NEW MEXICO OIL CONSERVATION COMMSSION

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

Type Test: [X] Initial [ ] Annual [ ] Special — Test Date: 4-29-85

Company: Amoco Production Company — Connection:

Pool: Bravo Dome Carbon Dioxide Gas Unit 640-Acre Area — Formation: Tubb — Unit: BDCDGU

Completion Date	Total Depth	Plug Back TD	Elevation	Farm or Lease Name
3/4/81	2651'	2603	4895	

Csg. Size	Wt.	d	Set At	Perforations	Well No.
5.5	14		2651'	From 2256 To 2517	1934 201G
Tbg. Size	Wt.	d	Set At	Perforations	Unit / Sec. / Twp. / Rge.
2-7/8	6.4		2141	From To	G / 20 / 19 / 34

Type Well – Single – Bradenhead – G.G. or G.O. Multiple: Single — Packer Set At: 2110' — County: Union

Producing Thru	Reservoir Temp. °F	Mean Annual Temp. °F	Baro. Press. – P_a	State
Tubing	90 @ 2387	50	12.2	New Mexico

L	H	Gg	% CO_2	% N_2	% H_2S	Prover	Meter Run	Taps
2387	2387	1.529	100	0	0		4.0	Flange

FLOW DATA / TUBING DATA / CASING DATA

NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h_w	Temp. °F	Tubing Press. p.s.i.g.	Tubing Temp. °F	Casing Press. p.s.i.g.	Casing Temp. °F	Duration of Flow
SI							307	50			
1.	4.026	x	2.500	200	33	57	212.2	50			24 hr
2.	4.026	x	2.500	222	23	58	234.2	50			24 hr
3.	4.026	x	2.500	248	14	59	260.2	50			24 hr
4.	4.026	x	2.500	275	5	60	287.2	50			24 hr
5.											

RATE OF FLOW CALCULATIONS

NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P_m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1							
2.							2194
3.							2024
4.							1625
5.							1033

NO.	P_t	Temp. °R	T_r	Z
1.				
2.				
3.				
4.				
5.				

Gas Liquid Hydrocarbon Ratio 0 Mcf/bbl.
A.P.I. Gravity of Liquid Hydrocarbons 0 Deg.
Specific Gravity Separator Gas 1.529 XXXXXXXXX
Specific Gravity Flowing Fluid XXXXX
Critical Pressure 1072 P.S.I.A. ____ P.S.I.A.
Critical Temperature 547 R ____ R

P_c 319.2 P_c^2 101.0

NO	P_t^2	P_w	P_w^2	$P_c^2 - P_w^2$
1		212.2		56.860
2		234.2		47.039
3		260.2		34.185
4		287.2		19.405
5				

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.776$

(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 1.495$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 3300$

Absolute Open Flow 3300 Mcfd @ 15.025 — Angle of Slope θ ____ — Slope, n .70

Remarks:

Approved By Commission:	Conducted By:	Calculated By:	Checked By:
		D. D. Kimble	