

**REOPENED CASE NO. 11089**

**March 20, 1997**

**EXHIBIT NO. 10**

**Examiner Catanach**



MERIDIAN OIL, INC.

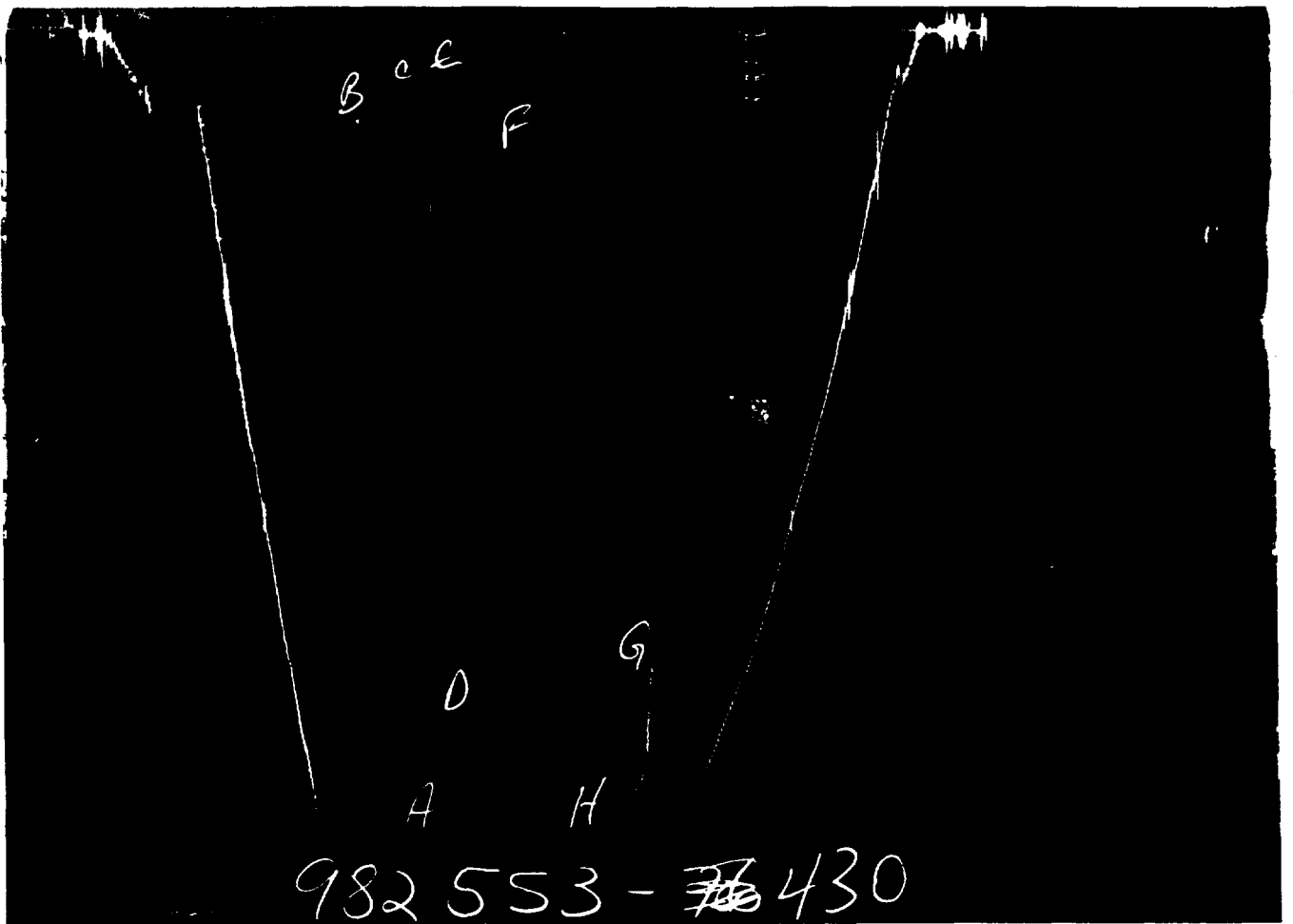
LEASE : UTE MOUNTAIN

WELL NO.: UTE 41

TEST NO.: 1

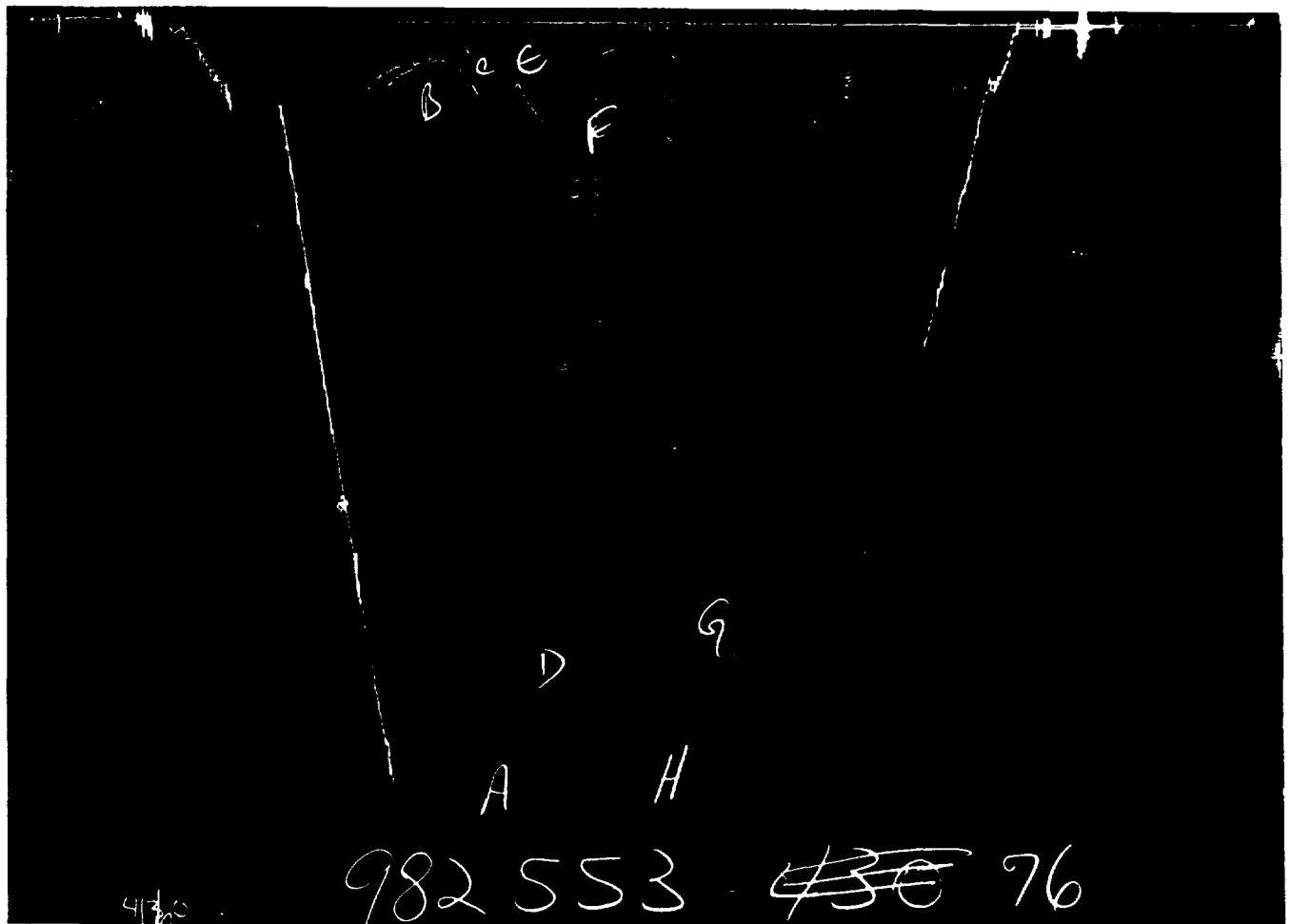
## DRILL STEM TEST REPORT





GAUGE NO: 430 DEPTH: 8851.3 BLANKED OFF: NO HOUR OF CLOCK: 24

ID	DESCRIPTION	PRESSURE		TIME		TYPE
		REPORTED	CALCULATED	REPORTED	CALCULATED	
A	INITIAL HYDROSTATIC		4172.0			
B	INITIAL FIRST FLOW		464.7			
C	FINAL FIRST FLOW		328.4	15.0	15.2	F
C	INITIAL FIRST CLOSED-IN		328.4			
D	FINAL FIRST CLOSED-IN		3494.0	45.0	44.6	C
E	INITIAL SECOND FLOW		431.4			
F	FINAL SECOND FLOW		587.7	60.0	59.8	F
F	INITIAL SECOND CLOSED-IN		587.7			
G	FINAL SECOND CLOSED-IN		3495.9	180.0	180.4	C
H	FINAL HYDROSTATIC		4146.5			



GAUGE NO: 76 DEPTH: 8983.0 BLANKED OFF: YES HOUR OF CLOCK: 24

ID	DESCRIPTION	PRESSURE		TIME		TYPE
		REPORTED	CALCULATED	REPORTED	CALCULATED	
A	INITIAL HYDROSTATIC		4239.0			
B	INITIAL FIRST FLOW		448.2			
C	FINAL FIRST FLOW		381.9	15.0	15.2	F
C	INITIAL FIRST CLOSED-IN		381.9			
D	FINAL FIRST CLOSED-IN		3546.0	45.0	44.6	C
E	INITIAL SECOND FLOW		490.4			
