

**NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL**

Form C-122
Revised 9-1-65

Type Test <input checked="" type="checkbox"/> Initial <input type="checkbox"/> Annual <input type="checkbox"/> Special				Test Date					
Company Amoco Production Company				Connection					
Pool Bravo Dome Carbon Dioxide Gas Unit-640 Acre Area				Formation		Unit BDCDGU			
Completion Date 12-15-85		Total Depth 2395		Plug Back TD 2320		Elevation 4608			
Csq. Size 7	Wt. 20	d	Set At 2374	Perforations: From 2046 To 2220		Well No. 1935 171K			
Tbg. Size 3-1/2	Wt. 9.3	d	Set At 1913	Perforations: From To		Unit K	Sec. Twp. Rge. 17 19 35		
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single				Packer Set At 1883		County Union			
Producing Thru Tubing		Reservoir Temp. °F 90 @ 2133		Mean Annual Temp. °F 50		Baro. Press. - P _a 12.25			
State New Mexico									
L 2133	H 2133	G _g 1.529	% CO ₂ 100	% N ₂ 0	% H ₂ S 0	Prover	Meter Run Taps 4.0 Flange		
FLOW DATA				TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	X Orifice Size	Press. p.s.i.g.	Diff. h _w '	Temp. °F	Press. p.s.i.g.	Temp. °F		
SI						354			
1.	4.026 x 3.000		188.1	46	48	200.35	48	1.5	
2.	4.026 x 3.000		162.1	66	48	174.35	48	1.5	
3.	4.026 x 3.000		136.8	90	47	149.05	47	1.5	
4.	4.026 x 3.000		128.5	96.5	46	140.75	46	1.5	
5.									
RATE OF FLOW CALCULATIONS									
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd		
1.							4175		
2.							4479		
3.							4678		
4.							4739		
5.									
NO.	P _f	Temp. °R	T _f	Z	Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.				
1.					A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.				
2.					Specific Gravity Separator Gas 1.529 X X X X X X X X X X				
3.					Specific Gravity Flowing Fluid X X X X X				
4.					Critical Pressure 1072 P.S.I.A. P.S.I.A.				
5.					Critical Temperature 496 R R				
P _c 366.2		P _c ² 134,102							
NO.	P _i ²	P _w	P _w ²	P _c ² - P _w ²	(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.2$		(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.1$		
1.		200		94,102					
2.		174		103,826					
3.		149		111,901					
4.		141		114,221	AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 5142$				
5.									
Absolute Open Flow 5142				Mcf/d @ 15.025		Angle of Slope θ		Slope, n .59	
Remarks:									
Approved By Commission:			Conducted By:			Calculated By: Don Kimble		Checked By:	