

CAMPBELL & BLACK, P.A.

LAWYERS

JACK M. CAMPBELL
BRUCE D. BLACK
MICHAEL B. CAMPBELL
WILLIAM F. CARR
BRADFORD C. BERGE
J. SCOTT HALL
PETER N. IVES
LOURDES A. MARTINEZ

JEFFERSON PLACE
SUITE 1 - 110 NORTH GUADALUPE
POST OFFICE BOX 2208
SANTA FE, NEW MEXICO 87501
TELEPHONE: (505) 988-4421
TELECOPIER: (505) 983-6043

August 30, 1985

HAND DELIVERED

Case 8712

R. L. Stamets, Director
Oil Conservation Division
New Mexico Department of
Energy & Minerals
State Land Office Building
Santa Fe, New Mexico 87503

RE: Application for Hardship Well Classification

Dear Mr. Stamets:

Enclosed is the application of Kimbell Oil Co. of Texas for Hardship Gas Well Classification for the Salazar 4-E Basin-Dakota Well located in Unit E, Section 34, Township 25 North, Range 6 West, in Rio Arriba County. We request that this matter be set for hearing at the next regularly scheduled examiner hearing.

Additionally, we are requesting emergency approval for the relief request on a temporary basis not to exceed ninety days. In this regard, a copy of this application is being forwarded to Frank Chavez in Aztec.

Thank you for your cooperation.

Very truly yours,


J. Scott Hall

JSH/ba
enclosure

cc w/encl: Kimbell Oil Co. of Texas
Attn: Jack Redding, Jr.
Victor Salazar
Frank Chavez, OCD, Aztec

RECEIVED

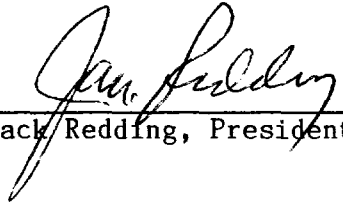
SEP 13 1985

OIL CON. DIV
DIST. 3

Statement of Certification
Hardship Gas Well Classification
Kimbell Oil Company of Texas
Salazar Well No. 4-E
N½ section 34, T25N., R.6W., N.M.P.M.
Rio Arriba County, New Mexico
Basin Dakota Pool

KIMBELL OIL COMPANY OF TEXAS, OPERATOR, as required by the State of New Mexico Energy and Minerals Department, Oil Conservation Division, certifies that:

1. All information submitted with this application is true and correct to the best of his knowledge;
2. One copy of this application has been submitted to the Farmington District Office of the Oil Conservation Division;
3. Notice of this application has been given to El Paso Natural Gas Company, the transporter and purchaser; and
4. Notice of this application has been given to all offset Basin Dakota operators.

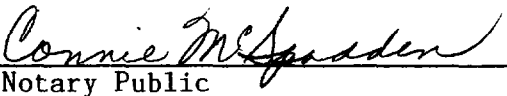


 Jack Redding, President

THE STATE OF Texas
 COUNTY OF Tarrant

BEFORE ME, Notary Public, on this day personally appeared Jack Redding, known to me to be the person whose name is subscribed to the foregoing instrument and acknowledged to me that he executed the same for the purposes and consideration therein expressed.

GIVEN under my hand seal of office this 10th day of September, 1985.



 Notary Public

My Commission Expires:
July 13, 1987

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TELEPHONE: (505) 988-4421
TELECOPIER: (505) 983-6043

October 18, 1985

RECEIVED

OCT 18 1985

OIL CONSERVATION DIVISION

HAND DELIVERED

Mr. Michael Stogner
New Mexico Oil Conservation Division
New Mexico Department of
Energy and Minerals
310 State Land Office Building
Santa Fe, New Mexico 87501

Re: Case No. 8712: Application of Kimbell Oil Company of Texas
for Hardship Gas Well Classification

Dear Mike:

This will confirm that the above-referenced case, previously
set for the November 23, 1985 Examiner hearing has been continued
to the November 6, 1985 hearing.

Thanks for your cooperation.

Very truly yours,



J. Scott Hall

JSH/ba

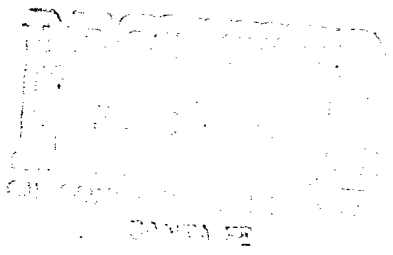


ENERGY AND MINERALS DEPARTMENT

OIL CONSERVATION DIVISION
AZTEC DISTRICT OFFICE

1000 RIO BRAZOS ROAD
AZTEC, NEW MEXICO 87410
(505) 334-6178

OIL CONSERVATION DIVISION
BOX 2088
SANTA FE, NEW MEXICO 87501



DATE 8-30-85

- RE: Proposed MC _____
- Proposed DHC _____
- Proposed NSL _____
- Proposed SWD _____
- Proposed WFX _____
- Proposed PMX _____

Hardship well application X

Case No.

-8712-

Gentlemen:

I have examined the application dated 8-22-85

for the Kimbell Oil Co. Salazar #4E F-34-25N-6W
Operator Lease and Well No. Unit, S-T-R

and my recommendations are as follows:

*Cannot approve administratively, docket for hearing.
No production curves submitted with or correct form of
application. From the evidence submitted it is doubtful
the well would qualify.*

Yours truly,

KIMBELL OIL COMPANY

OF TEXAS

3000 TEXAS AMERICAN BANK BLDG.

FT. WORTH, TEXAS 76102

(817) 335-2591

August 20, 1985

M.S.

Mr. Richard Stamets, Director
New Mexico Oil Conservation Division
P.O. Box 2088
Santa Fe, NM 87501

Re: Salazar No. 4-E
N/2 Sec. 34, T25N,
R6W, NMPM
Rio Arriba County, N.M.

Dear Mr. Stamets:

The purpose of this letter is to request an Administrative Order granting Kimbell Oil Company of Texas approval to produce the Salazar Well No. 4-E for a minimum of five (5) days or a volume of 13,550 MCF each month until the balancing period has been completed. This well is overproduced and is presently shut-in under the six (6) times over-produced rule.

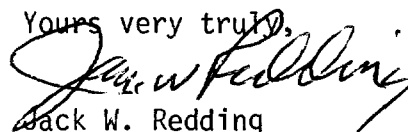
The Salazar Well No. 4-E produces from the Basin Dakota Reservoir and as shown by the enclosed Engineering Report, irreversible skin damage would occur if this well does not have periodic and regular production to remove the formation water from the wellbore. The report provides technical substantiation of the required flow-rate to prevent damage.

This well is overproduced by 317,158 MCF, which is eleven (11) times over its average allowable. Due to the current low market nominations, the balancing period for this well may be prolonged an additional 15 months and such a long shut-in period would cause formation damage that would be impossible to reverse completely with well treatment. This would result in lost reserves that would be trapped and unproducibile from the damaged well.

To protect this well from irreparable damage and prevent the waste of producible reserves, we therefore, request that the NMOCD approve the scheduling by El Paso Natural Gas Company of monthly minimum production of 13,550 MCF, or 5 days, until such time as this well is in balance with its allowable.

Thank you for your assistance.

Yours very truly,


Jack W. Redding
President

Encl.
JWR:cm



gulram, inc.

2828 12th street nw, suite C
p.o. box 6548
albuquerque, new mexico 87197-6548

petroleum engineering and government regulation consultants

505-345-2351

August 15, 1985

REPORT TO KIMBELL OIL CO. OF TX
FLOWRATE REQUIRED TO PREVENT SKIN DAMAGE OF THE
SALAZAR WELL NO. 4-E
SE $\frac{1}{4}$ NW $\frac{1}{4}$ section 34, T.25N., R.6W., N.M.P.M., Rio Arriba County, NM

SUMMARY

The Salazar Well No. 4-E produces from the Basin Dakota Reservoir, which is subject to irreversible formation (skin) damage if the well remains shut-in over an extended period without production. Producing the well on a regular interval is necessary to remove the water from the well-bore, which can interact with the clay constituents of the Dakota reservoir rocks and cause skin damage. Using the radial flow equation for gas, and setting the pressure drop for skin damage to zero, results in the required flow rate to prevent that damage from occurring and the possible loss of productive reserves. Based upon the June deliverability test, the required flowrate would be 13,550 MCF/month. Thus, this well must be produced for 5 days each month or a volume of about 13,550 MCF to prevent permanent damage.

FORMATION CHARACTERISTICS

The Salazar Well No. 4-E is being produced from the Basin Dakota formation. The basal Dakota "...deposits consist of dark-gray carbonaceous shales, a few thin coal seams, some siltstones, and thin channel sandstones."¹ The next unit consists of "...dark carbonaceous shales, mudstones, and thin siltstones and sandstones ..."¹ The clay materials present in the shales of this formation are capable of migration and clogging of the formation pore spaces if contacted by foreign water or altered formation water (ionic environment shifts are sufficient).

FORMATION DAMAGE

When the clay particles of a formation are disturbed or rearranged, it is impossible to restore the original pore configuration or "permeability." This formation damage should be prevented, since a complete cure is not possible with subsequent well treatments.

Formation damage occurs with the hydration or dehydration of swellable clays, which are present throughout the Dakota formation. The damage mechanism is the reduced "relative permeability," which results from water "wetting" the formation rock. The clay particles swell and move into the pore spaces, "clogging" them, and thus reduce the open space available for the hydrocarbons to travel to the well-bore. The critical area for damage to the formation is the first few feet away from the bore-hole, which affects the radial flow of the hydrocarbons into the hole. In radial flow systems, any reduction in the permeability around the well-bore can result in permanent loss of productivity.

Also, sandstone formations, as excellent depth filters, are highly sensitive to flow rate and pressure differentials. Increased water saturation near the well-bore will cause filtrate invasion or coning of the formation water, which creates a water blockage to hydrocarbon flow. This type of blockage can be corrected by regular water production.

Thus, to prevent permanent damage to the formation and effectively eliminate water blockage, the well must be produced to remove the water from the productive formation face or "skin" in the well-bore. The most effective treatment of well damage is prevention not corrective well treatments after the damage occurs.

FLOWRATE REQUIRED TO PREVENT DAMAGE

To prevent entrapment of reserves in a potentially productive zone, since irreversible formation damage can restrict or prevent effective depletion, we must determine an adequate flow rate to minimize skin damage to this well by removal of formation water.

Using the radial flow equation for gas wells, we will set the p_{skin} (pressure drop due to skin damage) to zero and use the data from the 1985 well deliverability test report dated 6-12-85, which reflects the well's current undamaged condition.