F	FINAL SECOND FLOW		631.1	60.0	59.8	F
F	INITIAL SECOND CLOSED-IN		631.1			
G	FINAL SECOND CLOSED-IN		3539.0	180.0	180.4	C
H	FINAL HYDROSTATIC		4205.9			

## EQUIPMENT & HOLE DATA

FORMATION TESTED: DESERT CREEK

NET PAY (ft): 53.0

GROSS TESTED FOOTAGE: 112.0 PACKER TO T.D.

ALL DEPTHS MEASURED FROM: K.B.

CASING PERFS. (ft): \_\_\_\_\_

HOLE OR CASING SIZE (in): 7.875

ELEVATION (ft): 6902.0 AT GROUND LEVEL

TOTAL DEPTH (ft): 8986.0

PACKER DEPTH(S) (ft): 8866. 8874

FINAL SURFACE CHOKE (in): 0.25000

BOTTOM HOLE CHOKE (in): 0.750

MUD WEIGHT (lb/gal): 9.10

MUD VISCOSITY (sec): 46

ESTIMATED HOLE TEMP. (°F): \_\_\_\_\_

ACTUAL HOLE TEMP. (°F): 191 @ 8982.0 ft

TICKET NUMBER: 98255300

DATE: 07-20-96 TEST NO: 1

TYPE DST: OPEN HOLE

FIELD CAMP:

VERNAL

TESTER: RANDY RIPPLE  
MORRIS KIRKPATRICK

WITNESS: KURT SHIPLEY

DRILLING CONTRACTOR:

4 CORNERS DRILLING RIG #4

## FLUID PROPERTIES FOR RECOVERED MUD & WATER

SOURCE

RESISTIVITY

CHLORIDES

_____	_____ @ _____ °F	_____ ppm
_____	_____ @ _____ °F	_____ ppm
_____	_____ @ _____ °F	_____ ppm
_____	_____ @ _____ °F	_____ ppm
_____	_____ @ _____ °F	_____ ppm
_____	_____ @ _____ °F	_____ ppm

