OCD-ARTESIA

Form 3160-3 (February 2005)				OMB N	o. 1004-0137 March 31, 200	a F A	11-004
UNITED STATES DEPARTMENT OF THE				5 Lease Serial No.		· L IT	<u>//- </u>
BUREAU OF LAND MAN		RESUBA	ATTA	NM-864			
APPLICATION FOR PERMIT TO		•		6 If Indian, Allotee	or Tribe Na	me	
la. Type of work DRILL - REENT	ER			7 If Unit or CA Agre	eement, Nam	e and No)
Ib. Type of Well ☐Oıl Well ☐Other	✓ Si	✓ ngle Zone	ole Zone	8 Lease Name and Pacheco 3	Well No. 1 Fed Com	, <	36704
Name of Operator Devon Energy Production Co., LP	(613-	7		9. API Well No.	- 399	147	,
3a Address 20 North Broadway OKC, OK 73102	1	(include area code) 552-7802		10. Field and Pool, or Angel Ranch;	. ,	orrow	1709
4. Location of Well (Report location clearly and in accordance with an NENW 660' FNL & 1650' FWL (At proposed prod zone NENW 660' FNL & 1650' FWL	ty State requirem	nents.*)	,	11. Sec., T R M or E	3lk and Surve T19S-R28E		:a
4 Distance in miles and direction from nearest town or post office* Approximately 15 miles north of Carlsbad, NM.				12. County or Parish Eddy	1	3 State	NM
5 Distance from proposed* location to nearest property or lease line, ft	16 No of a	icres in lease	17. Spacii	ng Unit dedicated to this	well		
(Also to nearest drig unit line, if any) 660'	J	1.60		331.60			
8 Distance from proposed location* to nearest well, drilling, completed, applied for, on this lease, ft 661'	19. Propose	d Depth	20. BLM/	VBIA Bond No. on file CO-1104			
1. Elevations (Show whether DF, KDB, RT, GL, etc) 3409' GL	22. Approxi	mate date work will sta 08/15/2011	rt*	23. Estimated duration 45 days	on		
	24. Atta	chments					
he following, completed in accordance with the requirements of Onsho	ore Oil and Gas	Order No 1, must be a	ttached to th	us form			
Well plat certified by a registered surveyor A Drilling Plan. A Surface Use Plan (if the location is on National Forest System	Lands the	4 Bond to cover t Item 20 above). 5. Operator certification	•	ons unless covered by an	existing bor	nd on fil	e (see
SUPO must be filed with the appropriate Forest Service Office)				ormation and/or plans a	s may be req	uired by	the
25 Signature		(Printed/Typed) Stephanie A. Ysasa	ga		Date 06/02	/2011	
ttle Sr. Staff Engineering/Technician							
Approved by (Signature) /s/ Don Peterson		(Printed/Typed)			AUG	29	2011
FIELD MANAGER	Office	CARLSDAD					
Application approval does not warrant or certify that the applicant hold onduct operations thereon. Conditions of approval, if any, are attached.	ls legal or equi	table title to those righ	its in the sul	_		_	· <u>WO</u> YE
itle 18 U.S.C. Section 1001 and Title 43 U.S.C. Section 1212, make it a c tates any false, fictitious or fraudulent statements or representations as	rime for any p to any matter v	erson knowingly and vithin its jurisdiction.	willfully to i				
(Instructions on page 2)	Kro	99/2/11		RECEI	VED	7	_
·	r			SEP 06	2011		
Stan Controlled Mistor Deale				NMOCD A	RTESI	A	
itan Controlled Water Basin							<i></i>

SEE ATTACHED FOR CONDITIONS OF APPROVAL

Approval Subject to General Requirements & Special Stipulations Attached

DRILLING PROGRAM

Devon Energy Production Company, LP Pacheco 31 Fed Com 9

Surface Location: 660' FNL & 1650' FWL, Unit C, Sec 31 T19S R28E, Eddy, NM Bottom hole Location: 660' FNL & 1650' FWL, Unit C, Sec 31 T19S R28E, Eddy, NM