We will assume a radial drainage impact of 160 acres for a Dakota well; permeability (undamaged) equal to the pool average; and molecular weight of the gas to be 21.65 since test results show the gas to be "dry with a trace of condensate", indicating that the stream is not pure methane, but contains some liquids. See attached calculation pages for the details of the analysis. The calculation results in a flow rate of 444.34 MCF/day or 13,552 MCF per month. Based upon the 6-12-85 deliverability of 2698 MCF/day, this results in 5.02 days per month.

Thus, this well should be allowed to produce approximately 13,550 MCF per month or 5 days, to prevent permanent formation damage and loss of productive reserves.



Sue E. Umshler, P.E.



REFERENCES

1. W.F. Hoppe, 1978, Basin Dakota Gas Field in Oil & Gas Fields of the Four Corners Area: Four Corners Geological Society, pgs. 204-206.
2. Thomas O. Allen & Alan P. Roberts, 1978, Production Operations, Volume 2, Oil and Gas Consultants, Inc., pgs 95-107.
3. H.C. Slider, 1976, Practical Petroleum Reservoir Engineering Methods, PennWell Books.
4. Craft & Hawkins, 1959, Applied Petroleum Reservoir Engineering, Prentice Hall, Chemical Engineering Series.

$$q_{gas} = \frac{.703 K_{und} h (p_e^2 - p_w^2 - \Delta P_{skin}^2)^n}{\mu T_f z \ln \left(\frac{r_e}{r_w} \right)}$$

q_g = flow rate, Mcf/day

K_{und} = undamaged permeability, Darcies

h = net thickness, feet

p_e = External Boundary pressure (initial shut-in), psia

p_w = Flowing pressure (FTP), psia

ΔP_{skin} = pressure drop in damaged zone, psia

μ = viscosity, cp

r_e = external Boundary radius (ultimate drainage impact), feet

r_w = well radius, feet

T_f = formation Temperature, °R

z = gas deviation

Given: $T_f = 18^\circ F + 460 = 640^\circ R$ (well log)

$K_{Basin} \approx K = .175$ md avg or .000175 Darcies (Pool Report)

$h = 90$ feet (Completion Report)

$r_e = 1490$ feet (160 acre drainage radius)

$r_w = .7$ feet (Completion Report)

$p_e = 1350$ psia (back plot of SIRD vs. Cum)

6-12-85 well Test Data (well deliverability current)

$p_w = 787$ psia

gravity = .704 \Rightarrow by charts $\mu = .016$ cp
 $z = .885$

Calculate n

$$n = \frac{W}{29(\text{gravity})}$$

Gas is dry w/ trace condensate so Assume MW

W methane = 16.04 assume gas

W ethane = 30.07 70%

W propane = 44.09 20%

Weighted average $W = 16.04(.70) + 30.07(.70) + 44.09(.10) = 21.65$

So

$$n = \frac{21.65}{29(.704)} = 1.06$$

Set $\Delta P_{skin} = 0$ to determine q_g required to prevent damage to zone.

Calculate q_g .

$$q_g = \frac{.703 (1,000,175)(90)(1350^2 - 787^2 - 0^2)^{1.06}}{.016 (640)(.885) \ln\left(\frac{1490}{.7}\right)}$$

$$= 444.34 \text{ mcf/day}$$

Monthly production

$$q_m = 444.34 \times 30.5 = \underline{\underline{13552.37 \text{ mcf/month}}}$$

Deliverability on 6-12-85 was 2698 mcf/day

Calculate No. days for flow

$$13552.37 \div 2698 = \underline{\underline{5.02 \text{ days per month}}}$$

Sue E. Umshler
8-13-85

NEW MEXICO OIL CONSERVATION COMMISSION
WELL DELIVERABILITY TEST REPORT FOR 19 85

Form C122-A
Revised 1-1-66

POOL NAME Basin Dakota	POOL SLOPE n = .75	FORMATION Dakota	COUNTY Rio Arriba
----------------------------------	------------------------------	----------------------------	-----------------------------

Meter No. 94-932

COMPANY Kimbell Oil Company of Texas			WELL NAME AND NUMBER Salazar No. 4B		
UNIT LETTER F	SECTION 34	TOWNSHIP 25N	RANGE 6W	PURCHASING PIPELINE El Paso Natural Gas Co.	
CASING O.D. - INCHES 4.500	CASING I.D. - INCHES 4.000	SET AT DEPTH - FEET 6759	TUBING O.D. - INCHES 2.375	TUBING I.D. - INCHES 1.995	TOP - TUBING PERF. - FEET 6422
GAS PAY ZONE FROM 6422 TO 6672		WELL PRODUCING THRU CASING TUBING X		GAS GRAVITY .704	GRAVITY X LENGTH 4521
DATE OF FLOW TEST FROM 5/27/85 TO 6/4/85			DATE SHUT-IN PRESSURE MEASURED 6/18/85		

PRESSURE DATA - ALL PRESSURES IN PSIA

(a) Flowing Casing Pressure (DWt) 932	(b) Flowing Tubing Pressure (DWt) 787	(c) Flowing Meter Pressure (DWt) 262	(d) Flow Chart Static Reading 256	(e) Meter Error (Item c - Item d) +6	(f) Friction Loss (a - c) or (b - c) 525	(g) Average Meter Pressure (Integr.) 259
(h) Corrected Meter Pressure (g + e) 265	(i) Avg. Wellhead Press. P _i = (b + f) 787	(j) Shut-in Casing Pressure (DWt) 1322	(k) Shut-in Tubing Pressure (DWt) 1322	(l) P _c = higher value of (j) or (k) 1322	(m) Del. Pressure P _d = <u>40</u> % P _c 529	(n) Separator or Dehydrator Pr. (DWt) for critical flow only 784

FLOW RATE CORRECTION (METER ERROR)

Integrated Volume - MCF/D 2035	Quotient of $\frac{\text{Item c}}{\text{Item d}}$ 1.0234	$\sqrt{\frac{\text{Item c}}{\text{Item d}}}$ 1.0116	Corrected Volume Q = 2059 MCF/D
--	--	---	---

WORKING PRESSURE CALCULATION

$(1 - e^{-s})$.280	$(F_c Q_m)^2 (1000)$ 374,759	$R^2 = (1 - e^{-s}) (F_c Q_m)^2 (1000)$ 104,933	P_t^2 619,369	$P_w^2 = P_t^2 + R^2$ 724,302	$P_w = \sqrt{P_w^2}$ 851
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DELIVERABILITY CALCULATION

$D = Q \left[\frac{P_c^2 - P_d^2}{P_c^2 - P_w^2} \right]^n =$	2059	$\left(\frac{1,467,843}{1,028,483} \right)^n =$	1.4341	$=$	1.3105	$=$	2698 MCF/D
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REMARKS:

**This well has critical flow -
Use FIP (b) for P_c (i)**

SUMMARY

Item h	265	Psia
P _c	1322	Psia
Q	2059	MCF/D
P _w	851	Psia
P _d	529	Psia
D	2692	MCF/D

Company **Kimbell Oil Company of Texas**
 By **E. A. Clement**
 Title **Prod. Supt.**
 Witnessed By _____
 Company _____

UNITED STATES
DEPARTMENT OF THE INTERIOR
GEOLOGICAL SURVEY

SUBMIT IN DUPLICATE

(See other instructions on reverse side)

Form approved,
Budget Bureau No. 42-R855.6.

WELL COMPLETION OR RECOMPLETION REPORT AND LOG *

1. TYPE OF WELL: OIL WELL <input type="checkbox"/> GAS WELL <input checked="" type="checkbox"/> DRY <input type="checkbox"/> Other		5. LEASE DESIGNATION AND SERIAL NO. SF-080136	
2. NAME OF OPERATOR Curtis J. Little		6. IF INDIAN, ALLOTTEE OR TRIBE NAME	
3. ADDRESS OF OPERATOR P.O. Box 1258 Farmington, NM 87499		7. UNIT AGREEMENT NAME	
4. LOCATION OF WELL (Report location clearly and in accordance with any State requirements) At surface 1630' FNL & 1460' FWL At top prod. interval reported below At total depth Same		8. FARM OR LEASE NAME Salazar	
API # - 30-039-23368		9. WELL NO. 4-E	
14. PERMIT NO.		10. FIELD AND POOL, OR WILDCAT Basin Dakota	
DATE ISSUED		11. SEC. T. R. M. OR BLOCK AND SURVEY OR AREA Sec. 34-T25N-R6W	
15. DATE SPUNDED 1-16-84		12. COUNTY OR PARISH Rio Arriba	
16. DATE T.D. REACHED 1/27/84		13. STATE NM	
17. DATE COMPL. (Ready to prod.) 2/21/84		14. ELEVATIONS (DV, REB, RT, OR, ETC.) 6378' GR	
18. ELEVATIONS (DV, REB, RT, OR, ETC.) 6378' GR		15. ELEV. CASINGHEAD 6378'	
19. TOTAL DEPTH, MD & TVD 6753'		16. PLUG, BACK T.D., MD & TVD 6717'	
20. IF MULTIPLE COMPL., HOW MANY?		17. INTERVALS DRILLED BY 0-6753	
21. PRODUCING INTERVAL(S), OF THIS COMPLETION—TOP, BOTTOM, NAME (MD AND TVD) 6422-6672 KB Dakota		18. ROTARY TOOLS CABLE TOOLS	
22. TYPE ELECTRIC AND OTHER LOGS RUN IES, GR-CNL-Density		19. WAS DIRECTIONAL SURVEY MADE No	
23. CASING RECORD (Report all strings set in well)		20. WAS WELL CORRED No	
CASING SIZE	WEIGHT, LB./FT.	DEPTH SET (MD)	HOLE SIZE
8-5/8"	28	222 KB	12-1/4"
4-1/2"	11.6	6759	7-7/8"
24. LINER RECORD		25. TUBING RECORD	
SIZE	TOP (MD)	BOTTOM (MD)	SACKS CEMENT*
			SCREEN (MD)
			SIZE
			DEPTH SET (MD)
			PACKER SET (MD)
26. PERFORATION RECORD (Interval, size and number) 6632-72 KB, 21 holes, 0.33" dia. 24" apart. 6548-76 KB, 6514-28, 6432-36, 6422-26, 29 holes, 0.33" dia. 24" apart.		27. ACID, SHOT, FRACTURE, CEMENT SQUEEZE, ETC. DEPTH INTERVAL (MD) AMOUNT AND KIND OF MATERIAL USED 6632-72 Acidize 1200 gals. HCL, 41500 lbs. sd., 62930 gals. gel, BDP 2450 psi; ATP 3200 psi, AIR 28 BPM, ISIP 2100 psi. 6576-6422 Acidize 1700 gal. HCL, 60000-lbs. sd., 93780 gals. gel, BDP 1900 psi	
28. PRODUCTION RECORD (Interval, size and number) ATP 3400 psi, AIR 31 BPM, ISIP 2550 psi		29. PRODUCTION RECORD (Flowing, gas lift, pumping—size and type of pump) Flowing	
DATE FIRST PRODUCTION 2/21/84	PRODUCTION METHOD	WELL STATUS (Producing or shut-in)	SI
DATE OF TEST 2/21/84	HOURS TESTED 3	CHOKER SIZE 3/4"	PROD'N. FOR TEST PERIOD Trace
FLOW. TUBING PRESS. 391	CASING PRESSURE 787	CALCULATED 24-HOUR RATE Trace	OIL—BBL. 4984
			GAS—MCF. 623
			WATER—BBL. 0
			OIL GRAVITY-API (CORR.)
30. LIST OF ATTACHMENTS None		31. TEST WITNESSED BY Joe Elledge	
32. I hereby certify that the foregoing and attached information is complete and correct as determined from all available records		DATE 2/22/84	

