ADKINS AMOCO PRODUCTION COMPANY 501 AIRPORT DRIVE FARMINGTON, NM 87401 ED MARCUM MERIDIAN OIL CO. EPNG P.O. BOX 42899990 FARMINGTON, NM 87499-4209 ERNIE BUSCH NEW MEXICO OIL CONSERVATION DIV 1000 RIO BRAZOS ROAD AZTEC, NM 87410 1 FRANK CHAVEZ NEW MEXICO OIL CONSERVATION DIV 1000 RIO BRAZOS ROAD AZTEC, NM 87410 GARY HUDGINS

SOUTHERN UNION EXPLORATION

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RANDY RICKFORD AMOCO PRODUCTION COMPANY 501 AIRPORT DRIVE FARMINGTON, NM 87401 MAX WEBB ENGINEERING & PRODUCTION SERVICE P.O. BOX 190 FARMINGTON, NM 87401

ROBERT COVLIN AMOCO PRODUCTION COMPANY 1670 BROADWAY DENVER, CO 80202

MICHAEL L. DAVIES SOUTHERN UNION EXPLORATION P.O. BOX 2179 EARMINGTON, NM B799 DACCAS, Ty

RUDY MOTTO UNION TEXAS PETROLEUM P.O. BOX 1290 FARMINGTON, NM 87401

SANDY LIESE NORTHWEST PIPELINE CORP P.O. BOX 90 FARMINGTON, NM 87401

STELLA WHITAKER GAS COMPANY OF NEW MEXICO P.O. BOX 1899 BLOOMFIELD, NM 87413

STERGIE KATIRGIS UNION TEXAS PETROLEUM P.O. BOX 1290 FARMINGTON, NM 87401

STU McFARLAND AMOCO PRODUCTION COMPANY 1670 BROADWAY DENVER, CO 80202 MIKE TURNBAUGH NORTHWEST PIPELINE CORP P.O. BOX 90 FARMINGTON, NM 87401

MESA PETROLEUM COMPANY

FLORA VISTA, NM 87415

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P.O. BOX 579

R. L. STAMETS NEW MEXICO OIL CONSERVATION DIV P.O. BOX 2088 SANTA FE, NM 88501

RAEANNE LAMBERT GULF P.O. BOX 670 HOBBS, NM 88240

RALPH MONTOYA AMOCO PRODUCTION COMPANY 501 AIRPORT DRIVE FARMINGTON, NM 87401

TOM OLLE

A. R. KENDRICK FOUR CORNERS GAS PRODUCERS ASSOC. P.O. BOX 516 AZTEC, NM 87410

AL GREER BENSON-MONTIN-GREER

221 PETR. CENTER BLDG. Farmington, NM 87401

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Ordered Rows
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NAME
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name	NAME 2	COMPANY	ADDRESS	CITY	ZIP
MESA PETROLEUM		MESA OPERATING LIMITED PARTNERSHIP	P.O. BOX 579	FLORA VISTA, NM	87415
BOB	ADKINS	AMODO PRODUCTION COMPANY	SO1 AIRPORT DRIVE	FARMINGTON, NM	87401
JOHN	BARNETT	AMOCO PRODUCTION COMPANY	2325 E 30TH STREET	FARMINGTON, NH	87401
MARTIN	BOGGS	SOUTHERN UNION EXPLORATION CO	P.O. BOX 2179	FARMINGTON, NM	87499
ALAN	BOHLING	GULF	P.O. BOX 1150	MIDLAND, TX	79702
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FRANK	CHAVEZ	NEW MEXICO DIL CONSERVATION DIV	1000 RIO BRAZUS ROAD	AZTEC, NM	87410
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ROBERT	OOVLIN	AMOCO PRODUCTION COMPANY	1670 BROADWAY	DENVER, CO	80202
WARREN	CURTIS	NORTHWEST PIPELINE CORPORATION	(P. O. BOX 8900	SALT LAKE CITY, UT	84108
MICHAEL L.	DAVIES	SOUTHERN UNION EXPLORATION	1217 MAIN, SUITE 400	DALLAS, TX	75202
JACK	EVANS	SCHALK DEVELOPMENT COMPANY	P.O. BOX 2078	FARMINGTON, NM	87401
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JOEL	FOX	TENNECO OIL	P. D. BOX 3249	ENGLEWOOD, CO	80155
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AL	GREER	BENSON-HONTIN-GREER	221 PETR. CENTER BLDG.	FARMINGTON, NM	87401
DOUGLAS	HARRIS	MERIDIAN OIL CO.	P. D. BOX 4289	FARMINGTON, NM	87499-4289
GARY	HUDGINS	SOUTHERN UNION EXPLORATION	P. 0. BOX 2179	FARMINGTON, NM	87401
HUGH	INGRAM	CONOCO	P. 0. BOX 460	HOBBS, NM	86240
LOUIS	JONES	TENNECO OIL	P.O. BOX 3249	ENGLEWOOD, CO	80155
A. R.	KENDRIDK	FOUR CORNERS GAS PRODUCERS ASSOC.	P. 0. BOX 516	AZTEC, NM	87410
H. L. BABE	KENDRICK	el paso natural gas co	P. D. BOX 1492	EL PASO, TX	79978
JOEL		GAS COMPANY OF NEW MEXICO	2444 LOUISIANA NE	ALBUQUERQUE, NM	87125
SANDY	LIESE	NORTHWEST PIPELINE CORP	P.O. BOX 90	FARMINGTON, NM	87401
VICTOR T.	LYON	NHOOD	P. 0. BOX 2038	SANTA FE, NM	87501
E	MARCUM	el paso natural gas co	P. 0. BOX 990	FARMINGTON, NM	87401
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P IS	MOFARLAND	ANDCO PRODUCTION COMPANY	1670 BROADWAY	DENVER, CO	80202
RALPH	MONTOYA	AMOCO PRODUCTION COMPANY	501 AIRPORT DRIVE	FARMINGTON, NM	87401
RUDY	MOTTO	UNION TEXAS PETROLEUM	375 US HIGHWAY 64	FARMINGTON, NM	87401
GARY	MUNSON	AMOCO PRODUCTION COMPANY	501 AIRPORT DRIVE	FARMINGTON, NIT	87401
TOM		SOUTHLAND ROYALTY COMPANY	P.D. DRAWER 570	FARMINGTON, NH	87401
CON	READ	MERIDIAN OIL	P.O. BOX 4289	FARMINGTON, NM	87499-4289
RANDY	RICKFORD	ANDED PRODUCTION COMPANY	501 AIRPORT DRIVE	FARMINGTON, NM	87401
KEN	RODDY	UNION TEXAS PETROLEUM	375 US HIGHWAY 64	FARMINGTON, NO	87401
PHIL	SCHOFIELD	GAS COMPANY OF NEW MEXICO	P.O. BOX 1899	BLOOMFIELD, NII	87413
R, L,	STAMETS	NEW MEXICO UIL CONSERVATION DIV	P.O. BOX 2038	SANTA FE, NM	88501
HICHAEL E.	STOGNER	N-10CD	P. 0. BOX 2038	SANTA FE, MM	87501

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name	NAME 2	COMPANY	ADDRESS	CITY	dIZ
MIKE	TURNBAUGH	NORTHWEST PIPELINE CORP	P.0. BOX 90	FARMINGTON, NH	87401
CHARLES	VERQUER	CAULKINS OIL	P.O. BOX 780	FARMINGTON, NI1	87401
MAX	WEBB	ENGINEERING & PRODUCTION SERVICE	P.0. BOX 190	FARMINGTON, N11	87401
STELLA	WHITAKER	GAS COMPANY OF NEW MEXIDO	P.O. BOX 1899	BLOOMFIELD, N1	87413
BARBARA	WILL IAMS	INDEPENDENT	P.O. BOX 2038	FARMINGTON, NH	87401
BRUCE	WILLIAMS	AMODO PRODUCTION COMPANY	2325 E 30TH STREET	FARMINGTON, N1	87401
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MESA PETROLEUM		HESA OPERATING LINITED PARTNERSHIP	P.O. 60X 579	FLORA VISTA, NH	87415
BOB	ADKINS	AMODO PRODUCTION COMPANY	SO1 AIRPORT DRIVE	FARMINGTON, NI1	87401
NHOC	BARNETT	AMOCO PRODUCTION COMPANY	2325 E 30TH STREET	FARMINGTON, Nº1	87401
MARTIN	BOGGS	SOUTHERN UNION EXPLORATION CO	P. D. BOX 2179	FARMINGTON, NM	87499
ALAN	BOTTING	GULF	P.O. BOX 1150	MIDLAND, TX	79702
ERNIE	BUSCH	NEW MEXICO DIL CONSERVATION DIV	1000 RIO BRAZOS ROAD	AZTEC, NM	87410
FRANK	CHAVEZ	NEW MEXICO DIL CONSERVATION DIV	1000 RIO BRAZUS ROAD	AZTEC, NM	87410
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JACK	EVANS	SCHALK DEVELOPMENT DO PANY	P.O. BOX 2078	FARMINGTON, NI1	87401
BRENDA	FLAHERTY	MERIDIAN OIL CO	P.O. BOX 4289	FARMINGTON, NM	87499-4289
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AL	GREER	BENSON-MONTIN-GREER	221 PETR. CENTER BLDG.	FARI-INGTON, NIT	87401
DOUGLAS	HARRIS	MERIDIAN OIL CO.	P.0. BOX 4289	FARMINGTON, NM	87499-4289
GARY	HUDGINS	SOUTHERN UNION EXPLORATION	P.O. BOX 2179	FARMINGTON, NM	87401
HUGH	INGRAM	CONOCO	P.O. BOX 460	HOBBS, NM	88240
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A. R.	KENDRICK	FOUR CORNERS GAS PRODUCERS ASSOC.	P. 0. BOX 516	AZTEC, NH	87410
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JOEL	LEVINE	GAS COMPANY OF NEW MEXICO	2444 LOUISIANA NE	ALBUQUERQUE, NM	87125
SANDY	LIESE	NORTHWEST PIPELINE CORP	P.O. BOX 90	FARMINGTON, NM	87401
WICTOR-T	LYON	NHOCD	P.0. BUX 2088	SANTA FE, NM	87501
ED	MARCUM	EL PASO NATURAL GAS CO	P. D. BOX 990	FARMINGTON, NM	87401
7. 17	STILL ST	MESA OPERATING LIMITED PARTNERSHIP	P.0. BOX 2009	AMARILLO, TX	79189
2s	MCFARLAND	AMOCO PRODUCTION COMPANY	1670 BROADWAY	DENVER, CO	80202
RALPH	MONITOYA	ANDCO PRODUCTION COMPANY	501 AIRPORT DRIVE	FARMINGTON, NIT	87401
RUDY	MOTTO	UNION TEXAS PETROLEUM	375 US HIGHWAY 64	FARMINGTON, Nº1	87401
CIARY	NOSNAL	AHOCO PRODUCTION COMPANY	501 AIRPORT DRIVE	FARMINGTON, NIT	87401
MON	OLLE	SOUTHLAND ROYALTY COMPANY	P.O. DRAWER 570	FARMINGTON, NM	87401
THE REAL	-	MERIDIAN OIL	P.O. BOX 4289	FARMINGTON, NM	87499-4289
RANDY	RICKFORD	AHOCO PRODUCTION COMPANY	501 AIRPORT DRIVE	FARMINGTON, NH	87401
KEN	RODDY	UNION TEXAS PETROLEUM	375 US HIGHWAY 64	FARMINGTON, NM	87401
PHIL	SCHOFIELD.	GAS COMPANY OF NEW MEXICO	P.O. BOX 1899	BLOOMFIELD, NIT	87413
1. 1.	STANETS	NEW MEXICO DIL CONSERVATION DIV	P. 0. BOX 2058	SANTA FE, NM	88501
	STOCNER	N-10CD	P.O. BOX 2088	SANTA FE, NM	87501
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NAME 2	COMPANY	ADDRESS	CITY	ZIP
TURNBAUGH	NORTHWEST PIPELINE CORP	P.O. 650X 90	FARMINGTON, NM	87401
	CAULKINS OIL	P. 0. BOX 780	FARMINGTON, NIT	87401
	ENGINEERING & PRODUCTION SERVICE	P.0. BOX 190	FARMINGTON, NM	87401
WHITAKER	GAS COMPANY OF NEW MEXIDO	P.O. BOX 1899	BLOOMFIELD, NM	87413
WITH TANG	INDEPENDENT	P.0. BOX 2038	FARMINGTON, NM	87401
VILL IAMS	AMOCO PRODUCTION COMPANY	2325 E 30TH STREET	FARMINGTON, NM	87401
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ACKNOWLEDGMENT

NJIJ.

The New Mexico Oil Conservation Commission wishes to express its appreciation to the following men for their invaluable counsel and advice as well as their willing and effective work as members of the Industry Committee in analyzing the various materials used in this manual.

H.L. Kendrick, El Paso Natural Gas Company, Chairman, D. H. Ratney, El Paso Natural Gas Company, Shairman

C. E. Bowlin, Interstate Oil Compact Commission

T. M. Boyd, Jr., Consolidated Oil & Gas Company

C. R. Clement, Phillips Petroleum Company

A. J. Evans, Amerada Petroleum Corporation

R. L. Freeborn, Continental Oil Company

G. A. Hickson, El Paso Natural Gas Company

J. W. Meek, Pan American Petroleum Corporation

L. S. Muennick, Southern Union Gas Company

C. W. Rach, Northern Natural Gas Company

L. W. Rogers, Ir., Transwestern Pipeline Company

L. E. Thomas, Amerada Petroleum Corporation

G. L. Tribble, Northern Natural Gas Company

W. H. Williams, Consolidated Oil & Gas Company

Our appreciation is also expressed to the Interstate Oil Compact Commission for their permission to reproduce portions of their Manual of Back-Pressure Testing of Gas Wells.

R. t. Stumets, Director A. A. PORTER, Jr., Secretary-Director ELVIS A. UTZ, Gas Engineer

IN THAT I LEVAY MALFITTA



P. O. BOX 1492 EL PASO, TEXAS 79978 1-2600 September 3, 1986 **OIL CONSERVATION DIVISION** SANTA FE

William F. Carr, Chairman New Mexico Oil Conservation Division Gas Advisory Committee

> Subcommittee No. 3 Re: Priority of Takes Recommendations

Dear Mr. Chairman:

As you are aware subcommittee No. 3 convened on August 12, 1986 to discuss the priority of takes to be recommended to the advisory committee.

The committee expressed a desire to submit the following recommendations:

Rule 315 Priorities of Production

To prevent waste of New Mexico gas, producers shall to the extent permitted by operation of Rule 903, observe the following priority production schedule:

- (a) gas wells shall be the first restricted or shut in followed by;
- (b) downhole commingled wells involving one or more gas zones and one or more oil zones followed by; NOTE: (This item (b) was discussed and agreed that gas-gas downhole commingled wells would have a classification as gas wells and be viewed as being gas wells under (a) above; and, that gas-oil or oil-oil downhole commingled wells would have a classification as oil wells and would be viewed as being oil wells under (c) below.)
- (c) casinghead gas (including gas from associated pools) followed by:
- (d) hardship gas wells designated by the Division under Rule 410, Rule 411, or after hearing.

Rule 903 Priorities of Production

To prevent waste of New Mexico gas, purchasers shall observe the following priority production schedule:

(1) gas wells shall be the first restricted or shut in followed by;

William F. Carr, Chairman New Mexico Oil Conservation Division Gas Advisory Committee Page 2

- (2) downhole commingled wells involving one or more gas zones and one or more oil zones followed by; NOTE: (This item (2) was discussed and agreed that gas-gas downhole commingled wells would have a classification as gas wells and be viewed as being gas wells under (1) above; and, that gas-oil or
 - oil-oil downhole commingled wells would have a classification as oil wells and would be viewed as being oil wells under (3) below.)
- (3) casinghead gas (including gas from associated pools) followed by;
- (4) hardship gas wells designated by the Division under Rule 410, Rule 411, or after hearing.

It is the recommendation of the chairman of subcommittee No. 3 that the following be adopted:

Rule 315 Priorities of Production

To prevent waste of New Mexico gas, producers shall to the extent permitted by operation of Rule 903, observe the following priority production schedule:

- (a) gas wells shall be the first restricted or shut in followed by;
- (b) downhole commingled wells involving one or more gas zones and one or more oil zones followed by;

NOTE: (This item (b) was discussed and agreed that gas-gas downhole commingled wells would have a classification as gas wells and be viewed as being gas wells under (a) above; and, that gas-oil or oil-oil downhole commingled wells would have a classification as oil wells and would be viewed as being oil wells under (c) below.)

- (c) casinghead gas (including gas from associated pools) followed by;
- (d) hardship gas wells designated by the Division under Rule 410, Rule 411, or after hearing.

Rule 903 Priorities of Production

- (a) To prevent waste of New Mexico gas, purchasers shall observe the following priority production schedule:
 - gas wells shall be the first restricted or shut in followed by;

William F. Carr, Chairman New Mexico Oil Conservation Division Gas Advisory Committee Page 3

- (2) Downhole commingled wells involving one or more gas zones and one or more oil zones followed by; NOTE: (This item (2) was discussed and agreed that gas-gas downhole commingled wells would have a classification as gas wells and be viewed as being gas wells under (1) above; and, that gas-oil or oil-oil downhole commingled wells would have a classification as oil wells and would be viewed as being oil wells under (3) below.)
- (3) casinghead gas (including gas from associated pools) followed by;
- (4) hardship gas wells designated by the Division under Rule 410, Rule 411, or after hearing.
- (b) Nothing in this rule shall be construed or applied to require, directly or indirectly, any person to purchase gas of a quality or under a pressure or under any other condition by reason of which such gas cannot be economically and satisfactorily used by such purchaser by means of his gas transportation facilities then in service.
- (c) Should any purchaser be unable to take gas in accordance with the schedule described in paragraph (a) of this rule because of any of the conditions described in paragraph (b) above, such purchaser shall notify the operator of the affected wells of such condition.

With respect to the chairman's recommendations that (b) and (c) in Rule 903 be added to the committee's recommendations the producers of gas stated that they did not fully understand what paragraph (b) and (c) meant and for this reason preferred to delete these two paragraphs.

The chairman pointed out to the committee that paragraph (b) was quoted from the New Mexico statutes verbatim and he therefore felt that it should be added to Rule 903 for the edification of those who read and work with the rules and not with the statutes.

It is my feeling that paragraph (b) is the basis for the proration of gas in the state of New Mexico in order for the division to remain legal during periods when availability of gas exceeds the demand.

Respectfully,

E. R. Manning

je

William F. Carr, Chairman New Mexico Oil Conservation Division Gas Advisory Committee Page 4 - Distribution

James C. Allen William F. Clärk Warren Curtis Bill Duncan H. L. Kendrick

.

Vic Lyon Ernest Padilla R. L. Stamets George Safi ✓ Michael Stogner Jeff Taylor





August 20, 1986

Members of Subcommittee No. 3 Priority of Takes of the New Mexico Gas Advisory Committee

Attached are minutes of the August 12, 1986 meeting in Santa Fe, New Mexico.

If there is anything drastically in error, please so advise.

Very truly yours,

E.R. Manny E. R. Manning

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Attachments

NMOCD SUBCOMMITTEE NO. 3 PRIORITY OF TAKES, MINUTES AUGUST 12, 1986

The Priority of Takes Sub-committee of the Gas Advisory Committee to the NMOCD convened at 9:00 am on August 12, 1986 in the conference room of the State Land Office Building in Santa Fe, NM. A list of the attendees is attached.

Discussions were centered on Rules 315, 902 and 903.

Rule 315 was re-written as follows:

Rule 315 Priorities of Production

To prevent waste of New Mexico gas, producers shall to the extent permitted by operation of Rule 9D3, observe the following priority production schedule:

- (a) gas wells shall be the first restricted or shut in followed by;
- (b) downhole commingled wells involving one or more gas zones and one or more oil zones followed by;
 NOTE: (This item (b) was discussed and agreed that gas—gas downhole commingled wells would have a classification as gas wells and be viewed as being gas wells under (a) above; and, that gas—oil or oil—oil downhole commingled wells would have a classification as oil wells and would be viewed as being oil wells under (c) below.)
- (c) casinghead gas (including gas from associated pools) followed by:
- (d) hardship gas wells designated by the Division under Rule 410, Rule 411, or after hearing.

Rule 903 was rewritten and comments were made concerning paragraphs (b) and (c). The results of a poll taken of those members of the committee present at this meeting indicated:

- 1. the producers of gas do not fully understand what paragraph (b) and (c) mean; and,
- 2. the producers would prefer to see Rule 903 written with paragraphs (b) and (c) deleted from the rule; and,
- 3. the major pipelines represented at the meeting would prefer to have paragraphs (b) and (c) included in the rule.

With the above comments in mind, Rule 903 is written below with changes as preferred shown in paragraph (a) and paragraphs (b) and (c) are included for evaluation purposes:

Rule 903 Priorities of Production

X

- (a) To prevent waste of New Mexico gas, purchasers shall observe the following priority production schedule:
 - (1) gas wells shall be the first restricted or shut in followed by:
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- (3) casinghead gas (including gas multi associated pools, including gas multi associated pools, including (4) hardship gas wells designated by the Division under Rule 410, Rule
- (b) Nothing in this rule shall be construed or applied to require directly or indirectly, any person to purchase gas of a quality or under a pressure or under any other condition by reason of which such gas cannot be economically and satisfactorily used by such purchaser by means of his gas transportation facilities then in service.
- (c) Should any purchaser be unable to take gas in accordance with the schedule described in paragraph (a) of this rule because of any of the conditions described in paragraph (b) above, such purchaser shall notify the operator of the affected wells of such condition.

A proposal was submitted by Exxon with paragraphs (b) and (c) rewritten. Their proposal was withdrawn pending the assumption that paragraphs (b) and (c) as otherwise written would be eliminated from the rule.

A proposal was submitted by Blackwood & Nichols Co. suggested a change of wording for paragraph (a) of Rule 315 and paragraph (1) of Rule 903 (from that shown above) to indicate "that in prorated gas pools, gas proration units with overproduction shall be restricted or shut in before underproduced units".

A list of wells that have been approved as hardship classification within the State of New Mexico was presented to the committee by Michael Stogner.

Bill Clark submitted a memo dated August 6, 1986 to the group concerning the classification of wells and suggested changes to proration regulations. He asked for each person to read this proposal and give him as much feed back as possible.

The need for an additional meeting of this committee was left open pending the outcome of the poll of members of this committee concerning paragraphs (b) and (c) of Rule 903.



P O BOX 1492 EL PASO, TEXAS 79978 PHONE 915-541-2600

August 20, 1986

Members of Subcommittee No. 3 Priority of Takes of the New Mexico Gas Advisory Committee

Attached are minutes of the August 12, 1986 meeting in Santa Fe, New Mexico.

If there is anything drastically in error, please so advise.

Very truly yours, E. R. Manning

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With the above comments in mind, Rule 903 is written below with changes as preferred shown in paragraph (a) and paragraphs (b) and (c) are included for evaluation purposes:

Rule 903 Priorities of Production

7

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The need for an additional meeting of this committee was left open pending the outcome of the poll of members of this committee concerning paragraphs (b) and (c) of Rule 903.

Ordered Rows from SUBCOMMITTEE NO. 3 ATTENDANCE, SANTA FE, 8/12/86

ERNEST E.R. VIC GEORGE H. L. BILL JEFF CHAIRMAN* MICHAEL WARREN WILLIAM F. JAMES C. FIRST NAME BABE SAFI QLARK LYON ALLEN STOGNER PADILLA MANNING* KENDRICK DUNCAN CURTIS TAYLOR LAST NAME NHOOD **NHOOD** EXXON COOLN NHOOD EXXON EL PASO NATURAL GAS CO. NORTHWEST PIPELINE CORP. BLACKWOOD & NICHOLS CO. LTD. EL PASO NATURAL GAS CO. AMOCO PRODUCTION CO. COMPANY סס סס .D σ. סס σ P P 00000000 0000E D X Z BOX BOX BOX BOX BOX **B** S BOX BÖX BOX BOX 0068 2088 2088 2523 1492 2088 1492 1600 1237 1600 3092 ADORESS SANTA FE SANTA FE EL PASO SANTA FE EL PASO MIDLAND SALT LAKE CITY DURANGO SANTA FE MIDLAND HOUSTON CITY ZZZZ ΞZ **58* STATE 87504 87504 87504 84108 20664 79978 79978 79902 87504 81301 77253 ZIP

Page

8/12/86 Privity Committee - Santo Fe H.L. BARE KENDRICK BOX 1492 CARSS TO 79278 Corgo Safi Exxon, Dox 1600 Midland, TX19902 Bill Duncan " JAMes C. Allen Amoco Box 3092 Houston, Tx 77253 EN POBox 1257 Burringo 6 81302 Warren Curtis NWP P.O. Box 8900 SLC CAMA 8410 Peff Taylor OCD Santa Fe ERNEST PADILLA PO. Box 2523 Satz Ze 87504 Vic Lyon OCD Sonto Fe E.R. Bob MANNING BOY 1492 ECPASO TX 78978 915/541-5073 Michael F. Stormer MMOLD POBox 2088 Santa Fe 87504



TO Deliverability Test Committee

DATE: April 23, 1986

PLACE: Production Control

FROM H. L. "Babe" Kendrick

Subject: Additional Work by Committee

Recent discussions with others in the natural gas industry have indicated there is a need for some additional work to be done by this committee.

The work that was done in rewriting the test procedures for gas wells in the San Juan Basin was a job well done. However, there may be a few areas where conditions now exist which tell us that we may wish to add a few words or phrases into these test procedures.

In search of these "other ideas" that you may have, I ask that you write those ideas to me or call me on the phone and express them to me so that I can list each idea and notify the other members. Even just a yes, no or hello.

If there are ideas that you feel need tended to, please rush them to me so we can complete any action on them before we publish the San Juan Basin Test Manual.

Your support is appreciated.