1. Geologic Name of Surface Formation

a. Quaternary

2. Estimated Tops of Geological Markers & Depths of Anticipated Fresh Water, Oil or Gas:

b. Depth to Freshwater c. Rustler d. Salado 275' e. Tansil f. Yates 630' g. Seven Rivers h. Yates/Seven Rivers i. Queen j. San Andres k. Delaware l. Bone Spring Lime 3880' oil m. 3 rd Bone Spring Lime 7100' n. 3 rd Bone Spring Ss o. Wolfcamp b. Upper Penn q. Canyon q. Canyon q. Canyon yes Strawn yes Straw	a.	Alluvium	Surface		
d. Salado 275' e. Tansil 410' f. Yates 630' g. Seven Rivers 960' h. Yates/Seven Rivers 1050' i. Queen 1550' j. San Andres 1650' k. Delaware 2725' Oil l. Bone Spring Lime 3880' Oil m. 3 rd Bone Spring Lime 7100' Oil n. 3 rd Bone Spring Ss 8050' Oil o. Wolfcamp 8540' Oil p. Upper Penn 9050' Oil q. Canyon 9250' Gas/Oil r. Strawn 9775' Gas/Oil s. Atoka 10200' Gas t. Morrow 10525' Gas u. Middle Morrow Lime 10650' Gas v. Lower Morrow 10800' Gas w. Barnett Shale 10980'	b.	Depth to Freshwater	200'		
e. Tansil 410' f. Yates 630' g. Seven Rivers 960' h. Yates/Seven Rivers 1050' i. Queen 1550' j. San Andres 1650' k. Delaware 2725' l. Bone Spring Lime 3880' m. 3 rd Bone Spring Lime 7100' n. 3 rd Bone Spring Ss 8050' o. Wolfcamp 8540' p. Upper Penn 9050' q. Canyon 9250' r. Strawn 9775' s. Atoka 10200' s. Atoka 10200' t. Morrow 10525' Gas u. Middle Morrow Lime 10650' v. Lower Morrow 10800' Gas w. Barnett Shale 10980'	c.	Rustler	80'		
f. Yates 630' g. Seven Rivers 960' h. Yates/Seven Rivers 1050' Oil i. Queen 1550' Oil j. San Andres 1650' Oil k. Delaware 2725' Oil l. Bone Spring Lime 3880' Oil m. 3rd Bone Spring Lime 7100' Oil n. 3rd Bone Spring Ss 8050' Oil o. Wolfcamp 8540' Oil p. Upper Penn 9050' Oil q. Canyon 9250' Gas/Oil r. Strawn 9775' Gas/Oil s. Atoka 10200' Gas t. Morrow 10525' Gas u. Middle Morrow Lime 10650' Gas v. Lower Morrow 10800' Gas w. Barnett Shale 10980'	d.	Salado	275'		
g. Seven Rivers 960' h. Yates/Seven Rivers 1050' Oil i. Queen 1550' j. San Andres 1650' k. Delaware 2725' Oil l. Bone Spring Lime 3880' Oil m. 3 rd Bone Spring Lime 7100' Oil n. 3 rd Bone Spring Ss 8050' Oil o. Wolfcamp 8540' Oil p. Upper Penn 9050' Oil q. Canyon 9250' Gas/Oil r. Strawn 9775' Gas/Oil s. Atoka 10200' Gas t. Morrow 10525' Gas u. Middle Morrow Lime 10650' Gas v. Lower Morrow 10800' Gas w. Barnett Shale 10980' Tollow	e.	Tansil	410'		
h. Yates/Seven Rivers i. Queen j. San Andres j. San Andres l. Delaware l. Bone Spring Lime m. 3 rd Bone Spring Lime n. 3 rd Bone Spring Ss o. Wolfcamp l. Upper Penn l. Upper Penn l. Canyon l. Canyon l. Strawn l. Morrow l. Morrow l. Morrow l. Morrow l. Morrow l. Lower Morrow l. Morrow	f.	Yates	630'		
i. Queen 1550' j. San Andres 1650' k. Delaware 2725' Oil l. Bone Spring Lime 3880' Oil m. 3 rd Bone Spring Lime 7100' Oil n. 3 rd Bone Spring Ss 8050' Oil o. Wolfcamp 8540' Oil p. Upper Penn 9050' Oil q. Canyon 9250' Gas/Oil r. Strawn 9775' Gas/Oil s. Atoka 10200' Gas t. Morrow 10525' Gas u. Middle Morrow Lime 10650' Gas v. Lower Morrow 10800' Gas w. Barnett Shale 10980'	g.	Seven Rivers	960'		