## SAMPLER DATA

Psig AT SURFACE: 675.0 ??

cu.ft. OF GAS: 4.500

cc OF OIL: TRACE

cc OF WATER: \_\_\_\_\_

cc OF MUD: 500.0

TOTAL LIQUID cc: 500.0

## HYDROCARBON PROPERTIES

OIL GRAVITY (°API): \_\_\_\_\_ @ \_\_\_\_\_ °F

GAS/OIL RATIO (cu.ft. per bbl): \_\_\_\_\_

GAS GRAVITY: \_\_\_\_\_

## CUSHION DATA

TYPE

AMOUNT

WEIGHT

WATER (FT.) 815.0 8.33

RECOVERED :

MEASURED FROM  
TESTER VALVE

## REMARKS :

REPORTED SAMPLER PRESSURE IS QUESTIONABLE. IT APPEARS THE SAMPLER TRAPPED A PORTION OF THE CLOSED-IN PRESSURE AS THE SAMPLER PRESSURE SHOULD BE SOMEWHAT LESS THAN THE FINAL DOWNHOLE FLOWING PRESSURE.

REPORT NO.  
142614

PAGE NO. 1

TEST DATE:  
24-APR-1996

# STAR

## Schlumberger Transient Analysis Report Based on Model Verified Interpretation Of a Schlumberger Well Test

Schlumberger

COMPANY: MERIDIAN OIL, INC.

WELL: UTE COM #23

### TEST IDENTIFICATION

Test Type ..... S/L BUILDUP  
Test No. .... ONE (POST-FRAC)  
Test Interval (ft) ..... 8265 to 8325

### WELL LOCATION

Field ..... BARKER CREEK  
County ..... SAN JUAN  
State ..... COLORADO

### COMPLETION CONFIGURATION

Casing Size O.D./I.D. (in) ... 5.5 / 4.892  
Hole Size (in) ..... 7.875  
Perforated Interval (ft) ..... 8265 to 8325  
Shot Density (shots/ft) ..... 4  
Net Pay (ft) ..... 46

### TEST STRING CONFIGURATION

Tubing Length (ft)/I.D. (in) .. 8276 / 2.441  
Packer Depth (ft) ..... 8205  
Gauge Depth (ft)/Type ..... 8236 / 9531

### TEST CONDITIONS

Prod. Time (since frac) (hrs) .. 1320  
Buildup Duration (hrs) ..... 159

### INTERPRETATION RESULTS

Model of Behavior ..... HYD. FRAC.  
Fluid Type Used for Analysis.. GAS  
Reservoir Pressure (psi) ..... 3075 @ 8236 Ft  
Transmissibility (md.ft/cp) .. 32.6  
Effective Permeability (md) .. 0.014 (to Gas)  
Fracture Half-Length (ft) .... 33  
Fracture Capacity (Md.Ft) ..... 168.7  
Equivalent Skin ..... -3.9  
Radius of Investigation (ft).. 63

### ROCK/FLUID/WELLBORE PROPERTIES

Oil Density (deg. API) ..... 50  
Gas Gravity ..... 0.65  
Liquid/Gas Ratio (STB/MMSCF) . 0  
Res.Saturations, Sg/So/Sw (%). 72/0/28  
Water Cut (%) ..... 0  
Viscosity (cp) ..... 0.01961  
Total Compressibility (1/psi). 2.131E-04  
Porosity (%) ..... 11.2  
Reservoir Temperature (F) .... 208

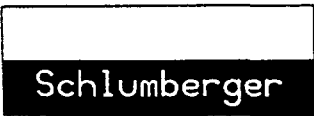
PRODUCTION RATE DURING TEST: 63.65 MSCF/D = Q-Last

### COMMENTS:

A 7-DAY BOTTOMHOLE PRESSURE BUILDUP TEST WAS CONDUCTED FROM 24-APR-1996 TO 01-MAY-1996 AFTER 55-DAYS PRODUCTION SINCE HYDRAULICALLY FRACTURE- TREATING THE WELL. ANALYSIS OF THE DIAGNOSTIC LOG-LOG PLOT OF PRESSURE AND DERIVATIVE INDICATES THE PRESENCE OF A HOMOGENEOUS SYSTEM WITH SKIN AND VARIABLE WELLBORE STORAGE EFFECTS AT EARLY TIME AND TRANSITIONAL FLOW REGIME AT MID TO LATE TIMES; INFINITE ACTING RADIAL FLOW WAS NOT REACHED DURING THE BUILDUP. THE BUILDUP RESPONSE WAS CHARACTERISTIC OF EITHER A SHORT HIGHLY CONDUCTIVE FRACTURE OR SIMPLY A LOW VALUE OF SKIN AND WELLBORE STORAGE, i.e., LOW CD\* $\epsilon$  (2s). SINCE THE ZONE HAD BEEN FRACTURE TREATED, THE BUILDUP DATA WAS MATCHED USING A HOMOGENEOUS, FINITE CONDUCTIVITY VERTICAL FRACTURE RESERVOIR MODEL (SEE ANALYSIS RESULTS AND PLOTS, PAGES 2-5).

THE TESTED INTERVAL HAS THE CHARACTERISTICS OF VERY LOW EFFECTIVE PERMEABILITY TO GAS AND A HIGHLY STIMULATED WELLBORE CONDITION, WITH AN EQUIVALENT SKIN FACTOR OF -3.9. HOWEVER, THE EFFECTIVE FRACTURE HALF-LENGTH AT THE TIME OF THE TEST WAS ONLY 33 FT, WHICH COULD INDICATE THAT THE FRACTURE IS STILL CLEANING UP. FOR QUESTIONS ABOUT THIS REPORT, PLEASE CONTACT DEBORA HALLFORD AT (303) 843-9090.