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Ordered Rows from MAIL LIST 4/23/86 TEST COMMITTEE

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name	company	address	city/state	zip code
BRADLEY SALZMAN	AMOOD PRODUCTION 00.	501 AIRPORT DR.	FARMINGTON, NM	87401
CHARLES BOYCE	AMOCO PRODUCTION CO.	P.O. BOX 800	DENVER, CO	80201
BOB ADKINS	AMOOD PRODUCTION COMPANY	501 AIRPORT DRIVE	FARMINGTON, NM	87401
GARY MUNSON	AMOOD PRODUCTION COMPANY	501 AIRPORT DRIVE	FARMINGTON, NM	87401
RALPH MONTOYA	AMOCO PRODUCTION COMPANY	501 AIRPORT DRIVE	FARMINGTON, NM	87401
RANDY RICKFORD	AMOOD PRODUCTION COMPANY	501 AIRPORT DRIVE	FARMINGTON, NM	87401
ROBERT COVLIN	AMOCO PRODUCTION COMPANY	1670 BROADWAY	DENVER, CO	80202
STU MOFARLAND	AMOOD PRODUCTION COMPANY	1670 BROADWAY	DENVER, CO	80202
AL GREER	BENSON-MONTIN-GREER	221 PETR. CENTER BLDG.	FARMINGTON, NM	87401
MIKE CASEY	CHEVRON U.S.A. INC.	P.O. BOX 670	HOBBS, NM	88240
JOSEPH D. STEWART	COLUMBLIS ENERGY CORP.	1860 LINCOLN ST.	DENVER, CO	80295
HUGH INGRAM	CONDCO	P.O. BOX 460	HOBBS, NM	88240
STEVE CATHEY	CONDO, INC	501 AIRPORT #115	FARMINGTON, NM	87401
EMERY C. ARNOLD	CONSULTANT	200 CRANDALL	AZTEC, NM	87410
JOHN ROE	DUGAN PRODUCTION CORP.	P.O. BOX 208	FARMINGTON, NM	87499
H. L. BABE KENDRICK	EL PASO NATURAL GAS CO	P.O. BOX 1492	EL PASO, TX	87928
MAX WEBB	ENGINEERING & PRODUCTION SERVICE	P.O. BOX 190	FARMINGTON, NM	87401
A. R. KENDRICK	FOUR CORNERS GAS PRODUCERS ASSOC.	P.O. BOX 516	AZTEC, NM	87410
STELLA WHITAKER	GAS COMPANY OF NEW MEXICO	P.O. BOX 1899	BLOOMFIELD, NM	87413
BOB LARGE	GAS COMPANY OF NM	P.O. BOX 1899	BLOOMFIELD, NM	87413
CYNDI PERRY	GAS COMPANY OF NM	P.O. BOX 1899	BLOOMFITELD, NM	87413
JOEL LEVINE	GAS COMPANY OF NM	P.O. BOX 26400	ALBUQUERQUE, NM	87110
PAUL MOLLO	GAS COMPANY OF NM	P.O. BOX 26400	ALBUQUERQUE, NM	87110
ALAN BOHLING	GUF	P.O. BOX 1150	MIDLAND, TX	20167
RAEANNE LAMBERT	GULF	P.O. BOX 670	HOBBS, NM	88240
BARBARA WILLIAMS	INDEPENDENT	P.O. BOX 2038	FARMINGTON, NM	87401
JAMES W. SMITH	MERIDIAN 011. CO	P.O. BOX 4289	FARMINGTON, NM	87499
ED MARCUM	MERIDIAN OIL CO.	P.0. BOX 4289	FARMINGTON, NM	87499-4289
L. E. MABE	MERIDIAN DIL CO.	P.0. BOX 4239	FARMINGTON, NM	87499-4289
MIKE MASER	MESA PETROLEUM COMPANY	P.O. BOX 579	FLORA VISTA, NM	87415
RANDY NORDSVEN	MESA PETROLEUM COMPANY	P.O. BOX 2009	AMARILLO, TX	79189
ERNIE BUSCH	NEW MEXICO DIL CONSERVATION DIV	1000 RID BRAZOS ROAD	AZTEC, M	87410
FRANK CHAVEZ	NEW MEXICO OIL CONSERVATION DIV	1000 RIO BRAZOS FOAD	AZTEC, NH	87410
HAROLD GARCIA	NEW MEXICO DIL CONSERVATION DIV	F.O. BOX 2083	SANTA FE, NM	87501
R. L. STAMETS	NEW MEXICO DIL CONSERVATION DIV	P.O. BOX 2033	SANTA FE, NM	88501
ALICE DUGGER	NTOCD CONTRACTOR	1000 RIO BRAZOS HOAD	AZTEC, NM	87410
VICTOR T. LYON	NHOOD	P.O. BOX 2038	SANTA FE, NM	87501
MIKE TURNBAUGH	NORTHWEST PIPELINE CORP	P.O. BOX 90	FARMINGTON, NM	87401

Ordered Rows from MAIL LIST 4/23/86 TEST COMMITTEE

name	company	address	city/state	zip code
SANDY LIESE	NORTHWEST PIPELINE CORP	P. 0. BOX 90	FARMINGTON, NM	87401
WARREN OURTIS	NORTHWEST PIPELINE CORP.	295 CHIPETA WAY	SALT LAKE CITY, UT	84108
JACK EVANS	SCHALK DEVELOPMENT COMPANY	P.O. BOX 2078	FARMINGTON, NM	87401
MICHAEL L. DAVIES	SOUTHERN UNION EXPLORATION	1217 MAIN, SUITE 400	DALLAS, TX	75202
GARY HUDGINS	SOUTHERN UNION EXPLORATION	P.O. BOX 2179	FARMINGTON NM	87401
TOM OLLE	SOUTHLAND ROYALTY COMPANY	P.O. DRAWER 570	FARMINGTON, NM	87401
808 GIB8	TENNECO	P.0. BOX 3249	ENGLEWOOD, CO	80155
JOHN COOK	TENNECO	P.0. BOX 3249	ENGLEWOOD, CD	80155
BARBARA REX	U-TEX	6331 BOXWOOD ROAD	SALT LAKE CITY, UT	84121
KEN RODOY	UNION TEXAS PETROLEUM	P.O. BOX 1290	FARMINGTON, NM	87499
RUDY MOTTO	UNION TEXAS PETROLEUM	P.0. BOX 1290	FARMINGTON, NM	87401
STERGIE KATIRGIS	UNION TEXAS PETROLEUM	P.0. BOX 1290	FARMINGTON, NM	87401
W. K. COOPER	UNION TEXAS PETROLEUM	375 U.S. HIGHWAY 64	FARMINGTON, NM	87401

MEMORANDUM

TO:DELIVERABILITY TEST COMMITTEEPLACE:EL PASO, TEXASFROM:H. L. BABE KENDRICKDATE:AUGUST 23, 1985

SUBJECT: PITOT TUBE FLOW CHART TABLES

Some time ago I sent out a plea for information to a few of you members to obtain data necessary to calculate a new set of flow rates for Pitot Tube Test Tables. What had happened through the years was that a set of values had been published for all to use, but, I was unable to come up with the same values by any method of calculation that I knew. So therefore the request for HELP!. I did get several responses and I have made an attempt at calculating a new set of flow tables for measurement by use of the Pitot Tube for the San Juan Basin of New Mexico. This now sends out another plea for help! I need you to look through these attached tables for any errors, miscalculations, advice, suggestions, whatever that comes to your mind, and let me know how they can best be put together and be published in the booklet of test procedures for the San Juan Basin.

If I have made this table in the manner that I think is correct, then the only corrections to any flow rate as measured by using the Pitot Tube would be to correct the rate for any difference in specific gravity of the gas from 0.600 and adjust the flow rate for any flowing temperature difference from 60⁰F.

Also, I do not place much value on showing flow rates in a Pitot Tube Table with MCF/D measured to one-tenth MCF/D. With your approval, I will remake the table with your corrections to show only whole numbers for the flow rates.

Do you have any pictures of any gas production equipment that you would permit us to use on the cover of the Test Manual For the San Juan Basin. I looked for something appropriate and did not have much luck in finding something good. This could be approximately 2 inches high and up to 6.5 inches wide. I looked at the NMOCD stationery and found a picture of a pump jack, which leaves me cold for a gas well test manual. Maybe a hand drawing of gas production equipment or....your suggestions. Thanks.

(I printed the calculation routine tables on 2 sides of the paper to conserve paper and postage. I hope this is OK with you.)

Sincerely,

EXPLANATION OF CALCULATION OF PITOT TUBE TABLES 8/15/85

THESE PAGES ARE INTENDED TO DESCRIBE THE CALCULATIONS USED IN DETERMINING THE VALUES DISPLAYED IN THE ATTACHED 43 PAGE TABLE OF PITOT TUBE VALUES TO BE USED IN THE SAN JUAN AREA OF NEW MEXICO.

A PAGE LIST DESCRIBES WHAT VALUES CAN BE FOUND ON WHICH PAGE. THE COLUMNS RUN ACROSS THE PAGE FROM LEFT TO RIGHT FROM "A" TO "R". VALUES FOR THE PITOT TABLES WILL BE FOUND ONLY IN COLUMNS "A THRU H". ROWS RUN DOWN THE PAGE FROM 1 TO 255. A "CELL" IS DEFINED AS ONE BOX IN THE CHART THAT CAN BE IDENTIFIED AS "COLUMN NO.--ROW NO.". FOR INSTANCE IF YOU LOOK IN "COLUMN D ROW 5" YOU FIND A VALUE PRINTED AS 1.049 AND THIS "CELL" IS IDENTIFIED AS D5.

NOW FOR SOME OF THE DATA ON THIS CHART.

COLUMN A DISPLAYS THE IMPACT PRESSURE AS MEASURED IN INCHES OF WATER AND "CELL" A7 STARTS THE LIST WITH A VALUE OF 0.1 INCHES AND THE PRESSURE INCREASES AS YOU PROGRESS TO ADDITIONAL ROWS GOING DOWN THE PAGE.

COLUMN B DISPLAYS THE IMPACT PRESSURE AS MEASURED IN INCHES OF MERCURY WITH THE FIRST VALUE ENTERED IN THIS COLUMN BEING IN "CELL" B33 AS A VALUE OF 0.2 INCHES. THE IMPACT PRESSURES SHOWN IN INCHES OF MERCURY ARE ONLY INDICATED SPASMODICALLY UNTIL A PRESSURE OF 1.21 INCHES MERCURY IS FOUND AT "CELL" B119. THESE PRESSURES IN INCHES OF MERCURY ARE SHOWN ONLY AS VALUES ASSOCIATED WITH THE IMPACT PRESSURES IN INCHES OF WATER AS INDICATED IN COLUMN A DOWN TO "CELL" A166. BEGINNING WITH "CELL" B167 THE TABLE PROGRESSES WITH INCREASED PRESSURES SYSTEMATICALLY IN THE B COLUMN USING INCHES OF MERCURY IMPACT PRESSURE.

COLUMN C DISPLAYS THE IMPACT PRESSURE AS MEASURED IN POUNDS PER SQUARE INCH GAUGE. THE FIRST ENTRY IS A VALUE OF 0.25 FOUND IN "CELL" C75. THE VALUES OF PSIG ONLY APPEAR SPASMODICALLY UNTIL "CELL" C175 BEGINS WITH A VALUE OF 2.26 PSIG AND FROM THERE DOWN TO "CELL" C231 THE VALUES CORRESPOND TO THE INCHES OF MERCURY COLUMN.

AT ROW 232 THE SPACING BETWEEN NUMBERS REPRESENTING THE IMPACT PRESSURES PROGRESSES WITH SPACINGS IN THE PSIG COLUMN TO THE END OF THE CHART AT "CELL" C255 WITH AN IMPACT PRESSURE OF 39.00 PSIG.

THE REASONING BEHIND THE CHOSEN VALUES OF IMPACT PRESSURE IS:

1. GENERALLY THE FLOW RATE TO BE MEASURED BY PITOT TUBE TYPE MEASUREMENT WILL BE A VERY SMALL NUMBER SO THE INCHES OF WATER TABLE WAS MADE TO COVER THOSE VALUES.

2. UP TO 30 INCHES OF WATER CAN USUALLY BE MEASURED WITHOUT MUCH TROUBLE. ABOVE THAT POINT THE MEASUREMENT CAN BE MEASURED IN INCHES OF MERCURY. 3. IF THE FLOW RATE IS SUCH THAT THE IMPACT PRESSURE CAN BE MEASURED IN PSIG, THEN THE COLUMN FOR THAT TYPE MEASUREMENT IS PROVIDED.

4. THERE ARE TIMES WHEN THE FLOW RATE THROUGH A FLOW NIPPLE IS QUITE LARGE AND FOR THAT REASON VALUES ARE PROVIDED FOR DETERMINING FLOW RATES THROUGH LARGER FLOW NIPPLES UP TO 6 INCHES.

COLUMNS D, E, F, G AND H ARE PROVIDED TO INDICATE THE FLOW RATE THROUGH FLOW NIPPLES OF NOMINAL SIZES OF 1, 2, 3, 4 AND 6 INCHES.

"CELL" D5 INDICATES A VALUE OF 1.049 INCHES. THIS IS CONSIDERED THE INSIDE DIAMETER OF 1 INCH LINE PIPE. IF THIS VALUE IS INCORRECT, IT CAN BE CHANGED OR THE FLOW RATE CAN BE CORRECTED BY USING THE CORRECT DIAMETER OF THE FLOW NIPPLE.

"CELL" E5 INDICATES A VALUE OF 2.067 INCHES. THIS IS CONSIDERED THE INSIDE DIAMETER OF 2 INCH LINE PIPE. IF THIS VALUE IS INCORRECT, IT CAN BE CHANGED OR THE FLOW RATE CAN BE CORRECTED BY USING THE CORRECT DIAMETER OF THE FLOW NIPPLE.

"CELL" F5 INDICATES A VALUE OF 3.068 INCHES. THIS IS CONSIDERED THE EVENDE DIAMETER OF 3 INCH LINE PIPE. IF THIS VALUE IS INCORRECT, IT CAN BE CHANGED OR THE FLOW RATE CAN BE CORRECTED BY USING THE CORRECT DIAMETER OF THE FLOW NIPPLE.

"CELL" G5 INDICATES A VALUE OF 4.026 INCHES. THIS IS CONSIDERED THE INSIDE DIAMETER OF 4 INCH LINE PIPE. IF THIS VALUE IS INCORRECT, IT CAN BE CHANGED OR THE FLOW RATE CAN BE CORRECTED BY USING THE CORRECT DIAMETER OF THE FLOW NIPPLE.

"CELL" H5 INDICATES A VALUE OF 6.065 INCHES. THIS IS CONSIDERED THE INSIDE DIAMETER OF 6 INCH LINE PIPE. IF THIS VALUE IS INCORRECT, IT CAN BE CHANGED OR THE FLOW RATE CAN BE CORRECTED BY USING THE CORRECT DIAMETER OF THE FLOW NIPPLE.

A TABLE IS ATTACHED TO INDICATE HOW THE PAGES ARE NUMBERED THROUGHOUT THIS REPORT. COLUMNS A THRU F ARE PRINTED ON PAGES 1 THRU 21. COLUMNS G THRU L ARE PRINTED ON PAGES 22 THRU 42 AND COLUMNS M THRU R ARE PRINTED ON PAGES 43 THRU 63. I HAVE ONLY SUBMITTED TO YOU PAGES 1 THRU 43. THESE PAGES CONTAIN ALL THE DATA THAT WAS USED IN CALCULATING THE VALUES OF FLOW NECESSARY TO THESE TABLES.

NOW THAT I HAVE TRIED TO INTRODUCE YOU TO SOME OF THE PECULIARITIES OF THE APPLE LISA COMPUTER, LET ME ASK YOU TO LOOK AT CERTAIN VALUES THAT WERE APPLIED IN THE COMPUTATIONS. START WITH PAGE 22, "CELL" L1. (IN LISA LANGUAGE * MEANS MULTIPLY, / MEANS DIVIDE, = MEANS EQUALS, AND ^ MEANS EXPONENT.)

- "CELL" L1: (36DD*24*52D*Π)/10DD*4*144*14.7) = 16.6696753 THIS IS PART OF THE FLOW FORMULA FROM THE HANDBOOK OF NATURAL GAS.
- "CELL" L3: $((62.4*10.73*64.4)/(12*29))^{.5} = 11.13128923$ THIS IS ANOTHER PART OF THE FLOW FORMULA FROM THE HANDBOOK OF NATURAL GAS.
- "CELL" L7: L1*L3 = 185.5549772 THIS TAKES THE VALUES DETERMINED IN L1 AND L3 ABOVE AND MULTIPLIES THEM TOGETHER.
- "CELL" L9: D.86*((14.7)/(D.6*52D))^{*}.5 = .1866722756 AT THIS POINT I PLACED THE EFFICIENCY FACTOR OF D.86 INTO THE FLOW FORMULA FROM THE NATURAL GAS HANDBOOK AND ALSO APPLIED A GRAVITY OF D.6 AND A TEMPERATURE OF 63⁰ F (OR 520⁰ Abs.).

"CELL" L11: L7*L9 = 34.63796984 THIS TAKES THE VALUES DETERMINED IN L7 AND L9 ABOVE AND MULTIPLIES THEM TOGETHER. THIS VALUE IS THE ONE THAT HAS BEEN USED TO DETERMINE THE FLOW RATE FOR EACH VALUE OF THE IMPACT PRESSURE.

IN EACH OF THE CELL VALUES OF D7, E7, F7, G7, AND H7 AND ON DOWN THE PAGES THROUGH CELL VALUES OF D255, E255, F255, G255 AND H255, L11 IS THE MAIN MULTIPLYING FACTOR. OTHER FACTORS ARE INCLUDED ALSO. SINCE THE FORMULA FROM THE NATURAL GAS ENGINEERING HANDBOOK CALCULATES THE FLOW RATE AT 14.7 PSIA I ADDED A FACTOR OF (14.7/15.025) TO ADJUST THE FLOW RATE TO A PRESSURE BASE OF 15.025 NECESSARY TO THE STATE OF NEW MEXICO. THIS COULD HAVE BEEN INCORPORATED INTO THE L11 VALUE BUT I DID NOT CHOOSE TO DO SO. (REALLY I WANTED TO SHOW THE VALUE I USED FOR L11 AS BEING SOMEWHAT DIFFERENT FROM THE VALUE SHOWN IN THE NATURAL GAS ENGINEERING HANDBOOK, AND PROBABLY THE ONLY DIFFERENCE IS BY THE AMOUNT OF ROUND OFF THEY USED IN COMPARISON TO WHAT I HAVE USED. ANYWAY THE VALUES ARE DIFFERENT!)

ALSO INCLUDED IN EACH "CELL" CALCULATION IS THE VALUE OF THE DIAMETER OF THE FLOW NIPPLE SQUARED TIMES THE SQUARE ROOT OF THE IMPACT PRESSURE IN INCHES OF WATER TIMES THE L11 VALUE TIMES THE CORRECTION FOR PRESSURE BASE.

 $L11*D5^{2}*(A7)^{.}5*(14.7/15.025) = 12 = CELL D7$

AT ROW 167 THE CALCULATION ROUTINE WAS CHANGED A LITTLE TO CHANGE THE MULTIPLIER FROM INCHES OF WATER IMPACT DIRECTLY TO INCHES OF MERCURY TIMES 13.59.

 $L11*D5^{2}*(B167*13.59)^{.}5*(14.7/15.025) = 238 = CELL D167$

AT ROW 231 THE CALCULATION ROUTINE WAS CHANGED A LITTLE TO CHANGE THE MULTIPLIER FROM INCHES OF MERCURY IMPACT TO POUNDS PER SQUARE INCH IMPACT. THIS WAS DOWN BY TAKING THE POUNDS PER SQUARE INCH IMPACT PRESSURE TIMES 144 TIMES 12 AND DIVIDING BY 62.428.

> L11*D5²*(C231*144*12/62.428)^{.5*}(14.7/15.025) = 760 = CELL D231

TO DETERMINE THE RATE OF FLOW BY PITOT TUBE MEASUREMENT:

1. MEASURE THE IMPACT PRESSURE AND FLOWING TEMPERATURE AND GAS GRAVITY.

2. FIND THE FLOW RATE IN THESE TABLES CORRESPONDING TO THE MEASURED IMPACT PRESSURE.

3. MULTIPLY THAT FLOW RATE BY THE APPROPRIATE CORRECTION FACTOR FOR TEMPERATURE AND GRAVITY.

NOTES;

EACH CALCULATION FOR EACH CELL VALUE FROM D7-D255 AND E, F, G, AND H FROM 7-255 WERE EACH CALCULATED <u>SEPARATELY</u> AND ONE VALUE WAS NOT ESTABLISHED AS A MULTIPLE OF ANOTHER PREVIOUSLY CALCULATED FLOW RATE VALUE.

NOW FOR THE HARD PART: I NEED EACH OF YOU (OR ANYONE YOU CAN GET) TO LOOK THIS OVER <u>VERY CAREFULLY</u> TO FIND OUT WHAT HAS BEEN DONE WRONG. I THINK THAT I CAN GET PRINTED ANY ANSWER THAT YOU FEEL IS THE CORRECT ANSWER TO BE APPLIED FOR THIS TABLE. IT MAY SEEM STRANGE THAT AFTER ALL THESE YEARS WE NOW ARE UNABLE TO CALCULATE THE SAME ANSWER FOR THESE TABULAR VALUES AS HAS BEEN PUBLISHED FOR THIS AREA.

IF YOU HAVE ANY QUESTIONS WHATEVER ABOUT WHAT I HAVE DONE OR WHY I DID IT THIS WAY PLEASE FEEL FREE TO CALL ME SO WE CAN DISCUSS IT.

	COLUMNS	COLUMNS	COLUMNS
ROW	A-F	G-L	M-R
NUMBERS	PAGE NO.	PAGE NO.	PAGE NO.
4 47	1	9 9	40
117	1	22	43
1831	2	23	44
3245	3	24	45
4659	4	25	45
6 073	5	26	47
7487	6	27	4 8
88101	7	28	49
102115	8	29	50
116129	9	30	51
130143	10	31	52
144157	11	32	53
158170	12	33	54
171181	13	34	55
182192	14	35	56
193203	15	36	57
204214	16	37	58
215225	17	3 8	59
225235	18	39	60
236244	19	40	61
245253	20	41	62
254255	21	42	63

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PITOT TA	BLEC 8/12/95	NQ. 2	2				Page	1 נ
PITOT TU	BE IMPACT PRE	SSURE	FLOW	NIPPLE	INSIDE	DIAMETER	INCHES	
INCHES	INCHES LBS.	PER	1" nominal	2" nominal	3" nominal	4" nominal	6" nominal	
WATER	MERCURY SQ.	IN.	actual dia.					
			1.049	2.067	3.068	4.026	6.065	
. 1			12	46	101	174	394	
. 2			17	65	143	246	557	
. 3			20	79	175	301	683	
. 4			24	92	202	347	788	
.5			26	102	226	388	881	
.6			29	112	247	425	966	
.7			31	121	267	460	1.043	
. 8			33	130	285	491	1, 115	
g			35	137	303	521	1, 183	
1.0			37	145	319	549	1 247	
1.1			39	152	335	576	1.307	
1.2			41	159	349	602	1 366	
1.3			43	165	364	626	1 421	
1.4			44	171	377	650	1 475	
1.5			46	177	391	673	1 527	
1.6			47	183	403	695	1 577	
1.7			49	189	416	716	1,625	
1.8			50	194	428	737	1,672	
1.9			51	200	440	757	1.718	
2.0			53	205	451	777	1, 763	
2.1			54	210	462	796	1,806	
2.2			55	215	473	815	1,849	
2.3			57	220	484	833	1,891	
2.4			58	224	494	851	1,931	
2.5			59	229	504	869	1,971	
2.6			60	233	514	886	2,010	
2.7	. 20		61	238	524	903	2,048	
2.8			62	242	534	919	2,086	
2.9			64	247	543	9 35	2, 123	
3.0			65	251	552	951	2, 159	
3.1			66	255	562	967	2, 195	
3.2			67	259	571	983	2,230	
3.3			68	263	579	998	2, 265	
3.4			69	267	588	1,013	2,299	
3.5			70	271	597	1, 028	2, 332	
3.6			71	275	605	1,042	2,365	
3.7			72	279	614	1,057	2, 398	
3.8			73	282	622	1,071	2, 430	
3.9			74	286	630	1,085	2, 462	
4.0			75	290	638	1,099	2, 493	
4.1	. 30		76	293	64 6	1, 112	2, 524	
4.2			76	297	654	1, 126	2, 555	

2, 585 2,615 2,644 2,674 2,703 2,731 2,759 2,787 2,815 2,843 2,870 2,897 2,923 2,950 2,976 3,002 3,028 3,053 3,079 3, 104 3, 129

2.4		58	224	494	851
2.5		59	229	504	869
2.6		60	233	514	886
2.7	. 20	61	238	524	903
2.8		62	242	534	919
2.9		64	247	543	9 35
3.0		65	251	552	951
3.1		66	255	562	967
3.2		67	259	571	983
3.3		68	263	579	998
3.4		69	267	588	1.013
3.5		70	271	597	1.028
3.6		71	275	605	1.042
3.7		72	279	614	1 057
3.8		73	282	622	1 071
3.9		74	286	630	1 085
4 0		75	290	638	1 000
4.0	30	76	203	646	1,055
T. 1 A 2	. 50	76	295	654	1,112
4.2		70	297	661	1,120
4.5 A A		78	304	660	1 152
4.4 A C		70	207	677	1, 102
4.J		80	211	694	1,100
4.0		81	214	602	1,170
4.7 A Q		82	217	600	1,191
4.0		02	217	099	1,203
4.9		03	321	710	1,210
5.0		03	324	713	1,220
5.1		04	327	720	1, 240
5.2		60 00	330	121	1,253
5.3	40	00	333	734	1.205
5.4	. 40	87	335	/41	1,276
ნ. ნ		87	340	/48	1,288
5.6		88	343	755	1,300
5.7		89	346	762	1, 311
5.8		90	349	768	1, 323
5.9		91	352	775	1, 334
6.0		91	355	781	1, 345
6.1		92	358	788	1,357
6.2		93	361	794	1,368
6.3		94	363	801	1,379

