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appropriate district office.
See Rule 401 & Rule 1122

State of New Mexico
Energy Minerals and Natural Resources
Oil Conservation Division
2040 South Pacheco
Santa Fe, NM 87505

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Form C-122
Revised October, 1999

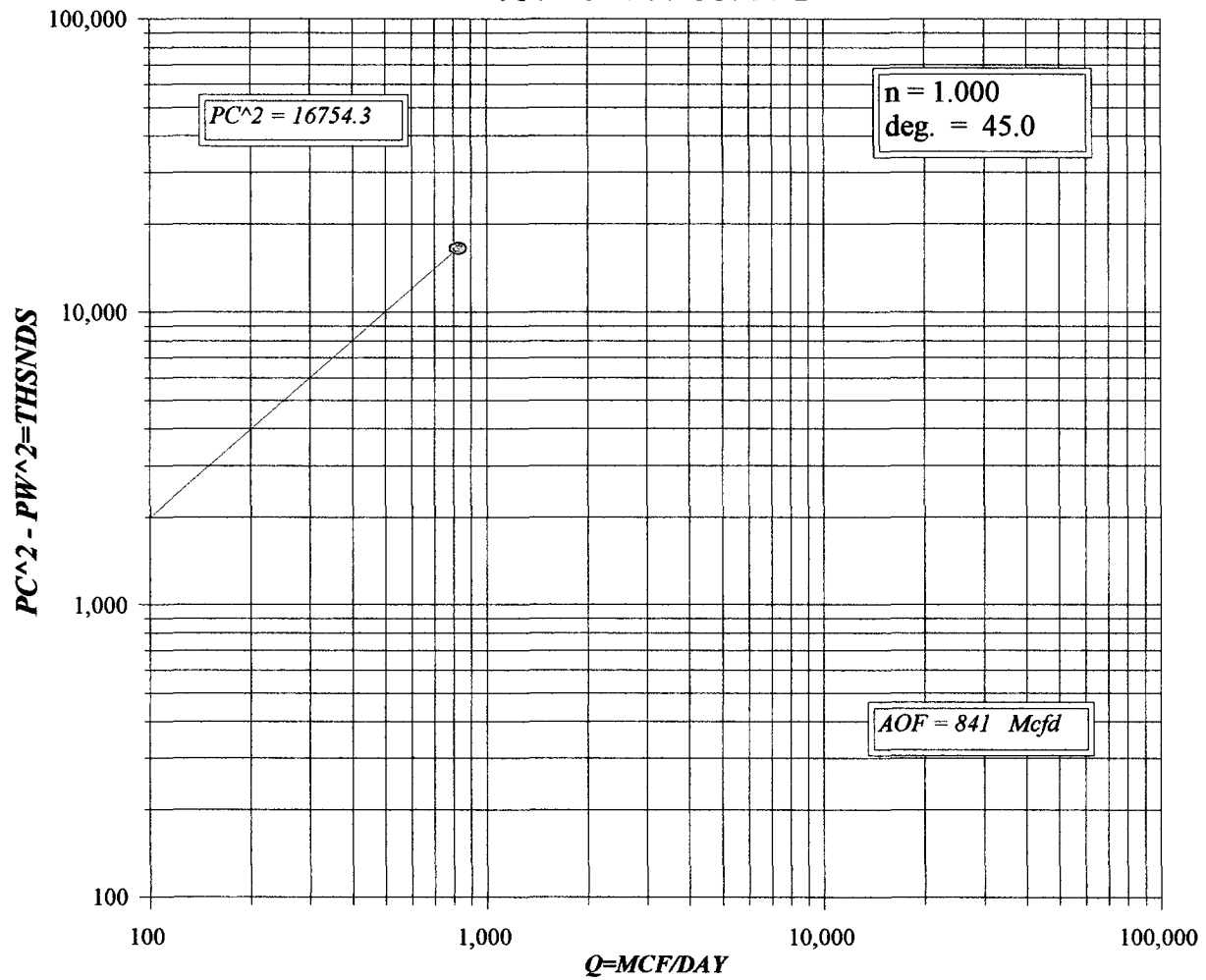
FEB 17 2005

OCB-ARTESIA

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Operator MEWBOURNE OIL COMPANY					Lease or Unit Name JUSTICE FED COM				
Type Test ☒ Initial ☐ Annual ☐ Special					Test Date 2/1/2005		Well No. 2		
Completion Date 12/25/2004		Total Depth 11784		Plug Back TD 11461		Elevation 3194		Unit Ltr - Sec - TWP - Rge LOT 14 1 21S 27E	
Csg. Size 5 1/2	Wt. 17	d 4.892	Set At 11780	Perforations: From: 11416 To: 11493			County EDDY		
Tbg. Size 2 7/8	Wt. 6.5	d 2.44	Set At 10991	Perforations: From: 11299 To: 11432			Pool UNDES BURTON FLAT		
Type Well-Single-Bradenhead-G.G. or G.O. Multiple SINGLE				Packer Set At 10979			Formation MORROW		
Producing Thru TUBING		Reservoir Temp. 181		Mean Annual Temp. 60		Baro. Press.-P _a 13.2		Connection SALES	
L 10991	H 10991	Gg 0.619	%CO ₂ 1.836	%N ₂ 0.693	%H ₂ S 0	Prover N/A	Meter Run 3.068	Taps FLG	
FLOW DATA					TUBING DATA			CASING DATA	
No.	Prover Line Size	Orifice x Size	Press p.s.i.g.	Diff. h _w	Temp.	Press p.s.i.g.	Temp.	Press p.s.i.g.	Temp.
SI	3.0 X 1.250					4080			
1			492	15.33	89	500			24 HRS.
2									
3									
4									
5									
RATE OF FLOW CALCULATIONS									
No.	COEFFICIENT (24 Hour)		$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress Factor F _{pv}	Rate of Flow Q, Mcfd	
1	9.64							827	
2			TOTAL	FLOW					
3									
4									
5									
No.	P _r	Temp. R	T _r	Z	Gas Liquid Hydrocarbon Ratio _____ Mcf bbl.				
1					A.P. I. Gravity of Liquid Hydrocarbons _____ Deg.				
2	TOTAL	FLOW	METER		Specific Gravity Separator Gas _____ XXXXXXXX				
3					Specific Gravity Flowing Fluid _____ XXXXXX				
4					Critical Pressure 677 P.S.I.A. N/A P.S.I.A.				
5					Critical Temperature 357 R. N/A R				
P _c 4693.2 P _{c2} 16754.3					$(1) \quad \frac{P_c^2}{P_c^2 - P_w^2} = 1.017$ $AOF = Q \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 0.841$ $(2) \quad \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.017$				
No.	P _t ²	P _w	P _w ²	P _c ² - P _w ²					
1		521.6	272.1	16482.2					
2									
3									
Absolute Open Flow 841 Mcfd @ 15.025 Angle of Slope Q: 45 Slope, n: 1									
Remarks: 0 - BO 9- BW									