j. San Andres k. Delaware 2725' Oil l. Bone Spring Lime 3880' Oil m. 3 rd Bone Spring Lime 7100' Oil n. 3 rd Bone Spring Ss 8050' Oil o. Wolfcamp 8540' Oil p. Upper Penn 9050' Oil q. Canyon 9250' Gas/Oil r. Strawn 9775' Gas/Oil s. Atoka 10200' Gas t. Morrow 10525' Gas u. Middle Morrow Lime V. Lower Morrow 10800' Gas w. Barnett Shale	h.	Yates/Seven Rivers	1050'	4	Oil
k. Delaware 2725' Oil 1. Bone Spring Lime 3880' Oil m. 3 rd Bone Spring Lime 7100' Oil n. 3 rd Bone Spring Ss 8050' Oil o. Wolfcamp 8540' Oil p. Upper Penn 9050' Oil q. Canyon 9250' Gas/Oil r. Strawn 9775' Gas/Oil s. Atoka 10200' Gas t. Morrow 10525' Gas u. Middle Morrow Lime 10650' Gas v. Lower Morrow 10800' Gas w. Barnett Shale 10980'	i.	Queen	1550'		
1.Bone Spring Lime3880'Oilm.3rd Bone Spring Lime7100'Oiln.3rd Bone Spring Ss8050'Oilo.Wolfcamp8540'Oilp.Upper Penn9050'Oilq.Canyon9250'Gas/Oilr.Strawn9775'Gas/Oils.Atoka10200'Gast.Morrow10525'Gasu.Middle Morrow Lime10650'Gasv.Lower Morrow10800'Gasw.Barnett Shale10980'	j.	San Andres	1650'		
m. 3 rd Bone Spring Lime 7100' Oil n. 3 rd Bone Spring Ss 8050' Oil o. Wolfcamp 8540' Oil p. Upper Penn 9050' Oil q. Canyon 9250' Gas/Oil r. Strawn 9775' Gas/Oil s. Atoka 10200' Gas t. Morrow 10525' Gas u. Middle Morrow Lime 10650' Gas v. Lower Morrow 10800' Gas w. Barnett Shale 10980'	k.	Delaware	2725'		Oil
n. 3 rd Bone Spring Ss 8050' Oil o. Wolfcamp 8540' Oil p. Upper Penn 9050' Oil q. Canyon 9250' Gas/Oil r. Strawn 9775' Gas/Oil s. Atoka 10200' Gas t. Morrow 10525' Gas u. Middle Morrow Lime 10650' Gas v. Lower Morrow 10800' Gas w. Barnett Shale 10980'	1.	Bone Spring Lime	3880'		Oil
o. Wolfcamp 8540' Oil p. Upper Penn 9050' Oil q. Canyon 9250' Gas/Oil r. Strawn 9775' Gas/Oil s. Atoka 10200' Gas t. Morrow 10525' Gas u. Middle Morrow Lime 10650' Gas v. Lower Morrow 10800' Gas w. Barnett Shale 10980'	m.	3 rd Bone Spring Lime	7100'		Oil
p. Upper Penn 9050' Oil q. Canyon 9250' Gas/Oil r. Strawn 9775' Gas/Oil s. Atoka 10200' Gas t. Morrow 10525' Gas u. Middle Morrow Lime 10650' Gas v. Lower Morrow 10800' Gas w. Barnett Shale 10980'	n.	3 rd Bone Spring Ss	8050'		Oil
q. Canyon 9250' Gas/Oil r. Strawn 9775' Gas/Oil s. Atoka 10200' Gas t. Morrow 10525' Gas u. Middle Morrow Lime 10650' Gas v. Lower Morrow 10800' Gas w. Barnett Shale 10980'	0.	Wolfcamp	8540'		Oil
r. Strawn 9775' Gas/Oil s. Atoka 10200' Gas t. Morrow 10525' Gas u. Middle Morrow Lime 10650' Gas v. Lower Morrow 10800' Gas w. Barnett Shale 10980'	p.	Upper Penn	9050'		Oil
s. Atoka 10200' Gas t. Morrow 10525' Gas u. Middle Morrow Lime 10650' Gas v. Lower Morrow 10800' Gas w. Barnett Shale 10980'	q.	Canyon	9250'		Gas/Oil
t. Morrow 10525' Gas u. Middle Morrow Lime 10650' Gas v. Lower Morrow 10800' Gas w. Barnett Shale 10980'	r.	Strawn	9775'		Gas/Oil
u. Middle Morrow Limev. Lower Morroww. Barnett Shale10650'GasGasU0980'	s.	Atoka	10200'		Gas
v. Lower Morrow 10800' Gas w. Barnett Shale 10980'	t.	Morrow	. 10525'		Gas .
w. Barnett Shale 10980'	u.	Middle Morrow Lime	10650'		Gas
	v.	Lower Morrow	10800'		Gas
x. Total Depth 11100'	w.	Barnett Shale	10980'		
	x.	Total Depth	11100'		•