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b. 4			94	366	807	1,390	3, 154
6.5			95	369	813	1,400	3, 178
6.6			96	372	819	1, 411	3, 202
67			07	375	826	1 422	3 227
6 0	50		07	070	020	1 400	0,227
0.0	. 50		97	310	032	1,432	3,201
6.9		. 25	98	380	838	1, 443	3,274
7.0			99	383	844	1, 453	3, 298
7.1			QQ	386	850	1 464	3.322
7 2			100	280	956	1 474	2 245
7.2			100	309	000	1,414	3,343
1.3			101	391	862	1,484	3,368
7.4			101	394	868	1, 494	3, 391
7.5			102	397	874	1, 504	3, 414
7.6			103	300	879	1 514	3 437
			100	402	005	1 604	2 450
1.1			103	402	000	1, 524	3,439
7.8			104	404	891	1, 534	3, 481
7.9			105	407	897	1, 544	3, 504
8.0			105	410	902	1.554	3, 526
8 1			106	A12	009	1 562	2 549
0.1	~~		100	412	900	1,000	3, 340
8.2	.60		107	415	913	1,5/3	3,570
8.3			107	417	9 19	1, 582	3, 591
8.4			108	420	Q24	1 592	3 613
8 5			100	422	020	1 601	2,674
0.0			109	422	930	1,001	3,034
8.6			109	425	935	1,611	3,656
8.7			110	427	941	1,620	3,677
8.8			111	430	946	1,629	3, 698
8 0			111	422	052	1 620	2 710
0.5			110	404	902	1,009	0,719
9.0			112	434	957	1,048	3, 140
9.1			112	437	962	1,657	3, 760
9.2			113	439	968	1,666	3, 781
03			114	442	073	1 675	3 802
5.0			114	444	970	1,070	0,002
9.4			114	444	9/8	1,004	3,822
9.5	. 70		115	446	98 3	1,693	3, 842
9.6			116	449	988	1,702	3, 862
97			116	451	003	1 711	3 882
0.0			110	450	330	1 700	0,002
9.0			117	453	222	1, 720	3, 902
9.9			117	456	1,004	1,728	3, 922
10.0			118	458	1,009	1,737	3, 942
10.5			121	460	1 034	1 780	4 039
11 0	01		104	490	1 059	1 900	A 10A
	.01		124	400	1,000	1,022	4,134
11.5			126	491	1,082	1,863	4, 221
12.0			129	502	1, 105	1,903	4, 318
12.5			132	512	1, 128	1, 942	4, 407
13 0			134	522	1 150	1 080	4 405
10.0	00	40	107	502	1,100	2 010	4 590
13.5	. 99	. 49	137	532	1, 172	2,010	4, 500
14.0			140	542	1, 194	2,055	4,664
14.5			142	551	1,215	2,092	4, 747
15.0	1, 10		144	561	1 235	2 127	4,828
15 5			147	570	1 256	2 162	4 008
10.0			147	570	1,230	2,103	4, 300
10. U			149	5/9	1,210	Z, 197	4,900
16.5	1.21		151	588	1,296	2,231	5,064
17.0	1.25		154	597	1, 315	2, 265	5, 140
17 5	1 20		156	606	1 334	2 208	5 215
10.0	1.23		150	000	1,004	2,290	5,210
10.0	1.32		120	014	1, 333	2, 330	5, 209
18.5	1.36		160	623	1, 372	2, 363	5, 362
19.0	1.40		163	631	1,390	2, 394	5, 434
19.5	1 43		165	630	1 400	2 426	5 505
20.0	1 47		167	649	1 427	2 457	5 575
20.0	1.47		107	040	1,427	2,407	5,575
20.5	1.51		169	656	1, 444	2,487	5, 644
21.0	1.55	. 76	171	664	1, 462	2, 517	5,713
21.5	1.58		173	671	1, 479	2,547	5, 780
22 0	1 62		175	670	1 406	2 576	5 847
22.U	1.02		170	019	1,430		
22.5	1.00		1//	DQ /	1,513	2, DUD	5,913
23.0	1.69		179	694	1, 530	2,634	5,978
23.5	1.73		181	702	1, 546	2,663	6,043
24.0	1 77		183	700	1 563	2.691	6 107
24 5	1 20		100	717	1 570	2 710	6 170
24.0	1.00		601	717	1, 3/9	2,719	0,170
25. U	1.84		180	724	1, 595	/ Z. /4b	0,233
25.5	1.88		188	731	1,611	2,774	6, 295
26.0	1.91		190	738	1,626	2,801	6, 356

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$\begin{array}{c} 26.5\\ 27.0\\ 27.5\\ 28.0\\ 28.5\\ 29.0\\ 29.5\\ 30.0\\ 30.5\\ 31.0\\ 31.5\\ 32.0\\ 32.5\\ 33.0\\ \end{array}$	1.95 1.99 2.02 2.06 2.10 2.13 2.17 2.21 2.24 2.28 2.32 2.35 2.39 2.43	. 99	192 194 196 197 201 203 204 206 208 209 211 213 214	745 752 759 766 773 780 786 793 800 806 813 819 825 832	1, 642 1, 657 1, 673 1, 688 1, 703 1, 718 1, 733 1, 747 1, 762 1, 776 1, 790 1, 804 1, 818 1, 832	2, 828 2, 854 2, 881 2, 907 2, 932 2, 958 2, 983 3, 009 3, 034 3, 058 3, 083 3, 107 3, 131 3, 155	6, 417 6, 537 6, 596 6, 655 6, 713 6, 771 6, 828 6, 884 6, 941 6, 996 7, 052 7, 107 7, 161
33.5 34.0 34.5 35.0 35.5 36.0 36.5 37.0 37.5 38.0 38.5 39.0 39.5	2.47 2.50 2.54 2.61 2.65 2.69 2.72 2.76 2.80 2.83 2.87 2.91	1.25	216 217 219 221 222 224 225 227 228 230 231 233 234	838 844 850 857 863 869 875 881 887 893 893 898 904 910	1, 846 1, 860 1, 874 1, 887 1, 901 1, 914 1, 927 1, 940 1, 953 1, 966 1, 979 1, 992 2, 005	3, 179 3, 203 3, 226 3, 250 3, 273 3, 296 3, 319 3, 341 3, 364 3, 386 3, 408 3, 430 3, 452	7, 215 7, 269 7, 322 7, 375 7, 427 7, 479 7, 531 7, 583 7, 634 7, 684 7, 735 7, 785 7, 785 7, 835
40.0 *40.8 43.5 46.2 48.9 51.6 57.4 57.1 59.8	2.94 3.00 3.20 3.40 3.60 3.80 4.00 4.20 4.40	1.47 1.96	236 238 246 253 261 268 275 282 288	916 924 955 984 1,013 1,040 1,068 1,094 1,120	2,017 2,037 2,104 2,168 2,231 2,292 2,352 2,410 2,467	3, 474 3, 507 3, 622 3, 734 3, 842 3, 947 4, 050 4, 150 4, 248	7,884 7,960 8,221 8,474 8,719 8,958 9,191 9,418 9,639
62.5 65.2 68.0 70.7 73.4 76.1 78.8 81.5	4.60 4.80 5.00 5.20 5.40 5.60 5.80 6.00 6.50 7.00	2.26 2.35 2.45 2.55 2.65 2.75 2.84 2.94 3.19 3.43	295 301 307 313 319 325 331 337 350 364	1, 145 1, 169 1, 194 1, 217 1, 240 1, 263 1, 263 1, 285 1, 307 1, 361 1, 412	2, 522 2, 576 2, 629 2, 681 2, 733 2, 783 2, 783 2, 832 2, 880 2, 998 3, 111	4, 343 4, 436 4, 528 4, 618 4, 706 4, 792 4, 877 4, 960 5, 163 5, 357	9, 856 10, 068 10, 276 10, 479 10, 679 10, 875 11, 067 11, 256 11, 716 12, 158
	7.50 8.00 8.50 9.00 9.50 10.00 10.50 11.00 11.50 12.00 12.50	3.68 3.92 4.17 4.41 4.66 4.91 5.15 5.40 5.64 5.89 6.13	376 389 401 412 424 435 445 456 466 476 486	1, 462 1, 510 1, 556 1, 601 1, 645 1, 688 1, 730 1, 770 1, 810 1, 849 1, 887	3, 220 3, 326 3, 428 3, 528 3, 624 3, 719 3, 810 3, 900 3, 988 4, 073 4, 157	5, 546 5, 727 5, 904 6, 075 6, 241 6, 403 6, 562 6, 716 6, 867 7, 015 7, 159	12, 585 12, 998 13, 398 13, 786 14, 164 14, 532 14, 891 15, 241 15, 584 15, 919 16, 247
	13.00 13.50 14.00 14.50 15.00 15.50 16.00 16.50 17.00 17.50 18.00 18.50	6.38 6.62 6.87 7.11 7.36 7.60 7.85 8.09 8.34 8.58 8.83 9.07	496 505 514 523 532 541 550 558 567 575 583 591	1, 924 1, 961 1, 997 2, 032 2, 067 2, 101 2, 135 2, 168 2, 201 2, 233 2, 265 2, 296	4, 240 4, 321 4, 400 4, 478 4, 554 4, 630 4, 704 4, 777 4, 848 4, 919 4, 989 5, 058	7, 301 7, 440 7, 577 7, 711 7, 843 7, 972 8, 100 8, 225 8, 349 8, 349 8, 471 8, 591 8, 710	16, 569 16, 885 17, 195 17, 499 17, 798 18, 092 18, 382 18, 667 18, 947 19, 224 19, 497 19, 766

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19.00	9, 32	599	2,327	5, 126	8,827	20, 031
10 50	0 56	607	2 257	5 102	8 042	20 203
20 00	0.01	615	2,007	5,155	0,942	20, 250 00 EE1
20.00	9.01	015	2,301	5,239	9,000	20, 551
20.50	10.06	622	2,41/	5, 324	9, 168	20,807
21.00	10.30	630	2, 446	5, 389	9, 279	21,059
21.50	10.55	637	2, 475	5, 452	9, 389	21, 308
22.00	10.79	645	2,504	5, 516	9, 498	21, 555
22,50	11.04	652	2, 532	5, 578	9,605	21,798
23 00	11 28	650	2 560	5 630	0 711	22 030
20.00	11 50	666	2,000	5,003	0.916	22,000
23.00	11.00	670	2,307	5,700	9,010	22,211
24.00	11.77	0/3	2,015	5, 701	9,920	22, 513
24.50	12.02	680	2,642	5,820	10, 023	22, 745
25.00	12.26	687	2,669	5, 880	10, 125	22, 977
25.50	12.51	694	2,695	5, 938	10, 225	23, 206
26.00	12.75	701	2,722	5, 996	10, 325	23, 432
26.50	13,00	708	2 748	6 053	10 424	23,656
27 00	13 24	714	2,110	6 110	10 522	23,870
27.00	10.24	701	2,773	6 167	10,522	24,000
27.00	10.49	721	2,199	U , 107	10,019	24,099
20.00	13.73	121	2,024	0, 222	10,715	24, 317
28.50	13.98	734	2,849	D, 278	10,810	24, 533
29.00	14.22	/40	2,8/4	6, 332	10, 905	24, 141
29.50	14.47	747	2, 899	6, 387	10, 998	24, 9 60
30.00	14.72	753	2, 924	6, 441	11,091	25, 170
* 30.58	15.00	760	2,950	6, 500	11, 193	25, 401
32.62	16.00	785	3,047	6,713	11, 560	26, 234
34.66	17.00	809	3, 141	6,919	11, 915	27,041
36.70	18,00	832	3,232	7, 120	12, 261	27,825
38 74	19 00	855	3,320	7 315	12 597	28 587
40 77	20 00	877	2 407	7 505	12,007	20,330
40.77	20.00	900	2 401	7,505	12, 324	29,000
42.01	21.00	033	0,491	7,091	10,240	30,034
44.00	22.00	920	3, 5/3	1,012	13, 333	30, 102
40.89	23.00	941	3, 553	8,048	13,860	31,453
48.93	24.00	961	3, 732	8, 222	14, 158	32, 130
50.97	25.00	981	3, 809	8, 391	14, 450	32, 792
53.01	26.00	1,000	3, 884	8, 557	1 4, 73 6	33, 441
55.04	27.00	1,019	3, 958	8,720	15, 016	34, 079
57.08	28.00	1,038	4, 031	8, 8 80	15, 292	34, 704
59.12	29.00	1,057	4, 102	9,037	15, 563	35, 318
61, 16	30,00	1,075	4, 172	9, 192	15, 829	35, 922
63.20	31 00	1 092	4 241	9 344	16 090	36, 516
65 24	32 00	1 110	4 309	0 403	16 348	37 100
00.24	22.00	1,110	4,003	0 6/1	16,601	27 675
	24 00	1, 127 1 1AA	T, 310	0 706	16 951	20,010
	34.00	1,144	4,442	9, 700	10,001	30, 242
	35.00	1, 101	4,50/	9, 928	17,097	30, 800
	36.00	1, 1//	4,571	10,069	17,339	39,351
	37.00	1, 193	4,634	10,208	17, 579	39, 893
	38.00	1,209	4,696	10, 345	17,815	40, 429
	39.00	1, 225	4, 757	10 , 4 80	18, 048	40, 957

2

	A	В	С	D	E	F
1	PITOT TU	BE IMPACT	PRESSURE	FLOW	NIPPLE	INSIDE
2	TNCHES	INCHES	LBS. PER	l" nominal	2 ¹¹ nominal	3" nominal
	Indiado	1.0.20		1 Homender	2 nominut	5 Homender
3	WATER	MERCURY	SO. IN.	actual dia.	actual dia.	actual dia.
4	<u> </u>	l				
5		l		1.049	2 067	3.068
6				1.04)	2.007	5.000
7	1			(111*05*2*(*	(1)1*5572*(4	(11)*F5*2*(4
ľ	• •			$(211^{\circ}D)^{\circ} 2^{\circ}(R)^{\circ}$	(B11°E) 2°(R	(1112) 2.0(R)
				/15 025)=	// •)/•(14•/	/15 025)-
				12	/15•025)	101
0		l		12	40 (111*E5*2*(A	101
°	A/+•1-			$(L11^{+}D)^{-}2^{+}(A)^{+}$	$(L11^{-1}L)^{-2}(A)^{-2}$	$(L11^{+}r) 2^{+}(R)$
	• 2			/15 025)-	(15, 025) -	0/ 0/ 1/140/
				17	/1J•02J)- 45	1/2
0	A 9+ 1-			1/ /111+D5^2+(A	03	143 (111+F5^2+(A
2	2			$(L11^{+})^{-} 2^{+}(R)$	$(LII^{+}EJ^{-}Z^{+}(R)$	$(LII^{+}J) 2^{+}(A)$
	• 5			/15 025)-	/15 025)-	/15 025)-
				/15.025)=	713.023)=	175
		L	<u> </u>	20	/9	1/5
10	A9+.1=			(LII*D5-2*(A	(L11*E5*2*(A	(L11*F5*2*(A
	• 4			$10)^{10}.5)*(14.$	$10)^{-5}$, $5)*(14.)$	$10)^{-5}$, $5)*(14$.
				//15.025)=	//15.025)=	//15.025)=
		<u> </u>		24	92	202
11	A10+.1=			(LII*D5*2*(A	(LII*E5~2*(A	(LII*F5~2*(A
	•2			$(11)^{-1} \cdot 5)^{*} (14 \cdot 1)^{-1} \cdot 5)^{*} (14 \cdot 1)^{-1} \cdot 10^{-1} \cdot 10^{-1$	$(14.)^{-1}$	$(11)^{5} \times (14)^{5}$
				//15.025)=	//15.025)=	//15.025)=
		1			102	226
12	A11+.1=			(LIIADS 2*(A	(LI1*E5'2*(A	
	•0			$(12)^{(1)} \cdot 5)^{(14)}$	12)**•5)*(14•	$(12)^{-1} \cdot 5)^{*} (14 \cdot 12)^{-1} \cdot 5)^{*} (14 \cdot 12)^{-1} \cdot 5)^{*} (14 \cdot 12)^{-1} \cdot 12$
				//15.025)=	//15.025)=	//15.025)=
		1		29		247
13	A12+•1=			(LII*D)~2*(A	(LII*E5"2*(A	(LII*F5*2*(A
	•/			13)**•5)*(14•	$13)^{5} (14.$	13)~.5)*(14.
1				(/15.025)=	//15.025)=	(//15.025)=
		ļ		31	121	267
14	A13+.1=			(L11*D5*2*(A	(L11*E5*2*(A	(LI1*F5*2*(A
1	8.	1		14)"•>)*(14•	14)".)*(14.	14)~.5)*(14.
1				//10.025)=	//13.025)=	//13.025)=
1.5	L	 				285
115	A14+.1=	1			LLITES	(LII*F5"2*(A
	• 9	1		15)"•5)*(14•	15) .5)*(14.	1)/~•)*(14.
				//15.025)=	(/15.025)=	//15.025)=
	L	<u> </u>		35	137	303
16	A15+.1=			[(L11*D5*2*(A	(L11*E5*2*(A	(L11*F5 ² *(A
	1.0			16)~.5)*(14.	16)".5)*(14.	16)~.5)*(14.
	ł			//15.025)=	//15.025)=	//15.025)=
L		ļ		37	145	319
17	A16+.1=			(L11*D5^2*(A	(L11*E5 ² *(A	(L11*F5^2*(A
	1.1			17)^.5)*(14.	17)^.5)*(14.	17)^.5)*(14.
				7/15.025)=	//15.025)=	7/15.025)=
·				39	152	335

	A	В	С	D	E	F
18	A17+.1=			(L11*D5^2*(A	(L11*E5^2*(A	(L11*F5^2*(A
	1.2			18)^.5)*(14.	18)^.5)*(14.	18)^.5)*(14.
				7/15.025) =	7/15.025)=	7/15.025)=
				41	159	349
19	A18+.1=			(L11*D5^2*(A	(L11*E5^2*(A	(L11*F5^2*(A
	1.3			19)^.5)*(14.	19)^.5)*(14.	19)^.5)*(14.
				7/15.025) =	7/15.025)=	7/15.025)=
				43	165	364
20	A19+.1=	· · · · · · · · · · · · · · · · · · ·		(L11*D5^2*(A	(L11*E5^2*(A	(L11*F5^2*(A
	1.4			20)^.5)*(14.	20)^.5)*(14.	20)^.5)*(14.
				7/15.025)=	7/15.025)=	7/15.025)=
				44	171	377
21	A20+.1=			(L11*D5^2*(A	(L11*E5^2*(A	(L11*F5^2*(A
	1.5			21)^.5)*(14.	21)^.5)*(14.	21)^.5)*(14.
				7/15.025)=	7/15.025)=	7/15.025)=
				46	177	391
22	A21+.1=			(L11*D5~2*(A	(L11*E5^2*(A	(L11*F5^2*(A
	1.6			22)^.5)*(14.	22)^.5)*(14.	22)^.5)*(14.
				7/15.025)=	7/15.025)=	7/15.025)=
				47	183	403
23	A22+.1=			(L11*D5^2*(A	(L11*E5 ² *(A	(L11*F5 ² *(A
	1.7			23)^.5)*(14.	23)^.5)*(14.	23)^.5)*(14.
				7/15.025)=	7/15.025)=	7/15.025)=
				49	189	416
24	A23+.1=			(L11*D5~2*(A	(L11*E5~2*(A	(L11*F5^2*(A
	1.8			24)^.5)*(14.	24)^.5)*(14.	24)^.5)*(14.
				7/15.025)=	7/15.025)=	7/15.025)=
				50	194	428
25	A24+.1=			(LII*D) 2*(A	(LII*E) 2*(A	(LII*F) Z*(A
	1.9			$25)^{-}.5)^{(14)}$	257.57(14)	$(25) \cdot 5)^{(14)}$
				51	200	//13.025)-
26	2.0	I		(111*D5^2*(A	(111*F5*2*(A	(11)*F5^2*(A
-				$(26)^{-}, 5)*(14)$	$(26)^{,5} \times (14)$	26)^.5)*(14.
				7/15.025)=	7/15.025)=	7/15.025)=
				53	205	451
27	A26+.1=			(L11*D5^2*(A	(L11*E5^2*(A	(L11*F5^2*(A
	2.1			27)^.5)*(14.	27)^.5)*(14.	27)^.5)*(14.
				7/15.025)=	7/15.025)=	7/15.025)=
				54	210	462
28	A27+.1=			(L11*D5^2*(A	(L11*E5^2*(A	(L11*F5^2*(A
	2.2			28)^.5)*(14.	28)^.5)*(14.	28)^.5)*(14.
				7/15.025)=	7/15.025)=	7/15.025)=
				55	215	473
29	A28+.1=			(L11*D5^2*(A	(L11*E5^2*(A	(L11*F5^2*(A
	2.3			29)^.5)*(14.	29)^.5)*(14.	29)^.5)*(14.
				7/15.025)=	//15.025)=	//15.025)=
		<u> </u>			220	484
30	A29+.1=			(LII*D)~2*(A	(LII*E5"2*(A	12010 E1+(1)
	2.4			JUJ • 5 J*(14•	7/15 0251-	$507 \cdot 57^{(14)}$
				[//10.025]= 	//13·025J=	//15.025)=
21	A 30+ 1-		l	<u> </u>	224	474 (T11*05*0*/*
121				(LII-D) 2^(A 31)^ 5)*/14	(1)^.5)*(14	31)^.5)*(14
	2 • 2			7/15.025) =	7/15-025)=	7/15.025) =
				59	229	504

•			<u> </u>			
	<u> </u>	<u> </u>	0			r
32	A31+.1=			(L11*D5 2*(A	(L11*E5 2*(A	(LII*F5-2*(A
	2.6			32)^.5)*(14.	32)^.5)*(14.	32)^.5)*(14.
				7/15.025)=	7/15.025)=	7/15.025)=
				60	233	514
33	A32+.1=	A33/13.59=	· · · · · · · · · · · · · · · · · · ·	(L11*D5^2*(A	(L11*E5 ² *(A	(L11*F5^2*(A
	2.7	.20		33)^.5)*(14.	33)^.5)*(14.	33)^.5)*(14.
				7/15.025)=	7/15.025)=	7/15.025) =
				61	238	524
34	A33+,1=			(1.11*D5^2*(A	(1.11*E5^2*(A	(111*F5^2*(A
	2.8			$(211 \ 5) = (1)$	341 51*(14	$341^{5}5)*(14)$
	2.0				$\frac{1}{15}$	$\frac{1}{2}$
	ł			//13.023)=	//15.025)=	//15.025)=
L		<u> </u>		62	242	534
35	A34+.1=			(L11*D5~2*(A	(L11*E5~2*(A	(L11*F5~2*(A
	2.9			35)^.5)*(14.	35)^.5)*(14.	35)^.5)*(14.
				7/15.025)=	7/15.025)=	7/15.025)=
				64	247	543
36	3.0			(L11*D5^2*(A	(L11*E5 ² *(A	(L11*F5^2*(A
				36)^.5)*(14.	36)^.5)*(14.	36)^.5)*(14.
				7/15.025)=	7/15.025)=	7/15.025)=
				65	251	552
37	A36+.1='	1	· <u> </u>	(L11*D5^2*(A	(L11*E5^2*(A	(L11*F5^2*(A
	3.1			$(37)^{5}(14)$	$(37)^{,5}(14)$	$(37)^{,5}(14)$
	5.1			7/15 025) =	7/15 025) =	7/15 025 =
				//IS•025)=	7715.0257-	F()
-				00	200	502
38	A3/+.1=			(LII*D5 2*(A	(LII*E5°2*(A	(L11*F5*2*(A
	3.2			38)^.5)*(14.	38)~.5)*(14.	38)~.5)*(14.
ł		I		7/15.025)=	7/15.025)=	7/15.025)=
		1		67	259	571
39	A38+.1=			(L11*D5^2*(A	(L11*E5 ² *(A	(L11*F5^2*(A
	3.3			39)^.5)*(14.	39)^.5)*(14.	39)^.5)*(14.
				7/15.025)=	7/15.025)=	7/15.025)=
				68	263	579
40	A39+.1=			(L11*D5^2*(A	(L11*E5^2*(A	(L11*F5^2*(A
	3.4			40)^.5)*(14.	40)^.5)*(14.	40)^.5)*(14.
				7/15.025)=	7/15.025) =	7/15.025) =
				69	267	588
41			·····	(I11*D5*2*(A	(111*F5*2*(A	(T11*E5*2*(A
	2 5			(1)^ 5)+(1)	(LII	(LII - F) 2 - (A
	3.5			41) •3)*(14•	41) •5)~(14•	41) .5)^(14.
				//15.025)=	//15.025)=	//15.025)=
	<u> </u>			70	271	597
42	A41+.1=			(L11*D5~2*(A)	(L11*E5~2*(A	(L11*F5^2*(A
	3.6			42)^.5)*(14.	42)^.5)*(14.	42)^.5)*(14.
				7/15.025)=	7/15.025)=	7/15.025)=
L				71	275	605
43	A42+.1=			(L11*D5^2*(A	(L11*E5 ^ 2*(A	(L11*F5^2*(A
	3.7			43)^.5)*(14.	43)^.5)*(14.	43)^.5)*(14.
				7/15.025)=	7/15.025)=	7/15.025)=
				72	279	614
44	A43+.1=			(L11*D5^2*(A	(L11*E5^2*(A	(L11*F5^2*(A
	3.8			44)^.5)*(14.	44)^.5)*(14.	44)^.5)*(14.
1				7/15.025)=	7/15.025)=	7/15.025)=
				73	282	622
45	A44+.1=	<u> </u>	<u> </u>	(L11*D5^2*(A	(1.11*F5^2*/A	(1.11*F5^2*(A
	3 0			45)^.5)*(1/	45) ~ 5) */14	(5) 5)*(1/
	5.7			7/15 0251-	7/15 0951-	7/15 0251-
				(/13·025)= 7/	//ID•U2DJ=	(20
1	1	1		/4	280	020