* (See Instructions and Spaces for Additional Data on Reverse Side)

INSTRUCTIONS

General: This form is designed for submitting a complete and correct well completion report and log on all types of lands and leases to either a Federal agency or a State agency, or both, pursuant to applicable Federal and/or State laws and regulations. Any necessary special instructions concerning the use of this form and the number of copies to be submitted, particularly with regard to local, area, or regional procedures and practices, either are shown below or will be issued by, or may be obtained from, the local Federal and/or State office. See instructions on items 22 and 24, and 33; below regarding separate reports for separate completions.

If not filed prior to the time this summary record is submitted, copies of all currently available logs (drillers, geologists, sample and core analysis, all types electric, etc.) formations and pressure tests, and directional surveys, should be attached hereto, to the extent required by applicable Federal and/or State laws and regulations. All attachments should be listed on this form, see item 35.

Item 4: If there are no applicable State requirements, locations on Federal or Indian land should be described in accordance with Federal requirements. Consult local State or Federal office for specific instructions.

Item 18: Indicate which elevation is used as reference (where not otherwise shown) for depth measurements given in other spaces on this form and in any attachments. Items 22 and 24: If this well is completed for separate production from more than one interval zone (multiple completion), so state in item 22, and in item 24 show the producing interval, or intervals, top(s), bottom(s), and name(s) (if any) for only the interval reported in item 33. Submit a separate report (page) on this form, adequately identified, for each additional interval to be separately produced, showing the additional data pertinent to such interval.

Item 29: "Sacks Cement": Attached supplemental records for this well should show the details of any multiple stage cementing and the location of the cementing tool.

Item 33: Submit a separate completion report on this form for each interval to be separately produced. (See instruction for items 22 and 24 above.)

FORMATION	TOP	BOTTOM	PROBABLY	DESCRIPTION, CONTENTS, ETC.	NAME	MEAS. DEPTH	TRUE MEAS. DEPTH
Ojo Alamo	1450	1522	Probably Water		Ojo Alamo	1450	Same
					Kirtland	1522	Same
					Fruitland	2033	Same
					Pictured Cliffs	2158	Same
					Lewis	2252	Same
					Cliff House	3713	Same
					Menefee	3761	Same
					Point Lookout	4368	Same
					Mancos	4508	Same
					Gallup	5502	Same
					Greenhorn	6310	Same
					Graneros Shale	6371	Same
					Graneros Sand	6411	Same
					Dakota	6512	Same

33. SUMMARY OF POROUS ZONES: SHOW ALL IMPORTANT ZONES OF POROSITY AND CONTENTS THEREOF, CORED INTERVALS; AND ALL DRILL-STEM TESTS, INCLUDING DEPTH INTERVAL TESTED, CURSION USED, TIME TOOL OPEN, FLOWING AND SHUT-IN PRESSURES, AND RECOVERY

38. GEOLOGIC MARKERS

Kimbell Oil Co of Tex

SALAZAR FEB E4 F 34 25NO6W

	OIL	WATER	GAS	DAYS
JAN	666	120	61697	31
FEB	340	92	38233	23
Mar	54	8	649	1
APR	∅	∅	4696	2
May	425	70	29205	14
Jun	143	30	16285	9
July	∅	∅	∅	∅
Aug	∅	∅	∅	∅
Sept	∅	∅	∅	∅

10/17/85

Memo

From
MICHAEL STOGNER
Petroleum Engineer

To Florine

Please

Continue

Case No. 8712

*OK'd
By ALS
m.s.*

To

11/6/85

@ The request of Scott Hall

*Frank
M.S.*



STATE OF NEW MEXICO
ENERGY AND MINERALS DEPARTMENT
 OIL CONSERVATION DIVISION

TONEY ANAYA
 GOVERNOR

November 22, 1985

POST OFFICE BOX 2088
 STATE LAND OFFICE BUILDING
 SANTA FE, NEW MEXICO 87501
 (505) 827-5800

Mr. Scott Hall
 Campbell & Black,
 Attorneys at Law
 Post Office Box 1208
 Santa Fe, New Mexico

Re: CASE NO. 1712
 ORDER NO. R-2033

Applicant:

Kimbell Oil Company of Texas

Dear Sir:

Enclosed herewith are two copies of the above-referenced
 Division order recently entered in the subject case.

Sincerely,

R. L. STAMETS
 Director

RLS/fd

Copy of order also sent to:

Hobbs OCD X
 Artesia OCD X
 Aztec OCD X

Other _____

CAMPBELL & BLACK, P.A.

LAWYERS

JACK M. CAMPBELL
BRUCE D. BLACK
MICHAEL B. CAMPBELL
WILLIAM F. CARR
BRADFORD C. BERGE
J. SCOTT HALL
PETER N. IVES
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JEFFERSON PLACE
SUITE 1 - 110 NORTH GUADALUPE
POST OFFICE BOX 2208
SANTA FE, NEW MEXICO 87501
TELEPHONE: (505) 988-4421
TELECOPIER: (505) 983-6043

September 12, 1985

HAND DELIVERED

Case 8712

R. L. Stamets, Director
Oil Conservation Division
New Mexico Department of
Energy & Minerals
State Land Office Building
Santa Fe, New Mexico 87503

Re: Kimbell Oil Company of Texas - Application for Hardship Gas
Well Classification

Dear Mr. Stamets:

In connection with the above-referenced application, I am enclosing to you herewith a submission of supplemental information prepared by Sue E. Umshler, the petroleum engineer for Kimbell Oil Company.

It is my hope that this supplemental submission contains sufficient information for the area supervisor to grant temporary emergency relief for the subject well. In this connection, copies of this information have been supplied to Frank Chavez in Aztec under separate cover.

Thank you for your cooperation.

Very truly yours,



J. Scott Hall

JSH/ba
enclosures

cc: Sue E. Umshler, P.E.
Victor Salazar
Frank Chavez

Supplement to
APPLICATION FOR CLASSIFICATION AS
HARDSHIP GAS WELL
Kimbell Oil Company of Texas
Salazar Well No. 4-E
N $\frac{1}{2}$ section 34, T.25N., R.6W., N.M.P.M.
Rio Arriba County, New Mexico
Basin Dakota Pool

1. The applicant expects that total restriction of gas production from this well over an extended period of time will result in "underground waste" (as defined by the General Information Applicable to Hardship Gas Well Classification). This expectation is based on two points discussed below.

First, this well has produced a regular amount of water, which means that suppression of the gas flow will also suppress removal of this water from the wellbore. As shown in the Report prepared on 8-15-85, this could cause permanent "skin" damage to the formation face. The water production averaged 4.5 bbls/day or an average gas/water ratio of 2.17 bbls/MMCF. Regular production, which will prevent this water from accumulating in the wellbore, is indicated as the only preventative action against permanent formation damage.

Secondly, the wells in the surrounding area indicate that formation damage due to water accumulation may have occurred. Two of these wells have been abandoned and may have not produced their true potential due to water damage. These wells are the Farming E No. 3-E in D-2-24N-6W and the Salazar No. 4 in H-34-25N-6W. There are two wells in the south half of section 34 which may have suffered damage due to shut-in periods in the last 5 years. These wells are the Federal Wells No. 3 and 3-E. We will attempt to prove that these wells experienced lost productivity and potential recoverable reserves in the hearing. Their performance is documented on the enclosed Production Tables.

As discussed in the Engineering Report dated 8-15-85 (which calculated a minimum flow rate to prevent damage to this well), unless sufficient gas production and incumbent water production is allowed this water cannot be removed from the wellbore. The exposure to accumulated water could cause permanent formation damage and this would result in loss of gas reserves due to the reduction in permeability. Prolonged shut-in of this well could produce this result and it has already been shut-in since June 1985.

2. The well had not been damaged as of June based on the deliverability test. The potential problem of damage to this well cannot be solved by completion practices because it is just that--a "potential" problem and not an actual problem at this

time. Therefore, no mechanical operations are appropriate until such time as damage has actually occurred. The historical attempt to prevent the problem was full production of this well initially to remove excess frac water and formation water. This led to the overproduced status of the well. Also, El Paso Natural Gas Co. (the purchaser) was contacted when the well was shut-in to determine what preventative steps could be taken to alleviate the overproduction problem and also prevent the possibility of long-term damage to the formation by water accumulation due to lack of production. The result of those contacts was our Administrative Request in August, and upon subsequent discussions with the NMOCD staff in Santa Fe, the scheduling of the hearing and this application for temporary relief. Our motivation is to prevent damage, as being the best cure for formation damage. We seek a minimum flow rate to prevent damage and potential loss of reserves.

3. As illustrated by the attached production table and graph, initial production of this well was on May 12, 1984 and water production has varied from essentially 3.3 to 8.9 bbls/day with water ratios between 1.75 bbls/MMCF and 12.33 bbls/MMCF, with an average of 2.17 bbls/MMCF. This performance indicates that the water influx is a regular occurrence and only regular production of the gas will prevent any water accumulation. The Report dated 8-15-85 shows that gas production of about 13,550 MCF/month is required to prevent the pressure drop which would occur if the well were damaged.
4. Gas Reserves Lost:
 - Estimated Original Gas-In-Place:
 - Volumetric Calculation = 3.95 BCF
 - BHP/Z vs. Cumulative plot = 4.45 BCF
 - Recoverable Reserves (assume 85% recovery)
 - 3.35 to 3.78 BCF
 - Preliminary decline curve projection:
 - 1.8 BCF
 - Cumulative Recovered as of 6-85:
 - 586,993 MCF

Both the materials balance and decline curve analysis are subject to error at this point, due to the limited production history and pressure tests available.

