Submit in duplicate to appropriate district office.
See Rule 401 & Rule 1122

State of New Mexico
Energy Minerals and Natural Resources
Oil Conservation Division
2040 South Pacheco
Santa Fe, NM 87505

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Form C-122
Revised October, 1999

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL 30-015-33470

Operator	MEWBOURNE OIL COMPANY	Lease or Unit Name	ANGEL DRAW 2 ST. COM

Type Test	Test Date	Well No.
☑ Initial ☐ Annual ☐ Special	1/5/2005	1

Completion Date	Total Depth	Plug Back TD	Elevation	Unit Ltr - Sec - TWP - Rge
11/6/2004	11150'	11060'	3372'	P 2 20S 27E

Csg. Size	Wt.	d	Set At	Perforations:		County
5 1/2	17	4.892	11121'	From: 10735'	To: 10824'	EDDY

Tbg. Size	Wt.	d	Set At	Perforations:		Pool
2 7/8	6.5	2.44	9996'	From:	To:	Angel Ranch Atoka Morrow

Type Well-Single-Bradenhead-G.G. or G.O. Multiple	Packer Set At	Formation
SINGLE	9970'	ATOKA - MORROW

Producing Thru	Reservoir Temp.	Mean Annual Temp.	Baro. Press.-P_a	Connection
TUBING	181	60	13.2	SALES

L	H	Gg	%CO_2	%N_2	%H_2S	Prover	Meter Run	Taps
9996	9996	0.639	0.973	3.071	N/A	N/A	3"	FLG

	FLOW DATA				TUBING DATA		CASING DATA		
No.	Prover Line Size x Orifice Size	Press p.s.i.g.	Diff. h_w	Temp.	Press p.s.i.g.	Temp.	Press p.s.i.g.	Temp.	Duration of Flow
SI	3.0 X 1.75				4300				
1	TOTAL FLOW	458	1.5		3400	79			
2		460	7		3160	80			
3		465	17		2900	81			
4		465	23		2780	80			
5									

RATE OF FLOW CALCULATIONS

No.	COEFFICIENT (24 Hour)	$\sqrt{h_w P_m}$	Pressure P_m	Flow Temp. Factor Ft.	Gravity Factor F_g	Super Compress Factor F pv	Rate of Flow Q. Mcfd
1							521
2	19.89	TOTAL	FLOW				1,100
3							1,630
4							2,056
5							

No.	P_r	Temp. R	T_r	Z
1				
2	TOTAL	FLOW	METER	
3				
4				
5				

Gas Liquid Hydrocarbon Ratio	13.007		Mcf bbl.
A.P. I. Gravity of Liquid Hydrocarbons	56.3 @ 60		Deg.
Specific Gravity Separator Gas	0.639		XXXXXXX
Specific Gravity Flowing Fluid	XXXXX		GMIX = .854
Critical Pressure	667 P.S.I.A.	N/A	P.S.I.A.
Critical Temperature	360 R.	N/A	R

P_c 4313.2 P_c^2 18603.7

No.	P_t^2	P_w	P_w^2	$P_c^2 - P_w^2$
1		3413.6	11653	6950.7
2		3175.3	10082.5	8521.2
3		2918.1	8515.3	10088.4
4		2801.2	7847	10756.7
5				

(1) $\frac{P_c^2}{P_c^2 - P_w^2} =$ 1.729 (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n =$ 1.729