1						,
	A	В	<u>C</u>	D	E	F
46	4.0			(L11*D5^2*(A	(L11*E5 ² *(A	(L11*F5 ² *(A
				46)^.5)*(14.	46)^.5)*(14.	46)^.5)*(14.
				7/15.025)=	7/15.025)=	7/15.025)=
				75	290	638
47	A46+.1=	A47/13.59=	· · · · · ·	(L11*D5^2*(A	(L11*E5 ² *(A	(L11*F5^2*(A
]	4.1	.30		47)^.5)*(14.	47)^.5)*(14.	47)^.5)*(14.
				7/15.025)=	7/15.025)=	7/15.025)=
				76	293	646
48	A47+.1=			(L11*D5^2*(A	(L11*E5^2*(A	(L11*F5 ² *(A
	4.2			48)^.5)*(14.	48)^.5)*(14.	48)^.5)*(14.
				7/15.025)=	7/15.025)=	7/15.025)=
				76	297	654
49	A48+.1=			(L11*D5^2*(A	(L11*E5 ² *(A	(L11*F5 ² *(A
	4.3			49)^.5)*(14.	49)^.5)*(14.	49)^.5)*(14.
				7/15.025)=	7/15.025)=	7/15.025) =
				77	300	661
50	A49+.1=		<u> </u>	(111*D5^2*(A	(T11*F5^2*(A	(111*F5 ² *(A
	4.4			$(217 \ b) 2 \ (R \ 50)^{2} \ 5) (14)$	(011 0) 2 (A)	50) [•] 5)*(14
	'''			7/15.025) =	7/15.025	7/15.025) =
				78	304	669
51	450+.1=			(111*D5^2*(A	(111*F5*2*(A	(111*F5*2*(A
	4 5			$(L11 \ D) \ 2^{-1}(A \ 51)^{-1} \ 5) \times (16)$	(LII L) 2 (A	51)^ 5)*(14
	4.5			7/15 025) =	7/15 025) =	7/15 (025) -
				70	207	677
52	 ∧51± 1=			/7 (T11*D5*2*/A		(111*5^2*()
52	AJ1+•1-			(LII*D) 2*(A	(LII*E) 2*(A	52) ~ 5) + (16
	4.0			52 - 5 - 14	$\frac{52}{16} \cdot \frac{5}{16} \cdot \frac{5}{14} \cdot \frac{5}{16} \cdot \frac{5}{16}$	$\frac{32}{15}$
				//15.025)=	//15.025)=	//15.025)=
50					311	084
53	AJ2+.1=			(LII*D) 2*(A	(LII*E) 2*(A	(LIIAFO 24(A
İ	4./			$(53) \cdot 5)^{*}(14)$	$(33) \cdot 5)^{*}(14)$	53) •5)*(14•
				//15.025)=	(//15.025)=	//15.025)=
51	4521 1-		[314	092
54	AJ J+.1=			(L11^D) 2^(A	(LII^E) 2^(A	(LIIAF5 24(A
	4.0			(14)	$(34) \cdot (3)^{(14)}$	54) •5)*(14•
				(//15.025)=	//15.025)=	//15.025)=
			<u> </u>	82	31/	699
222	A54+.1=			(L11*D5 2*(A	(LII*E) 2*(A	(LII*F) 2*(A
	4.9			55)*•5)*(14.	55) •5)*(14.	55)*.5)*(14.
				//15.025)=	//15.025)=	//15.025)=
				83	321	706
56	A55+.1=			(L11*D5~2*(A	(L11*E5~2*(A	(L11*F5~2*(A
	5.0			56)~.5)*(14.	56)~.5)*(14.	56)*.5)*(14.
				7/15.025)=	7/15.025)=	7/15.025)=
				83	324	713
57	A56+.1=			(L11*D5~2*(A	(L11*E5~2*(A	(L11*F5~2*(A
	5.1			57)~.5)*(14.	57)~.5)*(14.	57)^.5)*(14.
				7/15.025)=	7/15.025)=	7/15.025)=
				84	327	720
58	A57+.1=			(L11*D5^2*(A	(L11*E5^2*(A	(L11*F5^2*(A
	5.2			58)^.5)*(14.	58)^.5)*(14.	58)^.5)*(14.
			l	7/15.025)=	7/15.025)=	7/15.025)=
			l	85	330	727
59	A58+.1=			(L11*D5 ² *(A	(L11*E5 ² *(A	(L11*F5^2*(A
	5.3			59)^.5)*(14.	59)^.5)*(14.	59)^.5)*(14.
				7/15.025)=	7/15.025)=	7/15.025)=
				86	333	734

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	A	R R			E	
60						F
00	AJ9+.1-	A00/13.39=			(LII*E) 2*(A	(LII*F) 2*(A
	5.4	•40		00) .5)*(14.	60) •5)*(14•	(14.
				//15.025)=	//15.025)=	//15.025)=
				87	336	741
61	A60+.1=			(L11*D5~2*(A	(L11*E5 ² *(A	(L11*F5 ² *(A
	5.5			61)^.5)*(14.	61)^.5)*(14.	61)^.5)*(14.
				7/15.025)=	7/15.025)=	7/15.025)=
				87	340	748
62	A61+.1=			(L11*D5^2*(A	(L11*E5^2*(A	(L11*F5 ² *(A
	5.6			62)^.5)*(14.	62)^.5)*(14.	62)^.5)*(14.
				7/15.025)=	7/15.025)=	7/15.025)=
L				88	343	755
63	A62+.1=			(L11*D5 ² *(A	(L11*E5^2*(A	(L11*F5^2*(A
	5.7			63)^.5)*(14.	63)^.5)*(14.	63)^.5)*(14.
				7/15.025)=	7/15.025)=	7/15.025)=
				89	346	762
64	A63+.1=			(L11*D5^2*(A	(L11*E5 ² *(A	(L11*F5 ² *(A
1	5.8		1	64)^.5)*(14.	64)^.5)*(14.	64)^.5)*(14.
				7/15.025)=	7/15.025)=	7/15.025)=
				90	349	768
65	A64+.1=			(L11*D5^2*(A	(L11*E5 ² *(A	(L11*F5^2*(A
	5.9			65)^.5)*(14.	65)^.5)*(14.	65)^.5)*(14.
				7/15.025)=	7/15.025)=	7/15.025)=
				91	352	775
66	A65+.1=			(L11*D5^2*(A	(L11*E5 ² *(A	(L11*F5 ² *(A
	6.0			66)^.5)*(14.	66)^.5)*(14.	66)^.5)*(14.
				7/15.025)=	7/15.025)=	7/15.025)=
				51	355	781
67	A66+.1=			(L11*D5^2*(A	(L11*E5^2*(A	(L11*F5 ² *(A
	6.1			67)^.5)*(14.	67)^.5)*(14.	67)^.5)*(14.
				7/15.025)=	7/15.025)=	7/15.025)=
				92	358	788
68	A67+.1=			(L11*D5 ² *(A	(L11*E5 ² *(A	(L11*F5^2*(A
	6.2			68)^.5)*(14.	68)^.5)*(14.	68)^.5)*(14.
				7/15.025)=	7/15.025)=	7/15.025)=
				93	361	794
69	A68+.1=			(L11*D5^2*(A	(L11*E5^2*(A	(L11*F5^2*(A
	6.3			69)^.5)*(14.	69)^.5)*(14.	69)^.5)*(14.
				7/15.025)=	7/15.025)=	7/15.025)=
				94	363	801
70	A69+.1=			(L11*D5^2*(A	(L11*E5^2*(A	(L11*F5^2*(A
1	6.4			70)^.5)*(14.	70)^.5)*(14.	70)^.5)*(14.
				7/15.025)=	7/15.025)=	7/15.025)=
L				94	366	807
71	A70+.1=			(L11*D5^2*(A	(L11*E5 ² *(A	(L11*F5 ^ 2*(A
	6.5			71)^.5)*(14.	71)^.5)*(14.	71)^.5)*(14.
				7/15.025)=	7/15.025)=	7/15.025)=
				95	369	813
72	A71+.1=			(L11*D5 ² *(A	(L11*E5^2*(A	(L11*F5 ² *(A
	6.6			72)^.5)*(14.	72)^.5)*(14.	72)^.5)*(14.
				7/15.025)=	7/15.025)=	7/15.025)=
	1			96	372	819
73	A72+.1=			(L11*D5^2*(A	(L11*E5^2*(A	(L11*F5 ² *(A
	6.7			73)^.5)*(14.	73)^.5)*(14.	73)^.5)*(14.
1				7/15.025)=	7/15.025)=	7/15.025)=
				97	375	826

	·					
	A	В	С	D	E .	F
74	A73+.1=	A74/13.59=		(L11*D5 ^ 2*(A	(L11*E5 ² *(A	(L11*F5^2*(A
	6.8	.50		74)^.5)*(14.	74)^.5)*(14.	74)^.5)*(14.
				7/15.025)=	7/15.025)=	7/15.025)=
				97	378	832
75	A74+, 1=	· · · · · · · · · · · · · · · · · · ·	T112*475=	(T11*D5*2*(A	(T11*E5*2*(A	(111*F5^2*(A
	6.9		25	(511 5) 2 (A	(BII B) 2 (A	751 51+(1)
	0.9		•25	7.5) •5)"(14•	$7 J J \cdot J = 0.05$	7 / 15 0 25 \-
				//15.025)=	//15.025)=	//15.025)=
			1	98	380	838
76	A75+.1=			(L11*D5~2*(A	(L11*E5~2*(A	(L11*F5~2*(A
	7.0			76)^.5)*(14.	76)^.5)*(14.	76)^.5)*(14.
				7/15.025) =	7/15.025)=	7/15.025)=
				99	383	844
77	A76+.1=	1		(L11*D5^2*(A	(L11*E5 ² *(A	(L11*F5 ² *(A
	7.1			77)^.5)*(14.	77)^.5)*(14.	77)^.5)*(14.
				7/15.025)=	7/15.025)=	7/15.025)=
				99	386	850
78	A77+.1=	1		(L11*D5^2*(A	(L11*E5^2*(A	(L11*F5^2*(A
1	7.2			78)^.5)*(14-	78)^.5)*(14.	78)^.5)*(14.
ļ				7/15.025) =	7/15.025) =	7/15.025) =
				100	380	856
70	A79+ 1-		<u> </u>	100	J07	(111+1:5-2)+(A
/ 3	A/0+.1-				(L11~E) 2~(A)	(LIIAF) 24(A
	1.5			79) .5)*(14.	79) .5)*(14.	79) .5)*(14.
				//15.025)=	7/15.025)=	7/15.025)=
		<u></u>	<u> </u>	101	391	862
80	A/9+.1=			(L11*D5~2*(A	(L11*E5 ² *(A	(L11*F5^2*(A
	7.4	1		80)^.5)*(14.	80)^.5)*(14.	80)^.5)*(14.
				7/15.025)=	7/15.025)=	7/15.025)=
					394	868
81	A80+.1=			(L11*D5^2*(A	(L11*E5 ² *(A	(L11*F5 ² *(A
	7.5			81)^.5)*(14.	81)^.5)*(14.	81)^.5)*(14.
				7/15.025)=	7/15.025)=	7/15.025)=
				102	397	874
82	A81+.1=			(L11*D5^2*(A	(L11*E5^2*(A	(L11*F5^2*(A
	7.6			82)^.5)*(14.	82)^.5)*(14.	82)^.5)*(14.
				7/15.025) =	7/15.025) =	7/15.025) =
				103	399	879
83	L 482+.1=	 		(T11*D5*2*(A	(T)1*F5*2*(A	(111*F5*2*(A
0.5	7 7			(DI1*D) 2*(A	(L11°L) 2°(A	(LII''F) 2"(A
				7/15 025	7/15 025)-	$(3) \cdot (14)$
				102	//13.025)=	//15.025)=
				103	402	638
84	A83+.1=			(L11*D5~2*(A	(L11*E5*2*(A	(LII*F5*2*(A
	/.8			84)~.5)*(14.	84)~.5)*(14.	84)~.5)*(14.
				7/15.025)=	7/15.025)=	7/15.025)=
				104	404	891
85	A84+.1=			(L11*D5^2*(A	(L11*E5^2*(A	(L11*F5 ² *(A
	7.9			85)^.5)*(14.	85)^.5)*(14.	85)^.5)*(14.
				7/15.025)=	7/15.025)=	7/15.025)=
		1		105	407	897
86	A85+.1=		1	(L11*D5^2*(A	(L11*E5^2*(A	(L11*F5^2*(A
	8.0			86)^.5)*(14.	86)^.5)*(14.	86)^.5)*(14.
				7/15.025)=	7/15.025)=	7/15.025)=
]			105	410	902
87	A86+,1=	<u> </u>	······	(1.11*D5^2*(4	(1)1*E5^2*(A	(1.11*F5^2*(A
· ·	<u>R</u> 1	1		87) 5)*/14	87) 5)*(14	87) 5)*(14
	U•1	1		7/15 0251-	7/15 0251-	7/15 0251-
			1		(11).02)=	000
1	I	1	1	1 100	I 41Z	1 908

		· · · · · · · · · · · · · · · · · · ·		· · · · · · · · · · · · · · · · · · ·	1	· · · · · · · · · · · · · · · · · · ·
·	A	В	С	D	E	F
88	A87+.1=	A88/13.59=		(L11*D5^2*(A	(L11*E5 ² *(A	(L11*F5 ² *(A
	8.2	.60		88)^.5)*(14.	88)^.5)*(14.	88)^.5)*(14.
				7/15.025)=	7/15.025)=	7/15.025)=
				107	415	913
89	A88+.1=			(L11*D5^2*(A	(L11*E5^2*(A	(L11*F5^2*(A
	8.3			89)^.5)*(14.	89)^.5)*(14.	89)^.5)*(14.
				7/15.025)=	7/15.025) =	7/15.025) =
				107	417	919
90	A89+,1=	l		(I.11*D5^2*(A	(111*E5*2*(A	(T11*F5*2*(A
	8.4			90) [•] 5)*(14	00)^ 5)+(14	Q01^ 5)+(14
	0.7			7/15 025)-	7(15,025)	$\frac{1}{2}$
				//15.025)=	//15.025)=	//15.025)=
				108	420	924
91	A90+.1=			(LI1*D5*2*(A	(LI1*E5*2*(A	(L11*F5~2*(A
	8.5			91)~.5)*(14.	91)~.5)*(14.	91)^.5)*(14.
				7/15.025)=	7/15.025)=	7/15.025)=
				109	422	93 0
92	A91+.1=			(L11*D5^2*(A	(L11*E5^2*(A	(L11*F5 ² *(A
	8.6			92)^.5)*(14.	92)^.5)*(14.	92)^.5)*(14.
				7/15.025)=	7/15.025)=	7/15.025)=
				109	425	935
93	A92+.1=			(L11*D5^2*(A	(L11*E5^2*(A	(L11*F5^2*(A
	8.7			93)^.5)*(14.	93)^.5)*(14.	93)^.5)*(14.
				7/15.025)=	7/15.025)=	7/15.025)=
				110	427	941
94	A93+.1=			(L11*D5^2*(A	(L11*E5^2*(A	(L11*F5^2*(A
	8.8			94)^.5)*(14.	94)^.5)*(14.	94)^.5)*(14.
				7/15.025)=	7/15.025)=	7/15.025) =
			•	111	430	340
95	A94+.1=			(L)1*D5^2*(A	(1.11*E5^2*(A	(1.11*F5^2*(A
	8.9			95)^.5)*(14.	95)^.5)*(14.	95)^.5)*(14.
				7/15.025) =	7/15.025)=	7/15 025) =
				111	//15.025)=	052
96	A95+.1=			(111*D5^2*(A	(111*F5*2*()	/I11*F5^2*(A
	9.0			(211 0) 2 (1)	(D11 D) 2 (R)	(LII) 2"(R
	3.0			7/15 025) -	7/15 025) -	$\frac{90}{15}$ $\frac{30}{14}$
				//13.023)=	//15.025)=	//15.025)=
					434	957
97	A90+.1=			(L11*D5 2*(A	(LII*E5'2*(A	(L11*F5*2*(A
	9.1			9/)~.5)*(14.	9/)~.5)*(14.	97)~.5)*(14.
				7/15.025)=	7/15.025)=	7/15.025)=
				112	437	962
98	A97+.1=			(L11*D5~2*(A	(L11*E5 ² *(A	(L11*F5 ² *(A
	9.2			98)~.5)*(14.	98)^.5)*(14.	98)^.5)*(14.
				7/15.025)=	7/15.025)=	7/15.025)=
				113	439	9 68
99	A98+.1=			(L11*D5^2*(A	(L11*E5 ² *(A	(L11*F5 ² *(A
	9.3			99)^.5)*(14.	99)^.5)*(14.	99)^.5)*(14.
				7/15.025)=	7/15.025)=	7/15.025)=
				114	442	973
100	A99+.1=			(L11*D5^2*(A	(L11*E5 ² *(A	(L11*F5^2*(A
	9.4			100)^.5)*(14	100)^.5)*(14	100)^.5)*(14
				.7/15.025)=	.7/15.025)=	.7/15.025)=
				114	444	978
101	A100+.1=	A101/13.59=		(L11*D5^2*(A	(L11*E5^2*(A	(L11*F5^2*(A
-	9.5	.70		101)^.5)*(14	101)^.5)*(14	101)^.5)*(14
]				.7/15.025)=	•7/15.025)=	.7/15.025)=
				115	446	983
	A	1				

	A	В	С	D	E	F
102	A101+.1=			(L11*D5^2*(A	(L11*E5^2*(A	(L11*F5^2*(A
	9.6			102)^.5)*(14	102)^.5)*(14	102)^.5)*(14
				.7/15.025) =	.7/15.025) =	.7/15.025) =
				116	449	988
103	A102+.1=			(L11*D5^2*(A	(L11*E5^2*(A	(L11*F5^2*(A
	9.7			103)^.5)*(14	103)^.5)*(14	$(103)^{,5} \times (14)$
				.7/15.025)=	.7/15.025)=	.7/15.025)=
				116	451	993
104	A103+.1=			(L11*D5*2*(A	(L11*E5^2*(A	(L11*F5^2*(A
	9.8			104)^.5)*(14	$104)^{.5} \times (14)$	$104)^{,5)*(14)}$
				.7/15.025)=	•7/15•025)=	.7/15.025)=
				117	453	999
105	A104+.1=			(L11*D5^2*(A	(L11*E5*2*(A	(L11*F5^2*(A
	9.9			105)^.5)*(14	105)^.5)*(14	105)^.5)*(14
				.7/15.025)=	.7/15.025)=	.7/15.025)=
				117	456	1.004
106	A105+.1=			(L11*D5^2*(A	(L11*E5^2*(A	(L11*F5*2*(A
	10.0			106)^.5)*(14	106)^.5)*(14	106)^.5)*(14
				.7/15.025)=	.7/15.025)=	.7/15.025)=
				118	458	1.009
107	A106+.5=		1	(L11*D5^2*(A	(L11*E5^2*(A	(L11*F5^2*(A
	10.5			107)^.5)*(14	107)^.5)*(14	107)^.5)*(14
				.7/15.025)=	.7/15.025)=	.7/15.025)=
				121	469	1.034
108	A107+.5=	A108/13.59=		(L11*D5^2*(A	(L11*E5^2*(A	(L11*F5^2*(A
	11.0	.81		108)^.5)*(14	108)^.5)*(14	108)^.5)*(14
				.7/15.025) =	•7/15•025)=	.7/15.025)=
				124	480	1.058
109	A108+.5=	L		(L11*D5^2*(A	(L11*E5*2*(A	(L11*F5*2*(A
	11.5			109)^.5)*(14	109)^.5)*(14	109)^.5)*(14
				.7/15.025)=	.7/15.025)=	.7/15.025)=
				126	491	1,082
110	A109+.5=			(L11*D5^2*(A	(L11*E5^2*(A	(L11*F5^2*(A
	12.0			110)^.5)*(14	110)^.5)*(14	110)^.5)*(14
				.7/15.025)=	.7/15.025)=	.7/15.025)=
				129	502	1,105
111	A110+.5=			(L11*D5^2*(A	(L11*E5^2*(A	(L11*F5^2*(A
	12.5			111)^.5)*(14)	111)^.5)*(14	111)^.5)*(14
				.7/15.025)=	.7/15.025)=	.7/15.025)=
				132	512	1,128
112	A111+.5=			(L11*D5^2*(A	(L11*E5^2*(A	(L11*F5^2*(A
	13.0	1		112)^.5)*(14	112)^.5)*(14	112)^.5)*(14
				.7/15.025)=	.7/15.025)=	.7/15.025)=
				134	522	1,150
113	A112+.5=	A113/13.59=	L112*A113=	(L11*D5^2*(A	(L11*E5^2*(A	(L11*F5^2*(A
	13.5	.99	.49	113)^.5)*(14	113)^.5)*(14	113)^.5)*(14
				.7/15.025)=	.7/15.025)=	.7/15.025)=
L	1		1	137	532	1,172
114	A113+.5=	1		(L11*D5^2*(A	(L11*E5 ² *(A	(L11*F5^2*(A
	14.0			114)^.5)*(14	114)^.5)*(14	114)^.5)*(14
				.7/15.025)=	.7/15.025)=	.7/15.025)=
	<u> </u>			140	542	1,194
115	A114+.5=			(L11*D5*2*(A	(L11*E5^2*(A	(L11*F5^2*(A
1	14.5			115)^.5)*(14	115)^.5)*(14	115)^.5)*(14
			1	.7/15.025)=	•7/15 • 025) =	.7/15.025)=
				142	551	1,215

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	A	В	С	D	Е	F
116	A115+.5=	A116/13.59=		(L11*D5^2*(A	(L11*E5^2*(A	(L11*F5^2*(A
	15.0	1.10		116)^.5)*(14	116)^.5)*(14	116)^.5)*(14
				.7/15.025)=	.7/15.025)=	.7/15.025)=
				144	561	1,235
117	A116+.5=			(L11*D5^2*(A	(L11*E5^2*(A	(L11*F5^2*(A
	15.5			117)^.5)*(14	117)^.5)*(14	117)^.5)*(14
				.7/15.025)=	.7/15.025)=	.7/15.025)=
				147	570	1,256
118	A117+.5=			(L11*D5^2*(A	(L11*E5^2*(A	(L11*F5^2*(A
	16.0			118)^.5)*(14	118)^.5)*(14	118)^.5)*(14
				.7/15.025)=	•7/15 [,] 025)=	.7/15.025)=
				149	579	1,276
119	A118+.5=	A119/13.59=		(L11*D5^2*(A	(L11*E5^2*(A	(L11*F5^2*(A
	16.5	1.21		119)^.5)*(14	119)^.5)*(14	119)^.5)*(14
				•7/15•025)=	•7/15•025)=	.7/15.025)=
ļ				151	588	1,296
120	A119+.5=	A120/13.59=		(L11*D5^2*(A	(L11*E5^2*(A	(L11*F5^2*(A
	17.0	1.25		120)^.5)*(14	120)^.5)*(14	120)^.5)*(14
				•7/15•025)=	•7/15•025)=	.7/15.025)=
ļ				154	597	1,315
121	A120+.5=	A121/13.59=		(L11*D5^2*(A	(L11*E5 ² *(A	(L11*F5 ^ 2*(A
	17.5	1.29		121)^.5)*(14	121)^.5)*(14	121)^.5)*(14
				.7/15.025)=	•7/15•025)=	.7/15.025)=
				156	606	1,334
122	A121+.5=	A122/13.59=		(L11*D5^2*(A	(L11*E5*2*(A	(L11*F5^2*(A
	18.0	1.32		122)~.5)*(14	122)^.5)*(14	122)^.5)*(14
				•//15.025)=	•//15•025)=	•7/15.025)=
122	A1224 5-	A122/12 50-			b14	1,303
125	A122 + J = 10	1 24		(LIIAD) 24(A	(LIIAES ZA(A	(LII*P) 2*(A
	10.5	1.50		7/15 025) =	7/15 025) -	$\frac{123}{7/15}$ $\frac{3}{7}$
	i			160	•7713•023)- 623	•7713•023)-
124	A123+.5=	1 = 124/13.59 =		(1.11*D5^2*(A	(111*F5*2*(A	1,372 (111*F5*7*(A
	19.0	1.40		(211 25) = (14)	(212 - 25) = (14)	$(211 + 15) \ge (14)$
				.7/15.025) =	.7/15.025) =	.7/15.025) =
				163	631	1.390
125	A124+.5=	A125/13.59=		(L11*D5^2*(A	(L11*E5^2*(A	(L11*F5^2*(A
	19.5	1.43		125)^.5)*(14	125)^.5)*(14	125)^.5)*(14
		:		.7/15.025)=	.7/15.025)=	.7/15.025)=
				165	639	1,409
126	A125+.5=	A126/13.59=		(L11*D5^2*(A	(L11*E5^2*(A	(L11*F5^2*(A
	20.0	1.47		126)^.5)*(14	126)^.5)*(14	126)^.5)*(14
				.7/15.025)=	.7/15.025)=	.7/15.025)=
				167	648	1,427
127	A126+.5=	A127/13.59=		(L11*D5^2*(A	(L11*E5^2*(A	(L11*F5^2*(A
	20.5	1.51		127)^.5)*(14	127)^.5)*(14	127)^.5)*(14
				.7/15.025)=	•7/15•025) =	•7/15.025)=
		İ		169	656	1,444
128	A127+.5=	A128/13.59=	L112*A128=	(L11*D5^2*(A	(L11*E5^2*(A	(L11*F5^2*(A
	21.0	1.55	•76	128)^.5)*(14	128)^.5)*(14	128)^.5)*(14
			-	.7/15.025)=	.7/15.025)=	.7/15.025)=
ļ				171	664	1,462
129	A128+.5=	A129/13.59=		(L11*D5^2*(A	(L11*E5^2*(A	(L11*F5^2*(A
	21.5	1.58		129)^.5)*(14	129)^.5)*(14	129)^.5)*(14
				•7/15•025)=	.7/15.025)=	.7/15.025)=
		l		173	671	1,479
Page						