Lost reserves are not possible to determine at this point because the well has not suffered the pressure drop and erratic productivity loss resulting from damage. However using the radial flow equation developed in the 8-15-85 Engineering Report and setting the parameters to 1 (indicating no change) except

for q (flow-rate) and pressure drop, one can see that a pressure drop of 50 psi will result in a 75% drop in flowrate. If the portion of this drop due to skin damage equals 10 psi, the reduced flow due to damage would be 20%. Also, according to Allen and Roberts in Production Operations, Vol. 2, a loss of 50% of the producibility will occur with a 5-fold decrease in permeability at the well face due to damage. Thus the resultant loss of reserves could be large with formation and pressure alterations as outlined above. During the hearing we will attempt to show the amount of loss the adjacent wells may have experienced due to water accumulation.

5. The producibility of this well is shown by the attached deliverability tests of 1984 and 1985 and the Production Table and plot. The well has had an average production rate to date of 1947 MCF/day. At present we believe that production is necessary to maintain this potential flow rate and prevent irreversible loss due to damage. But currently available tests show that abnormal producibility decline has not yet occurred.
6. A plat of the area is attached and list of adjacent wells.
7. See attached Production Tables of adjacent wells.
8. This well is overproduced by 317,158 MCF, which is 11 times over its allowable.

**UNITED STATES
DEPARTMENT OF THE INTERIOR
GEOLOGICAL SURVEY**

SUBMIT IN DUPLICATE

(See other instructions on reverse side)

Form approved,
Budget Bureau No. 42-R365.5.

WELL COMPLETION OR RECOMPLETION REPORT AND LOG *

1. TYPE OF WELL: OIL WELL GAS WELL DRY Other _____

2. TYPE OF COMPLETION: NEW WELL WORK OVER DEEP-EN PLUG BACK DIFF. REVR. Other _____

3. NAME OF OPERATOR
Curtis J. Little

4. ADDRESS OF OPERATOR
**P.O. Box 1258
Farmington, NM 87499**

5. LOCATION OF WELL (Report location clearly and in accordance with any State requirements)*
At surface **1630' FNL & 1460' FWL**
At top prod. interval reported below _____
At total depth **Same**

API # - **30-039-23368**

6. LEASE DESIGNATION AND SERIAL NO.

SF-080136

7. IF INDIAN, ALLOTTEE OR TRIBE NAME

8. UNIT AGREEMENT NAME

9. FARM OR LEASE NAME

Salazar

10. WELL NO.

4-B

11. FIELD AND POOL, OR WILDCAT

Basin Dakota

12. SEC. T., R., M., OR BLOCK AND SURVEY OR AREA

Sec. 34-T25N-R6W

13. COUNTY OR PARISH

Rio Arriba

14. STATE

NM

15. DATE SPUNDED **1-16-84** 16. DATE T.D. REACHED **1/27/84** 17. DATE COMPL. (Ready to prod.) **2/21/84** 18. ELEVATIONS (DP, RB, RT, OR, ETC.)* **6378' GR** 19. ELEV. CASINGHEAD **6378'**

20. TOTAL DEPTH, MD & TVD **6753'** 21. PLUG, BACK T.D., MD & TVD **6717'** 22. IF MULTIPLE COMPL., HOW MANY* _____ 23. INTERVALS DRILLED BY _____ ROTARY TOOLS **0-6753** CABLE TOOLS _____

24. PRODUCING INTERVAL(S), OF THIS COMPLETION—TOP, BOTTOM, NAME (MD AND TVD)*
6422-6672 KB Dakota

25. TYPE ELECTRIC AND OTHER LOGS RUN
IES, GR-CNL-Density

26. CASING RECORD (Report all strings set in well)

CASING SIZE	WEIGHT, LB./FT.	DEPTH SET (MD)	HOLE SIZE	CEMENTING RECORD	AMOUNT PULLED
8-5/8"	28	222 KB	12-1/4"	145' sx. (171 cuft. slurry)	none
4-1/2"	11.6	6759	7-7/8"	DV Tool 4574, 600 sx. Poz top 5458 KB. 2nd Stage w/ Glass B (1891 cuft.) Top	(774 cuft.) Bond 875' sx. & 75' cnt. 1300 KB

27. LINER RECORD

SIZE	TOP (MD)	BOTTOM (MD)	SACKS CEMENT*	SCREEN (MD)	SIZE	DEPTH SET (MD)	PACKER SET (MD)
					2-3/8	6548	

28. PERFORATION RECORD (Interval, size and number)

6632-72 KB, 21 holes, 0.33" dia. 24" apart.
6548-76 KB, 6514-28, 6432-36, 6422-26, 29 holes, 0.33" dia. 24" apart.

29. ACID, SHOT, FRACTURE, CEMENT SQUEEZE, ETC.

6632-72 Acidize 1200 gals. HCL, 41500 lbs. sd., 62930 gals. gel, BDP 2450. psi; ATP 3200 psi, AIR 28 BPM; ISIP 2100 psi. 6576-6422 Acidize 1700 gal. HCL, 60000-lbs. sd., 93780 gals. gel, BDP 1900 psi

30. PRODUCTION ATP 3400 psi, AIR 31 BPM, ISIP 2550 psi

31. DATE FIRST PRODUCTION **2/21/84** PRODUCTION METHOD (Flowing, gas lift, pumping—size and type of pump) **Flowing** WELL STATUS (Producing or shut-in) **SI**

32. DATE OF TEST **2/21/84** HOURS TESTED **3** CHOKER SIZE **3/4"** PROD'N. FOR TEST PERIOD **Trace** OIL—BBL. **Trace** GAS—MCF. **623** WATER—BBL. **Trace (Frac)** GAS-OIL RATIO _____

33. FLOW. TUBING PRESS. **391** CASING PRESSURE **787** CALCULATED 24-HOUR RATE **Trace** OIL—BBL. **Trace** GAS—MCF. **4984** WATER—BBL. **0** OIL GRAVITY-API (CORR.) _____

34. DISPOSITION OF GAS (Sold, used for fuel, vented, etc.) **To be sold** TEST WITNESSED BY **Joe Elledge**

35. LIST OF ATTACHMENTS
None

36. I hereby certify that the foregoing and attached information is complete and correct as determined from all available records
SIGNED **Curtis J. Little** TITLE **Operator** DATE **2/27/84**

* (See Instructions and Spaces for Additional Data on Reverse Side)

PRODUCTION

INSTRUCTIONS

General: This form is designed for submitting a complete and correct well completion report and log on all types of lands and leases to either a Federal agency or a State agency, or both, pursuant to applicable Federal and/or State laws and regulations. Any necessary special instructions concerning the use of this form and the number of copies to be submitted, particularly with regard to local, area, or regional procedures and practices, either are shown below or will be issued by, or may be obtained from, the local Federal and/or State office. See instructions on items 22 and 24, and 33; below regarding separate reports for separate completions.

If not filed prior to the time this summary record is submitted, copies of all currently available logs (drillers, geologists, sample and core analysis, all types electric, etc.), formation and pressure tests, and directional surveys, should be attached hereto, to the extent required by applicable Federal and/or State laws and regulations. All attachments should be listed on this form, see item 33.

Item 4: If there are no applicable State requirements, locations on Federal or Indian land should be described in accordance with Federal requirements. Consult local State or Federal office for specific instructions.

Item 18: Indicate which elevation is used as reference (where not otherwise shown) for depth measurements given in other spaces on this form and in any attachments. Items 22 and 24: If this well is completed for separate production from more than one interval zone (multiple completion), so state in item 22, and in item 24 show the producing interval, or intervals, top(s), bottom(s), and name(s); (if any) for only the interval reported in item 33. Submit a separate report (page) on this form, adequately identified, for each additional interval to be separately produced, showing the additional data pertinent to such interval.

Item 29: "Seals Cement": Attached supplemental records for this well should show the details of any multiple stage cementing and the location of the cementing tool.

Item 33: Submit a separate completion report on this form for each interval to be separately produced. (See instruction for items 22 and 24 above.)

FORMATION	TOP	BOTTOM	DESCRIPTION, CONTENTS, ETC.	NAME	MEAS. DEPTH	TRULY SET DEPTH
Ojo Alamo	1450	1522	Probably Water	Ojo Alamo	1450	Same
				Kirtland	1522	Same
				Fruitland	2033	Same
				Pictured Cliffs	2158	Same
				Lewis	2252	Same
				Cliff House	3713	Same
				Menefee	3761	Same
				Point Lookout	4368	Same
				Mancos	4508	Same
				Gallup	5502	Same
				Greenhorn	6310	Same
				Graneros Shale	6371	Same
				Graneros Sand	6411	Same
				Dakota	6512	Same