CALCULATIONS  
GAS WELL  
LOG-LOG ANALYSIS



LOG (DELTA M(P)) VS. LOG (DELTA T) PLOT

HOMOGENEOUS, INFINITE SYSTEM  
VARIABLE WELLBORE STORAGE  
FINITE CONDUCTIVITY VERTICAL FRACTURE  
PD VS. TD/CD

DATA IDENTIFICATION

FLOW PERIOD = 3, BUILDUP  
M(P) = 3.203E+07 PSI\*\*2/CP @ DELTA T=0  
FLOW RATE CHANGE = 63.650 MSCF/D

TYPE-CURVE MATCH

CURVE MATCH, FCD = 370.919  
CDF = 1.93151E-01  
PRESSURE MATCH, PD/DELTA M(P) = 1.060E-08 1/(PSI\*\*2/CP)  
TIME MATCH, (TOF)/DELTA T = 7.3224E-03 1/HR

CALCULATIONS

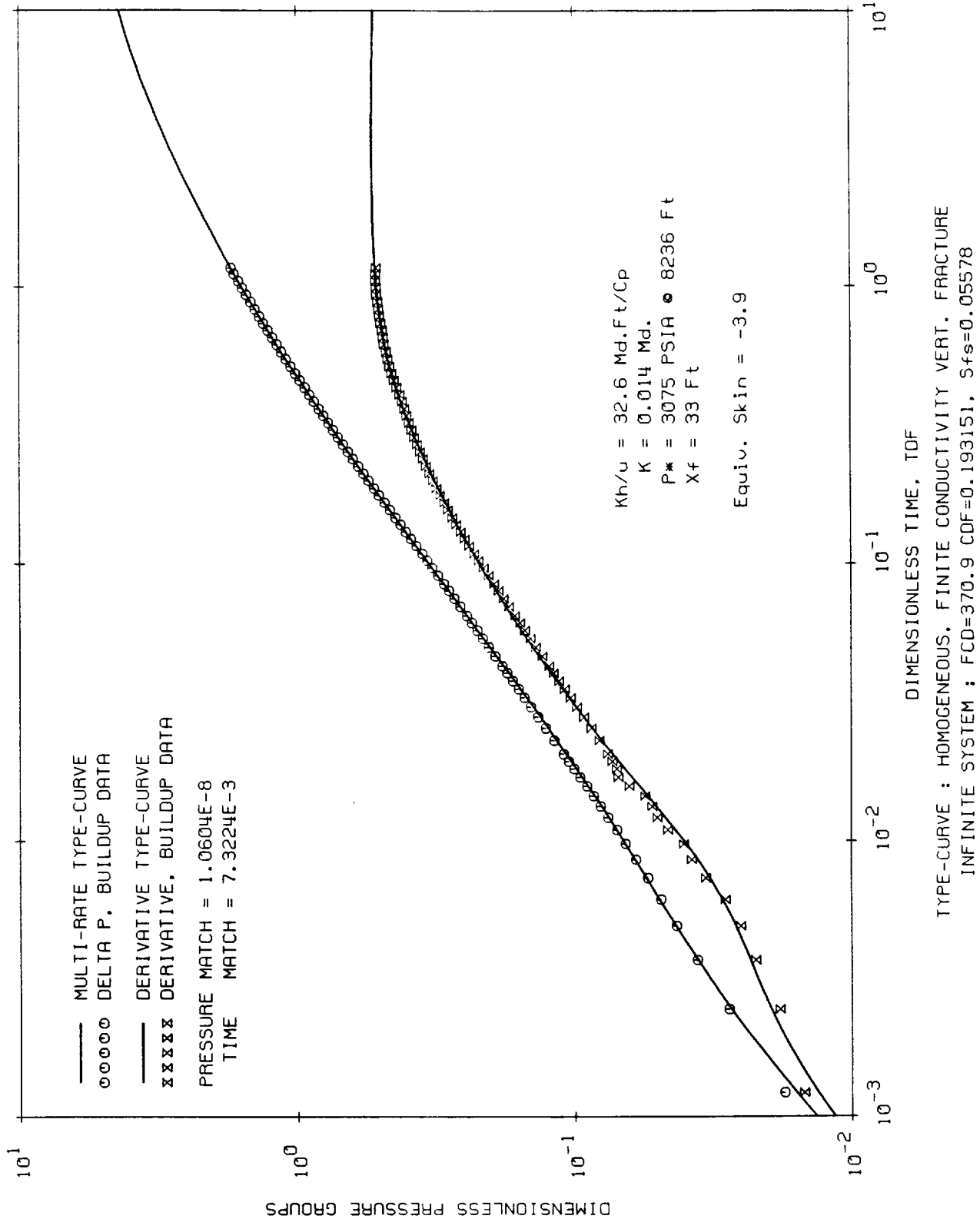
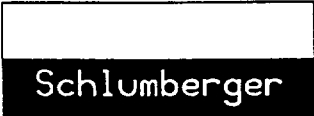
KH ..... 0.6398 MD.FT  
KH/MU ..... 32.626 MD.FT/CP  
K ..... 0.01391 MD  
C ..... 0.2539 BBL/PSI  
CD ..... 1919.3  
FRACTURE HALF-LENGTH, Xf .. 32.7 FT  
EQUIVALENT SKIN, S ..... -3.909  
RADIUS OF INVESTIGATION ... 63.062 FT (@ 159.126 HR)

COMMENTS

USING HOMOGENEOUS, INFINITE SYSTEM RESERVOIR MODEL WITH  
VARIABLE WELLBORE STORAGE AND A FINITE CONDUCTIVITY  
VERTICAL FRACTURE ; Ca/C=0.32 (1) 1.08 (2) CoD=0.027 (1) 0.159 (2)



DIMENSIONLESS MULTI-RATE  
PLOT: LOG-LOG MATCH WITH  
FINITE COND. VERT. FRACTURE



REPORT NO.  
142613

PAGE NO. 1

TEST DATE:  
25-APR-1996

S T A R

Schlumberger Transient Analysis Report  
Based on Model Verified Interpretation  
Of a Schlumberger Well Test

Schlumberger

COMPANY: MERIDIAN OIL, INC.