	٨	l p	C	<u>م</u> ا	<u></u>	
120	A120± 5-	A130/13 50-		U	E	F
130	22 0	1 62		(LII*D) 2*(A	$(L11^{-}L)^{-}$ 5)+(14	$(L11^{+}J) 2^{+}(A)$
	22.00	1.02		7/15 025) -	7/15 025) -	7/15 025) - 7/15 025
				175	670	•//15•025)-
131	A130+ 5=	A131/13.59=		1/5 (T11*D5*2*(A	075 (1)1*F5*2*(A	1,490
1.51	22.5	1.66		131) [•] 5)*(14	$(131)^{5}.5)*(14)$	(211015) 20(R)
	22.05	1.00		7/15 025) -	7/15 025)	7/15 025) =
				177	687	1 513
132	A131+.5=	$ _{A132/13.59=}$		(T11*D5*2*(A	(111*E5*2*(A	(111*F5*2*(A
1.32	23.0	1 69		$(211 \ 0.5) \ge (14)$	$(211 \ 25 \ 2 \ (R)$	$(211^{\circ}15) \ge (A)$
	25.0	1.05		7/15 025) =	7/15 025) =	7/15 025 =
				179	•//15•025)- 69/	1 530
133	A132+ 5=	A133/13 59=		(T11*D5*2*(A	(111#F5^2*(A	1,550 (111*F5*2*(A
133	23.5	1 73		(LI100) 20(A	$(133)^{5} = 5)*(14)$	133) 5) * (14
	25.5	1.75		7/15.025	$(135)^{-}(135)^{-}(14)^{-}(1$	7/15.025
				181	702	1 546
134	A133+.5=	A 34/13.59=		(111*D5*2*(A	(1.11*E5*2*(A	(1.11*F5^2*(A
	24.0	1.77		$(311 \ b)^{2} \ (14)^{3}$	$(311 \ 25 \ 2 \ (14)$	(211, 13, 2)
	2400			.7/15.025) =	.7/15.025)#	.7/15.025) =
				183	709	1 563
135	A134+,5=	A135/13.59=		(1.11*D5^2*(A	(I11*F5*2*(A	(111*F5^2*(A
	24.5	1.80		$(311, 5)^{\circ}, 5) * (14)$	$(312 - 5) \neq (14)$	(211, 15, 2, (14))
	2403	1.00		7/15.025) =	.7/15.025)=	.7/15.025) =
				185	717	1 579
136	A135+,5=	$\frac{1}{ A 36/13.59=}$		(T11*D5*2*(A	(111*F5*2*(A	(111*F5^2*(A
1.50	25.0	1.84		136)^.5)*(14	$(136)^{-}, 5)*(14)$	$(211^{10})^{2} (8)$
	25.0	1.04		.7/15.025) =	.7/15.025) =	.7/15.025) =
				186	724	1.595
137	A136+.5=	A137/13.59=		(L11*D5^2*(A	(L11*E5^2*(A	(L11*F5^2*(A
	25.5	1.88		137)^.5)*(14	137)^.5)*(14	137)^.5)*(14
				.7/15.025)=	.7/15.025)=	.7/15.025)=
·				188	731	1,611
138	A137+.5=	A138/13.59=	· · · · ·	(L11*D5^2*(A	(L11*E5^2*(A	(L11*F5^2*(A
1	26.0	1.91		138)^.5)*(14	138)^.5)*(14	138)^.5)*(14
				.7/15.025)=	.7/15.025)=	.7/15.025)=
				190	738	1,626
139	A138+.5=	A139/13.59=	1	(L11*D5^2*(A	(L11*E5^2*(A	(L11*F5^2*(A
	26.5	1.95		139)^.5)*(14	139)^.5)*(14	139)^.5)*(14
				.7/15.025)=	.7/15.025)=	.7/15.025)=
				192	745	1,642
140	A139+.5=	A140/13.59=	1	(L11*D5^2*(A	(L11*E5^2*(A	(L11*F5^2*(A
	27.0	1.99		140)^.5)*(14	140)^.5)*(14	140)^.5)*(14
1				.7/15.025)=	.7/15.025)=	.7/15.025)=
				194	752	1,657
141	A140+.5=	A141/13.59=	L112*A141=	(L11*D5^2*(A	(L11*E5^2*(A	(L11*F5^2*(A
	27.5	2.02	.99	141)^.5)*(14	141)^.5)*(14	141)^.5)*(14
				.7/15.025)=	.7/15.025)=	.7/15.025)=
				196	759	1,673
142	A141+.5=	A142/13.59=		(L11*D5^2*(A	(L11*E5^2*(A	(L11*F5^2*(A
	28.0	2.06		142)^.5)*(14	142)^.5)*(14	142)^.5)*(14
1				.7/15.025)=	.7/15.025)=	.7/15.025)=
L				197	766	1,688
143	A142+.5=	A143/13.59=		(L11*D5^2*(A	(L11*E5^2*(A	(L11*F5^2*(A
	28.5	2.10		143)^.5)*(14	143)^.5)*(14	143)^.5)*(14
				.7/15.025)=	.7/15.025)=	.7/15.025)=
L	<u> </u>			199	773	1,703

	A	В	С	D	E	F
144	A143+.5=	A144/13.59=		(L11*D5^2*(A	(L11*E5^2*(A	(L11*F5^2*(A
	29.0	2.13		144)^.5)*(14	144)^.5)*(14	144)^.5)*(14
				.7/15.025)=	.7/15.025)=	.7/15.025)=
				201	780	1.718
145	A144+.5=	A145/13.59=		(L11*D5^2*(A	(L11*E5^2*(A	(L11*F5^2*(A
	29.5	2.17		$(45)^{,5}(14)$	$(45)^{,5} \times (14)$	145)^.5)*(14
				7/15.025) =	.7/15.025) =	.7/15.025) =
				203	786	1.733
146	A145+.5=	A146/13.59=	· · · · · · · · · · · · · · · · · · ·	(1.11*D5^2*(A	(L11*E5*2*(A	(1.11*F5^2*(A
	30.0	2.21		$(211, 25, 2) \times (14)$	(242, 25, 2, 14) 146)^, 5)*(14)	$(146)^{,5} \times (14)$
	5000			.7/15.025)=	.7/15.025) =	.7/15.025) =
				204	793	1,747
147	A146+.5=	A147/13.59=		(L11*D5^2*(A	(L11*E5^2*(A	(L11*F5^2*(A
	30.5	2.24		147)^.5)*(14	147)^.5)*(14	147)^.5)*(14
				.7/15.025)=	.7/15.025)=	.7/15.025)=
				206	800	1,762
148	A147+.5=	A148/13.59=		(L11*D5^2*(A	(L11*E5^2*(A	(L11*F5^2*(A)
	31.0	2.28		148)^.5)*(14	148)^.5)*(14	$148)^{,5)*(14)}$
				.7/15.025) =	.7/15.025) =	.7/15.025)=
				208	806	1.776
149	A148+.5=	A149/13.59=		(L11*D5*2*(A	(L11*E5^2*(A	(L11*F5^2*(A
	31.5	2.32		149)^.5)*(14	149)^.5)*(14	149)^.5)*(14
				.7/15.025)=	.7/15.025)=	.7/15.025)=
				209	813	1,790
150	A149+.5=	A150/13.59=		(L11*D5^2*(A	(L11*E5*2*(A	(L11*F5^2*(A
	32.0	2.35		150)^.5)*(14	150)^.5)*(14	150)^.5)*(14
		}		.7/15.025)=	.7/15.025)=	.7/15.025)=
				211	819	1,804
151	A150+.5=	A151/13.59=		(L11*D5^2*(A	(L11*E5^2*(A	(L11*F5^2*(A
	32.5	2.39		151)^.5)*(14	151)^.5)*(14	151)^.5)*(14
				.7/15.025)=	.7/15.025)=	.7/15.025)=
				213	825	1,818
152	A151+.5=	A152/13.59=		(L11*D5^2*(A	(L11*E5^2*(A	(L11*F5^2*(A
	33.0	2.43		152)^.5)*(14	152)^.5)*(14	152)^.5)*(14
]				.7/15.025)=	.7/15.025)=	.7/15.025)=
				214	832	1,832
153	A152+.5=	A153/13.59=		(L11*D5^2*(A	(L11*E5^2*(A	(L11*F5^2*(A
	33.5	2.47		153)^.5)*(14	153)^.5)*(14	153)^.5)*(14
				.7/15.025)=	.7/15.025)=	.7/15.025)=
				216	838	1,846
154	A153+.5=	A154/13.59=		(L11*D5^2*(A	(L11*E5^2*(A	(L11*F5^2*(A
1	34.0	2.50		154)^.5)*(14	154)^.5)*(14	154)^.5)*(14
				.7/15.025)=	.7/15.025)=	.7/15.025)=
				217	844	1,860
155	A154+.5=	A155/13.59=	L112*A155=	(L11*D5^2*(A	(L11*E5^2*(A	(L11*F5^2*(A
	34.5	2.54	1.25	155)^.5)*(14	155)^.5)*(14	155)^.5)*(14
				.7/15.025)=	.7/15.025)=	.7/15.025)=
		<u> </u>		219	850	1,874
156	A155+.5=	A156/13.59=		(L11*D5^2*(A	(L11*E5^2*(A	(L11*F5^2*(A
	35.0	2.58		156)^.5)*(14	156)^.5)*(14	156)^.5)*(14
				•7/15•025)=	•7/15.025)=	.7/15.025)=
			ļ	221	857	1,887
157	A156+.5=	A157/13.59=		(L11*D5^2*(A	(L11*E5^2*(A	(L11*F5^2*(A
	35.5	2.61		157)^.5)*(14	157)^.5)*(14	157) •• 5)*(14
				•7/15.025)=	•7/15.025)=	.7/15.025)=
1	1	1	1	222	863	1,901

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1.50	A	B	С	D	E	F
158	A15/+.5=	A158/13.59=		(L11*D5^2*(A	(L11*E5~2*(A	(L11*F5 ² *(A
	36.0	2.65		158)^.5)*(14	158)^.5)*(14	158)^.5)*(14
				•7/15•025)=	•7/15•025)=	.7/15.025)=
				224	869	1,914
159	A158+.5=	A159/13.59=		(L11*D5^2*(A	(L11*E5^2*(A	(L11*F5 ^ 2*(A
	36.5	2.69		159)^.5)*(14	159)^.5)*(14	159)^.5)*(14
				.7/15.025)=	.7/15.025)=	.7/15.025)=
				225	875	1,927
160	A159+.5=	A160/13.59=		(L11*D5^2*(A	(L11*E5^2*(A	(L11*F5^2*(A
}	37.0	2.72		160)^.5)*(14	160)^.5)*(14	160)^.5)*(14
				.7/15.025)=	.7/15.025)=	.7/15.025)=
<u> </u>				227	881	1,940
161	A160+.5=	A161/13.59=		(L11*D5^2*(A	(L11*E5^2*(A	(L11*F5^2*(A
	37.5	2.76		161)^.5)*(14	161)^.5)*(14	161)^.5)*(14
				•7/15•025)=	.7/15.025)=	.7/15.025)=
				228	887	1,953
162	A161+.5=	A162/13.59=		(L11*D5^2*(A	(L11*E5^2*(A	(L11*F5^2*(A
	38.0	2.80		162)^.5)*(14	162)^.5)*(14	162)^.5)*(14
				.7/15.025)=	.7/15.025)=	.7/15.025)=
				230	893	1,966
163	A162+.5=	A163/13.59=		(L11*D5^2*(A	(L11*E5^2*(A	(L11*F5^2*(A
	38.5	2.83		163)^.5)*(14	163)^.5)*(14	163)^.5)*(14
				.7/15.025)=	.7/15.025)=	.7/15.025)=
				231	898	1,979
164	A163+.5=	A164/13.59=		(L11*D5^2*(A	(L11*E5^2*(A	(L11*F5^2*(A
	39.0	2.87		164)^.5)*(14	164)^.5)*(14	164)^.5)*(14
				•7/15•025)=	•7/15•025) =	•7/15•025)=
L				233	904	1,992
165	A164+.5=	A165/13.59=		(L11*D5^2*(A	(L11*E5^2*(A	(L11*F5 ² *(A
	39.5	2.91		165)^.5)*(14	165)^.5)*(14	165)^.5)*(14
				•7/15•025)=	•7/15•025)=	•7/15•025)=
				234	910	2,005
166	A165+.5=	A166/13.59=		(L11*D5^2*(A	(L11*E5^2*(A	(L11*F5^2*(A
	40.0	2.94		166)^.5)*(14	166)^.5)*(14	166)^.5)*(14
				.7/15.025)=	.7/15.025)=	.7/15.025)=
				236	916	2,017
16/	*40.8	3.00	(14.676/29.9	(L11*D5^2*(B	(L11*E5^2*(B	(L11*F5^2*(B
			2)*B16/=	16/*13.59)~.	16/*13.59)~.	16/*13.59)~.
			1.4/	()*(14+//1)•	5)*(14.//15.	5)*(14.//15.
		1		(025)=	025)=	025)=
160	121(9412 50		1	238	924	2,03/
108	B108*13.59=	B10/+.2=		(LII*D)~2*(B	(LII*E) 2*(B	(LII*F5"2*(B
ł	43.5	3.20		108*13.59)**	108*13.59)**	168*13.59)
				()*(14•//1)•	5)*(14•//15•	5)*(14.7/15.
				025)*	025)=	025)=
160	D140+13 50-	D1691 2-	l T		900	2,104
109	B109~13.59=	B100+.2=		(LII*D) 2*(B	(LIIAE) 24(B	(LIIAF) 24(B
	40.2	3.40		$109^{1}3.39$	$107^{1}3.57$	$109^{1}3.39$
				0.25) =	0.25) = 0.25) = 0.251 = 0.25	025) =
				252	02374	2 168
170	B170*13 50-	B169± 2=		200 (111*D5*0*/P	704 (1)*r5^?*(P	4,100 (1)1*F5*7*(D
1.10	=92.0°13.39 م	2 40		170*13 50\A	170+13 5014	170*13 5014
	40.9	3.00		5)*(1/ 7/15	5)*(1/ 7/15	5)*(1/ 7/15
				0.25) =	025)=	025)=
1				261	1 012	9 921
L	<u> </u>	1	I	201	1,015	۷,۷۵۱

Page

		D	<u> </u>	D	F	
		D	<u> </u>		E	F
1/1	BI/1×13•34=	B1/0+.2=			(LII*E5~2*(B	(LII*F5~2*(B
	51•0	3.80		1/1*13.59)**.	1/1*13.59)*.	1/1*13.59)*.
				5)*(14.7/15.	5)*(14.7/15.	5)*(14.7/15.
				025)=	025)=	025)=
				268	1,040	2,292
172	B172*13.59=	B171+•2=	(14.676/29.9	(L11*D5~2*(B	(L11*E5^2*(B	(L11*F5~2*(B
	54.4	4.00	2)*B1/2=	1/2*13.59)~.	1/2*13.59)~.	1/2*13.59)^.
			1.96	5)*(14.7/15.	5)*(14.//15.	5)*(14.//15.
				025)=	025)=	025)=
170	2172412 50	D1704 0		2/5	1,068	2,352
1/3	B1/3~13.39=	B1/2+.2=		(LII~D) Z~(B	(LII~E) 2~(B	(LIIAF) 20(B)
	57+1	4.20		$1/3^{1}3.39$	$1/3^{1}3 \cdot 3^{1}3 \cdot$	$1/3^{1}3.59$
				5)*(14•//15• 025)-	5)*(14•//15• 025)-	$5)^{(14.//15.)}$
				025)=	1.00/	(25)=
174	p17/+12 50-	P172+ 2-		202	1,094	2,410
11/4	50 9	b1/J+•2-		(LII*DJ 2*(D	(LII~EJ 2~(B	$(L11^{r}L) 2^{n}(D)$
	37.0	4.40		$1/4^{1} \cdot 13 \cdot 33 = 33$	$1/4^{-1} (3 \cdot 5) $	$1/4^{-1} \cdot 13 \cdot 39$
				025) =	(14.771)	(14.771)
				288	1.120	2.467
175	B175*13.59=	B174+.2=	(14.676/29.9	(L11*D5^2*(B	(L11*E5*2*(B	(L11*F5^2*(B
	62.5	4.60	$(2) \times B175 =$	175*13.59)^.	175*13.59)*	175*13.59)^.
			2.26	(14.7/15)	5)*(14.7/15.	5)*(14.7/15.)
				(25) =	025)=	025)=
				295	1.145	2,522
176	B176*13.59=	B175+.2=	(14.676/29.9	(L11*D5^2*(B	(L11*E5^2*(B	(L11*F5^2*(B
	65.2	4.80	2)*B176=	176*13.59)^.	176*13.59)^.	176*13.59)^.
			2.35	5)*(14.7/15.	5)*(14.7/15.	5)*(14.7/15.
				025)=	025)=	025)=
				301	1,169	2,576
177	B177*13.59=	B176+.2=	(14.676/29.9	(L11*D5^2*(B	(L11*E5^2*(B	(L11*F5^2*(B
	68.0	5.00	2)*B177=	177*13.59)^.	177*13.59)^.	177*13.59)^.
			2.45	5)*(14.7/15.	5)*(14.7/15.	5)*(14.7/15.
				025)=	025)=	025)=
				307	1,194	2,629
178	B178*13.59=	B177+.2=	(14.676/29.9	(L11*D5^2*(B	(L11*E5^2*(B	(L11*F5^2*(B
	70.7	5.20	2)*B178=	178*13.59)^.	178*13.59)^.	178*13.59)^.
			2.55	5)*(14.7/15.	5)*(14.7/15.	5)*(14.7/15.
				025)=	025)=	025)=
1.80			(11, (7, (10, 0))	313	1,217	2,681
179	B1/9*13.59=	B1/8+•2=	(14.6/6/29.9	(L11*D5~2*(B	(L11*E5*2*(B	(L11*F5~2*(B
	73.4	5.40	2)~81/9=	1/9*13·39) ·	$1/9 \times 13.59$).	$1/9*13.59)^{-1}$
1			2.05	025)-	(14.7/15)	$3)^{(14.7/15)}$
				319	1 240	2 733
180	B18(1*13,59=	B179+,2=	(14.676/29.9	(L11*D5*2*(B	(1.11*E5^2*(B	(111*F5*2*(B
100	76.1	5.60	$(2) \times B180 =$	180*13.59)^.	180*13.59)^.	180*13.59)^.
			2.75	5)*(14.7/15.	5)*(14.7/15.	5)*(14.7/15.
				025)=	025)=	025)=
	ļ	l	ł	325	1,263	2,783
181	B181*13.59=	B180+.2=	(14.676/29.9	(L11*D5^2*(B	(L11*E5^2*(B	(L11*F5^2*(B
	78.8	5.80	2)*B181=	181*13.59)^.	181*13.59)^.	181*13.59)^.
			2.84	5)*(14.7/15.	5)*(14.7/15.	5)*(14.7/15.
l				025)=	025)=	025)=
				331	1,285	2,832

	A	В	С	D	E	F
182	B182*13.59=	B181+.2=	(14.676/29.9	(L11*D5^2*(B	(L11*E5^2*(B	(L11*F5^2*(B
	81.5	6.00	2)*B182=	182*13.59)^.	182*13.59)^.	182*13.59)^.
			2.94	5)*(14.7/15.	5)*(14.7/15.	5)*(14.7/15.
				025)=	025)=	025)=
				337	1,307	2,880
183		B182+.5=	(14.676/29.9	(L11*D5^2*(B	(L11*E5*2*(B	(L11*F5^2*(B
		6.50	2)*B183=	183*13.59)^.	183*13.59)^.	183*13.59)^.
			3.19	5)*(14.7/15.	5)*(14.7/15.	5)*(14.7/15.
				025)=	025)=	025)=
				350	1,361	2,998
184		B183+.5=	(14.676/29.9	(L11*D5^2*(B	(L11*E5^2*(B	(L11*F5^2*(B
		7.00	2)*B184=	184*13.59)^.	184*13.59)^.	184*13.59)^.
			3.43	5)*(14.7/15.	5)*(14.7/15.	5)*(14.7/15.
				025) =	025)=	025)=
				364	1,412	3,111
185		B184+.5=	(14.676/29.9	(L11*D5^2*(B	(L11*E5~2*(B	(L11*F5^2*(B
		7.50	2)*B185=	185*13.59)^.	185*13.59)^.	185*13.59)~.
			3.68	5)*(14.7/15.	5)*(14.7/15.	5)*(14.7/15.
				025)=	025)=	025)=
164	l	D1051 5	(14 676/20 0	3/b	1,402	3,220
100		B10JT.J=	(14.070/29.9	(LII~D) Z~(D	(LIIAE) 24(B	(LII~r) 2~(B
		0.00	2)^0100=	$100^{1} \cdot 13 \cdot 37$	$100^{1} \cdot 13 \cdot 39$	$100^{1}13.57$
			5.92	025)-	025)-	0.25) =
				380	1 510	3 326
197		P186+ 5-	(14 676/20 0	J07	1,510	$(11) \times 5^{2}$
10/		8 50	(14.070/23.5	187*13 50)*	187*13 59)*	187*13.59)^.
		0.50	2)**B10/=	5)*(14, 7/15)	$5) \star (14, 7/15)$	5)*(14.7/15.
			4.17	(14.771)	0=	025) =
				401	1.556	3,428
188		B187+.5=	(14.676/29.9	(L11*D5^2*(B	(L11*E5^2*(B	(L11*F5^2*(B
		9.00	2)*B188=	188*13.59)^.	188*13.59)^.	188*13.59)^.
			4.41	5)*(14.7/15.	5)*(14.7/15.	5)*(14.7/15.
				025)=	025)=	025)=
				412	1,601	3,528
189		B188+.5=	(14.676/29.9	(L11*D5^2*(B	(L11*E5^2*(B	(L11*F5^2*(B
		9.50	2)*B189=	189*13.59)^.	189*13.59)^.	189*13.59)^.
			4.66	5)*(14.7/15.	5)*(14.7/15.	5)*(14.7/15.
				025)=	025)=	025)=
				424	1,645	3,624
190		B189+.5=	(14.676/29.9	(L11*D5^2*(B	(L11*E5^2*(B	(L11*F5^2*(B
		10.00	2)*B190=	190*13.59)^.	190*13.59)^.	190*13.59)^.
			4.91	5)*(14.7/15.	5)*(14.7/15.	5)*(14.7/15.
				025)=	025)=	025)=
			()) (7(/00.0	435	1,688	3,719
191		B190+.5=	(14.6/6/29.9	(LII*D5*2*(B	(LI1*E5*2*(B	(LII*F5"2*(B
		10.50	2)*BIAI=	191413.24)~.	191*13.59)~.	191-13.39)
1			5.15	025)-)/(14+//1)+ 025)-	025)-
				1.1.5	1 720	3 810
102		P101± 5-	(14 676/20 0	44J	1,/JU (111±55^2±/D	J,010 (111*E5^0*/D
192			2)+0102-	102+12 5014	102#12 501A	192*13 501*
		11.00	2 J* D192=	172~13·37) · 5)*(1/ 7/15	172"13.37) · 5)*(1/ 7/15	5)*(14 7/15
			5.40	(0.25) =	025)=	025)=
				456	1 770	3.900
	1		<u>.1</u>		1, 1,170	5,500

Г	Α	B	С	D	F	F
193		B192+.5=	(14.676/29.9	(L1)*D5^2*(B	(L11*E5^2*(B	(L11*F5^2*(B)
		11.50	2)*B193=	193*13.59)^.	193*13.59)^.	193*13.59)^.
			5.64	5)*(14.7/15.	5)*(14.7/15.	5)*(14.7/15.)
				(25) =	(25) =	(25) =
				466	1.810	3,988
194		B193+.5=	(14.676/29.9	(L11*D5^2*(B	(L11*E5^2*(B	(L11*F5^2*(B
		12.00	2)*B194=	194*13.59)^.	194*13.59)^.	194*13.59)^.
			5.89	5)*(14.7/15.	5)*(14.7/15.	5)*(14.7/15.
				025)=	025)=	025)=
				476	1,849	4,073
195		B194+.5=	(14.676/29.9	(L11*D5^2*(B	(L11*E5^2*(B	(L11*F5^2*(P
1		12.50	2)*B195=	195*13.59)^.	195*13.59)^.	195*13.59)^.
			6.13	5)*(14.7/15.	5)*(14.7/15.	5)*(14.7/15.
				025)=	025)=	025)=
				486	1,887	4,157
196		B195+.5=	(14.676/29.9	(L11*D5^2*(B	(L11*E5*2*(B	(L11*F5^2*(B
		13.00	2)*B196=	196*13.59)^.	196*13.59)^.	196*13.59)^.
			6.38	5)*(14.7/15.	5)*(14.7/15.	5)*(14.7/15.
				025)=	025)=	025)=
				496	1,924	4,240
197		B196+.5=	(14.676/29.9	(L11*D5^2*(B	(L11*E5^2*(B	(L11*F5^2*(B
		13.50	2)*B197=	197*13.59)^.	197*13.59)^.	197*13.59)^.
1			6.62	5)*(14.7/15.	5)*(14.7/15.	5)*(14.7/15.
				025)=	025)=	025)=
				505	1,961	4,321
198		B197+.5=	(14.676/29.9	(L11*D5^2*(B	(L11*E5^2*(B	(L11*F5^2*(B
		14.00	2)*B198=	198*13.59)^.	198*13.59)^.	198*13.59)^.
			6.87	5)*(14.7/15.	5)*(14.7/15.	5)*(14.7/15.
				025)=	025)=	025)=
				514	1,997	4,400
199		B198+.5=	(14.676/29.9	(L11*D5^2*(B	(L11*E5^2*(B	(L11*F5^2*(B
		14.50	2)*B199=	199*13.59)^.	199*13.59)^.	199*13.59)^.
			7.11	5)*(14.7/15.	5)*(14.7/15.	5)*(14.7/15.
				025)=	025)=	025)=
		L		523	2,032	4,478
200		B199+.5=	(14.676/29.9	(L11*D5^2*(B	(L11*E5^2*(B	(L11*F5^2*(B
		15.00	2)*B200=	200*13.59)^.	200*13.59)^.	200*13.59)^.
			7.36	5)*(14.7/15.	5)*(14.7/15.	5)*(14.7/15.
1 1				(025)=	025)=	(025)=
0.01		17000 t 5-	(14 (76/20 0	<u>532</u>	2,06/	4,554
201		15 EA	114.0/0/29.9	1 L11 × D2 2× (B	101412 ED.4	101175072*(B
		15.50	Z)*BZUI=	$201*13.59)^{-1}$	$201 \times 13.59)^{-1}$	201*13.39)**.
			7.60	5)*(14•//15•	5)*(14.//15.	5)*(14.//15.
				023)=	025)=	(25) = (25)
202		P201+ 5-	(14 676/29 9	J41	2,101 (1)1*E5^2*(P	4,030
202		16.00	(14.070/25.5)	202*13 5010	202*13 59)*	202*13 50)°
		10.00	7_85	5)*(16 7/15	5)*(16 7/15	5) + (14 7/15)
1 1				(025) =	(14.7715)	(0.25) =
				550	2.135	4.704
203		B202+.5=	(14.676/29.9	(L11*D5^2*(R	(L11*E5*2*(R	(L11*F5^2*(R
		16.50	2)*B203=	203*13.59)^-	203*13.59)^	203*13.59)*-
			8.09	5)*(14.7/15.	5)*(14.7/15.	5)*(14.7/15.
				025)=	025)=	025)=
				558	2.168	4.777
L			L	L		