No other formations are expected to yield oil, gas or fresh water in measurable volumes. The surface fresh water sands will be protected by setting 13 3/8" casing at 400' and circulating cement back to surface. Fresh water sands will be protected by setting 9 5/8" casing at 2850' and circulating cement to surface. The Morrow intervals will be isolated by setting 5 ½" casing to total depth and circulating cement above the base of the 9 5/8" casing.

3. Casing Program:

<u>Hole</u>	: <u>Hole</u>	OD Csg	<u>Casing</u>	Weight	<u>Collar</u>	<u>Grade</u>
<u>Size</u>	<u>Interval</u>		<u>Interval</u>			
17 1/2"	0'-400'	13 3/8"	0'-400'	48#/ft	ST&C	H-40
12 1/4"	400'-2850'	9 5/8"	0-2850'	40#/ft	LT&C	J-55
8 3/4"	2850'- 11100'	5 1/2"	0'-11100'	1 7 #/ft	LT&C	HCP-110

Design Parameter Factors:

Casing Size	Collapse Design	Burst Design	Tension Design
	Factor	Factor	Factor
13 3/8"	3.56	4.33	16.78
9 5/8"	1.74	1.39	4.56
5 ½"	1.35	1.68	2.36

4. Cement Program: (Note: All cement volumes are calculated with 25% excesses.)

a. 13 3/8" Surface

Cement Lead Slurry: 345 sacks Premium Plus C Cement + 2% bwoc Calcium Chloride + 0.125 lbs/sack Cello Flake + 4% bwoc Bentonite + 81.4% Fresh Water; Yield: 1.75 cf/sack. Tail Slurry: 200 sacks Class C Cement + 2% bwoc Calcium Chloride + 0.125 lbs/sack Cello Flake + 56.3% Fresh Water; Yield: 1.35 cf/sack. Displacement: 56.9 bbls Mud @ 9.0 ppg. TOC to surface.