Approved By Division:			Conducted By:		Calculated By:		Checked By:		
			MEWBOURNE OIL		MREV BUECKER		MB		

MEWBOURNE OIL
JUSTICE FED COM # 2



COMPANY : MEWBOURNE OIL LEASE : JUSTICE FED COM WELL NO. : 2
 UNIT : LOT 14 SECTION : 1 TOWNSHIP : 21S
 L : 10991 H : 10991 L/H : 1 G/GMIX : 0.619
 %CO2 : 1.836 %N2 : 0.693 H2S : DATE : 2/1/05
 d : 2.441 Fr : 0.010763 GH : 6803.4 RANGE : 27E

VOL 1 : 827 PSIA 1 : 513.2 RESV.TEMP : 183.9
 VOL 2 : PSIA 2 : SHUT-IN PRI = 4093.2
 VOL 3 : PSIA 3 :
 VOL 4 : PSIA 4 :
 PCR : 677
 TCR : 357

Pc = 4093.2 Pc2 = 16754.3
 P2 = 263.4 Pw = 521.6
 0.0 #DIV/0!
 0.0 #DIV/0!
 0.0 #DIV/0!

Pc2-Pw2 = 16482.2 Pw2 = 272.1
 #DIV/0!
 #DIV/0!
 #DIV/0!

n = 1.000
 Pc2/(Pc2-Pw2) = 1.017
 #DIV/0!
 #DIV/0!
 #DIV/0!
 [Pc2/Pc2-Pw2]n = 1.017
 #DIV/0!
 #DIV/0!
 #DIV/0!
 AOF= Q 0.841
 #DIV/0!
 #DIV/0!
 #DIV/0!

LINE		RATE 1		RATE 2		RATE 3		RATE 4	
		1ST	2ND	1ST	2ND	1ST	2ND	1ST	2ND
1	QM	0.827	0.827	0.000	0.000	0.000	0.000	0.000	0.000
2	TW	534	534	534	534	534	534	534	534
3	Ts	643.9	643.9	643.9	643.9	643.9	643.9	643.9	643.9
4	T	589.0	589.0	589.0	589.0	589.0	589.0	589.0	589.0
	PR (est)	0.76		0.00		0.00		0.00	
5	Z(est)	0.923	0.917	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
6	TZ	543.9	539.8	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
7	GH/TZ	12.509	12.603	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
8	eS	1.599	1.604	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
9	I-e-S	0.374	0.377	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
10	Pt	513.2	513.2	0.0	0.0	0.0	0.0	0.0	0.0
11	P2 /1000	263.4	263.4	0.0	0.0	0.0	0.0	0.0	0.0
12	Fr	0.010763	0.010763	0.010763	0.010763	0.010763	0.010763	0.010763	0.010763
13	Fc=FrTZ	5.854	5.810	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
14	FcQm	4.84	4.80	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
15	L/H(FcQm)	23.4	23.1	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
16	Fw	8.775645	8.695408	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
17	Pw2	272.1	272.1	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
18	Ps2	435.0	436.5	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
19	Ps	659.6	660.6	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
20	P	586.4	586.9	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
21	Pr	0.87	0.87	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
22	Tr	1.65	1.65	1.65	1.65	1.65	1.65	1.65	1.65
23	Z	0.917	0.917	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!

FORM C122-D