Г						
0.04	A	B	С	D	E	F
204		B203+.5=	(14.676/29.9	(L11*D5~2*(B	(L11*E5~2*(B	(L11*F5 ² *(B
		17.00	2)*B204=	204*13.59)^.	204*13.59)^.	204*13.59)^.
			8.34	5)*(14.7/15.	5)*(14.7/15.	5)*(14.7/15.
				025)=	025)=	025)=
				567	2,201	4,848
205		B204+.5=	(14.676/29.9	(L11*D5^2*(B	(L11*E5^2*(B	(L11*F5 ² *(B
		17.50	2)*B205=	205*13.59)^.	205*13.59)^.	205*13.59)^.
			8.58	5)*(14.7/15.	5)*(14.7/15.	5)*(14.7/15.
				025)=	025)=	025)=
				575	2,233	4,919
206	• •	B205+.5=	(14.676/29.9	(L11*D5^2*(B	(L11*E5^2*(B	(L11*F5^2*(B
		18.00	2)*B206=	206*13.59)^.	206*13.59)^.	206*13.59)^.
			8.83	5)*(14.7/15.	5)*(14.7/15.	5)*(14.7/15.
				025)=	(025) =	025)=
				583	2.265	4.989
207		B206+.5=	(14,676/29,9	(1.11*D5^2*(B	(111*E5*2*(B	(111*F5*2*(B
		18.50	2)*B207=	207*13.59)^.	207*13.59)^.	207*13.59)^.
		10.50	9.07	5)*(14.7/15.	5)*(14.7/15.	5)*(14.7/15.
			3.07	025) =	025) =	0251=
				501	2 204	5 059
208		D2071 5	() (7 (/ 20 0	391 (11155634(D	2,290	5,038
208		B207+.5=	(14.0/0/29.9	(L11*D2 2*(B	(LIIAES ZA(B	
		19.00	2)*.B208=	208*13.59)**	208*13.59)**.	208*13.59)**•
			9.32	5)*(14.7/15.	5)*(14•7/15•	5)*(14.7/15.
				0 25) =	025)=	025)=
				599	2,327	5,126
209		B208+.5=	(14.676/29.9	(L11*D5*2*(B	(L11*E5^2*(B	(L11*F5 ² *(B
		19.50	2)*B209=	209*13.59)^.	209*13.59)^.	209*13.59)^.
			9.56	5)*(14.7/15.	5)*(14.7/15.	5)*(14.7/15.
				025)=	025)=	025)=
				607	2,357	5,193
210		B209+.5=	(14.676/29.9	(L11*D5^2*(B	(L11*E5 ^ 2*(B	(L11*F5 ² *(B
		20.00	2)*B210=	210*13.59)^.	210*13.59)^.	210*13.59)^.
			9.81	5)*(14.7/15.	5)*(14.7/15.	5)*(14.7/15.
				025)=	025)=	025)=
				615	2,387	5,259
211		B210+.5=	(14.676/29.9	(L11*D5^2*(B	(L11*E5^2*(B	(L11*F5^2*(B
		20.50	2)*B211=	211*13.59)^.	211*13.59)^.	211*13.59)^.
			10.06	5)*(14.7/15.	5)*(14.7/15.	5)*(14.7/15.
				025)=	025)=	025)=
				622	2,417	5,324
212		B211+.5=	(14.676/29.9	(L11*D5^2*(B	(L11*E5^2*(B	(L11*F5^2*(B
		21.00	(2) * B212 =	212*13.59)^.	212*13.59)^.	212*13.59)^.
			10.30	5)*(14.7/15.	5)*(14.7/15.	5)*(14.7/15.
				025)=	025)=	025)=
				630	2.446	5.389
213		B212+.5=	(14.676/29.9	(L11*D5*2*(B	(L11*E5^2*(B	(L11*F5^2*(B
		21,50	2)*R213=	213*13.59)^-	213*13.59)^-	213*13.59)^-
			10.55	5)*(14.7/15	5)*(14.7/15	5)*(14.7/15.
				025)=	025)=	025)=
				637	2 475	5 452
21/		122124 5-	(1/ 676/20 0	(111±D5^2±(P	(111*F5*9*(P	//////////////////////////////////////
214			2)+2214-	21/+12 EON	21/+12 50\A	21/412 501A
	,	22.00	2 J ~ DZ14=	214-13.37J ·	5 + (1/ 7/15	5)+(1, 7/1E
			10.79	5)*(14.//15.	0.25.	025)-
				020)=	020)=	020)=
	L		I	645	2,504	5,516

[A	В	С	D	E	F
215		B214+.5≠	(14.676/29.9	(L11*D5^2*(B	(L11*E5^2*(B	(L11*F5^2*(B
		22.50	2)*B215=	215*13.59)^.	215*13.59)^.	215*13.59)^.
			11.04	5)*(14.7/15.	5)*(14.7/15.	5)*(14.7/15.
				025)=	025)=	025)=
1				652	2,532	5,578
216		B215+.5=	(14.676/29.9	(L11*D5^2*(B	(L11*E5^2*(B	(L11*F5^2*(B
		23.00	2)*B216=	216*13.59)^.	216*13.59)^.	216*13.59)^.
			11.28	5)*(14.7/15.	5)*(14.7/15.	5)*(14.7/15.
				025)=	025) =	025)=
				659	2,560	5,639
217		B216+•5=	(14.676/29.9	(L11*D5^2*(B	(L11*E5 ^ 2*(B	(L11*F5^2*(B
		23.50	2)*B217=	217*13.59)^.	217*13.59)^.	217*13.59)^.
			11.53	5)*(14.7/15.	5)*(14.7/15.	5)*(14.7/15.
				025)=	025)=	025)=
				666	2,587	5,700
218		B217+.5=	(14.676/29.9	(L11*D5^2*(B	(L11*E5^2*(B	(L11*F5^2*(B
		24.00	2)*B218=	218*13.59)^.	218*13.59)^.	218*13.59)^.
			11.77	5)*(14.7/15.	5)*(14.7/15.	5)*(14.7/15.
				025)=	025)=	025)=
				673	2,615	5,761
219		B218+.5=	(14.676/29.9	(L11*D5^2*(B	(L11*E5^2*(B	(L11*F5^2*(B
		24.50	2)*B219=	219*13.59)^.	219*13.59)^.	219*13.59)^.
			12.02	5)*(14.7/15.	5)*(14.7/15.	5)*(14.7/15.
				025)=	025)=	025)=
				680	2,642	5,820
220		B219+.5=	(14.676/29.9	(L11*D5 ^ 2*(B	(L11*E5^2*(B	(L11*F5 ^ 2*(B
		25.00	2)*B220=	220*13.59)^.	220*13.59)^.	220*13.59)^.
			12.26	5)*(14.7/15.	5)*(14.7/15.	5)*(14.7/15.
				025)=	025)=	025)=
			(1) (7) (00 0	687	2,669	5,880
221		B220+.5=	(14.0/0/29.9)	(LII*D2"2*(B	(LII*E5"2*(B	(LII*F5"2*(B
		25.50	$2)^{B221}$	$221^{1} \cdot 3 \cdot 39$	$221^{1}3.39$	$221^{1}3.39$
			12.51	J)~(14•//1J• 025)-	(14.771)	025)-
				69/	2 605	5 039
222		R221 + 5 =	(14 676/29 9	094	2,075	J,930
222		26.00	(14.07072). 2)*P222=	222*13 59*	(LII*L) 2*() 222#13 50*	(L1101) 20(D
		20.00	12.75	5)*(16.7/15)	5)*(14, 7/15)	5)*(14 7/15)
			12075	(1407) = (025)=	(14.7,1)
		i i		701	2 7 7 2 7	5 996
223	······································	B222+.5=	(14.676/29.9	(1.11*D5^2*(B	(L11*E5^2*(B	(L11*F5^2*(B)
		26.50	(2) * B223 =	223*13.59)^.	223*13.59)^	223*13.59)^
			13.00	5)*(14.7/15.	5)*(14.7/15.	5)*(14.7/15.
				025)=	025)=	025)=
		i		708	2,748	6.053
224		B223+.5=	(14.676/29.9	(L11*D5^2*(B	(L11*E5^2*(B	(L11*F5^2*(B
		27.00	2)*B224=	224*13.59)^.	224*13.59)^.	224*13.59)^.
			13.24	5)*(14.7/15.	5)*(14.7/15.	5)*(14.7/15.
				025)=	025)=	025)=
		1		714	2,773	6,110
225	<u></u>	B224+.5=	(14.676/29.9	(L11*D5^2*(B	(L11*E5^2*(B	(L11*F5^2*(B
		27.50	2)*B225=	225*13.59)^.	225*13.59)^.	225*13.59)^.
			13.49	5)*(14.7/15.	5)*(14.7/15.	5)*(14.7/15.
				025)=	025)=	025)=
				721_	2,799	6,167
	and the second second second second second second second second second second second second second second second			and the second se	and the second data and the se	

Г	A	В	С	D	E	F
226		B225+.5=	(14.676/29.9	(L11*D5^2*(B	(L11*E5^2*(B	(L11*F5^2*(B
		28.00	2)*B226=	226*13.59)^.	226*13.59)^.	226*13.59)^.
			13.73	5)*(14.7/15.	5)*(14.7/15.	5)*(14.7/15.
				025)=	025)=	025)=
				727	2,824	6,222
227		B226+.5=	(14.676/29.9	(L11*D5^2*(B	(L11*E5^2*(B	(L11*F5^2*(B
		28.50	2)*B227=	227*13.59)^.	227*13.59)^.	227*13.59)^.
			13.98	5)*(14.7/15.	5)*(14.7/15.	5)*(14.7/15.
	•			025)=	025)=	025)=
				734	2,849	6,278
228		B227+•5=	(14.676/29.9	(L11*D5^2*(B	(L11*E5^2*(B	(L11*F5^2*(B
		29.00	2)*B228=	228*13.59)^.	228*13.59)^.	228*13.59)^.
			14.22	5)*(14.7/15.	5)*(14.7/15.	5)*(14.7/15.
				025)=	025)=	025)=
				740	2,874	6,332
229		B228+.5=	(14.676/29.9	(L11*D5^2*(B	(L11*E5^2*(B	(L11*F5^2*(B
		29.50	2)*B229=	229*13.59)^.	229*13.59)^.	229*13.59)^.
			14.47	5)*(14.7/15.	5)*(14.7/15.	5)*(14.7/15.
				025)=	025)=	025)=
				747	2,899	6,387
230		B229+.5=	(14.676/29.9	(L11*D5^2*(B	(L11*E5^2*(B	(L11*F5^2*(B
		30.00	2)*B230=	230*13.59)^.	230*13.59)^.	230*13.59)^.
			14.72	5)*(14.7/15.	5)*(14.7/15.	5)*(14.7/15.
				025)=	025)=	025)=
				753	2,924	6,441
231	·	*30.58	15.00	(L11*D5^2*(C	(L11*E5^2*(C	(L11*F5^2*(C
				231*144*12/6	231*144*12/6	231*144*12/6
				2.428)^.5)*(2.428)^.5)*(2.428)^.5)*(
				14.7/15.025)	14.7/15.025)	14.7/15.025)
				=	=	=
				760	2,950	6,500
232		C232*(29.92/	C231+1=	(L11*D5^2*(C	(L11*E5*2*(C	(L11*F5^2*(C
		14.676)=	16.00	232*144*12/6	232*144*12/6	232*144*12/6
		32.62		2.428)^.5)*(2.428)^.5)*(2.428)^.5)*(
				14.7/15.025)	14.7/15.025)	14.7/15.025)
				=	=	=
				785	3,047	6,713
233		C233*(29.92/	C232+1=	(L11*D5~2*(C	(LI1*E5~2*(C	(LII*F5~2*(C
		14.676)=	17.00	233*144*12/6	233*144*12/6	233*144*12/6
		34.66		2.428)~.5)*(2.428)~.5)*(2.428)
				14.//15.025)	14.//15.025)	14.//15.025)
				=	=	=
0.04	•	000/4/00 00/	0000011	809	3,141	0,919
234		(234*(29.92))	1233+1=	(L11×D5 2×(C	(LII*E) 2*(U	(LIIAF5 24(C
		14.0/0)=	10.00	2 4 2 9 1 4 4 ~ 1 2 / 0	2 42810 5)+(2 / 28) ~ 5) * (
		30.70		2.420 · J)*(2.420 · J)*(1/1 - 7/15 - 0.000
				-	_	=
				832	3 222	7 120
225	<u>_</u>	C235+(20 02/	C23/+1-	(T11±D5*2±(C	J,232	(111***5*****
233		14 6761-	10 00	235+14/+19/4	235*144*19/4	235*144*12/6
	ł		19.00	2 / 2 2 1 4 4 ~ 1 2 / 0	2 672144412/0	2.4281 51+(
		30.14		14 7/15 025	14 7/15 0251	14.7/15 025)
				=	=	=
1				855	3,320	7.315
1	1	1	1	1		· · · ·

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	A	B	C	D	E	F
236		0236*(29.92/	10235+1=	(L11*D5°2*(C	(LI1*E5*2*(C	(LI1*F5~2*(C
		14.0/0)=	20.00	230*144*12/0	$236 \times 144 \times 12/6$	236*144*12/6
		40.77		2.420 .).	2.420 .5)*(2.428) .5)*(
					-	14.//15.025)
				877	-	= 7 505
227	·····	C237*(20 02/	LC236+1-	0//	3,407	(11)+======
237		$(23)^{(23)}(23)^{(23$	21 00	237*144*12/6	(LII~E) Z~(C	(LII^F) 2^(C
		42 81	21.00	$2.57 \times 144 \times 1270$	2 / 281 5 5 + (2 / 281 5 5 4
		42.01		14 7/15 025	2.420 - 3)	$2 \cdot 420 \cdot 5)^{(1)}$
				=	-	_
				890	- 2 / 01	7 601
238		C238*(29.92/	C237+1=	(111*D5^2*(C	J,471	/,071
2.30		14.676)=	22.00	238*144*12/6	(LII*E) 2*(() 238*144*12/6	238*144*12/6
		44.85	22.00	$2.428)^{-5} + ($	$2.428)^{-}.5)*($	2.4281 51*(
				14.7/15.025	14.7/15.025	14.7/15.025
				=	=	=
				920	3,573	7.872
239		C239*(29.92/	C238+1=	(L11*D5^2*(C	(L11*E5 ² *(C	(L11*F5 ² *(C
		14.676)=	23.00	239*144*12/6	239*144*12/6	239*144*12/6
		46.89		2.428)^.5)*(2.428)^.5)*(2.428)^.5)*(
				14.7/15.025)	14.7/15.025)	14.7/15.025)
				=	=	=
				941	3,653	8,048
240		C240*(29.92/	C239+1=	(L11*D5^2*(C	(L11*E5^2*(C	(L11*F5^2*(C
		14.676)=	24.00	240*144*12/6	240*144*12/6	240*144*12/6
		48.93		2.428)^.5)*(2.428)^.5)*(2.428)^.5)*(
				14.7/15.025)	14.7/15.025)	14.7/15.025)
				=	=	=
				961	3,732	8,222
241		C241*(29.92/	C240+1=	(L11*D5^2*(C	(L11*E5^2*(C	(L11*F5^2*(C
		14.676)=	25.00	241*144*12/6	241*144*12/6	241*144*12/6
		50.97		2.428)^.5)*(2.428)^.5)*(2.428)^.5)*(
				14.7/15.025)	14.7/15.025)	14.7/15.025)
				=	=	=
				981	3,809	8,391
242		C242*(29.92/	C241+1=	(L11*D5^2*(C	(L11*E5 ² *(C	(L11*F5 ² *(C
		14.676)=	26.00	242*144*12/6	242*144*12/6	242*144*12/6
		53.01		2.428)^.5)*(2.428)^.5)*(2.428)^.5)*(
				14.7/15.025)	14.7/15.025)	14.7/15.025)
	:			=	=	=
				1,000	3,884	8,557
243		C243*(29.92/	C242+1=	(L11*D5 ² *(C	(L11*E5 ² *(C	(L11*F5^2*(C
		14.676)=	27.00	243*144*12/6	243*144*12/6	243*144*12/6
		55.04		2.428)^.5)*(2.428)^.5)*(2.428)^.5)*(
				14.7/15.025)	14.7/15.025)	14.7/15.025)
				=	=	=
				1,019	3,958	8,720
244		C244*(29.92/	C243+1=	(LI1*D5 ² *(C	(L11*E5 ² *(C	(L11*F5 ² *(C
		14.676)=	28.00	244*144*12/6	244*144*12/6	244*144*12/6
	i	57.08		2.428)~.5)*(2.428)~.5)*(2.428)^.5)*(
				14.//15.025)	14•//15•025)	14.//15.025)
				=		=
1		1	1	1,038	4,031	8, 880

Page	2
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245		C2/5*(20 02/	C244+1-	U111+D502+(C	L (111+F5^0+(C	1
245		$(24)^{(29.92)}$	244+1-	(L11 - D) 2 - (C)	$(LII^{L}L) 2^{(0)}$	$(L11^{+}J) 2^{+}(C)$
		14.6/6)=	29.00	$243 \times 144 \times 12/6$	243~144~12/6	245*144*12/6
		59.12	1	2.428)~.5)*(2.428)~.5)*(2.428)*.5)*(
				14.7/15.025)	14.//15.025)	14.7/15.025)
				=	=	=
				1,057	4,102	9,037
246		C246*(29.92/	C245+1=	(L11*D5^2*(C	(L11*E5^2*(C	(L11*F5^2*(C
		14.676)=	30.00	246*144*12/6	246*144*12/6	246*144*12/6
		61.16		2.428)^.5)*(2.428)^.5)*(2.428)^.5)*(
				14.7/15.025)	14.7/15.025)	14.7/15.025)
				=	=	=
		1		1,075	4,172	9,192
247		C247*(29.92/	C246+1=	(L11*D5^2*(C	(L11*E5^2*(C	(L11*F5^2*(C
		14.676)=	31.00	247*144*12/6	247*144*12/6	247*144*12/6
		63.20		2.428)^.5)*(2.428)^.5)*(2.428)^.5)*(
				14.7/15.025)	14.7/15.025)	14.7/15.025)
				=	3	=
				1.092	4.241	9.344
248		C248*(29.92/	$C_{247+1=}$	(T11*D5*2*(C	(111*F5*2*()	(1)1*F5*2*(C
240		14 676)=	32 00	248*144*12/6	248*144*12/6	248*144*12/6
		65 24	52.00	2 4 28 1 5 1 * ($2 + 0^{-1} + 4^{-1} + 12 = 0^{-1}$	$2 + 0^{-1} + 12 = 12 = 0$
		05.24		14 7/15 025	$2 \cdot 4 2 \cdot 5 \cdot 5 \cdot 5 \cdot 5 \cdot 5 \cdot 5 \cdot 5 \cdot 5 \cdot 5 \cdot$	$2.420 - 5)^{-1}$
				14.//15.025)	14.7/15.025)	14.7/15.0257
				=	= / 200	=
				1,110	4,309	9,493
249			C248+1=	(L11*D5 ² *(C	(L11*E5~2*(C	(L11*F5~2*(C
			33.00	249*144*12/6	249*144*12/6	249*144*12/6
				2.428)^.5)*(2.428)^.5)*(2.428)^.5)*(
				14.7/15.025)	14.7/15.025)	14.7/15.025)
				=	=	=
				1,127	4,376	9,641
250			C249+1=	(L11*D5^2*(C	(L11*E5^2*(C	(L11*F5 ^ 2*(C
			34.00	250*144*12/6	250*144*12/6	250*144*12/6
				2.428)^.5)*(2.428)^.5)*(2.428)^.5)*(
				14.7/15.025)	14.7/15.025)	14.7/15.025)
				=	=	=
				1,144	4,442	9,786
251			C250+1=	(L11*D5^2*(C	(L11*E5^2*(C	(L11*F5^2*(C
			35.00	251*144*12/6	251*144*12/6	251*144*12/6
				2.428)^.5)*(2.428)^.5)*(2.428)^.5)*(
				14.7/15.025)	14.7/15.025)	14.7/15.025)
				=	=	=
				1,161	4,507	9,928
252		1	C251+1=	(1.11*D5^2*(C	(1.11*E5^2*(C	(L11*F5^2*(C
			36.00	252*144*12/6	252*144*12/6	252*144*12/6
1				$(2,428)^{-},5)*($	$(2,428)^{+},5)*($	$(2.428)^{-5}$
				14.7/15.025	14.7/15.025	14.7/15.025
				=	=	=
				1 177		10.069
252		<u> </u>	C252+1-	1,1//	7,7/1	10,007
در ۲			27 00		1 1 1 1 E J 2 A (C	1 1 1 1 r J 2 r (U
			37.00	233~144*12/0	2 / 20 / 6 5 2 4	2227144412/0
				2.428)5)*(2.428)	2.428) .)*(
				14.//15.025)	14.//15.025)	14.//15.025)
				=	=	=
	<u>l</u>		<u> </u>	1,193	4,634	10,208

.

	A	В	С	D	E	F
254			C253+1=	(L11*D5^2*(C	(L11*E5^2*(C	(L11*F5^2*(C
			38.00	254*144*12/6	254*144*12/6	254*144*12/6
				2.428)^.5)*(2.428)^.5)*(2.428)^.5)*(
				14.7/15.025)	14.7/15.025)	14.7/15.025)
				=	=	=
				1,209	4,696	10,345
255			C254+1=	(L11*D5^2*(C	(L11*E5^2*(C	(L11*F5^2*(C
			39.00	255*144*12/6	255*144*12/6	255*144*12/6
				2.428)^.5)*(2.428)^.5)*(2.428)^.5)*(
				14.7/15.025)	14.7/15.025)	14.7/15.025)
				=	=	=
				1,225	4,757	10,480

	G	н	T		ĸ	1 1
1	DIAMETED	TNCHEC	-			(2600+24+520)
	DIANEIEK	INCRES				(3000-24-320
						*(p1))/(1000
						*4*144*14.7)
						=
						16.6696753
2	4" nominal	6" nominal				
3	actual dia.	actual dia.				((62,4*10,73)
-						+64 4)/(12+2
						0))0 5
						9)) .5=
ļ						11.13128923
4						
5	4.026	6.065				
6						
7	(L11*G5^2*(A	(L11*H5^2*(A7				L1*L3=
	7)^.5)*(14.7)^.5)*(14.7/1				185.5549772
	/15.025)=	5.025)=				
	174	394				
8	(111*65*2*(A	(111*45*2*(48				
ľ	(211 0) 2 (R)	(11 - 13) 2 (R)				
	$(17, 0)^{-1}$) •))^(14•//1				
	/15.025)=	5.025)=				
	246	557				
9	(L11*G5 ^ 2*(A	(L11*H5^2*(A9				.86*((14.7)/
	9)^.5)*(14.7)^.5)*(14.7/1				(.6*520))^.5
	/15.025)=	5.025)=				=
	301	683				.1866722756
10	(L11*G5^2*(A	(L11*H5^2*(A1				
	10)^.5)*(14.	$(0)^{5}, 5) * (14.7)$				
	7/15.025) =	15.025) =				
	247	700				
11	J4/	/00	<u> </u>			1.7.47.0
	(LIIAGS ZA(A	(LIIAHO ZA(AI				
	11)~.5)*(14.	1)~.5)*(14.//				34.63/96984
	7/15.025)=	15.025)=				
	388	881				
12	(L11*G5*2*(A	(L11*H5^2*(A1				
	12)^.5)*(14.	2)^.5)*(14.7/				
	7/15.025)=	15.025)=				
	425	9 66				
13	(L11*G5^2*(A	(L11*H5^2*(A1				1
	13)^.5)*(14.	3)^.5)*(14.7/				
	7/15.025) =	15.025) =				
	460	1 043				
14	400	1,045				
14	(LII***********************************	(LII-II) 2. (AI				
	$(14) \cdot 5)^{(14)}$	4) •5)*(14•//				
	//15.025)=	15.025)=				
	491	1,115				
15	(L11*G5^2*(A	(L11*H5^2*(A1				
1	15)^.5)*(14.	5)^.5)*(14.7/				
	7/15.025)=	15.025)=				
	521	1,183				
16	(L11*G5^2*(A	(L11*H5^2*(A1				
	16)^.5)*(14.	6)^.5)*(14.7/				
1	7/15.025)=	15.025)=				
1	549	1 247			1	
17	(111±0502±(*	1 + 3 - 7 /	l	I	l	
1'	11710 E14/1/	7 x 2 x 1 x 7 x 1 x 7 x 1 x 1 x 1 x 1 x 1 x 1				
	1/1 .5)*(14.	11 • 5)*(14•//		ļ		
	//15.025)=	15.025)=				
	576	1,307	l		l	

	G	Н	I	J	ĸ	L
18	(L11*G5^2*(A	(L11*H5^2*(A1				
	18)^.5)*(14.	8)^.5)*(14.7/				
	7/15.025)=	15.025)=				
	602	1,366				
19	(L11*G5^2*(A	(L11*H5^2*(A1				
	19)^.5)*(14.	9)^.5)*(14.7/				
	7/15.025)=	15.025)=				
	626	1.421				
20	(L11*G5^2*(A	(L11*H5^2*(A2		· · · · · · · · · · · · · · · · · · ·		
	20)^.5)*(14.	0)^.5)*(14.7/				
	7/15.025)=	15.025)=				
	650	1,475				
21	(L11*G5^2*(A	(L11*H5^2*(A2				
	21)^.5)*(14.	1)^.5)*(14.7/				
	7/15.025) =	15.025)=			1	
	673	1.527				
22	(111*G5*2*(A	(1.11*H5*2*(A2				
	(222 - 5) = (12)	$(2)^{,5} \times (14.7)$				
	7/15.025) =	15.025) =				
	695	1.577				
23	(L11*G5*2*(A	(L11*H5^2*(A2				
	23)^.5)*(14.	3)^.5)*(14.7/				
	7/15.025) =	15.025)=				
	716	1.625				
24	(L11*G5*2*(A	(L11*H5^2*(A2	-			
	24)^.5)*(14.	4)^.5)*(14.7/				
	7/15.025)=	15.025)=				
	737	1.672				
25	(L11*G5^2*(A	(L11*H5^2*(A2				
	25)^.5)*(14.	5)^.5)*(14.7/				
	7/15.025)=	15.025)=				
	757	1,718			:	
26	(L11*G5^2*(A	(L11*H5^2*(A2				
	26)^.5)*(14.	6)^.5)*(14.7/				
	7/15.025)=	15.025)=				
	777	1,763				
27	(L11*G5^2*(A	(L11*H5^2*(A2			·	
	27)^.5)*(14.	7)^.5)*(14.7/				
	7/15.025)=	15.025)=				
	796	1,806				
28	(L11*G5^2*(A	(L11*H5^2*(A2				
	28)^.5)*(14.	8)^.5)*(14.7/				
	7/15.025)=	15.025)=				
	815	1,849				
29	(L11*G5^2*(A	(L11*H5^2*(A2				
	29)^.5)*(14.	9)^.5)*(14.7/				
	7/15.025)=	15.025)=				
	833	1,891				
30	(L11*G5^2*(A	(L11*H5^2*(A3				
	30)^.5)*(14.	0)^.5)*(14.7/				
	7/15.025)=	15.025)=				
	851	1,931				
31	(L11*G5^2*(A	(L11*H5^2*(A3				
	31)^.5)*(14.	1)^.5)*(14.7/				
	7/15.025)=	15.025)=				
	869	1,971				