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n =$ 3.556

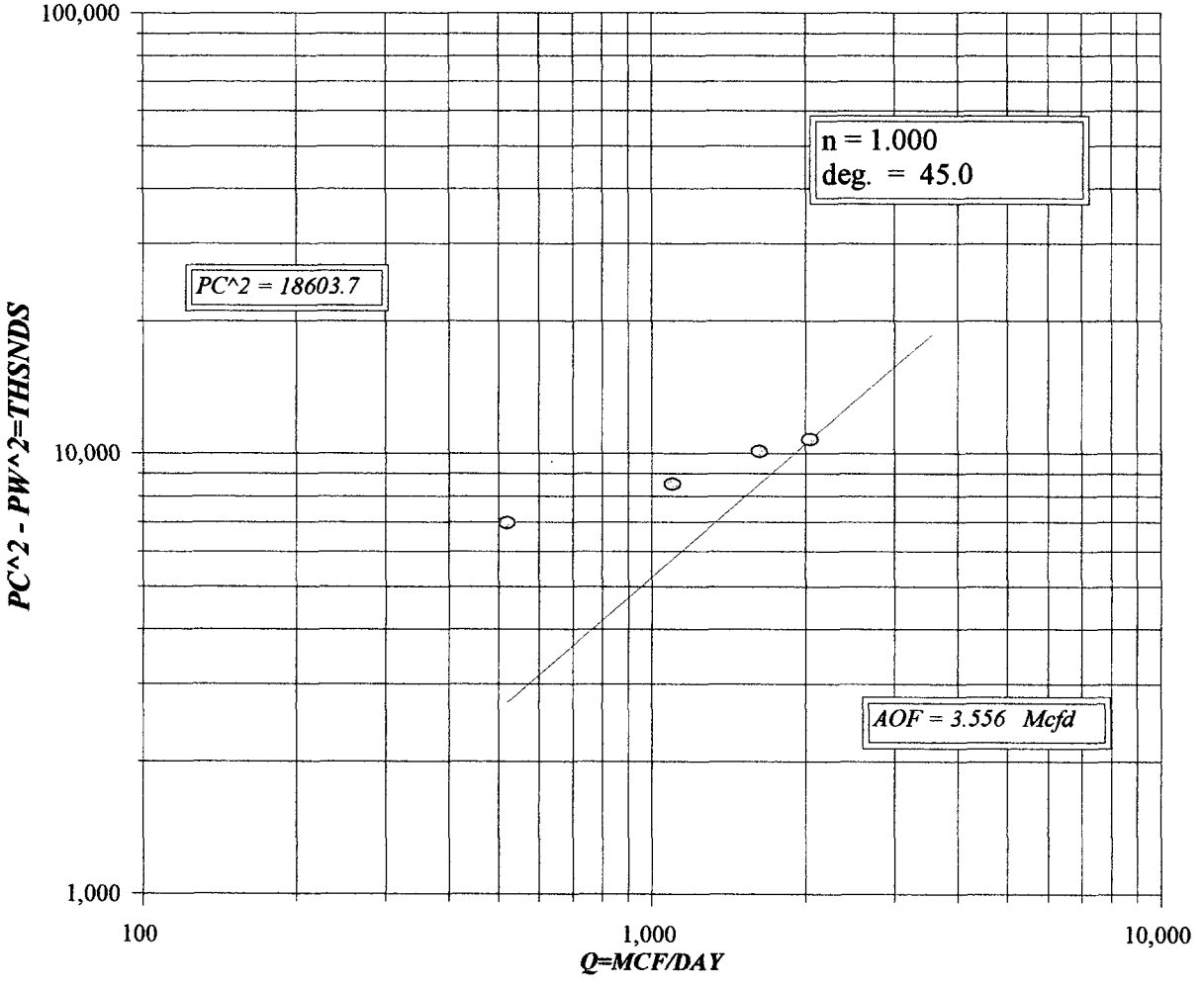
Absolute Open Flow	Mcfd @ 15.025	Angle of Slope ():	Slope, n:
3,556		45	1

Remarks: * WELL MADE 17 BBLS OF 56.3 API GRAVIT CONDENSATE DURING TEST

Approved By Division:	Conducted By:	Calculated By:	Checked By:
	MEWBOURNE OIL	PRO WELL TESINT	MB

