NEW MEXICO OIL CONSERVATION COMMSSION

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

Type Test: [X] Initial [ ] Annual [ ] Special				Test Date: 6-26-87	
Company: Amoco Production Company		Connection:			
Pool: Bravo Dome		Formation: Tubb			Unit: BDCDGU
Completion Date: 6-20-81	Total Depth: 2515		Plug Back TD: 2466	Elevation: 4665	Farm or Lease Name:
Csg. Size: 5.50 / Wt.: 14 / d: 4.9	Set At: 2515		Perforations: From 2107 To 2253		Well No.: 1934-241G
Tbg. Size: 2.875 / Wt.: 6.5 / d: 2.441	Set At: 2122		Perforations: From To		Unit: G / Sec.: 24 / Twp.: 19 / Rge.: 34
Type Well – Single – Bradenhead – G.G. or G.O. Multiple: Single			Packer Set At: 2084		County: Union
Producing Thru: Tubing	Reservoir Temp. °F: 90	Mean Annual Temp. °F: 50	Baro. Press. – P_a: 12.25		State: New Mexico
L:	H:	Gg:	% CO_2: 100	% N_2: 0	% H_2S: 0
Prover:	Meter Run: 4.0	Taps: Flange			

FLOW DATA / TUBING DATA / CASING DATA

NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h_w	Temp. °F	Tubing Press. p.s.i.g.	Tubing Temp. °F	Casing Press. p.s.i.g.	Casing Temp. °F	Duration of Flow
SI							302		0		24 hrs
1.	4.026	x	2.375	188	29	57	187	57	0		24 hrs
2.	4.026	x	2.375	200	23	58	200	58	0		24 hrs
3.	4.026	x	2.375	210	19	58	210	58	0		24 hrs
4.	4.026	x	2.375	225	13	59	225	59	0		24 hrs
5.											

RATE OF FLOW CALCULATIONS

NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P_m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1							
2.							1976
3.							1745
4.							1605
5.							1426

NO.	P_t	Temp. °R	T_t	Z
1.				
2.				
3.				
4.				
5.				

Gas Liquid Hydrocarbon Ratio 0 Mcf/bbl.
A.P.I. Gravity of Liquid Hydrocarbons ____ Deg.
Specific Gravity Separator Gas 1.529 XXXXXXXXX
Specific Gravity Flowing Fluid XXXXX
Critical Pressure 1072 P.S.I.A. ____ P.S.I.A.
Critical Temperature 496 R ____ R

P_c 314.25 P_c^2 98,753

NO	P_t^2	P_w	P_w^2	$P_c^2 - P_w^2$
1		199.25	39,700	59,053
2		212.25	45,050	53,703
3		222.25	49,395	49,358
4		237.25	56,287	42,466
5				

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.6722$

(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 1.6652$

$AOF = Q \left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 3290$

Absolute Open Flow 3290 Mcfd @ 15.025 | Angle of Slope θ 44.76 | Slope, n .9919

Remarks: Test was run from a low flowing tubing pressure to a high flowing tubing pressure to minimize liquid loading effects.

Approved by Commission:	Conducted By:	Calculated By:	Checked By:
	RANDY MAHANNAH	RICHARD ROETH	