

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

Type Test: ☒ Initial ☐ Annual ☐ Special				Test Date: 6-9-85	
Company: Amoco Production Company				Connection:	
Pool: Bravo Dome Carbon Dioxide Gas Unit 640 Acre Area				Formation: Tubb	
Completion Date: 1-23-84		Total Depth: 2715'		Plug Back TD: 2586'	
				Elevation: 4632 GL	
Csg. Size: 7"	Wt.: 20#	d:	Set At: 2707'	Perforations: From 2110' To 2300'	
Thq. Size: 3-1/2"	Wt.: 9.3#	d:	Set At: 2053'	Perforations: From To	
Type Well - Single - Bradenhead - G.G. or G.O. Multiple: Single				Packer Set At: 2021'	
Producing Thru: Tubing		Reservoir Temp. °F: @ 2205'		Baro. Press. - P _a : 12.2	
Mean Annual Temp. °F: 50		County: Union		State: New Mexico	
L: 2205'	H: 2205'	G _g : 1.529	% CO ₂ : 100	% N ₂ : 0	% H ₂ S: 0
Prover:		Meter Run: 4.0"		Taps: Flange	

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F
SI							322				
1.	4.026 x 2.75			234	38	57	246.2	50			24 hr.
2.	4.026 x 2.75			249	25	60	261.2	50			24 hr.
3.	4.026 x 2.75			269	15	60	281.2	50			24 hr.
4.	4.026 x 2.75			293	4	60	305.2	50			24 hr.
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1							3276
2							2850
3							2256
4							1298
5							

NO.	P _t	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	Mcf/bbl.
1					0	
2					0	
3					1.529	
4						
5						

A.P.I. Gravity of Liquid Hydrocarbons _____ Deg. Specific Gravity Separator Gas _____ Specific Gravity Flowing Fluid _____ Critical Pressure _____ P.S.I.A. Critical Temperature _____ °R			
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$P_c = 334.2$ $P_c^2 = 111.7$	$(1) \frac{P_c^2}{P_c^2 - P_w^2} = 2.187$	$(2) \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 2.038$																														
<table border="1" style="width:100%; border-collapse: collapse;"> <tr> <th>NO.</th> <th>P_t</th> <th>P_w</th> <th>P_w²</th> <th>P_c² - P_w²</th> </tr> <tr> <td>1</td> <td></td> <td>246.2</td> <td></td> <td>51.075</td> </tr> <tr> <td>2</td> <td></td> <td>261.2</td> <td></td> <td>43.464</td> </tr> <tr> <td>3</td> <td></td> <td>281.2</td> <td></td> <td>32.616</td> </tr> <tr> <td>4</td> <td></td> <td>305.2</td> <td></td> <td>18.543</td> </tr> <tr> <td>5</td> <td></td> <td></td> <td></td> <td></td> </tr> </table>	NO.	P _t	P _w	P _w ²	P _c ² - P _w ²	1		246.2		51.075	2		261.2		43.464	3		281.2		32.616	4		305.2		18.543	5					$AOF = Q \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 6677$	
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Absolute Open Flow: 6677 Mcfd @ 15.025	Angle of Slope θ: _____	Slope, n: .91
Remarks: _____		

Approved By Commission:	Conducted By:	Calculated By: D. D. Kimble	Checked By:
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1835 0516

K ϕ E LOGARITHMIC 2 x 2 CYCLES
KEUFFEL & ESSER CO. MADE IN U.S.A.

AOF = 6677

Q = MCF