			т	7	v	1 T I
20	G		1	J	N	LL
32	(LII*G) Z*(A	(LII*H5*2*(A3				
	$32)^{-}.5)*(14.$	2)~.5)*(14.7/				
	//15.025)=	15.025)=				
	886	2,010				
33	(L11*G5 ^ 2*(A	(L11*H5^2*(A3				
	33)^.5)*(14.	3)^.5)*(14.7/				
	7/15.025)=	15.025)=				
	903	2,048				
34	(L11*G5 ^ 2*(A	(L11*H5^2*(A3				
	34)^.5)*(14.	4)^.5)*(14.7/				
	7/15.025)=	15.025)=				
	919	2,086				
35	(L11*G5^2*(A	(L11*H5^2*(A3				
	35)^.5)*(14.	5)^.5)*(14.7/				
	7/15.025)=	15.025)=				
	935	2,123				
36	(L11*G5^2*(A	(ll1*H5^2*(A3				
	36)^.5)*(14.	6)^.5)*(14.7/				
	7/15.025)=	15.025)=				
	951	2,159				
37	(L11*G5^2*(A	(L11*H5^2*(A3				
	37)^.5)*(14.	7)^.5)*(14.7/				
	7/15.025)=	15.025)=				
	967	2,195				
38	(L11*G5~2*(A	(L11*H5^2*(A3				
	38)^.5)*(14.	8)^.5)*(14.7/				
	7/15.025)=	15.025)=				
	983	2,230		Ļ		
39	(L11*G5*2*(A	(L11*H5^2*(A3	i	Ì		
	39)~.5)*(14.	9)^.5)*(14.7/				
	//15.025)=	15.025)=				
	998	2,265				
40	(L11*G5~2*(A	(LI1*H5~2*(A4				
	$(40)^{-1} \cdot 5)^{*}(14 \cdot 1)^{-1}$	(14.77)				
	//15.025)=	15.025)=				
41	1,015	2,277				
41	$(L11^{-0})^{-2}(R)$	$(L11^{-11}) 2^{-1}(A4)$				
	7/15.025	15 025 =				
	1 028	2 332				
42	(1)1*C5^2*(A	(111+H5^2*(A4		l	l	
	$(211 \ 0)^{2} (14)$	(211 13) 2 (14)				
	7/15.025) =	15.025) =				
	1.042	2,365				
43	(L11*G5^2*(A	(L11*H5^2*(A4				
	43)^.5)*(14.	3)^.5)*(14.7/				
	7/15.025)=	15.025)=				
	1,057	2,398				
44	(L11*G5^2*(A	(L11*H5^2*(A4			L,	
	44)^.5)*(14.	4)^.5)*(14.7/				
	7/15.025)=	15.025)=				
	1,071	2,430				
45	(L11*G5^2*(A	(L11*H5^2*(A4	<u></u>			
	45)^.5)*(14.	5)^.5)*(14.7/				
	7/15.025)=	15.025)=				
	1,085	2,462				:

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		u u		7	1/	
,	$\frac{6}{(111 \pm c5^{2}) \pm (A)}$	n	1	J	<u>K</u>	L
40	$(L11^{G}) 2^{(A)}$	(LII*nJ 2*(A4				
	$40) \cdot 5)^{(14)}$	(15, 0.25) -				
	1 000	2 /03				
1.7	1,077	2,475 (1)1+15^0+(A/				
47	(LII*GJ 2*(A	(LII*nJ 2*(A4				
	$\frac{47}{15}$ $\frac{37}{15}$	(14.7)				
	1 112	2 524				
4.8	1,112	2,J24				
40	(LII*G) 2*(A	8)^ 5)*(1/ 7/				
	7/15 025) -	15 025) =				
	1 126	2 555				
60	1,120	2,JJJ (111±45^2*(A4				
4 9	(LI1*G) 2*(A	$(111 + 1)^{2} (14)^{4}$				
	$(43) (3)^{(14)}$	(14.7)				
	1 139	2 585				
50	(111±c5 ² 2*(A	(111*45*2*(45				
1	50)^.5)*(14	$(0)^{,5} \times (14.7)$				
ł	$7/15_025) =$	15.025)=				
	1,152	2.615				
51	(L11*G5^2*(A	(1.11*H5^2*(A5				
	$(211 0)^{-1}$	$(212, 12)^{-1}$				
	7/15.025) =	15.025)=				
	1,165	2,644				
52	(L11*G5*2*(A	(L11*H5 ² *(A5				
	52)^.5)*(14.	2)^.5)*(14.7/				
	7/15.025)=	15.025)=				
	1,178	2,674				
53	(L11*G5^2*(A	(L11*H5^2*(A5	·····			
	53)^.5)*(14.	3)^.5)*(14.7/				
	7/15.025)=	15.025)=				
	1,191	2,703				
54	(L11*G5^2*(A	(L]1*H5^2*(A5				
	54)^.5)*(14.	4)^.5)*(14.7/			•	
	7/15.025)=	15.025)=				
	1,203	2,731				
55	(L11*G5 ² *(A	(L11*H5^2*(A5				
	55)^.5)*(14.	5)^.5)*(14.7/				
	7/15.025)=	15.025)=				
	1,216	2,759				
56	(L11*G5*2*(A	(L11*H5 ² *(A5				
	56)~.5)*(14.	6)~.5)*(14.7/				
	//15.025)=	15.025)=				
	1,228	2,/8/				
57	(LII*G) 2*(A	(LIIAH) ZA(A)				
	5/)*.5)*(14.	/) •5)*(14•//				
	//15.025)=	15.025) =				
50	1,240	2,010				
, o	(LII "GO 2"(A	(LII "H) 2"(A)				
	JOJ +J/*(14+	01 .5)*(14.//				
	1 252	2 9 9/2				
50	<u> </u>	2,04J	l	[_]		
,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	59)~ 5)*/1/	(111 - 1) 2"(A)				
	$7/15_025) =$	15.025)=				
1	1 265	2 870				
L	1,205	-,070	I	I	L	1

	G	u	т	1	v	T I
60	(1)1+(50)+(4		1	J	~	L
60	$(LII^G) Z^A(A)$	(LIIAH) 2*(A0				
	(14.	(14.7)				
	//15.025)=	15.025)=				
	1,276	2,897				
61	(L11*G5 ^ 2*(A	(L11*H5 ^ 2*(A6				
	61)^.5)*(14.	1)^.5)*(14.7/				
	7/15.025)=	15.025)=				
	1,288	2,923				
62	(L11*G5^2*(A	(L11*H5 ² *(A6				
	62)^.5)*(14.	2)^.5)*(14.7/				
	7/15.025)=	15.025)=				
	1,300	2,950				
63	(L11*G5 ^ 2*(A	(L11*H5^2*(A6				
	63)^.5)*(14.	3)^.5)*(14.7/				
	7/15.025)=	15.025)=				
	1,311	2,976				
64	(L11*G5^2*(A	(L11*H5^2*(A6				
	64)^.5)*(14.	4)^.5)*(14.7/				
	7/15.025)=	15.025)=				
	1,323	3,002				
65	(L11*G5^2*(A	(L11*H5^2*(A6				
	65)^.5)*(14.	5)^.5)*(14.7/				
	7/15.025)=	15.025)=				
	1,334	3,028			· · · · · · · · · · · · · · · · · · ·	
66	(L11*G5 ^ 2*(A	(L11*H5^2*(A6				
	66)^.5)*(14.	6)^.5)*(14.7/				
	7/15.025)=	15.025)=				
	1,345	3,053				
67	(L11*G5^2*(A	(L11*H5^2*(A6				
	67)^.5)*(14.	7)^.5)*(14.7/				
	7/15.025)=	15.025)=				
	1,357	3,079				
68	(L11*G5*2*(A	(L11*H5^2*(A6				
	68)~.5)*(14.	8)^.5)*(14.7/				
	7/15.025)=	15.025)=				
	1,368	3,104				
69	(L11*G5*2*(A	(L11*H5*2*(A6				
	69)~.5)*(14.	9)~.5)*(14.//				
	//15.025)=	15.025)=				
70	1,379	3,129				
10	(LII*G5*2*(A	(LII*H5~2*(A7				
	$70)^{-5}$ *(14.	(14.7)				
	1 200	15.025) =				
71	1,390	3,134				
11	$(L11^{+}G) 2^{+}(A)$	$(L11^{-}R) 2^{-}(A)$				
	7/15 025	$1) \cdot 3)^{(14 \cdot 7)}$				
	1 400	13.023 = 2.179				
72	1,400	J,1/0				l
12	72) ~ 5)+(1/	2) ~ 5) +(1/ 7/				
	7/15 005	$ 2 \cdot 2/(14 \cdot 1)$				
	1/15.025)=	13.0257=				
72	1,411	3,202				<u> </u>
1'3	1 LIIAGD 2*(A	2) ~ 5) 4/1/ 7/				
	7/15 0251-	15 0251-				
	1 / 20					
L	1,422	5,227				L

1	G	Н	I	J	K	L
74	(111*G5*2*(A	(L11*H5*2*(A7		· · · · · · · · · · · · · · · · · · ·		
	74)^.5)*(14.	$(222)^{(12)} = (14)^{(12)}$				
	7/15.025) =	15.025)=				
	1 / 32	3 251				
75	1,452	(111+45^2*(A7				
(') 	(EII.G) 2. (R	(11101) 20(87)				
	7/15 025) -	15 025) -				
	1 443	3 274				
76	1,445	J,2/4				
10	(LII~G) 2~(A	$(LII^nJ 2^n(R))$				
	70) •3)*(14•	(0) (14.77)				
	//15.025)=	15.025 =				
	1,455	3,290				
//	(LIIAG) 24(A	(LIIAH) 24(A/				
	7/)~•>)*(14•	15 005				
	1/15.025)=	15.0257=				
70	1,404	3,322		 		
/0	(LII~GJ 2~(A	(LIIAN) 2~(A/				
	7/15 025)-	15 025)-				
	1 474	2 2/5				
70	1,4/4			······································		
/9	$(L11^{*}G) 2^{*}(A)$	$(L11^n) 2^n(A)$				
	$797 + 37^{14}$	9) • 5)^(14•//				
	1 494	15.025)=				
00	1,404	3,300 (111+u5^2+(AP		· · · · · · · · · · · · · · · · · · ·		
00	$(LII^G) 2^{(A)}$	$(L11^n) 2^n (A0)$:		
	7/15 025)	15 025)-				
	1 404	2 201		;		
01	1,474	J,J71				
01	(211.0) 2.0(A)	$(1)^{5}.5)*(14.7)$				
	7/15 025) =	15.025 =				
	1 504	3 414				
82	(111*65*2*(A	(111*H5^2*(A8	· · · · · · · · · · · · · · · · · · ·			
	82)^.5)*(14.	$(2)^{-}.5)*(14.7)$				
	7/15.025 =	15.025 =				
	1 514	3 437				
83	(111*65*2*()	(111*15*2*(48				
	$(311, 0) \neq (14, 0)$	(211, 1.9, 2, (10)) 3)^.5)*(14.7/				
	7/15.025) =	15.025)=				
	1,524	3,459				
84	(L11*G5^2*(A	(L11*H5^2*(A8			· · · · · · · · · · · · · · · · · · ·	
	84)^.5)*(14.	4)^.5)*(14.7/				
	7/15.025)=	15.025)=				
	1,534	3,481				
85	(L11*G5^2*(A	(L11*H5^2*(A8	····			
	85)^.5)*(14.	5)^.5)*(14.7/				
	7/15.025)=	15.025)=				
	1,544	3,504				
86	(L11*G5^2*(A	(L11*H5^2*(A8				
	86)^.5)*(14.	6)^.5)*(14.7/				
	7/15.025)=	15.025)=				
	1,554	3,526				
87	(L11*G5^2*(A	(L11*H5^2*(A8				
	87)^.5)*(14.	7)^.5)*(14.7/				
	7/15.025)=	15.025)=				
	1,563	3,548				

1	~	17		<u>і </u>	1/	·
	6	Н	<u> </u>	J	K	L
88	(L11*G5~2*(A	(L11*H5~2*(A8				
	88)^.5)*(14.	8)^.5)*(14.7/				
	7/15.025)=	15.025)=				
	1,573	3,570				
89	(L11*G5^2*(A	(L11*H5^2*(A8				
	89)^.5)*(14.	9)^.5)*(14.7/				
	7/15.025)=	15.025)=				
	1,582	3,591				
90	(L11*G5^2*(A	(L11*H5^2*(A9				
	90)^.5)*(14.	0)^.5)*(14.7/				
	7/15.025)=	15.025)=				
	1,592	3,613				
91	(L11*G5^2*(A	(1.11*H5^2*(A9)				
	$(212 \ 0)^{-} (14)$	$(212 h)^{2} (14 7)$				
	7/15 025) =	15 025) =				
	1 601	3 634				
02	(111+05-2+(A)	J,034			[J
92	(L11*G) 2*(A)	$(LII^{n}I) 2^{n}(A)$				
	7/15 025) =	$27 \cdot 37^{(14)}$				
	1 611	3 656				
03	(1)1*05*2*(A	(111+15^2+(AQ		l		
,,,	(111.0) 2.0(R)	$(L11^{-11}) 2^{-1}(R)$				
	7/15 025) -	$37 \cdot 37^{(14)}$				
	1 620	2 6 7 7				
0/	1,020	J,077				
74	(LII*G) 2*(A	$(LII^n) 2^n(A)$				
	$94) \cdot 5)^{(14)}$	(14.7)				
	1 620	(10.025) =				
0.5	1,029	3,090		l		
50	$(L11^{G}) 2^{A}(A)$	$(L11^n) 2^n(A)$				
	7/15 025)-	$37 \cdot 37^{(14+7)}$				
	1 639	3,710				
96	1,035	J,/17	· · · · ·	I		
50	(L11.05) 2.0(R)	$(L11^{-11}) 2^{-1}(R)$				
	7/15 025	(14.7)				
	1 6/0	3 740				
07	1,040	J,740				
17/	$(L11^{+}G)^{-}Z^{+}(A)$	(LII*H) 2*(A)				
	7/15 025	15 025				
	1 657	2 760				
0.8	1,007	(111+45-2+(AQ			l	
	(BI1*6) 2*(A	(1111) 2.(R)				
	7/15.025)=	(14.7)				
	1 666	3 781				
99	(111*65^2*(A	(111*H5*2*(A9				<u> </u>
1	$(211 + 0)^{-1} = (1)^{-1}$	(211 ll) 2 (R)				
	7/15 025) =	15 025) =				
	1 675	3 802				
100	(111*65^2*(A	(111 * H5 ^ 2 * (A)		l		
100	100) 2.5)*(14	(01100) 20(R)				
	(7/15, 025) =	(15, 025) =				
	1.684	3.822		l		
101	(L11*G5*2*(A	(L11*H5^2*(A1		<u> </u>		<u> </u>
	101)^.5)*(14	01)^.5)*(14.7				
	.7/15.025)=	/15.025)=				
	1.693	3.842				
1	1, -, -, -, -, -, -, -, -, -, -, -, -,		I	1	1	1

,

	G	Н	I	J	ĸ	L
102	(L11*G5^2*(A	(L11*H5^2*(A1				
	102)^.5)*(14	02)^.5)*(14.7				
	•7/15•025) =	/15.025)=				
	1,702	3,862				
103	(L11*G5^2*(A	(L11*H5^2*(A1				
	103)^.5)*(14	03)^.5)*(14.7				
	.7/15.025)=	/15.025)=				
	1,711	3,882				
104	(L11*G5^2*(A	(L11*H5^2*(A1				
	104)^.5)*(14	04)^.5)*(14.7				
	•7/15•025) =	/15.025)=				
	1,720	3,902				
105	(L11*G5^2*(A	(L11*H5^2*(A1				
	105)^.5)*(14	05)^.5)*(14.7				
	.7/15.025) =	/15.025)=				
	1,728	3,922				
106	(L11*G5^2*(A	(L11*H5^2*(A1				
	106)^.5)*(14	06)^.5)*(14.7				
	.7/15.025)=	/15.025)=				
	1,737	3,942				
107	(L11*G5^2*(A	(L11*H5^2*(A1				
	107)^.5)*(14	07)^.5)*(14.7				
	.7/15.025)=	/15.025)=				
	1,780	4,039				
108	(L11*G5 ^ 2*(A	(L11*H5 ² *(A1				
	108)^.5)*(14	08)^.5)*(14.7				
	.7/15.025)=	/15.025)=				
	1,822	4,134				
109	(L11*G5^2*(A	(L11*H5 ² *(A1				
	109)^.5)*(14	09)^.5)*(14.7				
	.7/15.025)=	/15.025)=				
	1,863	4,22/				
110	(LI1*G5*2*(A	(L11*H5~2*(A1				
	$110)^{5} (14)$	$(10)^{}5)*(14.7)$				
	•//15•025)=	/15.025)=				
	1,903	4,510				62 628/166-
111	$(L11^{-0})^{-2}(A)$	$(11)^{5} = 5 \times (16.7)$				420/144-
	.7/15.025) =	/15.025)=				•4333270
	1 942	4 407				
112	(1)1*G5*2*(A	(1.11*H5^2*(A1				62.428/(144*
	$(112)^{,5} \times (14)$	$(2)^{,5} \times (14.7)$				12)=
	.7/15.025)=	/15.025)=				.0361273
	1,980	4,495				
113	(L11*G5^2*(A	(L11*H5^2*(A1				
	113)^.5)*(14	13)^.5)*(14.7				
	.7/15.025)=	/15.025)=				
	2,018	4,580				
114	(L11*G5^2*(A	(L11*H5^2*(A1				
	114)^.5)*(14	14)^.5)*(14.7				
	.7/15.025)=	/15.025)=				
	2,055	4,664				
115	(L11*G5 ^ 2*(A	(L11*H5^2*(A1				
	115)^.5)*(14	15)^.5)*(14.7				
	•7/15.025)=	/15.025)=				
	2,092	4,747				

	<u> </u>	U I		т	v	
	G	n	1	J	N	L
110	(L11*G5~2*(A	(L11*H5~2*(A1				
	116)^.5)*(14	16)^.5)*(14.7				
	.7/15.025)=	/15.025)=				
	2,127	4,828				
117	(L11*G5^2*(A	(L11*H5^2*(A1				
	117)^.5)*(14	17)^.5)*(14.7				
	.7/15.025)=	/15.025)=				
	2,163	4,908				
118	(L11*G5^2*(A	(L11*H5^2*(A1	· · · · · · · · · · · · · · · · · · ·			
	118)^.5)*(14	18)^.5)*(14.7				
	-7/15.025) =	(15, 025) =				
	2 107	/ 986				
110	4,177 (111+C5+2+(A	4,900				
119	$(LII^{GJ} 2^{A}(A))$	$(L11^n) 2^n (A1)$				
	$119)^{-}.5)*(14)$	19)*•5)*(14•7				
	•//15•025)=	/15.025)=				
	2,231	5,064				
120	(L11*G5^2*(A	(L11*H5^2*(A1				
	120)^.5)*(14	20)^.5)*(14.7				
	.7/15.025)=	/15.025)=		i		
	2,265	5,140				
121	(L11*G5^2*(A	(L11*H5^2*(A1				
	121)^.5)*(14	21)^.5)*(14.7			-	
	.7/15.025)=	/15.025)=				
	2,298	5,215	•			
122	(L11*G5^2*(A	(L11*H5^2*(A1	· · · · · · · · · · · · · · · · · · ·		<u> </u>	, <u>.</u>
	122)^.5)*(14	22)^.5)*(14.7				
	.7/15.025) =	/15.025)=				
	2.330	5,289				
123	(111*G5*2*(A	(1.11*H5^2*(A1		<u> </u>		
	$(212 \circ 5) = (11)$	(312, 13) = (112)				
	7/15 025)-	(15, 0.25) =				
	2 363	5 262				-
1.26	2,303	J, 302				
124	(LII*G5 2*(A	$(LIIAH) Z^{(AI)}$				
	$124)^{-1} \cdot 5)^{*}(14)$	$(24)^{-1} \cdot 5)^{*}(14 \cdot 7)$				
	•//15•025)=	/15.025)=				
	2,394	5,434		<u> </u>		
125	(L11*G5*2*(A	(L11*H5^2*(A1				
	125)^.5)*(14	25)^.5)*(14.7				
	.7/15.025)=	/15.025)=				
	2,426	5,505				
126	(L11*G5*2*(A	(L11*H5 ² *(A1				
	126)^.5)*(14	26)^.5)*(14.7				
	.7/15.025)=	/15.025)=				
	2,457	5,575				
127	(L11*G5^2*(A	(L11*H5^2*(A1				
	127)^.5)*(14	27)^.5)*(14.7				
	.7/15.025)=	/15.025)=				
	2,487	5,644				
128	(L11*G5^2*(A	(L11*H5^2*(A1				
	128)^.5)*(14	28)^.5)*(14.7				
1	.7/15.025)=	/15.025)=				
	2 517	5 713				
120	1 <u></u> (1)1±05^0±(*	(1);;;; (1);;;;;		l	!	<u> </u>
127	120) 5)+(1/	20) ~ 5) ±(1/ 7				
1	7/15 005	1277 • JJ~(14•/				
1	(//13·025)=	[/15·025]=				
	2,547	5,780]		<u> </u>

	G	н	T	T	r v	T
1100	(111+0500+()	11	*	5	K	<u>ل</u>
130	(LII*65 2*(A	$(LII^{H}) 2^{A}(AI)$				
	130)~.5)*(14	30)~•5)*(14•/				
	•7/15•025)=	/15.025)=				
l	2,576	5,847				
131	(L11*G5^2*(A	(L11*H5^2*(A1				
	131)^.5)*(14	31)^.5)*(14.7				
	.7/15.025)=	/15.025)=				
1	2,606	5,913				
132	(L11*G5^2*(A	(L11*H5^2*(A1				
	132)^.5)*(14	32)^.5)*(14.7				
	.7/15.025)=	/15.025)=				
	2.634	5,978				
133	(L11*G5*2*(A	(L11*H5^2*(A1		· · ·		
	$(212 \circ 5) = (14)$	(212, 5) = (14, 7)				
	7/15 025)-	(15 025)-				
	•//IJ•025)-	6 0/3				
	2,005	0,043				
134	(L11*G5"2*(A					
	$(134)^{(1)} \cdot 5) \times (14)$	$(14.7)^{-1}$				
	•//15•025)=	/15.025)=				
	2,691	6,107				
135	(LII*G5~2*(A	(L11*H5~2*(A1				
	135)^.5)*(14	35)^.5)*(14.7				
	•7/15•025)=	/15.025)=				
	2,719	6,170				
136	(L11*G5*2*(A	(L11*H5^2*(A1				
	136)^.5)*(14	36)^.5)*(14.7		-		
'	.7/15.025)=	/15.025)=				
	2,746	6,233				
137	(L11*G5^2*(A	(L11*H5^2*(A1	1			
	137)^.5)*(14	37)^.5)*(14.7				
	•7/15•025)=	/15.025)=				
	2,774	6,295	•			
138	(L11*G5*2*(A	(L11*H5~2*(A1				
	138)~.5)*(14	38)~•5)*(14•/				
	•//15•025)=	/15.025)=				
	2,801	6,356				
139	(L11*G5~2*(A	(L11*H5~2*(A1				
	139)~.5)*(14	39)~•5)*(14•/				
	•//15•025)=	/15.025)=	-			
	2,828	6,41/				
140	(L11*G5~2*(A	(LII*H5~2*(AI				
	$(140)^{-5} \times (14)^{-140}$	40)~.5)*(14.7				
	•//15•025)=	/15.025)=				
	2,854	0,4//				
141	$(L11^{+}G) 2^{+}(A)$	$(L11^{-1}) 2^{-1}(A1)$				
	$(141) \cdot 5)^{(14)}$	(15, 025)				
	•//15•025/=	/10.020)=				
1/0	2,001	0,00/				L
142	(LIIAG) 24(A	$(LII^nJ 2^n(AI)$				
	142) •D)*(14	447 •37*(14•/				
	•//10•025)=	/13+025]=				
1/2	2,907	0,590				
143	(LII*G)~2*(A	(L11*H)~2*(A)				
	1437 •37*(14 7/15 005)-	437 +37*(14+/ /15 035)-				
	•//13•023)=	/1J•UZJ]= 6 6 6 6				
	2,932	دده,ه				