WELL: UTE COM #27

TEST IDENTIFICATION

Test Type ..... S/L BUILDUP  
Test No. .... ONE  
Test Interval (ft) ..... 8190 to 8288

WELL LOCATION

Field ..... BARKER CREEK  
County ..... SAN JUAN  
State ..... COLORADO  
Sec/Twn/Rng ..... 16/32N/14W

COMPLETION CONFIGURATION

Casing Size O.D./I.D. (in) ... 5.5 / 4.892  
Hole Size (in) ..... 7.875  
Perforated Interval (ft) ..... 8190 to 8288  
Shot Density (shots/ft) ..... 4  
Net Pay (ft) ..... 46

TEST STRING CONFIGURATION

Tubing Length (ft)/I.D. (in).. 8064 / 2.441  
Packer Depth (ft) ..... 7999  
Gauge Depth (ft)/Type ..... 8031 / 9060

TEST CONDITIONS

Producing Time (hrs) ..... 1272  
Buildup Duration (hrs) ..... 265.4

INTERPRETATION RESULTS

Model of Behavior ..... HYD. FRACTURE  
Fluid Type Used for Analysis.. GAS  
Reservoir Pressure (psi) ..... 2595 @ 8031 Ft  
Transmissibility (md.ft/cp) .. 59.3  
Effective Permeability (md) .. 0.023 (to Gas)  
Fracture Half-Length (ft) .... 236✓  
Fracture Capacity (md.ft) .... 741.4✓  
Equivalent Skin Factor ..... -5.9

ROCK/FLUID/WELLBORE PROPERTIES

Oil Density (deg. API) ..... 56  
Gas Gravity ..... 0.65  
Impurities, N2/CO2/H2S (mol.%) 0/0/0.5  
Liquid/Gas Ratio (STB/MMSCF) . 1.66  
Water Cut (%) ..... 0  
Viscosity (cp) ..... 0.01831  
Total Compressibility (1/psi). 2.70E-04  
Porosity (%) ..... 10.2  
Reservoir Temperature (F) .... 208

PRODUCTION RATE DURING TEST: 659 MSCF/D = Q-Last

COMMENTS:

AN 11-DAY BOTTOMHOLE PRESSURE BUILDUP TEST WAS CONDUCTED FROM 25-APR-1996 TO 06-MAY-1996 FOLLOWING 53-DAYS PRODUCTION SINCE HYDRAULIC FRACTURE TREATMENT. ANALYSIS OF THE DIAGNOSTIC LOG-LOG PLOT OF PRESSURE AND DERIVATIVE INDICATES THE PRESENCE OF A HOMOGENEOUS SYSTEM WITH VARIABLE WELLBORE STORAGE EFFECTS AT EARLY TIMES. AT MID TIME, BILINEAR FLOW REGIME IS PRESENT (ONE/FOURTH SLOPE ON THE DERIVATIVE) WHEN THE BUILDUP RESPONSE IS LINEAR FROM THE MATRIX INTO THE FRACTURE AND LINEAR THROUGH THE FRACTURE. AT THE END OF THE TEST FORMATION LINEAR FLOW WAS PRESENT (ONE-HALF SLOPE ON THE DERIVATIVE). WHEN THE BUILDUP RESPONSE IS LINEAR FROM THE FORMATION INTO THE FRACTURE. UNTIL THIS FLOW REGIME ENDS (I.E., TRANSIENT EXTENDS BEYOND THE TIPS OF THE FRACTURE), ONLY THE PRODUCT OF  $KX_f$  IS UNIQUE. THE BUILDUP DATA WAS MATCHED USING A HOMOGENEOUS SYSTEM RESERVOIR MODEL WITH VARIABLE WELLBORE STORAGE AND A FINITE CONDUCTIVITY VERTICAL FRACTURE (SEE ANALYSIS RESULTS AND PLOTS, PAGES 2-5). ONLY THE PRODUCT OF THE FRACTURE HALF-LENGTH (236-ft) AND PERMEABILITY (0.024-md) ARE UNIQUE. THUS, IF PERMEABILITY IS INCREASED, FRACTURE HALF-LENGTH MUST DECREASE, AND VICE VERSA.

THE TESTED INTERVAL HAS THE CHARACTERISTICS OF LOW PERMEABILITY EFFECTIVE TO GAS AND A HIGHLY STIMULATED WELLBORE CONDITION AT THE TIME OF THE TEST. FOR QUESTIONS ABOUT THIS REPORT, PLEASE CONTACT DEBORA HALLFORD AT (303) 843-9090.

REPORT NO.  
142613

PAGE NO. 2

CALCULATIONS  
GAS WELL  
LOG-LOG ANALYSIS

Schlumberger

LOG (DELTA M(P)) VS. LOG (DELTA T) PLOT

HOMOGENEOUS, INFINITE SYSTEM  
VARIABLE WELLBORE STORAGE  
FINITE CONDUCTIVITY VERTICAL FRACTURE  
PD VS. TDF

DATA IDENTIFICATION

FLOW PERIOD = 7. BUILDUP  
M(P) = 2.497E+07 PSI\*\*2/CP @ DELTA T=0  
FLOW RATE CHANGE = 659.00 MSCF/D

TYPE-CURVE MATCH

CURVE MATCH, FCD = 1.33308E+02  
CDF = 7.02009E-02  
PRESSURE MATCH, PD/DELTA M(P) = 1.735E-09 1/(PSI\*\*2/CP)  
TIME MATCH, (TDF)/DELTA T = 2.22566E-04 1/HR