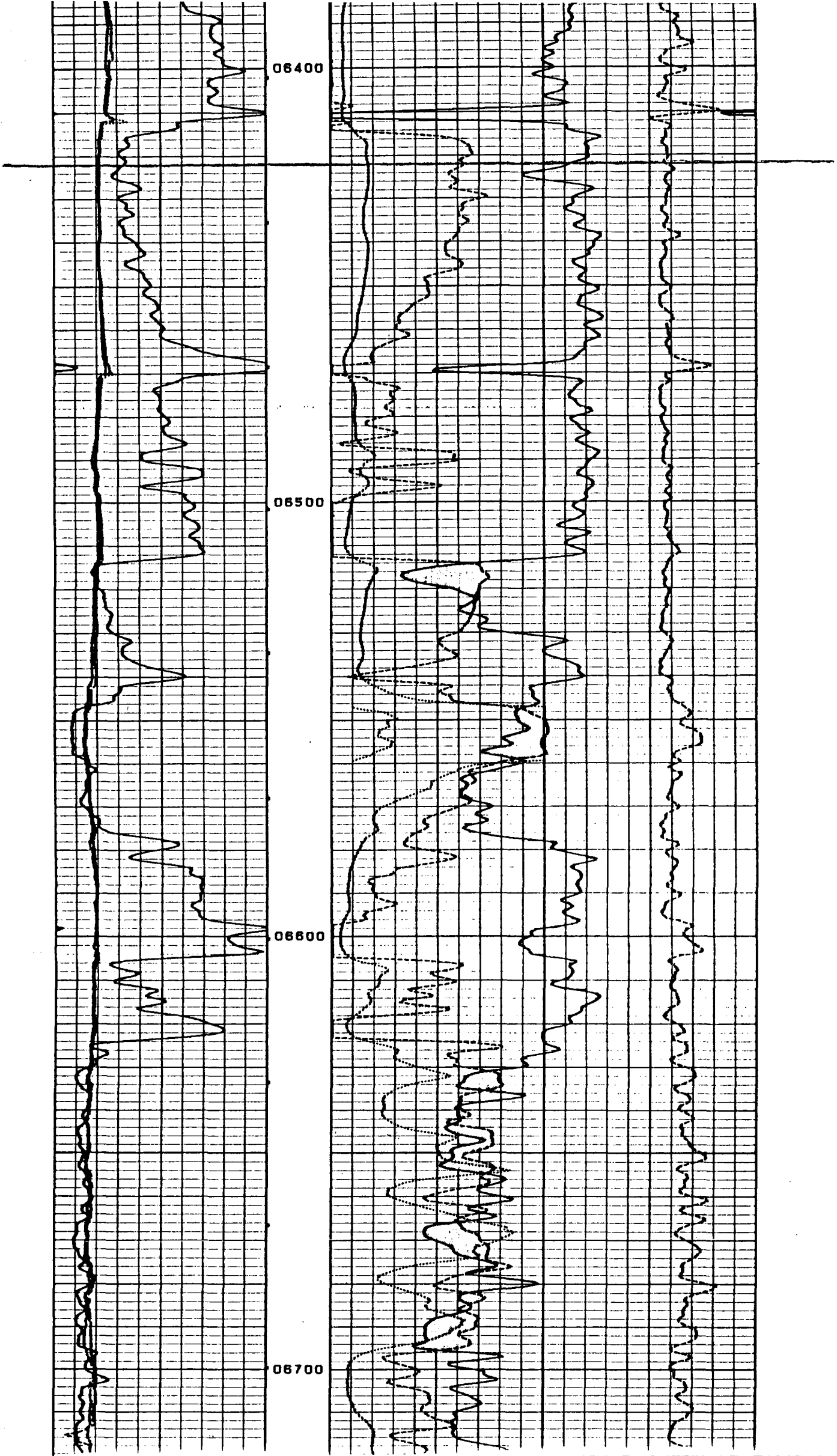
37. SUMMARY OF POROUS ZONES: SHOW ALL IMPORTANT ZONES OF POROSITY AND CONTENTS THEREOF; CORED INTERVALS; AND ALL DRILL-STEM TESTS, INCLUDING DEPTH INTERVAL TESTED, CUSHION USED, TIME TOOL OPEN, FLOWING AND SHUT-IN PRESSURE, AND RECOVERIES

FORMATION		TOP	BOTTOM	DESCRIPTION, CONTENTS, ETC.	NAME	MEAS. DEPTH	TRULY SET DEPTH
Ojo Alamo	1450	1522	Probably Water	Ojo Alamo	1450	Same	
				Kirtland	1522	Same	
				Fruitland	2033	Same	
				Pictured Cliffs	2158	Same	
				Lewis	2252	Same	
				Cliff House	3713	Same	
				Menefee	3761	Same	
				Point Lookout	4368	Same	
				Mancos	4508	Same	
				Gallup	5502	Same	
				Greenhorn	6310	Same	
				Graneros Shale	6371	Same	
				Graneros Sand	6411	Same	
				Dakota	6512	Same	

GEARHART

COMPENSATED DENSITY COMPENSATED NEUTRON LOG

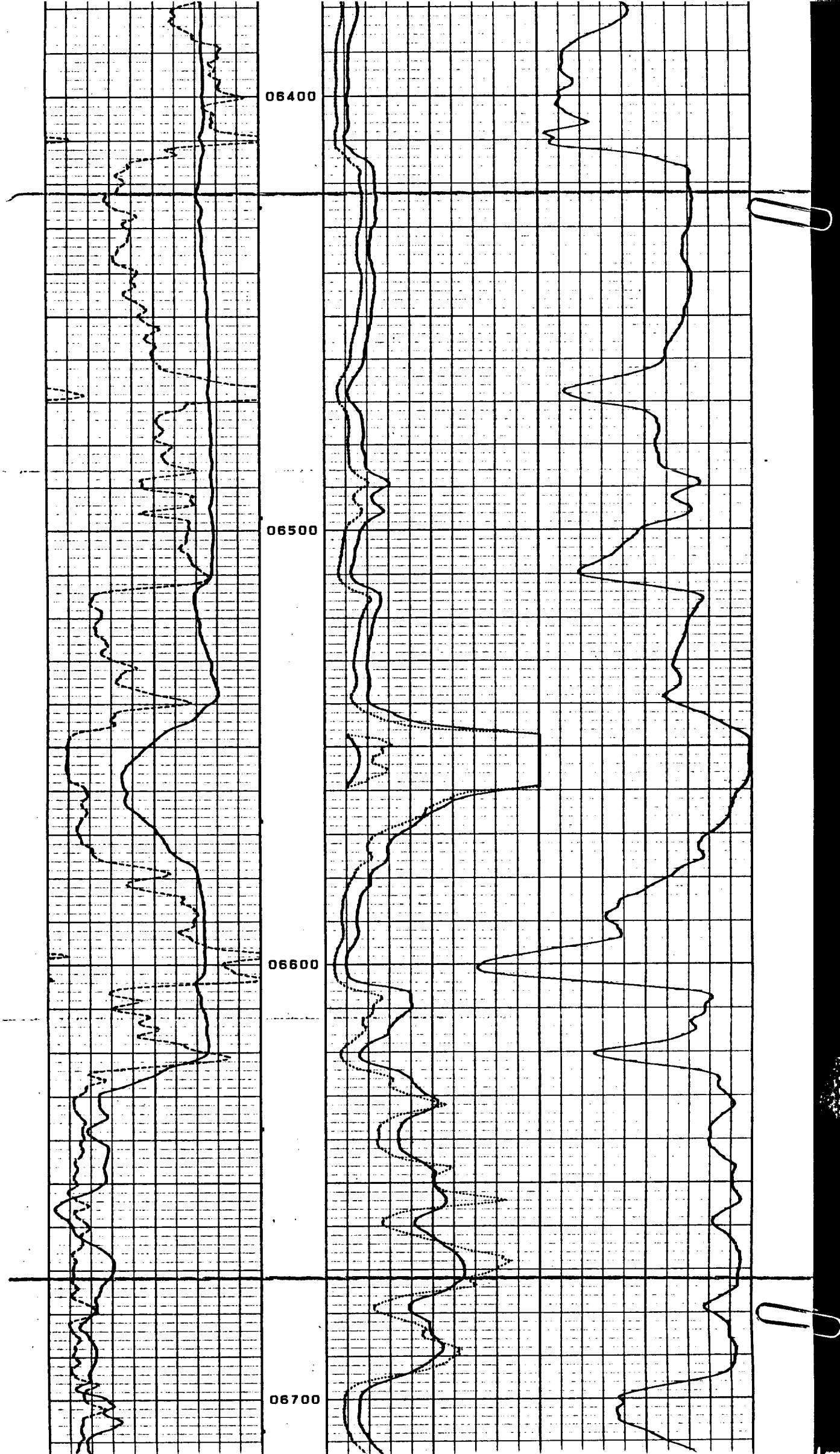
FILING NO.		COMPANY <u>CURTIS J. LITTLE</u>					
		WELL <u>SALAZAR NO.4-R</u>					
		FIELD <u>BASIN DAKOTA</u>					
		COUNTY <u>RIO ARRIBA</u> STATE <u>NEW MEXICO</u>					
		LOCATION: <u>1630' FNL x 1460' FWL</u>				Other Services <u>IEL/GR</u>	
		SEC <u>34</u> TWP <u>25N</u> RGE <u>6W</u>					
Permanent Datum <u>GROUND LEVEL</u>		Elev. <u>6378</u>				Elev.: K.B. <u>6391</u>	
Log Measured from <u>K.B.</u>		<u>13</u> Ft. Above Perm. Datum				D.F. <u>6390</u>	
Drifting Measured from <u>K.B.</u>						G.L. <u>6378</u>	
Date	<u>1-27-84</u>						
Run No.	<u>ONE</u>						
Depth - Driller	<u>6753</u>						
Depth-Logger	<u>6753</u>						
Bottom logged interval	<u>6752</u>						
Top logged interval	<u>6150</u>						
Type fluid in hole	<u>GEL</u>						
Density	Visc.	<u>9.0</u>	<u>60</u>				
pH	Fluid Loss	<u>7.5</u>	<u>7</u>				
Max rec. temp., deg F.	<u>180</u>	°F		°F	°F	°F	
Source of Samples	<u>Mud Pit</u>						
Rm @ Meas. Temp.	<u>1.8</u>	@ <u>74</u>	°F	@	°F	@ °F	
Rmf @ Meas. Temp.	<u>1.4</u>	@ <u>69</u>	°F	@	°F	@ °F	
Rmc @ Meas. Temp.	<u>1.2</u>	@ <u>68</u>	°F	@	°F	@ °F	
Source Rmf	Source Rmc	<u>M</u>	<u>M</u>				
Time	End Circulation	<u>20:00</u>					
	Logger on Bottom	<u>02:45</u>					
Recorded By	<u>Mease</u>						
Witnessed By	<u>Mr. Curtis Little</u>						
Run No.	Bore-Hole Record			Casing Record			
	Bit	From	To	Size	Wgt.	From To	
<u>One</u>	<u>12 1/2</u>	<u>Surface</u>	<u>222</u>	<u>8 5/8</u>	<u>---</u>	<u>Surface 222</u>	
<u>One</u>	<u>7 7/8</u>	<u>222</u>	<u>6753</u>				