	G	н	I	J	ĸ	L
144	(1.11*G5^2*(A	(T.11*H5^2*(A1)				
	(222 - 5) = (14)	$(41)^{5} (16)^{7}$				
	7/15 025) =	(15, 025) =				
	2 050	(7)				
1/5	2,900	0,/13				
145	(LII*G5 2*(A	(L11*H) 2*(AI				
	$(145)^{-1} \cdot 5)^{*} (14)$	45)**•5)*(14•7			-	
	•//15•025)=	/15.025)=				
116	2,983	6,//1	:	<u></u>		
146	(L11*G5*2*(A	(LII*H) ² *(AI				
	$(146)^{-1} \cdot 5) * (14)$	46)				
	•//15•025)=	/15.025)=				
	3,009	6,828			······	
14/	(LII*G5~2*(A	(LII*H5~2*(A1				
	147)^.5)*(14	47)^.5)*(14.7				
	•7/15•025)=	/15.025)=				
ļ	3,034	6,884		· · · · ·		· · · · · · · · · · · · · · · · · · ·
148	(L11*G5*2*(A	(L11*H5^2*(A1				
	148)^.5)*(14	48)^.5)*(14.7				
	.7/15.025)=	/15.025)=				
	3,058	6,941				<u> </u>
149	(L11*G5*2*(A	(L11*H5^2*(A1				
	149)^.5)*(14	49)^.5)*(14.7				
	•7/15•025)=	/15.025)=				
	3,083	6,996				
150	(L11*G5^2*(A	(L11*H5^2*(A1				
	150)^.5)*(14	50)^.5)*(14.7				
	.7/15.025)=	/15.025)=				
	3,107	7,052				
151	(L11*G5^2*(A	(L11*H5^2*(A1				
1	151)^.5)*(14	51)^.5)*(14.7				
	.7/15.025)=	/15.025)=				
	3,131	7,107				<u> </u>
152	(L11*G5^2*(A	(L11*H5^2*(A1				
	152)^.5)*(14	52)^.5)*(14.7				
	•7/15.025)=	/15.025)=				
	3,155	7,161				
153	(L11*G5^2*(A	(L11*H5^2*(A1				
	153)^.5)*(14	53)^.5)*(14.7				
	.7/15.025)=	/15.025)=			1	
	3,179	7,215				
154	(L11*G5^2*(A	(L11*H5^2*(A1				
	154)^.5)*(14	54)^.5)*(14.7				
	.7/15.025)=	/15.025)=				
ļ	3,203	7,269			ļ	
155	(L11*G5^2*(A	(L11*H5^2*(A1				
	155)^.5)*(14	55)^.5)*(14.7				
	•7/15.025)=	/15.025)=				
	3,226	7,322	l 	ļ		<u> </u>
156	(L11*G5*2*(A	(L11*H5^2*(A1				
	156)^.5)*(14	56)^.5)*(14.7				
1	•7/15.025)=	/15.025)=				
	3,250	7,375				<u> </u>
157	(L11*G5*2*(A	(L11*H5^2*(A1				
1	157)^.5)*(14	57)^.5)*(14.7				
	.7/15.025)=	/15.025)=				
	3,273	7,427			<u> </u>	<u> </u>

		u	т	т	v	
1.50	G		1	J	K	L
001	(LIIAG) 24(A	(LIIAH) 24(AI				
	$130 - 3)^{(14)}$	(14.7)				
	•7715•0257-	7 4 7 0				
150	3,270	/ ,4/3				
1.59	(LT100) 20(A	(21100) 20(R1) 59) (14.7)				
	7/15.025) =	(15, 025) =				
	3,319	7.531				
160	(L11*G5*2*(A	(L11*H5^2*(A1				
	160)^.5)*(14	60)^.5)*(14.7				
	.7/15.025)=	/15.025)=				
	3.341	7,583				
161	(L11*G5^2*(A	(L11*H5^2*(A1				·
	161)^.5)*(14	61)^.5)*(14.7				
	.7/15.025)=	/15.025)=				
	3,364	7,634				
162	(L11*G5^2*(A	(L11*H5^2*(A1				
	162)^.5)*(14	62)^.5)*(14.7				
	•7/15•025)=	/15.025)=				
	3,386	7,684			·····	
163	(L11*G5^2*(A	(L11*H5^2*(A1			i	
	163)^.5)*(14	63)^.5)*(14.7				
	•7/15•025)=	/15.025)=				
	3,408	7,735	· · · · · · · · · · · · · · · · · · ·			
164	(L11*G5*2*(A	(L11*H5~2*(A1				
	164)^.5)*(14	64)^.5)*(14.7				
	•//15•025)=	/15.025)=				
16	3,430	/,/80				
105	(LII~GJ 2~(A	$(L11^{n}) 2^{n}(A1)$				
	.7/15.025) =	(15.025) =				
	3-452	7.835				
166	(L11*G5^2*(A	(L11*H5^2*(A1				
	166)^.5)*(14	66)^.5)*(14.7				
	.7/15.025)=	/15.025)=				
	3,474	7,884				
167	(L11*G5^2*(B	(L11*H5^2*(B1				
	167*13.59)^.	67*13.59)^.5)				
	5)*(14.7/15.	*(14.7/15.025				
	025)=)=				
<u> </u>	3,507	7,960			, 	
168	(L11*G5^2*(B	(L11*H5^2*(B1				
	168*13.59)~.	68*13.59)^.5)				
)*(14•//15• 025)-	*(14.//15.025				
	(22) = 2 + 22)= ♀ 221				
160	J,022	0,221 (111+H5^2*(B)				
105	169*13.59) ^ .	$(1113,59)^{,5}$				
	5)*(14.7/15.	*(14.7/15.025				
	025)=)=				
	3,734	8,474				
170	(L11*G5^2*(B	(L11*H5^2*(B1		····	· · · · · · · · · · · · · · · · · · ·	
	170*13.59)^.	70*13.59)^.5)				
	5)*(14.7/15.	*(14.7/15.025				
	025)=)=				
	3,842	8,719				

1						
	G	Н	<u>I</u>	J	K	L
171	(L11*G5 ^ 2*(B	(L11*H5^2*(B1				
	171*13.59)^.	71*13.59)^.5)				
	5)*(14.7/15.	*(14.7/15.025				
	025)=)=				
	3,947	8,958				
172	(L11*G5^2*(B	(L11*H5^2*(B1	· · · · · · · · · · · · · · · · · · ·			
	172*13.59)^.	72*13.59)^.5)				
	5) * (14.7/15.	*(14.7/15.025				
	(25) =)=				
	0237- / 050	0 101				
172	4,000	7,171	· · · · · · · · · · · · · · · · · · ·			
1/3	(LII*G) 2*(B					
	1/3*13.39) •	/3*13.39) .3)				
	5)*(14.//15.	*(14.//15.025				
	025)=)=				
	4,150	9,418				
174	(L11*G5^2*(B	(L11*H5^2*(B1				
	174*13.59)^.	74*13.59)^.5)				
	5)*(14.7/15.	*(14.7/15.025				
	025)=)=				
	4,248	9,639				
175	(L11*G5^2*(B	(L11*H5^2*(B1				
	175*13.59)^.	75*13.59)^.5)				
	5)*(14.7/15.	*(14.7/15.025				
1 :	025)=)=		·		
	4,343	9,856				
176	(L11*G5^2*(B	(L11*H5^2*(B1		1		
	176*13.59)^.	76*13.59)^.5)				
	5)*(14.7/15.	*(14.7/15.025				
1	025)=)=				
	4,436	10,068				
177	(L11*G5*2*(B	(L11*H5^2*(B1				
	177*13.59)^.	77*13.59)^.5)				
	5)*(14.7/15.	*(14.7/15.025				
	025)=)=				
	4,528	10,276				
178	(L11*G5^2*(B	(L11*H5^2*(B1				
	178*13.59)^.	78*13.59)^.5)				
	5)*(14.7/15.	*(14.7/15.025				
	025)=)=				
	4.618	10,479				
179	(L11*G5^2*(B	(L11*H5^2*(B1	······································			
	179*13.59)^.	79*13.59)^.5)				
	5)*(14.7/15.	*(14.7/15.025				
	025)=)=				
	4.706	10,679				
180	(L11*G5^2*(B	(L11*H5^2*(B1	· · · · · · · · · · · · · · · · · · ·	<u> </u>		
	180*13.59)^.	80*13,59)^.5)				
	5)*(14.7/15.)	*(14.7/15.025				
	(0.25) =)=				
	1 792	10.875				
181	(T.11*C5*0*/P	(T11*H5*0*/¤1			l	· · · · · · · · · · · · · · · · · · ·
1.01	181*13 5010	81*13 501* 51				
1	5)*(1/ 7/15	*(1/ 7/15 0)				
	025)-					
	1. 277	11 067				
1	4,0//	1 11,007	1	1	1	1

	C	U	т	т	v	т I
	G	n		J	K	L
182	(LII*G5~2*(B	(LII*H5~2*(BI				
	182*13.59)^.	82*13.59)^.5)				
l	5)*(14.7/15.	*(14.7/15.025				
	025)=)=				
	4,960	11,256				
183	(L11*G5^2*(B	(L11*H5^2*(B1				
	183*13.59)^.	83*13,59)^,5)				
	5)*(14.7/15.	*(14.7/15.025				
	025)-)-				
	5 1(2))-				
1.0/	5,105	11,/10				
184	(LI1*G5*2*(B	(LI1*H)~2*(BI				
	184*13.59)~.	84*13.59)~.5)				
	5)*(14.7/15.	*(14.7/15.025				
[025)=)=				
	5,357	12,158				
185	(L11*G5^2*(B	(L11*H5^2*(B1				
	185*13.59)^.	85*13.59)^.5)				
	5)*(14.7/15.	*(14.7/15.025				
	025)=)=				
	5,546	12,585				
186	(L11*G5^2*(B	(L11*H5^2*(B1				
	186*13.59)^.	86*13.59)^.5)				
	5)*(14.7/15.	*(14.7/15.025				
ł	025)=)=				
	5 7 27	12 998				
197	(111*C5^2*(P	(111+H5^2*(B)		<u> </u>	<u></u>	
10/	(LII*0) 2*(B	(LIIAN) 2°(BI				
	$(10)^{(1)}(10, 0, 0, 0, 0, 0, 0, 0, 0, 0, 0, 0, 0, 0$	+(1/7)				
)^(14•//1J•	*(14•//1J•02J				
	(22) =)=				
100	5,904	13,390			<u> </u>	
188		(LIIAH) 24(BI				
	188*13.59)	88*13.39) .3)				
	5)*(14.//15.	*(14.//15.025				
	025)=)=				
	6,075	13,786				
189	(L11*G5^2*(B	(L11*H5~2*(B1				
	189*13.59)^.	89*13.59)*.5)				
	5)*(14.7/15.	*(14.7/15.025				
	025)=)=				
	6,241	14,164				-
190	(L11*G5~2*(B	(L11*H5~2*(BI				
	190*13.59)^.	90*13.59)^.5)				
	5)*(14.7/15.	*(14.7/15.025				
	025)=)=				
	6,403	14,532				
191	(L11*G5^2*(B	(L11*H5^2*(B1				
	191*13.59)^.	91*13.59)^.5)				
	5)*(14.7/15.	*(14.7/15.025				
	025)=)=				
	6,562	14,891				
192	(L11*G5^2*(B	(L11*H5^2*(B1				
	192*13.59)^.	92*13.59)^.5)				
	5)*(14.7/15.	*(14.7/15.025				
]	025)=)=		ļ		
	6.716	15,241				
1	1	·		a		· · · · · · · · · · · · · · · · · · ·

	C	ម	τ	т	ĸ	τ
102	(1)1+CEA0+(D	11 (111+115-00+(D1	<u>+</u>	5		Ľ
193	(LII*GJ 2*(B	$(DII^nJ 2^n(BI)$				
	193*13.39)	93*13·39) [•] ·3)				
	5)*(14.//15.	*(14•//15•025				
	025)=)=				
	6,867	15,584	·			
194	(L11*G5^2*(B	(L11*H5^2*(B1				
	194*13.59)^.	94*13.59)^.5)				
	5)*(14.7/15.	*(14.7/15.025				
	025)=)=				
	7,015	15,919				
195	(L11*G5^2*(B	(L11*H5^2*(B1				
	195*13.59)^.	95*13.59)^.5)				
	5)*(14.7/15.	*(14.7/15.025				
	025)=)=				
	7,159	16,247				
196	(L11*G5^2*(B	(L11*H5^2*(B1				
	196*13.59)^.	96*13.59)^.5)				
	5)*(14.7/15.	*(14.7/15.025		:		
	025)=)=				
	7.301	16,569				
197	(L11*G5^2*(B	(L11*H5^2*(B1				
	197*13.59)^	97*13,59)^,5)				
	5)*(14.7/15.	*(14.7/15.025				
	(140771))=	:			
	7 440	16 885				
198	(111*05*2*(P	(111±45^2±(P)				
190	102+13 50)^	(LII*II) 2*(BI				
	$170^{1}3.57$	+(1, 7, 15, 0.05)				
)/(14.//13.	^(14•//15•025				
)=				
100	/,J//	1/,190			l	
199	(LIIAGS 24(B	(LII n 2 2 (BI)				
	[199*13.39] .	99*13·39) ·3)				
	()^(14•//15•	^(14•//15•025)	2			
	025)=)=				
0.00	/,/11	17,499				1
200	(LI1*G5**2*(B	(L11*H5*2*(B2				
	200*13.59)*•	$00*13.59)^{5}$				
I	(14.7/15.	* (14•//15•025				
	U2D)=)=				
	7,843	17,798			<u>}</u>	
201	(LI1*G5*2*(B	(L11*H5~2*(B2				
	201*13.59)~.	01*13.59)^.5)				
	5)*(14.7/15.	*(14.7/15.025				
	025)=)=				
	7,972	18,092				
202	(L11*G5^2*(B	(L11*H5^2*(B2				
	202*13.59)^.	02*13.59)^.5)				
	5)*(14.7/15.	*(14.7/15.025				
	025)=)=				
	8,100	18,382]	
203	(L11*G5^2*(B	(L11*H5^2*(B2				
	203*13.59)^.	03*13.59)^.5)				
	5)*(14.7/15.	*(14.7/15.025				
	025)=)=				
	8,225	18,667				
			· · · · · · · · · · · · · · · · · · ·			

	G	Н	I	J	ĸ	I.
204	(L11*G5^2*(B	(L11*H5^2*(B2				
	204*13.59)^.	04*13,59)^.5)				
	(14.7/15)	*(14.7/15.025				
	(1,0,0,0) =)=				
	02J)- 8 3/0	18 9/7				
205	$(11) + (5^{2}) + (p)$	(111+15^2+(p2				
205	205*13 59)*	(E11°H) 2°(B2				
	5)*(1/ 7/15)	*(14 7/15 025				
	025)-)=				
	8 471	19 224				
206	(1.11*G5^2*(B	(L11*H5^2*(B2				
	206*13.59)^.	$()^{()} = ()^{()}$				
	5)*(14.7/15.	*(14.7/15.025				
	025)=)=				
	8,591	19,497				
207	(L11*G5^2*(B	(L11*H5^2*(B2				
	207*13.59)^.	07*13.59)^.5)				
	5)*(14.7/15.	*(14.7/15.025				
	025)=)=				
	8,710	19,766				
208	(L11*G5^2*(B	(L11*H5^2*(B2			· · · · · · · · · · · · · · · · · · ·	
	208*13.59)^.	08*13.59)^.5)		×		
	5)*(14.7/15.	*(14.7/15.025				
	025)=)=				
	8,827	20,031			:	
209	(L11*G5^2*(B	(L11*H5^2*(B2				
	209*13.59)^.	09*13.59)^.5)				
	5)*(14.7/15.	*(14.7/15.025				
	025)=)=				
	8,942	20,293				
210	(L11*G5^2*(B	(L11*H5^2*(B2				
	210*13.59)^.	10*13.59)^.5)				
	5)*(14.7/15.	*(14.7/15.025				
	025)=)=				
	9,056	20,551				
211	(L11*G5^2*(B	(L11*H5^2*(B2				
	211*13.59)^.	11*13.59)^.5)				
	5)*(14.7/15.	*(14.7/15.025				
	025)=)=		, 		
	9,168	20,807				
212	(L11*G5~2*(B	(L11*H5~2*(B2				
	212*13.59)*•	12*13.59)*.5)				
	5)*(14.//15.	*(14.//15.025				
	(025)=)=				
	9,279	21,059		l	<u> </u>	
213	(LII*G5*2*(B	(LII*H5°2*(B2				
	$(213^{13}, 39)$	+(1, 7/15, 0.25)				
	025)-)= ·(14+//13+023				
	9 280	21 308				
214	(L11*G5^2*(R	(L11*H5^2*(R2	<u> </u>		l	
	214*13.59)*	14*13.59)^.5)				
}	5)*(14.7/15	*(14.7/15-025				
	025)=)=				
	9.498	21.555				
1	1	1	L	L	L	L

	<u> </u>	11			ν	
0.1.5	G	Н	1	J	<u>л</u>	L
215	(L11*G5~2*(B	(L11*H5~2*(B2				
	215*13.59)^.	15*13.59)^.5)				
	5)*(14.7/15.	*(14.7/15.025				
	025)=)=				
	9,605	21,798				
216	(L11*G5^2*(B	(L11*H5^2*(B2				
	216*13.59)^.	16*13.59)^.5)				
	5)*(14.7/15.	*(14.7/15.025				
	025)=)=				
	9,711	22,039				
217	(L11*G5*2*(B	(L11*H5^2*(B2				
	217*13.59)^.	17*13.59)^.5)				
	5)*(14.7/15.	*(14,7/15,025				
	(25) =)=				
	9 816	, ,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,				
218	(111*C5^2*/P	(T11+45-2+(P2				
210	219+12 50)	(L11-11) 2-(B2				
	$210^{1} \cdot 13 \cdot 37$	10^{-1}				
	(14.7/1)	~(14•//1J•02J				
	025)=)=				
	9,920	22,513				
219	(L11*G5~2*(B	(L11*H5 ² *(B2				
	219*13.59)^.	19*13.59)^.5)				
	5)*(14.7/15.	*(14.7/15.025				
	025)=)=				
L	10,023	22,746				
220	(L11*G5^2*(B	(L11*H5^2*(B2				
ļ	220*13.59)^.	20*13.59)^.5)				
	5)*(14.7/15.	*(14.7/15.025				
	025)=)=				
	10,125	22,977				
221	(L11*G5^2*(B	(L11*H5^2*(B2				
	221*13.59)^.	21*13.59)^.5)				
	5)*(14.7/15.	*(14.7/15.025				
	025)=)=				
	10,225	23,206				
222	(L11*G5^2*(B	(L11*H5^2*(B2			· · · · · · · · · · · · · · · · · · ·	
	222*13.59)^.	22*13.59)^.5)				
	5)*(14.7/15.	*(14.7/15.025				
	025)=)=				
	10.325	23,432				
223	(L11*G5^2*(B	(L11*H5^2*(B2		l	· · · · ·	
	223*13.59)^.	23*13.59)^.5)				
	(14.7/15)	*(14.7/15.025				
	025)=)=				
	10 424	23 656				
224	(111+C5^2+(P	(111+45-2+(22		1		<u> </u>
224	(LII"GJ 2"(D	(LII*n) 2*(b2 24+12 50)* 5)				
	$(224^{1}3.39)$	24~13.39) .3)				
	025)-					
1		/-				
225	10,522	23,8/9	l	<u> </u>		<u> </u>
225		(LI1*H) 2*(B2				
	225*13.59)*•	25*13.59)*.5)	ł			
	5)*(14.7/15.	*(14.7/15.025				1
	025)=)=				
1	10,619	24,099				

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	C	н	т	Ţ	v	
	(T11+0540+(n	11	1		N	
226		(LIIAND 24(B2				
	226*13.59)~.	20*13.59)**.5)				
	5)*(14.7/15.	*(14.7/15.025				
	025)=)=				
	10,715	24,317				
227	(L11*G5^2*(B	(L11*H5^2*(B2				
	227*13.59)^.	27*13.59)^.5)				
	5)*(14.7/15.	*(14.7/15.025	:			
	025)=)=				
	10,810	24,533				
228	(L11*G5^2*(B	(L11*H5^2*(B2				
	228*13.59)^.	28*13.59)^.5)				
	5)*(14.7/15.	*(14.7/15.025				
	025)=)=				
	10,905	24,747	、			
229	(L11*G5^2*(B	(L11*H5*2*(B2				
	229*13.59)^.	29*13.59)^.5)			-	
	5)*(14.7/15.	*(14.7/15.025				
	025)=)=				
1	10,998	24,960				
230	(L11*G5^2*(B	(L11*H5^2*(B2				
	230*13.59)^.	30*13.59)^.5)				
	5)*(14.7/15.	*(14.7/15.025				
	025)=)=				
	11.091	25,170				
231	(1)1*65*2*(6	(1,1)*H5^2*(C2				
2.51	231*144*12/6	31*144*12/62				
	$2.428)^{-}.5)*($	$(428)^{-}, 5)*(14)$				
		7/15 025) =				
		25 (01			,	
	-	23,401				
222	(11)+(5^2+()	(11)+450+(0)		· · · · ·		
232	222+1//+12/6	(LII^n) 2*(02				
	2 / 22 / 144 - 12/0	(20) S S + (14				
	$2 \cdot 420 \cdot 5)^{(1)}$	$420) \cdot 000$				
	14•7/15•025)	7/13.023 = 26.024				
	=	20,234				
	11,560					
233		(L11*H) ² 2*(C2				
	233*144*12/6	55*144*12/62.				
	2.428)^.5)*(428)".5)*(14.				
	14.7/15.025)	7/15.025)=				
	=	27,041				
	11,915					
234	(L11*G5^2*(C	(L11*H5*2*(C2				
	234*144*12/6	34*144*12/62.				
	2.428)^.5)*(428)~.5)*(14.				
	14.7/15.025)	7/15.025)=				
	=	27,825				
L	12,261					
235	(L11*G5^2*(C	(L11*H5 ^ 2*(C2				
1	235*144*12/6	35*144*12/62.				
	2.428)^.5)*(428)^.5)*(14.				
	14.7/15.025)	7/15.025)=				
	=	28,587				
	12,597					

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	G	Н	I	J	ĸ	L
236	(L11*G5^2*(C	(L11*H5^2*(C2				
	236*144*12/6	36*144*12/62.				
	2.428)^.5)*(428)^.5)*(14.				
	14.7/15.025)	7/15.025)=				
	=	29,330				
	12,924	-				
237	(L11*G5^2*(C	(L11*H5^2*(C2				·······
	237*144*12/6	37*144*12/62.				
-	2.428)^.5)*(428)^.5)*(14.				
	14.7/15.025)	7/15.025)=				
	=	30,054				
	13,243					
238	(L11*G5^2*(C	(L11*H5^2*(C2	· · · · · · · · · · ·		· · · · · · · · · · · · · · · · · · ·	
	238*144*12/6	38*144*12/62.				
	2.428)^.5)*(428)^.5)*(14.				
	14.7/15.025)	7/15.025) =				
	=	30,762				
	13,555					
239	(L11*G5*2*(C	(L11*H5^2*(C2			· · · · · · · · · · · · · · · · · · ·	
	239*144*12/6	39*144*12/62.				
	2.428)^.5)*(428)^.5)*(14.				
	14.7/15.025)	7/15.025)=				
	=	31,453				
	13,860					
240	(L11*G5^2*(C	(L11*H5^2*(C2				
	240*144*12/6	40*144*12/62.				
	2.428)^.5)*(428)^.5)*(14.				
	14.7/15.025)	7/15.025)=			:	
	=	32.130			-	
	14,158					
241	(L11*G5^2*(C	(L11*H5^2*(C2				<u> </u>
	241*144*12/6	41*144*12/62.				
	2.428)^.5)*(428)^.5)*(14.				
	14.7/15.025)	7/15.025)=				
	=	32,792				
	14,450					
242	(L11*G5^2*(C	(L11*H5^2*(C2				
	242*144*12/6	42*144*12/62.				
	2.428)^.5)*(428)^.5)*(14.				
	14.7/15.025)	7/15.025)=				
	=	33,441				
	14,736					
243	(L11*G5^2*(C	(L11*H5^2*(C2				
	243*144*12/6	43*144*12/62.				
	2.428)^.5)*(428)^.5)*(14.	-			
	14.7/15.025)	7/15.025)=				
	=	34,079				
	15,016					
244	(L11*G5^2*(C	(L11*H5^2*(C2				
	244*144*12/6	44*144*12/62.				
	2.428)^.5)*(428)^.5)*(14.				
	14.7/15.025)	7/15.025)=				
	=	34,704				
	15,292					l

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	G	Н	I	J	K	L
245	(L11*G5^2*(C	(L11*H5 ² *(C2				
	245*144*12/6	45*144*12/62.				
	2.428)^.5)*(428)^.5)*(14.				
	14.7/15.025)	7/15.025) =				
	=	35,318				
	15,563	,				
246	(L11*G5^2*(C	(L11*H5^2*(C2	_			
	246*144*12/6	46*144*12/62.				
	2.428)^.5)*(428)^.5)*(14.				
	14.7/15.025)	7/15.025) =				
	=	35,922				
	15,829	,,				
247	(L11*G5^2*(C	(L11*H5^2*(C2				
	247*144*12/6	47*144*12/62.				
	2.428)^.5)*(428)^.5)*(14.				
	14.7/15.025)	7/15.025) =				
	=	36.516				
	16.090					
248	(L11*G5^2*(C	(L11*H5^2*(C2				
	248*144*12/6	48*144*12/62.				
	2.428)^.5)*(428)^.5)*(14.				
	14.7/15.025)	7/15.025)=				
1	=	37,100				
	16,348					
249	(L11*G5^2*(C	(L11*H5^2*(C2		· · · · · · · · · · · · · · · · · · ·		
	249*144*12/6	49*144*12/62.				
	2.428)^.5)*(428)^.5)*(14.				
	14.7/15.025)	7/15.025)=				
	=	37,675				
	16,601					
250	(L11*G5^2*(C	(L11*H5^2*(C2				
	250*144*12/6	50*144*12/62.				
	2.428)^.5)*(428)^.5)*(14.				
	14.7/15.025)	7/15.025)=				
	=	38,242				
	16,851					
251	(L11*G5^2*(C	(L11*H5^2*(C2				
	251*144*12/6	51*144*12/62.				
	2.428)^.5)*(428)^.5)*(14.				
	14.7/15.025)	7/15.025)=				
	=	38,800				
	17,097			·		
252	(L11*G5^2*(C	(L11*H5^2*(C2				
	252*144*12/6	52*144*12/62.				
	2.428)^.5)*(428)^.5)*(14.				
	14.7/15.025)	7/15.025)=				
	=	39,351				
L	17,339					
253	(L11*G5 ² *(C	(L11*H5 ² *(C2				
	253*144*12/6	53×144×12/62.				
	2.428)~.5)*(428)**•5)*(14•		:		
	14.//15.025)	//15.025)=				
	=	39,893				
	17,579					

	G	Н	I	J	ĸ	L
254	(L11*G5^2*(C	(L11*H5^2*(C2				
	254*144*12/6	54*144*12/62.				
	2.428)^.5)*(428)^.5)*(14.				
	14.7/15.025)	7/15.025)=				
	=	40,429				
	17,815					
255	(L11*G5^2*(C	(L11*H5^2*(C2				
	255*144*12/6	55*144*12/62.				
	2.428)^.5)*(428)^.5)*(14.				
	14.7/15.025)	7/15.025)=				
	=	40,957				
	18,048					

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1		
2	14.7/15.025= .9783693844	
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5	[]	
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