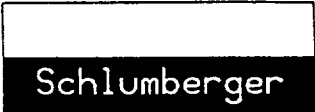
CALCULATIONS

KH ..... 1.086 MD.FT  
KH/MU ..... 59.304 MD.FT/CP  
K ..... 0.02361 MD  
C ..... 5.519 BBL/PSI  
CD ..... 36157  
FRACTURE HALF-LENGTH, X<sub>f</sub> .. 235.5 FT  
EQUIVALENT SKIN, S ..... -5.883  
FRACTURE CAPACITY, K<sub>f</sub>\*w ... 741.4 Md.Ft

COMMENTS

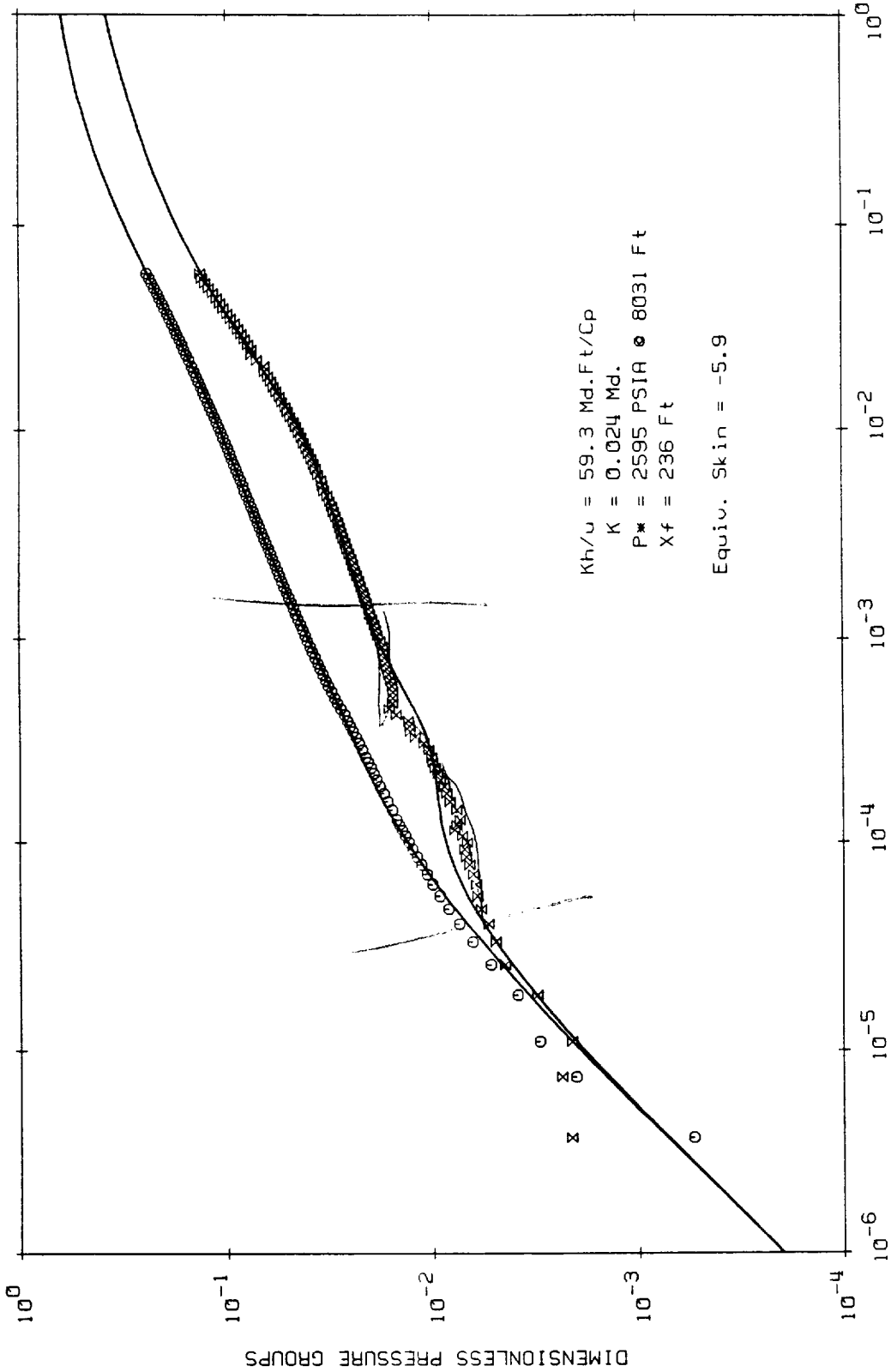
USING HOMOGENEOUS, INFINITE SYSTEM RESERVOIR MODEL WITH  
VARIABLE WELLBORE STORAGE AND A FINITE CONDUCTIVITY  
VERTICAL FRACTURE ; C<sub>a</sub>/C=2.75 (1) 0.010 (2) 2.3 (3) 1.1 (4)

DIMENSIONLESS MULTI-RATE  
PLOT: LOG-LOG MATCH WITH  
FINITE COND. VERT. FRACTURE



MULTI-RATE TYPE-CURVE  
PRESSURE MATCH = 1.7355E-9  
TIME MATCH = 2.2257E-4

DERIVATIVE TYPE-CURVE  
DERIVATIVE, BUILDUP DATA



DIMENSIONLESS TIME, tDf  
TYPE-CURVE : HOMOGENEOUS SYSTEM, FINITE COND. VERT. FRACTURE  
FCD=133.3 CDF=0.0702 Ca/C=2.75 CoD=8.65E-03

REPORT NO.  
UTE24

PAGE NO. 1

TEST DATE:  
19-JUN-1995

# STAR

## Schlumberger Transient Analysis Report Based on Model Verified Interpretation

Schlumberger

COMPANY: MERIDIAN OIL, INC.

WELL: UTE 24

### TEST IDENTIFICATION

Test Type ..... S/L BUILDUP  
Test No. .... ONE

### WELL LOCATION

County .....  
State .....