MEWBOURNE OIL

Angel Draw 2 St Com #1



COMPANY :	MEWBOURNE		LEASE :	ANGEL DRAW 2 ST COM	WELL NO. :	1			
UNIT :	P		SECTION :	2	TOWNSHIP :	20S			
L :	9996	H :	9996	L/H :	1	G/GMIX :	0.639		
%CO2 :	0.973	%N2 :	3.071	H2S :			DATE :	1/5/05	
d :	2.441	Fr :	0.010763	GH :	6387.4		RANGE :	27E	

VOL 1 :	521	PSIA 1 :	3413.2		RESV.TEMP	174.0	
VOL 2 :	1100	PSIA 2 :	3173.2				
VOL 3 :	1630	PSIA 3 :	2913.2		SHUT-IN PRI =	4313.2	
VOL 4 :	2056	PSIA 4 :	2793.2				

PCR :	667
TCR :	360

	LINE	RATE 1		RATE 2		RATE 3		RATE 4	
		`1ST	`2ND	`1ST	``2ND	`1ST	`2ND	`1ST	`2ND
1	QM	0.521	0.521	1.100	1.100	1.630	1.630	2.056	2.056
2	TW	534	534	534	534	534	534	534	534
3	Ts	634.0	634.0	634.0	634.0	634.0	634.0	634.0	634.0
4	T	584.0	584.0	584.0	584.0	584.0	584.0	584.0	584.0
	PR (est)	5.12		4.76		4.37		4.19	
5	Z(est)	0.843	0.870	0.832	0.854	0.822	0.839	0.818	0.833
6	TZ	492.2	508.2	485.6	498.8	479.9	489.8	477.9	486.2
7	GH/TZ	12.977	12.568	13.154	12.807	13.309	13.042	13.365	13.138
8	eS	1.627	1.602	1.638	1.616	1.647	1.631	1.651	1.637
9	I-e-S	0.385	0.376	0.389	0.381	0.393	0.387	0.394	0.389
10	Pt	3413.2	3413.2	3173.2	3173.2	2913.2	2913.2	2793.2	2793.2
11	Pt2 /1000	11649.9	11649.9	10069.2	10069.2	8486.7	8486.7	7802.0	7802.0
12	Fr	0.010763	0.010763	0.010763	0.010763	0.010763	0.010763	0.010763	0.0107631
13	Fc=FrTZ	5.298	5.470	5.227	5.368	5.165	5.271	5.144	5.233
14	FcQm	2.76	2.85	5.75	5.90	8.42	8.59	10.58	10.76
15	L/H(FcQm)^2	7.6	8.1	33.1	34.9	70.9	73.8	111.8	115.7
16	Fw	2.935423	3.052399	12.87004	13.298	27.85485	28.55705	44.08836	45.026879
17	Pw2	11652.9	11653.0	10082.1	10082.5	8514.6	8515.3	7846.1	7847.0
18	Ps2	18957.3	18669.0	16511.0	16298.2	14025.6	13886.8	12951.6	12843.2
19	Ps	4354.0	4320.8	4063.4	4037.1	3745.1	3726.5	3598.8	3583.7
20	P	3883.6	3867.0	3618.3	3605.2	3329.1	3319.8	3196.0	3188.5
21	Pr	5.82	5.80	5.42	5.41	4.99	4.98	4.79	4.78
22	Tr	1.62	1.62	1.62	1.62	1.62	1.62	1.62	1.62
23	Z	0.870	0.869	0.854	0.853	0.839	0.838	0.833	0.832

Pc =	4313.2	Pc2 =	18603.7
Pt2 =	11649.9	Pw =	3413.6
	10069.2		3175.3
	8486.7		2918.1
	7802.0		2801.2
Pc2-Pw2=	6950.7	Pw2 =	11653.0
	8521.2		10082.5
	10088.4		8515.3
	10756.7		7847.0
n =		1.000	
Pc2/(Pc2-Pw2) =		2.677	
		2.183	
		1.844	
		1.729	
[Pc2/Pc2-Pw2]n =		2.677	
		2.183	
		1.844	
		1.729	
AOF= Q		1.394	
		2.402	
		3.006	
		3.556	

FORM C122-D