

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
 Revised 9-1-65

Type Test: ☒ Initial ☐ Annual ☐ Special					Test Date: 4-19-85	
Company: Amoco Production Company				Connection:		
Pool: Bravo Dome Carbon Dioxide Unit - 640 acre area				Formation: Tubb		Unit: BDCDGU
Completion Date: 12-14-83		Total Depth: 2576		Plug Back TD: 2500		Elevation: 4826
Csg. Size: 7"	Wt.: 20	d:	Set At: 2576	Perforations: From 2232 To 2432		Well No. 2034 191G
Tng. Size: 3.5	Wt.: 9.3	d:	Set At: 2241	Perforations: From To		Unit Sec. Twp. Rge. G 19 20 34
Type Well - Single - Bradenhead - G.G. or G.O. Multiple				Packer Set At: 2211		County: Union
Producing Thru: Tubing		Reservoir Temp. °F: 90° 2332		Mean Annual Temp. °F: 50		Baro. Press. - P _a : 12.2
L: 2332		H: 2332	G _g : 1.529	% CO ₂ : 100	% N ₂ : 0	% H ₂ S: 0
				Prover:	Meter Run: 4.0	Taps: Flange

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F
SI							307				
1.	4.026 x 2.125			218	15	60	230.2	50			24 hr.
2.	4.026 x 2.125			220	15	58	232.2	50			24 hr.
3.	4.026 x 2.125			245	7	58	257.2	50			24 hr.
4.	4.026 x 2.125			269	3	56	281.2	50			24 hr.
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1							1127
2							1104
3							815
4							541
5							

NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	Mcf/bbl.
1					0	
2					0	
3						
4						
5						

A.P.I. Gravity of Liquid Hydrocarbons		Specific Gravity Separator Gas: 1.529		Specific Gravity Flowing Fluid: X X X X X	
Critical Pressure: 1072		Critical Temperature: 547		P.S.I.A. R	

P _c : 319.2	P _c ² : 101.889
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NO.	P _r	P _w	P _w ²	P _c ² - P _w ²	(1) $\frac{P_c^2}{P_c^2 - P_w^2} =$	(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n =$
1		230.2		48.897	2.08	1.99
2		232.2		47.972		
3		257.2		35.737		
4		281.2		22.815		
5						

AOF = $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 2247$

Absolute Open Flow: 2247 Mcfd @ 15.025	Angle of Slope θ	Slope, n: .94
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Remarks:

Approved By Commission:	Conducted By:	Calculated By: D. D. Kimble	Checked By:
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