### COMPLETION CONFIGURATION

Hole Size (in) ..... 7.875  
Net Pay (ft) ..... 46

### TEST STRING CONFIGURATION

### TEST CONDITIONS

Producing Time (hrs) ..... 6984  
Shut-in Duration (hrs) ..... 71.3

### INTERPRETATION RESULTS

Model of Behavior ..... HOMOGENEOUS  
Fluid Type Used for Analysis.. GAS  
Reservoir Pressure (psi) ..... 2929  
Transmissibility (md.ft/cp) .. 9170  
Effective Permeability (md) .. 3.5 (to Gas)  
Skin Factor ..... -1.8  
Equiv. Frac. Half-Length (ft). 4  
Wedge Angle (deg) ..... 96  
Distance to Sides (ft) ..... 112, 240  
Dist. to Intersect (ft) ..... 256

### ROCK/FLUID/WELLBORE PROPERTIES

Gas Gravity ..... 0.7  
Impurities, N2/CO2/H2S (mol.%) 0/0/0  
Liquid/Gas Ratio (STB/MMSCF) . 0  
Water Cut (%) ..... 0  
Viscosity (cp) ..... 0.01774  
Total Compressibility (1/psi). 3.158E-04  
Porosity (%) ..... 11.8  
Reservoir Temperature (F) .... 202

PRODUCTION RATE DURING TEST: 5200 MSCF/D = Q-Last

### COMMENTS:

A 3-DAY BOTTOMHOLE PRESSURE BUILDUP TEST WAS CONDUCTED FROM 19-JUN-1995 TO 22-JUN-1995 FOLLOWING 291-DAYS PRODUCTION. THE BUILDUP WAS ANALYZED BY GEOQUEST SCHLUMBERGER IN JUNE 1996 TO PROVIDE AN ALTERNATIVE INTERPRETATION TO THAT ALREADY PERFORMED INHOUSE BY MERIDIAN OIL, INC.

ANALYSIS OF THE DIAGNOSTIC LOG-LOG PLOT OF PRESSURE AND DERIVATIVE INDICATES THE PRESENCE OF SKIN AND DECREASING WELLBORE STORAGE EFFECTS AT EARLY TIME AND TRANSITIONAL FLOW REGIME AT MID TO LATE TIMES, WITH AN INCREASING DERIVATIVE SLOPE AFTER 3.5 HRS SHUT-IN TIME. THIS CHARACTERISTIC IS NOT UNIQUE, AS SEVERAL RESERVOIR MODELS EXHIBIT A SIMILAR RESPONSE; TWO-POROSITY, RADIALY COMPOSITE, AND MULTIPLE BOUNDARIES. THE BUILDUP WAS MATCHED USING A HOMOGENEOUS SYSTEM MODEL WITH SKIN AND DECREASING WELLBORE STORAGE AND WEDGE-SHAPED GEOMETRY OUTER SEALING (NO-FLOW) BOUNDARIES. BASED ON THE MATCH WITH THIS MODEL, THE WELL IS SITUATED ABOUT 112 ft FROM ONE SEALING BARRIER AND 240 ft FROM THE SECOND SEALING BARRIER, WITH 260-ft TO THE INTERSECT IN A 96-Degree WEDGE-SHAPED GEOMETRY. THE SEALING BOUNDARIES REPRESENT A MARKED DECREASE IN THE OVERALL TRANSMISSIBILITY (kh/u), AND COULD BE DRAINAGE PATTERN BOUNDARIES AS WELL AS PHYSICAL BOUNDARIES.

THE TESTED INTERVAL HAS THE CHARACTERISTICS OF GOOD PERMEABILITY EFFECTIVE TO GAS AND A STIMULATED WELLBORE CONDITION AT THE TIME OF THE TEST. OTHER SOURCES, SUCH AS LOGS, SEISMIC, CORES, ETC., SHOULD BE CONSULTED TO CONFIRM THE CORRECT RESERVOIR MODEL FOR THIS WELL. FOR QUESTIONS ABOUT THIS REPORT, PLEASE CONTACT DEBORA HALLFORD AT (303) 843-9090.

LOG [DELTA M(P)] VS. LOG (DELTA T) PLOT

HOMOGENEOUS, INFINITE SYSTEM  
SKIN AND DECREASING WELLBORE STORAGE  
WEDGE-SHAPED GEOMETRY OUTER SEALING BOUNDARIES  
PD VS. TD/CD

DATA IDENTIFICATION

FLOW PERIOD = 11. BUILDUP  
M(P) = 1.094E+08 PSI\*\*2/CP @ DELTA T=0  
FLOW RATE CHANGE = 5200.0 MSCF/D

TYPE-CURVE MATCH

CURVE MATCH, CD\*E(2S) = 3.00353  
WEDGE ANGLE = 95.9801 DEG  
WELL POSITION, THETA/WEDGE ANGLE = 0.270287  
RD = 779.678  
PRESSURE MATCH, PD/DELTA M(P) = 3.324E-08 1/(PSI\*\*2/CP)  
TIME MATCH, (TD/CD)/DELTA T = 43.338 1/HR

