

NEW MEXICO OIL CONSERVATION COMMISSION  
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122  
Revised 9-1-65

Type Test: <input checked="" type="checkbox"/> Initial <input type="checkbox"/> Annual <input type="checkbox"/> Special			Test Date: 9-6-87								
Company: Amoco Production Company			Connection:								
Pool: Bravo Dome			Formation: Tubb								
Completion Date: 12-5-83		Total Depth: 2615	Plug Back TD: 2380	Elevation: 4865	Unit: BDCDGU						
Csg. Size: 7	Wt.: 20#	d: 6.456	Set At: 2615	Perforations: From 2268 To 2372	Well No.: 2033-351M						
Tbg. Size: 3.5	Wt.: 9.5#	d: 3.00	Set At: 2191	Perforations: From To	Unit: M Sec: 35 Twp: 20 Rge: 33						
Type Well - Single - Bradenhead - G.G. or G.O. Multiple: Single			Packer Set At: 2191	County: Harding							
Producing thru Tubing		Reservoir Temp. °F: 90	Mean Annual Temp. °F: 50	Baro. Press. - P <sub>a</sub> : 12.25	State: New Mexico						
L	H	G <sub>g</sub>	% CO <sub>2</sub> : 100	% N <sub>2</sub> : 0	% H <sub>2</sub> S: 0						
FLOW DATA				Prover: Meter Run: 4.0	Taps: Flange						
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h <sub>w</sub>	Temp. °F	TUBING DATA		CASING DATA		Duration of Flow
							Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	
SI											
1.	4.026 x	1.375		220	86	62	293		0		24 hr.
2.	4.026 x	1.375		231	39	60	220	62	0		24 hr.
3.	4.026 x	1.375		241	19	60	231	60	0		24 hr.
4.	4.026 x	1.375		253	2	57	241	60	0		24 hr.
5.							253	57	0		24 hr.
RATE OF FLOW CALCULATIONS											
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P <sub>m</sub>	Flow Temp. Factor Ft.	Gravity Factor F <sub>g</sub>	Super Compress. Factor, F <sub>pv</sub>	Rate of Flow Q, Mcld				
1.											
2.											1153
3.											841
4.											619
5.											275
NO.	P <sub>r</sub>	Temp. °R	T <sub>r</sub>	Z	Gas Liquid Hydrocarbon Ratio _____ 0 _____ Mcf/bbl.						
1.					A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.						
2.					Specific Gravity Separator Gas _____ 1.529 _____						
3.					Specific Gravity Flowing Fluid _____ X X X X X _____						
4.					Critical Pressure _____ 1072 _____ P.S.I.A.						
5.					Critical Temperature _____ 496 _____ P.S.I.A. _____ R _____ R						
P <sub>c</sub> 305.25 P <sub>c</sub> <sup>2</sup> 93177											
NO.	F <sub>r</sub> <sup>2</sup>	P <sub>w</sub>	P <sub>w</sub> <sup>2</sup>	P <sub>c</sub> <sup>2</sup> - P <sub>w</sub> <sup>2</sup>	(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 2.300$		(2) $\left[ \frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 2.30$				
1		232.25	53940	39237							
2		243.25	59170	34007							
3		253.25	64135	29042							
4		265.25	70357	22820							
5											
AOF = Q $\left[ \frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 2300$											
Absolute Open Flow 2300 Mcld @ 15.025					Angle of Slope @ 45.0		Slope, n 1.0				
Remarks:											
Approved by Commission:			Conducted By: RANDY MAHANNAH			Calculated By: RICHARD ROETH			Checked By:		