

NEW MEXICO OIL CONSERVATION COMMISSION  
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122  
Revised 9-1-65

Type Test: <input checked="" type="checkbox"/> Initial <input type="checkbox"/> Annual <input type="checkbox"/> Special		Test Date: 4-4-85
Company: Amoco Production Company		Connection:
Pool: Bravo Dome Carbon Dioxide Unit - 640 acre area		Formation: Tubb
Completion Date: 12-5-80	Total Depth: 2775	Plug Back TD: 2718
Elevation: 5068	Farm or Lease Name: BDCDGU	
Csg. Size: 4-1/2	Wt.: 9.5	Set At: 2771
Perforations: From 2472 To 2708	Well No.: 2133 341K	
Tbg. Size: 2-3/8	Wt.: 4.7	Set At: 2388
Perforations: From To	Unit: K Sec. 34 Twp. 21 Rge. 33	
Type Well - Single - Bradenhead - G.G. or G.O. Multiple: Single		Packer Set At: 2388
Producing Thru: Tubing		County: Harding
Reservoir Temp. °F: 90 <sup>o</sup> @ 2590	Mean Annual Temp. °F: 50	Baro. Press. - P <sub>a</sub> : 12.2
State: New Mexico		Meter Run: 4.0
L: 2590	H: 2590	G <sub>g</sub> : 1.529
% CO <sub>2</sub> : 100	% N <sub>2</sub> : 0	% H <sub>2</sub> S: 0
Prover: Flange		Taps: Flange

  

FLOW DATA					TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	x	Orifice Size	Press. p.s.i.g.	Diff. h <sub>w</sub>	Temp. °F	Press. p.s.i.g.	Temp. °F	
SI							318		
1.	4.026 x 1.75			221	41	57	233.2	50	24 hr.
2.	4.026 x 1.75			241	31	55	263.2	50	24 hr.
3.	4.026 x 1.75			262	20	56	274.2	50	24 hr.
4.	4.026 x 1.75			294	8	57	306.2	50	24 hr.
5.									

  

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P <sub>m</sub>	Flow Temp. Factor Ft	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1							1202
2							1099
3							840
4							636
5							

  

NO.	P <sub>f</sub>	Temp. °R	T <sub>f</sub>	Z	Gas Liquid Hydrocarbon Ratio	0	Mcf/bbl.
1.					A.P.I. Gravity of Liquid Hydrocarbons	0	Deg.
2.					Specific Gravity Separator Gas	1.529	X X X X X X X X
3.					Specific Gravity Flowing Fluid	X X X X X	
4.					Critical Pressure	1072	P.S.I.A.
5.					Critical Temperature	547	P.S.I.A.
	P <sub>c</sub> 330.2	P <sub>c</sub> <sup>2</sup> 109.032					R

  

NO.	P <sub>i</sub> <sup>2</sup>	P <sub>w</sub>	P <sub>w</sub> <sup>2</sup>	P <sub>c</sub> <sup>2</sup> - P <sub>w</sub> <sup>2</sup>	(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 2.00$	(2) $\left[ \frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.4$
1		233.2		54.650		
2		263.2		39.758		
3		274.2		33.846		
4		306.2		15.274		
5						

AOF = Q  $\left[ \frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1698$

  

Absolute Open Flow	1698	Mcf/d @ 15.025	Angle of Slope $\theta$	Slope, n	50
Remarks:					
Approved By Commission:		Conducted By:		Checked By:	
		D. D. Kimble			