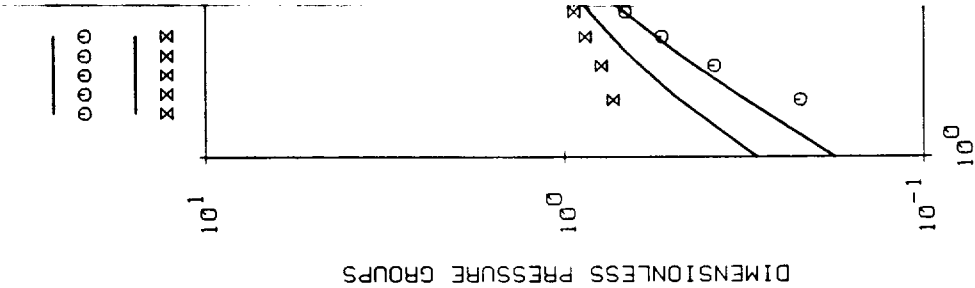
CALCULATIONS

KH ..... 162.68 MD.FT  
KH/MU ..... 9170.2 MD.FT/CP  
K ..... 3.536 MD  
C ..... 0.06242 BBL/PSI  
CD ..... 302.23  
SKIN, S ..... -1.757  
DISTANCE TO SIDES ..... 112 & 240 FT  
DISTANCE TO INTERSECT ..... 256 FT  
RADIUS OF INVESTIGATION ... 566.51 FT (@ 71.333 HR)

COMMENTS

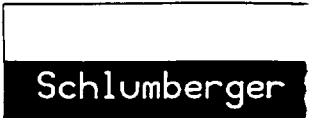
USING HOMOGENEOUS, INFINITE SYSTEM RESERVOIR MODEL WITH  
SKIN AND DECREASING WELLBORE STORAGE AND WEDGE-SHAPED  
GEOMETRY OUTER SEALING (NO-FLOW) BOUNDARIES;  
Ca/C=196.063 CoD=1.73045

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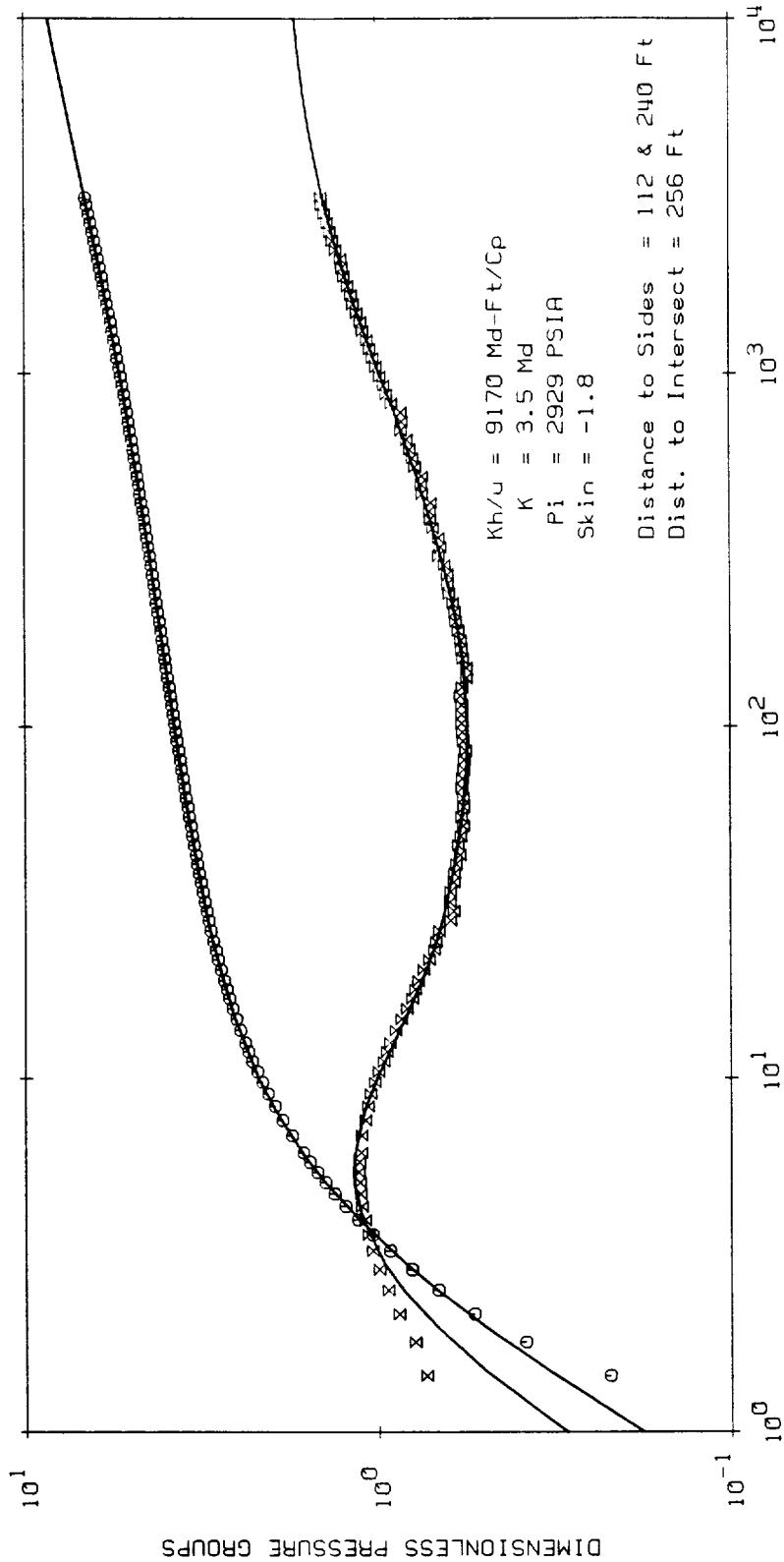
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DIMENSIONLESS MULTI-RATE  
PLOT: LOG-LOG MATCH WITH  
WEDGE GEOMETRY MODEL



MULTI-RATE TYPE-CURVE  
PRESSURE MATCH = 3.3235E-8  
TIME MATCH = 43.34

DERIVATIVE TYPE-CURVE  
DERIVATIVE, BUILDUP DATA



DIMENSIONLESS TIME, TD/CD

TYPE-CURVE : HOMOGENEOUS, INFINITE SYSTEM, WEDGE GEOMETRY  
SKIN & DECREASING WELLBORE STORAGE : CD\*E (2S) = 9.003 WEDGANGL=96