b. 95/8" Intermediate

Cement **Lead Slurry:** 700 sacks (35:65) Poz (Fly Ash): Premium Plus C Cement + 5% bwow Sodium chloride + 0.125 lbs/sack Cello Flake + 5 lbs/sack LCM-1 + 6% bwoc bentonite + 95.8% Fresh Water; Yield: 1.95 cf/sack. **Tail Slurry:** 250 sacks (60:40) Poz (Fly Ash): Premium Plus C Cement + 5% bwow Sodium chloride + 0.5% bwoc sodium Metasilicate + 4% bwoc MPA-5 + 64.8% Fresh Water; Yield: 1.37 cf/sack. **Displacement:** 204.04 bbls Mud @ 9.5 ppg. TOC to surface.

c. 5·1/2" Production

Cement with Stage 1:

Cement Slurry: 1000 sacks (15:61:11) Poz (Fly Ash): Premium Plus C Cement: CSE-2 + 0.3% bwoc R-3 + 1% bwow Potassium Chloride + 0.75% bwoc EC-1 + 0.125 lbs/sack Cello Flake + 0.4% bwoc CD-32 + 3 lbs/sack LCM-1 + 0.6% bwoc FL-25 + 0.6 bwoc FL-52A + 72.3% Fresh Water; **Yield:** 1.57 cf/sack.

Displacement: 256.2 bbls Displacement Fluid.

Stage 2

Lead Slurry: 715 sacks (35:65) Poz (Fly Ash): Class H Cement + 0.125 lbs/sack Cello Flake + 3 lbs/sack LCM-1 + 6% bwoc bentonite + 0.4% bwoc FL-52A + 99.3% Fresh water; Yield: 1.95 cf/sack. Tail Slurry: 515 sacks (60:40) Poz (Fly Ash): Class H

Cement + 1% bwow Sodium Chloride + 0.75% bwoc BA-10 + 0.1% woc R-3 + 2 lbs/sack Kol Seal + 4% bwoc MPA-1 + 0.125 lbs/sack Cello Flake + 61.3% Fresh Water; **Yield:** 1.34 cf/sack. **Displacement:** 197.6 bbls Displacement Fluid . DV tool @ 8000'. TOC @ 2350'.

The above cement volumes could be revised pending the caliper measurement from the open hole logs. The top of cement is designed to reach approximately 500' above the 9 5/8" casing shoe. All casing is new and API approved.

5. Pressure Control Equipment:

The BOP system used to drill the intermediate hole will consist of a 13-5/8" 3M Triple Ram and Annular preventer. The BOP system will be tested as per BLM Onshore Oil and Gas Order No. 2 as a 3M system prior to drilling out the surface casing shoe.

The BOP system used to drill the production hole will consist of a 13-5/8" 5M Triple Ram and Annular preventer. The BOP system will be tested as per BLM Onshore Oil and Gas Order No. 2 as a 5M system prior to drilling out the intermediate casing shoe.

The pipe rams will be operated and checked as per Onshore Order No 2. A 2" kill line and 3" choke line will be incorporated into the drilling spool below the ram BOP. In addition to the rams and annular preventer, additional BOP accessories include a kelly cock, floor safety valve, choke lines, and choke manifold rated at 5,000 psi WP.

6. Proposed Mud Circulation System

Depth	Mud Wt.	<u>Visc</u>	Fluid Loss	Type System
0'-400'	8.6-9.4	32-34	· NC	Fresh Water-Gel/Lime
400'-2850'	10	28	NC	Fresh Water
2850'-9600'	8.6-10	28	NC	Cut Brine
9600'-11100'	9.4-10.8	32-40	6-10cc	Brine/Brine/Polymer

The necessary mud products for weight addition and fluid loss control will be on location at all times.