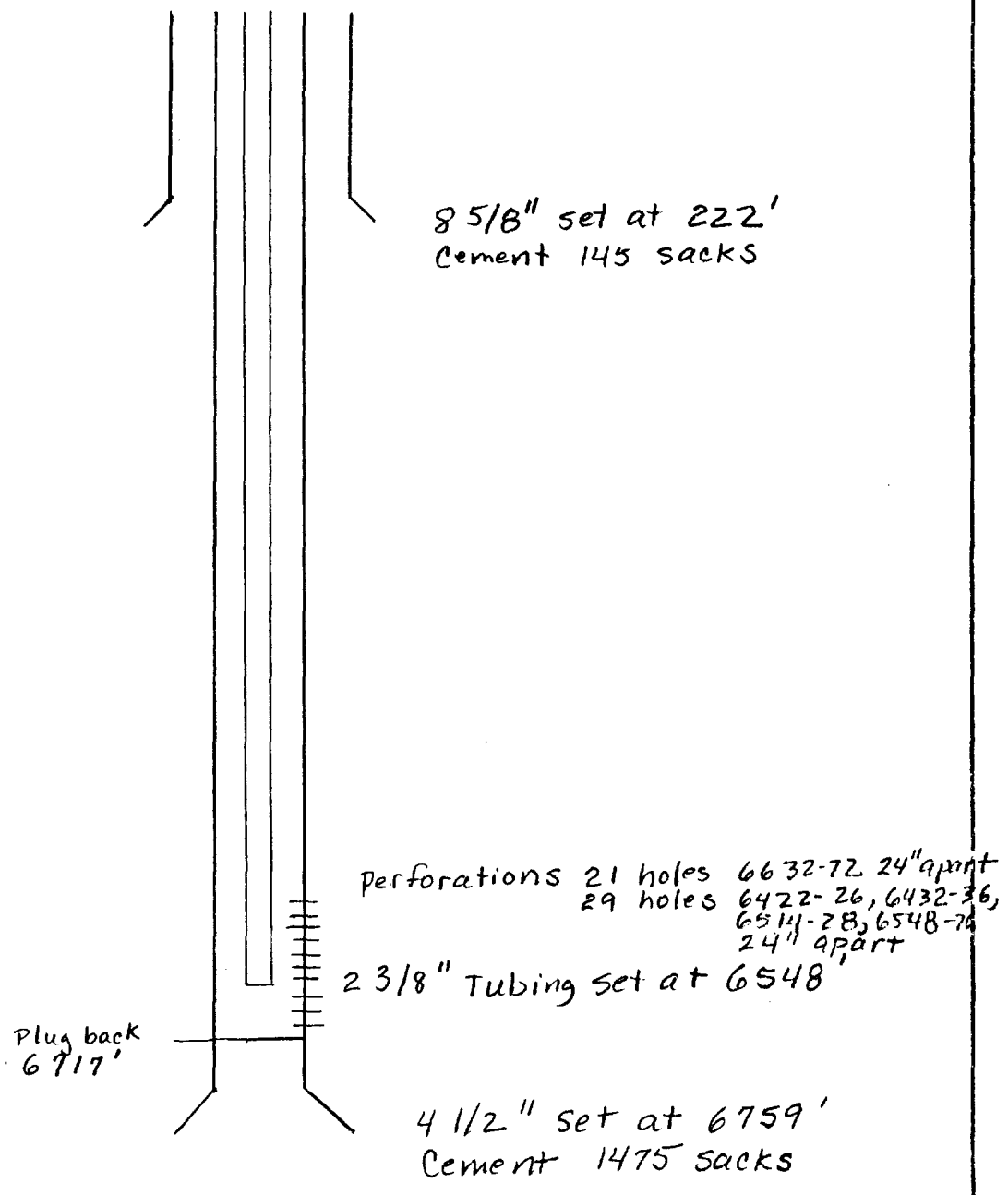
GEARHART

INDUCTION ELECTRICAL LOG

FILING NO.	COMPANY <u>CURTIS J. LITTLE</u>				
	WELL <u>SALAZAR NO.4-R</u>				
	FIELD <u>BASIN DAKOTA</u>				
	COUNTY <u>RIO ARRIBA</u> STATE <u>NEW MEXICO</u>				
LOCATION: <u>1630'FNL x 1460'FWL</u>			Other Services		
SEC <u>34</u> TWP <u>25N</u> RGE <u>6W</u>			CDL/CNL/GR		
Permanent Datum <u>GROUND LEVEL</u> Elev. <u>6378</u>			Elevations:		
Log Measured from <u>K.B.</u> , <u>13</u> Ft. Above Permanent Datum			KB <u>6391</u>		
Drilling Measured from <u>K.B.</u>			DF <u>6390</u>		
			GL <u>6378</u>		
Date	<u>1-27-84</u>				
Run No.	<u>ONE</u>				
Depth-Driller	<u>6753</u>				
Depth-Logger	<u>6753</u>				
Bottom Logged Interval	<u>6752</u>				
Top Logged Interval	<u>211</u>				
Casing-Driller	<u>8 5/8 @ 222</u>	@	@	@	@
Casing-Logger	<u>211</u>				
Bit Size	<u>7 7/8</u>				
Type Fluid in Hole	<u>GEL</u>				
Density and Viscosity	<u>9.0</u> <u>60</u>				
pH and Fluid Loss	<u>7.5</u> <u>7</u> cc		cc	cc	cc
Source of Sample	<u>Mud Pit</u>				
Rm @ Meas. Temp.	<u>1.8 @ 74 °F</u>	@	°F	@	°F
Rmf @ Meas. Temp.	<u>1.4 @ 69 °F</u>	@	°F	@	°F
Rmc @ Meas. Temp.	<u>1.2 @ 68 °F</u>	@	°F	@	°F
Source at Rmf and Rmc	<u>M</u> <u>M</u>				
Rm @ BHT	<u>---@ 180 °F</u>	@	°F	@	°F
Time	End Circulation	<u>20:00</u>			
	Logger on Bottom	<u>02:47</u>			
Max. Rec. Temp. Deg. F.	<u>180</u> °F		°F	°F	°F
Equip. No. and Location	<u>7607</u> <u>29-062</u>				
Recorded By	<u>Mease</u>				
Witnessed By	<u>Mr. Curtis Little</u>				



Kimbell oil of TX Well-bore sketch



8 5/8" set at 222'
Cement 145 sacks

Perforations 21 holes 6632-72 24" apart
29 holes 6422-26, 6432-36,
6511-28, 6548-74
24" apart

2 3/8" Tubing set at 6548'

Plug back
6717'

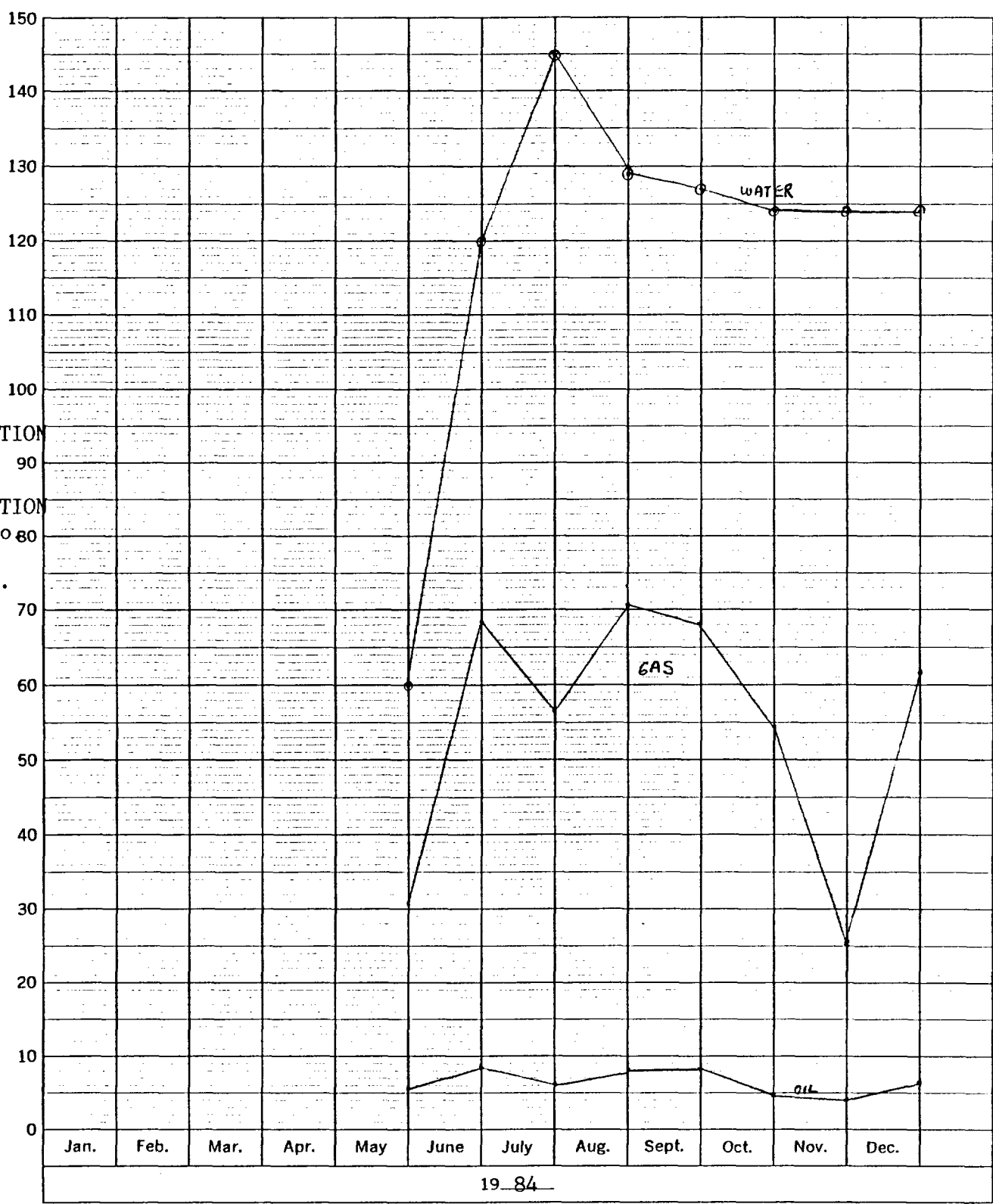
4 1/2" set at 6759'
Cement 1475 sacks

Basin Dakota
 Kimbell Oil Co. of TX
 Salazar Federal Well No. 4-E
 F-34-25N-6W
 Rio Arriba, New Mexico
 Date Production began: May 1984