7. Auxiliary Well Control and Monitoring Equipment:

- a. A Kelly cock will be in the drill string at all times.
- b. A full opening drill pipe stabbing valve having the appropriate connections will be on the rig floor at all times.
- c. Hydrogen Sulfide detection equipment will be in operation after drilling out the 13.3/8" casing shoe until the 5 1/2" casing is cemented. Breathing equipment will be on location upon drilling the 13 3/8" shoe until total depth is reached.

8. Logging, Coring, and Testing Program: See Coff

- a. Drill stem tests will be based on geological sample shows.
- b. If a drill stem test is anticipated; a procedure, equipment to be used and safety measures will be provided via sundry notice to the BLM.

- c. The open hole electrical logging program will be:
 - i. Total Depth to Intermediate Casing Dual Laterolog-Micro Laterolog with SP and Gamma Ray. Compensated Neutron Z Density log with Gamma Ray and Caliper.
 - ii. Total Depth to Surface Compensated Neutron with Gamma Ray
 - iii. No coring program is planned
 - iv. Additional testing will be initiated subsequent to setting the 5 ½" production casing. Specific intervals will be targeted based on log evaluation, geological sample shows and drill stem tests.

9. Potential Hazards:

a. No abnormal pressures or temperatures are expected. There is no known presence of H2S in this area. If H2S is encountered the operator will comply with the provisions of Onshore Oil and Gas Order No. 6 No lost circulation is expected to occur. All personnel will be familiar with all aspects of safe operation of equipment being used to drill this well. Estimated BHP 4700 psi and Estimated BHT 180°. No H2S is anticipated to be encountered.

10. Anticipated Starting Date and Duration of Operations:

a. Road and location construction will begin after the BLM has approved the APD. Anticipated spud date will be as soon after BLM approval and as soon as a rig will be available. Move in operations and drilling is expected to take 32 days. If production casing is run then an additional 30 days will be needed to complete well and construct surface facilities and/or lay flow lines in order to place well on production.

Well name:

Devon Energy

Operator: String type:

Surface

Location:

Section 31-19S-28E Eddy Co., NM

D	esign	parameters:

Collapse

Mud weight:

10.000 ppg Design is based on evacuated pipe.

Minimum design factors:

Pacheco Fed Com #9

Collapse:

Design factor

Environment:

H2S considered? Surface temperature: Bottom hole temperature:

75 °F 79 °F 0.90 °F/100ft

Temperature gradient: Minimum section length: Minimum Drift:

350 ft

No

Burst:

Design factor

1.25

1.80 (J)

1.80 (J)

1.100

1.000 in

<u>Burst</u>

Max anticipated surface

pressure: Internal gradient: Calculated BHP

352 psi 0.120 psi/ft 400 psi

No backup mud specified.

Tension:

8 Round STC: 8 Round LTC:

1.60 (J) **Buttress:** Premium: 1.50 (J) Body yield: 1.60 (B)

Tension is based on air weight. Neutral point:

Non-directional string.

Re subsequent strings:

Next setting depth: Next mud weight: Next setting BHP:

2,850 ft 10.000 ppg 1,481 psi 19.250 ppg

Fracture mud wt: Fracture depth: 400 ft Injection pressure 400 psi

Run Seq	Segment Length	Size	Nominal Weight	Grade	End Finish	True Vert	Depth	Drift Diameter	Est. Cost
1	(ft) 400	(in) 13.375	(Ibs/ft) 48.00	H-40	ST&C	(ft) 400	(ft) 400	(in) 12.59	(\$) 13071
Run	Collapse	Collapse	Collapse	Burst	Burst	Burst	Tension	Tension	Tension
Seq	Load (psi)	Strength (psi)	Design Factor	Load (psi)	Strength (psi)	Design Factor	Load (kips)	Strength (kips)	Design Factor
1	208	740	3.56	``40Ó	1730	4.33	19.2	322	16.78 J

Prepared

Don Jennings

Devon Energy

Date: July 29,2008 Oklahoma City, Oklahoma

Remarks:

Collapse is based on a vertical depth of 400 ft, a mud weight of 10 ppg. The casing is considered to be evacuated for collapse purposes. Collapse strength is based on the Westcott, Dunlop & Kemler method of biaxial correction for tension.

Burst strength is not adjusted for tension.

Engineering responsibility for use of this design will be that of the purchaser.

Well name:

Pacheco Fed Com #9

Operator: String type: Devon Energy Intermediate

Location:

Section 31-19S-28E Eddy Co., NM

Design	parameters:
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Collapse Mud weight:

10.000 ppg Design is based on evacuated pipe.

Minimum design factors: Collapse:

Design factor 1.100 **Environment:** H2S considered?

Surface temperature: Bottom hole temperature: Temperature gradient:

101 °F 0.90 °F/100ft 350 ft

Minimum section length: Minimum Drift:

7.875 in

No

75 °F

Burst:

Design factor

1.25

1.80 (J)

1.80 (J)

Non-directional string.

Burst

Max anticipated surface

No backup mud specified.

pressure: Internal gradient: Calculated BHP

2,508 psi 0.120 psi/ft 2,850 psi

Tension: 8 Round STC: 8 Round LTC:

> Buttress: Premium: Body yield:

1.60 (J) 1.50 (J) 1.60 (B)

Tension is based on air weight. 2,426 ft Neutral point:

Re subsequent strings:

Next setting depth: 11,100 ft Next mud weight: Next setting BHP:

11.000 ppg 6,343 psi 19.250 ppg

Fracture mud wt: Fracture depth: 2,850 ft Injection pressure 2,850 psi

Run	Segment		Nominal		End	True Vert	Measured	Drift	Est.
Seq	Length	Size	Weight	Grade	Finish	Depth	Depth	Diameter	Cost
	(ft)	(in)	(lbs/ft)			(ft)	(ft)	(in)	(\$)
1	2850	9.625	40.00	J-55	LT&C	2850	2850	8.75	68186
Run	Collapse	Collapse	Collapse	Burst	Burst	Burst	Tension	Tension	Tension
Seq	Load	Strength	Design	Load	Strength	Design	Load	Strength	Design
•	(psi)	(psi)	Factor	(isq)	(iaq)	Factor	(kips)	(kips)	Factor
1	1481	2570	1.74	2850	3950	1.39	114	`520´	4.56 J

Prepared

Don Jennings

by: Devon Energy

Date: July 29,2008 Oklahoma City, Oklahoma

Collapse is based on a vertical depth of 2850 ft, a mud weight of 10 ppg. The casing is considered to be evacuated for collapse purposes. Collapse strength is based on the Westcott, Dunlop & Kemler method of biaxial correction for tension.

Burst strength is not adjusted for tension.

Well name:

Pacheco Fed Com #9

Operator: -String type: **Devon Energy** Production

Location:

Section 31-19S-28E Eddy Co., NM

Design parameters:

Minimum design factors:

Environment:

Collapse

Mud weight: 11.000 ppg Collapse: Design factor H2S considered? Surface temperature: No 75 °F

Design is based on evacuated pipe.

Bottom hole temperature: Temperature gradient:

180 °F

Minimum section length:

0.95 °F/100ft

Burst:

Design factor

1.00

1.125

350 ft

Burst

Max anticipated surface

No backup mud specified.

pressure:

5,011 psi

Internal gradient: Calculated BHP

0.120 psi/ft

6,343 psi

Tension:

8 Round STC:

8 Round LTC:

1.80 (J) Buttress: 1.60 (J) Premium:

Body yield:

1.50 (J) 1.60 (B)

1.80 (J)

Non-directional string.