46 3090

GAS PRODUCTION
 MMCF/Month 90
 OIL PRODUCTION
 100 BBLs/Mo 80
 WATER PROD.
 BBLs/Month 70

1 YEAR BY MONTHS X 150 DIVISIONS
 KEUFFEL & ESSER CO. MADE IN U.S.A.

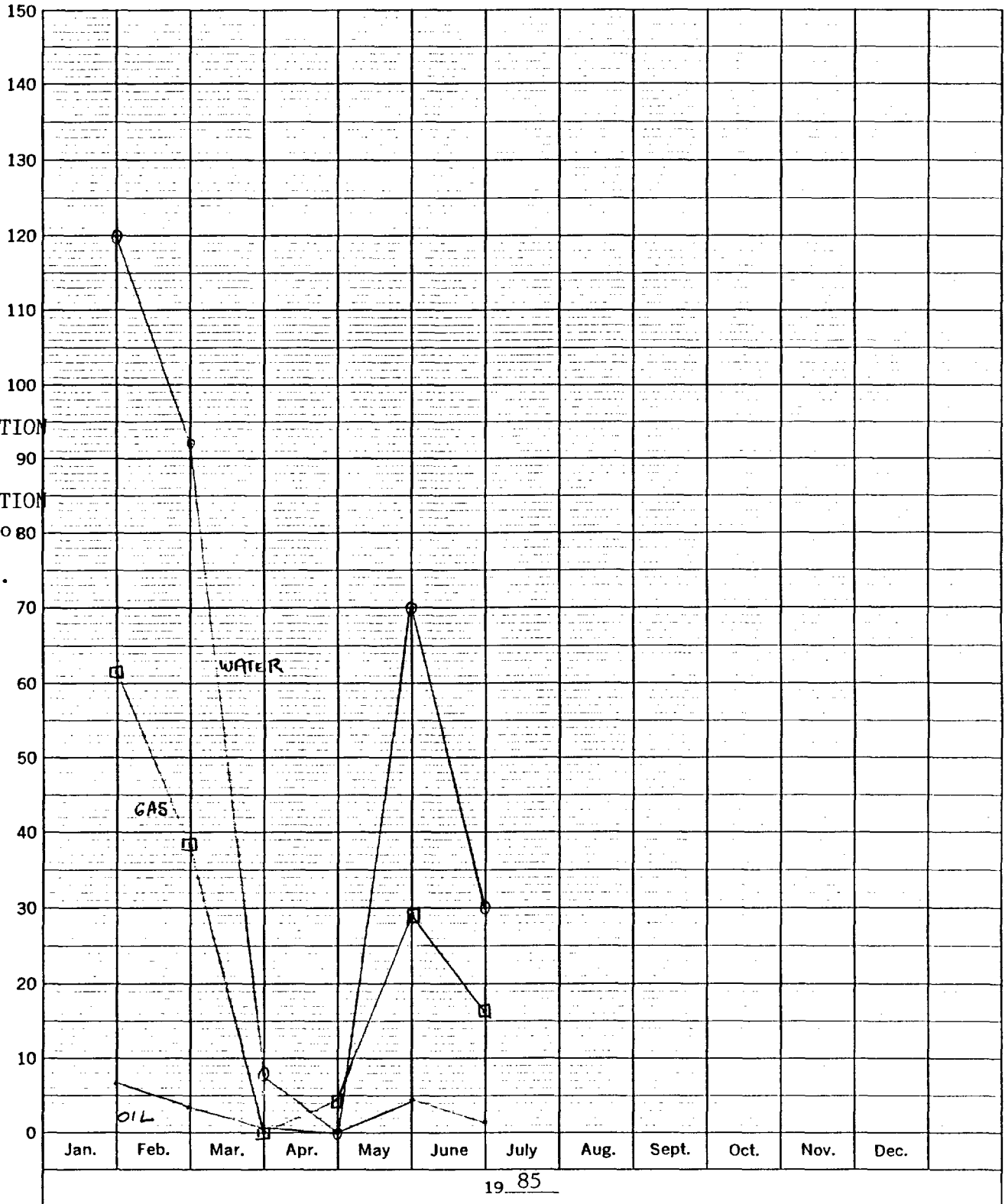


19 84

46 3090

GAS PRODUCTION
MMCF/Month 90
OIL PRODUCTION
100 BBL/Mo 80
WATER PROD.
BBL/Month 70

K&S 1 YEAR BY MONTHS X 150 DIVISIONS
KEUFFEL & ESSER CO. MADE IN U.S.A.



19 85

NEW MEXICO OIL CONSERVATION COMMISSION
WELL DELIVERABILITY TEST REPORT FOR 19 84

Form O-122-A
 Revised 1-1-66

POOL NAME Basin Dakota	POOL SLOPE n = .75	FORMATION Dakota	COUNTY Rio Arriba
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COMPANY Sims Oil Company, Inc.			WELL NAME AND NUMBER Salazar 4E		
UNIT LETTER F	SECTION 34h	TOWNSHIP 25N	RANGE 6W	PURCHASING PIPELINE El Paso Natural Gas Co.	
CASING O.D. - INCHES 4.500	CASING I.D. - INCHES 4.000	SET AT DEPTH - FEET 6759	TUBING O.D. - INCHES 2.375	TUBING I.D. - INCHES 1.995	TOP - TUBING PERF. - FEET 6422
GAS PAY ZONE FROM 6422 TO 6672		WELL PRODUCING THRU CASING TUBING X		GAS GRAVITY .661	GRAVITY X LENGTH 4245
DATE OF FLOW TEST FROM 7-12-84 TO 7-20-84			DATE SHUT-IN PRESSURE MEASURED 7-27-84		

PRESSURE DATA - ALL PRESSURES IN PSIA

(a) Flowing Casing Pressure (DWT) 812	(b) Flowing Tubing Pressure (DWT) 637	(c) Flowing Meter Pressure (DWT) 322	(d) Flow Chart Static Reading 317	(e) Meter Error (Item c - Item d) +5	(f) Friction Loss (a - c) or (b - c) 315	(g) Average Meter Pressure (Integr.) 311
(h) Corrected Meter Pressure (g + e) 316	(i) Avg. Wellhead Press. $P_t = (h + f)$ 637	(j) Shut-in Casing Pressure (DWT) 1337	(k) Shut-in Tubing Pressure (DWT) 1337	(l) $P_c =$ higher value of (j) or (k) 1337	(m) Del. Pressure $P_d = \frac{50}{669} \% P_c$ 669	(n) Separator or Dehydrator Pr. (DWT) for critical flow only 635

FLOW RATE CORRECTION (METER ERROR)

Integrated Volume - MCF/D 2295	Quotient of $\frac{\text{Item c}}{\text{Item d}}$ 1.0158	$\sqrt{\frac{\text{Item c}}{\text{Item d}}}$ 1.0079	Corrected Volume Q = 2313 MCF/D
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WORKING PRESSURE CALCULATION

$(1 - e^{-a})$.266	$(F_c Q_m)^2 (1000)$ 472,923	$R^2 = (1 - e^{-a}) (F_c Q_m)^2 (1000)$ 125,798	P_t^2 405,769	$P_w^2 = P_t^2 + R^2$ 531,567	$P_w = \sqrt{P_w^2}$ 729
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DELIVERABILITY CALCULATION

$D = Q \left[\frac{P_c^2 - P_d^2}{P_c^2 - P_w^2} \right]^n =$ 2313 $\left[\frac{1,340,008}{1,256,128} \right]^n \left(\frac{1.0667}{1.0667} \right)^n =$ 1,0496 $=$ 2428 MCF/D
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REMARKS:

This well has critical flow - Use FTP (b) for P_t (i).

SUMMARY

Item h	<u>316</u>	Psia
P_c	<u>1337</u>	Psia
Q	<u>2313</u>	MCF/D
P_w	<u>729</u>	Psia
P_d	<u>669</u>	Psia
D	<u>2428</u>	MCF/D

Company SIMS OIL COMPANY, INC.
 By E. A. Clement
 Title Prod. Supt.
 Witnessed By _____
 Company _____

NEW MEXICO OIL CONSERVATION COMMISSION
WELL DELIVERABILITY TEST REPORT FOR 19 85

Form CI 22-A
 Revised 1-1-66

POOL NAME Basin Dakota	POOL SLOPE n = .75	FORMATION Dakota	COUNTY Rio Arriba
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Meter No. **94-932**

COMPANY Kimbell Oil Company of Texas			WELL NAME AND NUMBER Salazar No. 4B		
UNIT LETTER F	SECTION 34	TOWNSHIP 25N	RANGE 6W	PURCHASING PIPELINE El Paso Natural Gas Co.	
CASING O.D. - INCHES 4.500	CASING I.D. - INCHES 4.000	SET AT DEPTH - FEET 6759	TUBING O.D. - INCHES 2.375	TUBING I.D. - INCHES 1.975	TOP - TUBING PERF. - FEET 6422
GAS PAY ZONE FROM 6422 TO 6672		WELL PRODUCING THRU CASING TUBING X		GAS GRAVITY .704	GRAVITY X LENGTH 4521
DATE OF FLOW TEST FROM 5/27/85 TO 6/4/85			DATE SHUT-IN PRESSURE MEASURED 6/12/85		

PRESSURE DATA - ALL PRESSURES IN PSIA

(a) Flowing Casing Pressure (DWt) 932	(b) Flowing Tubing Pressure (DWt) 787	(c) Flowing Meter Pressure (DWt) 262	(d) Flow Chart Static Reading 256	(e) Meter Error (Item c - Item d) +6	(f) Friction Loss (a - c) or (b - c) 525	(g) Average Meter Pressure (Integr.) 259
(h) Corrected Meter Pressure (g + e) 265	(i) Avg. Wellhead Press. $P_t = (h + f)$ 787	(j) Shut-in Casing Pressure (DWt) 1322	(k) Shut-in Tubing Pressure (DWt) 1322	(l) $P_c =$ higher value of (j) or (k) 1322	(m) Del. Pressure $P_d =$ <u>40</u> % P_c 529	(n) Separator or Dehydrator Pr. (DWt) for critical flow only 784

FLOW RATE CORRECTION (METER ERROR)

Integrated Volume - MCF/D 2035	Quotient of $\frac{\text{Item c}}{\text{Item d}}$ 1.0234	$\sqrt{\frac{\text{Item c}}{\text{Item d}}}$ 1.0116	Corrected Volume Q = 2059 MCF/D
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WORKING PRESSURE CALCULATION

$(1 - e^{-a})$.280	$(F_c Q_m)^2 (1000)$ 374,759	$R^2 = (1 - e^{-a}) (F_c Q_m)^2 (1000)$ 104,933	P_t^2 619,369	$P_w^2 = P_t^2 + R^2$ 724,302	$P_w = \sqrt{P_w^2}$ 851
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DELIVERABILITY CALCULATION

$$D = Q \left[\frac{P_c^2 - P_d^2}{P_c^2 - P_w^2} \right]^n = \frac{2059}{\left[\frac{1,467,843}{1,028,483} \right]^n} = \frac{1.4341}{1.3105} = 2698 \text{ MCF/D}$$

REMARKS:

**This well has critical flow -
 Use FIP (b) for P_t (i)**

SUMMARY

Item h	<u>265</u>	Psia
P_c	<u>1322</u>	Psia
Q	<u>2059</u>	MCF/D
P_w	<u>851</u>	Psia
P_d	<u>529</u>	Psia
D	<u>2692</u>	MCF/D

Company Kimbell Oil Company of Texas
 By E. A. Clement
 Title Prod. Supt.
 Witnessed By _____
 Company _____

$$G = 43560 (\phi)(1-S_w) \frac{(BHP/z)}{T_R} (35.3) (A) (h)$$

G = original gas in place, cf

ϕ = porosity

S_w = water saturation

BHP/z = initial Bottom hole Pressure / z , psi

T_R = temperature Reservoir, $^{\circ}R$

A = Area of drainage, acres

h = thickness, feet

Given:

$$BHP/z_{est} = 1900 \text{ psi}$$

$$T_R = 640^{\circ}R$$

$$h = 90 \text{ ft}$$

Assume:

$$\phi = 10\% \text{ (field avg)}$$

$$S_w = 40\% \text{ (" ")}$$

$$A = 160 \text{ acres}$$

Solution:

$$G = 43560 (.10) (1-.40) \frac{(1900)}{640} (35.3) (160) (90)$$

$$= 3,944,188,420 \text{ cf}$$

$$\text{or } 3.95 \text{ Bcf}$$

DIETZGEN CORPORATION
MADE IN U.S.A.