Tension is based on air weight. Neutral point:

9,248 ft

Run Seq	Segment Length (ft)	Size (in)	Nominal Weight (lbs/ft)	Grade	End Finish	True Vert Depth (ft)	Measured Depth (ft)	Drift Diameter (in)	Est. Cost (\$)
1	11100	5.5	17.00	HCP-110	LT&C	11100	11100	4.767	192747
Run	Collapse	Collapse	Collapse	Burst	Burst	Burst	Tension	Tension	Tension
Seq	Load (psi)	Strength (psi)	Design Factor	Load (psi)	Strength (psi)	Design Factor	Load (kips)	Strength (kips)	Design Factor
1	6343	8580	1.35	6343	10640	1.68	188.7	445	2.36 J

Prepared

Don Jennings

Devon Energy

Date: July 29,2008 Oklahoma City, Oklahoma

Collapse is based on a vertical depth of 11100 ft, a mud weight of 11 ppg. The casing is considered to be evacuated for collapse purposes. Collapse strength is based on the Westcott, Dunlop & Kemler method of biaxial correction for tension.

Burst strength is not adjusted for tension.

Engineering responsibility for use of this design will be that of the purchaser.

Attachment to Exhibit #1 NOTES REGARDING BLOWOUT PREVENTERS

Devon Energy Production Company, LP

Pacheco 31 Fed Com 9

Surface Location: 660' FNL & 1650' FWL, Unit C, Sec 31 T19S R28E, Eddy, NM Bottom hole Location: 660' FNL & 1650' FWL, Unit C, Sec 31 T19S R28E, Eddy, NM

- 1. Drilling nipple will be constructed so it can be removed mechanically without the aid of a welder. The minimum internal diameter will equal BOP bore.
- 2. Wear ring will be properly installed in head.
- 3. Blowout preventer and all associated fittings will be in operable condition to withstand a minimum 5000 psi working pressure.
- 4. All fittings will be flanged.
- 5. A full bore safety valve tested to a minimum 5000 psi WP with proper thread connections will be available on the rotary rig floor at all times.
- 6. All choke lines will be anchored to prevent movement.
- 7. All BOP equipment will be equal to or larger in bore than the internal diameter of the last casing string.
- 8. Will maintain a kelly cock attached to the kelly.
- 9. Hand wheels and wrenches will be properly installed and tested for safe operation.
- 10. Hydraulic floor control for blowout preventer will be located as near in proximity to driller's controls as possible.
- 11. All BOP equipment will meet API standards and include a minimum 40 gallon accumulator having two independent means of power to initiate closing operation.

DISTRICT I --- CHECKLIST FOR INTENTS TO DRILL

	Operator DEVON ENERGY PRODUCTION CO LP OGRID # 6137
16704	Well Name & # PACHECO 31 FEDERAL CON # 9 Surface Type (F) (S) (Location: UL, Sect 31, Twnship 19 s, RNG 28 e, Sub-surface Type (F) (S) (
C	A. Date C101 rec'd C101 reviewed
·	a District Grant APD but see number of inactive wells: No letter required, Sent Letter to Operator, to Santa Fe 3. Additional Bonding as of:// a. District Denial because operator needs addition bonding:
	No Letter required : Sent Letter to Operator, To Santa Fe b. District Denial because of Inactive well list and Financial Assurance: No Letter required : Sent Letter to Operator, To Santa Fe
	C. C102 YES, NO, Signature 1. Pool
	 2. 2nd. Operator in same acreage, Yes, No
	a. Pool #2
	D. Blowout Preventer Yes ——No, E. H2S Yes, No, F. C144 Pit Registration Yes, No,
	 G. Does APD require Santa Fe Approval: 1. Non-Standard Location: Yes, No, NSL # 2. Non-Standard Proration: Yes, No, NSP # 3. Simultaneous Dedication: Yes, No, SD # Number of wells Plus #
	4. Injection order Yes, No; PMX # or WFX # 5. SWD order Yes, NO; SWD # 6. DHC from SF; DHC-HOB; Holding
	7. OCD Approval Date