NO. 340-10 DIETZGEN GRAPH PAPER
10 X 10 PER INCH

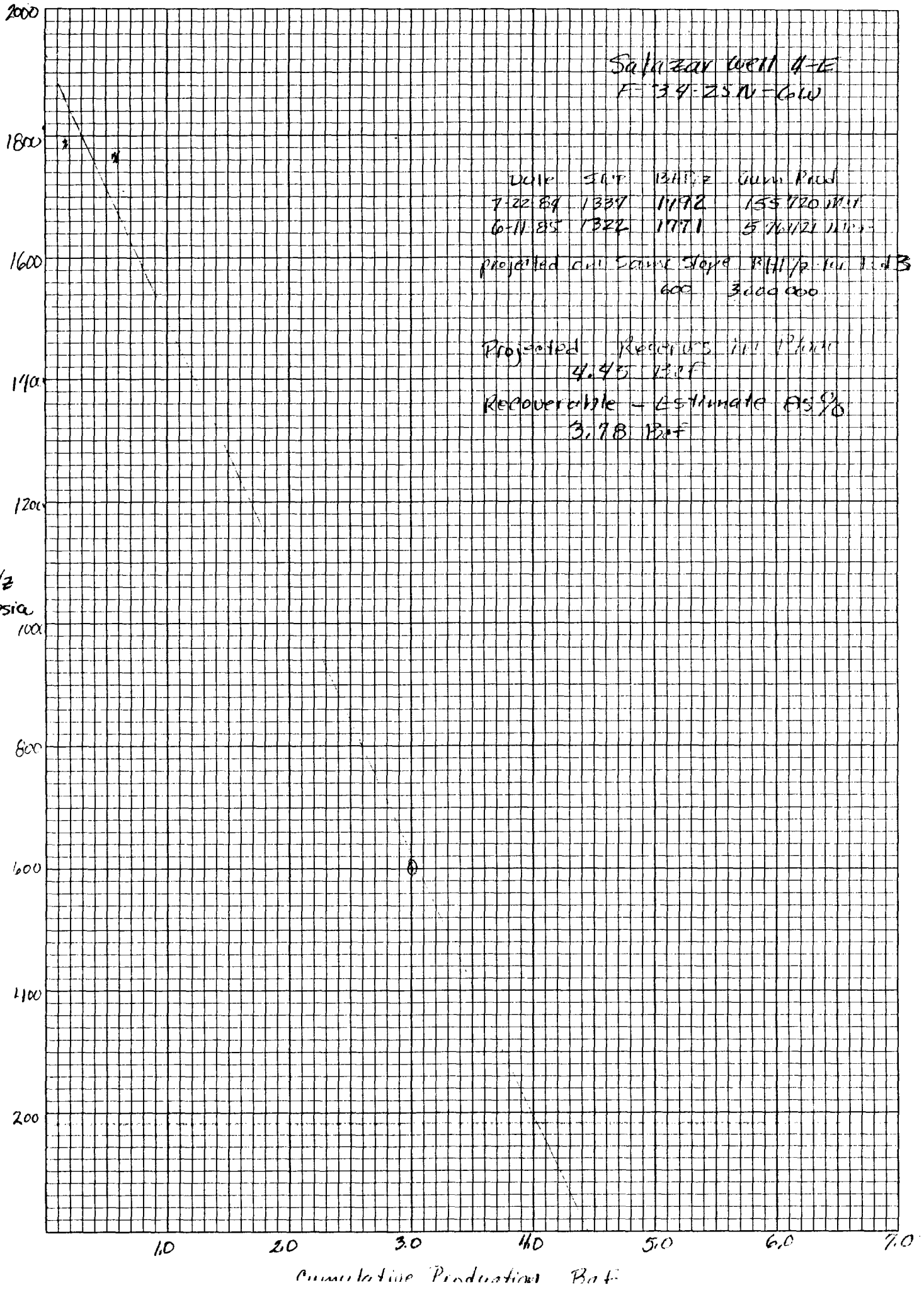
Safarzar Well 4-E
F-134-25N-61W

Date	SLP	13411/2	Sum Prod
7-22-84	1337	1772	155,720 MBF
6-11-85	1322	1771	5,761,21 MBF

projected on same slope BHP/2 for 134B
600 3,000,000

Projected Reserves in 1st Phase
4.45 Bcf
Recoverable - Estimate 85%
3.78 Bcf

BHP/2
psia
1000



1.0 2.0 3.0 4.0 5.0 6.0 7.0
Cumulative Production Bcf

PRODUCTION TABLE

WELL NAME Federal Well No. 3

Completion Date 11-1-63

WELL LOCATION L-34-25N-6W

Initial Potential 6152 MCF/Day

Perfs 6518-6662

Initial Pressure SICP = 2322

Initial GOR/Gravity _____

SICP psia	DATE	PRODUCTION DAYS / SHUT-IN <small>estimated</small>		OIL/H ₂ O PRODUCTION BCLS		RATE /Day WATER	CUMULATIVE WATER BCLS	GAS PRODUCTION MCF	RATE /Day	CUMULATIVE MCF
	1965	365	0	4350	0	0.00	0	182813	501	434736
1512	1970	335	30	2104	0	0.00	0	138997	415	1643882
1262	1973	358	7	2304	0	0.00	0	265392	741	2647309
	1974	365	0	2446	0	0.00	0	230591	632	2608809
1092 (75)	1976	365	0	1918	0	0.00	0	191954	526	3007041
	1977	365	0	1713	0	0.00	0	190858	523	3197890
	1978	365	0	1541	353	.97	353	181755	498	3379654
2-5-81 1037	1980	365	0	1194	368	1.01	1117	160931	441	3698353
5-12-81 992	1981	314	51	1372	307	.98	1424	129774	414	3828127
7-12-83	1982	231	134	1209	267	1.16	1691	96681	419	3924808
1132	1983	150	215	838	127	.85	1818	75708	505	4000517
	1984	115	250	555	163	1.42	1981	60147	523	4060663
	1985	69	51	475	105	1.52	2086	39034	566	4099697
	(through April)									

LIST OF ADJACENT WELLS/OPERATORS

Operator	Well Name	Well Location	Proration Unit
Merrion (abd)	Sal. G. Com 26 1	m-26-25N-6W	W $\frac{1}{2}$ section 26
Kimbell	Sal. Fed. 3	h-27-25N-6W	E $\frac{1}{2}$ section 27
Kimbell	Coral 2	m-27-25N-6W	W $\frac{1}{2}$ section 27
Merrion	Old Rock Com 2	p-28-25N-6W	E $\frac{1}{2}$ section 28
El Paso	Can. Largo Ut 135	h-33-25N-6W	E $\frac{1}{2}$ section 33
Kimbell	Federal 3 Federal 3-E	1-34-25N-6W i-34-25N-6W	S $\frac{1}{2}$ section 34
Kimbell	Federal A 3 Federal A 3-E	m-35-25N-6W e-35-25N-6W	W $\frac{1}{2}$ section 25

Solozer Well 4-E

1630N 1460W Section 34

Township 25 N, Range 6W

Meridian,

Dakota Wells

	28		27		26		
Can Largo *1319 Merrion	Oil Bank Dam 2 *1150 TRP=2197 Merrion	Coral 2 *2800 TRP=2190	Solozer 4-E *1984 TRP=2190 Merrion	Solozer 4-E *1984 TRP=2190 Merrion	Solozer 4-E *1984 TRP=2190 Merrion	Solozer 4-E *1984 TRP=2190 Merrion	Solozer 4-E *1984 TRP=2190 Merrion
	33						
Can Largo *188 TRP=180 Fed 3-E	Can Largo *195 TRP=2249	Fed 3 *1952 TRP=2222 1963 Kimbell	Solozer 4-E *1984 TRP=2190 Merrion	Solozer 4-E *1984 TRP=2190 Merrion	Solozer 4-E *1984 TRP=2190 Merrion	Solozer 4-E *1984 TRP=2190 Merrion	Solozer 4-E *1984 TRP=2190 Merrion
25N							
24N							

Notes

24N-6W
D-2 Farming 3-E Abd Getty

Cum gas: 13456 McF water = 20,000 bbls
oil = 142 bbls

25N-6W

M-26 Solozer 4-E Con 26 #1 Merrion
Abd Cum gas: 8096 McF water = 289 bbls
oil = 730 bbls

M-26 Canan Largo 319 Abd Merrion
Cum gas: 20524 McF Cum water = 22 bbls
oil = 23129 bbls

H-34 Solozer 4 DK Abd Merrion/Kim
Cum gas: 131654 McF Cum water = 2905
oil = 10408 bbls

A-35 Warren Fed 1 Abd Kimbell
Cum gas: 3302 McF Cum water = 0
Cum oil = 104 bbls

Farm 3-E
TRP=3050
GD=1150
1458
Getty

Farm 3
TRP=3331
1960
Getty

Farm 3-E
TRP=3359
1984

Farm 3-E
TRP=2324
1960
Getty

Farm 3-E
TRP=3331
1960
Getty

Farm 3-E
TRP=3331
1960
Getty

Farm 3-E
TRP=3331
1960
Getty

Farm 3-E
TRP=3331
1960
Getty

Farm 3-E
TRP=3331
1960
Getty

Farm 3-E
TRP=3331
1960
Getty